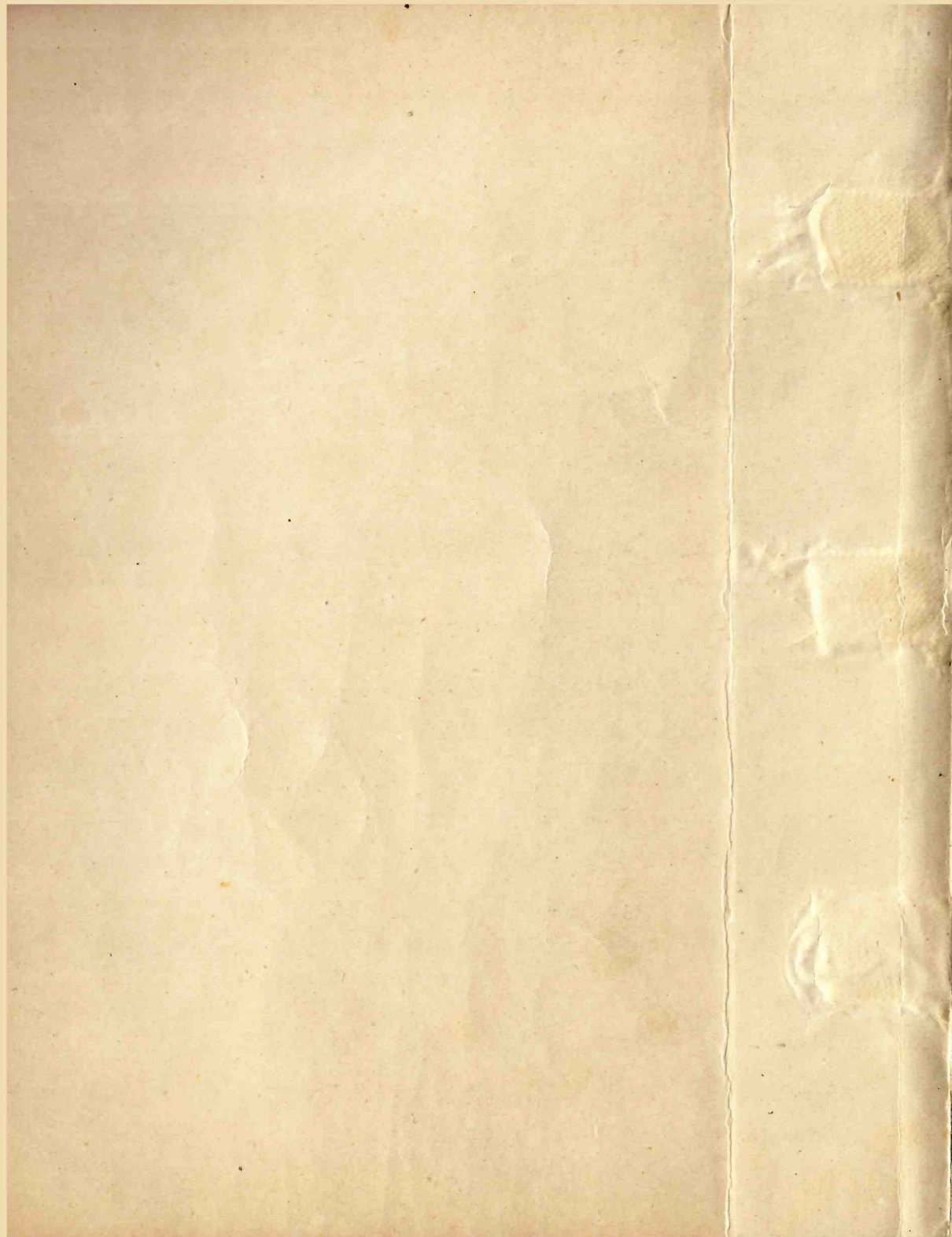
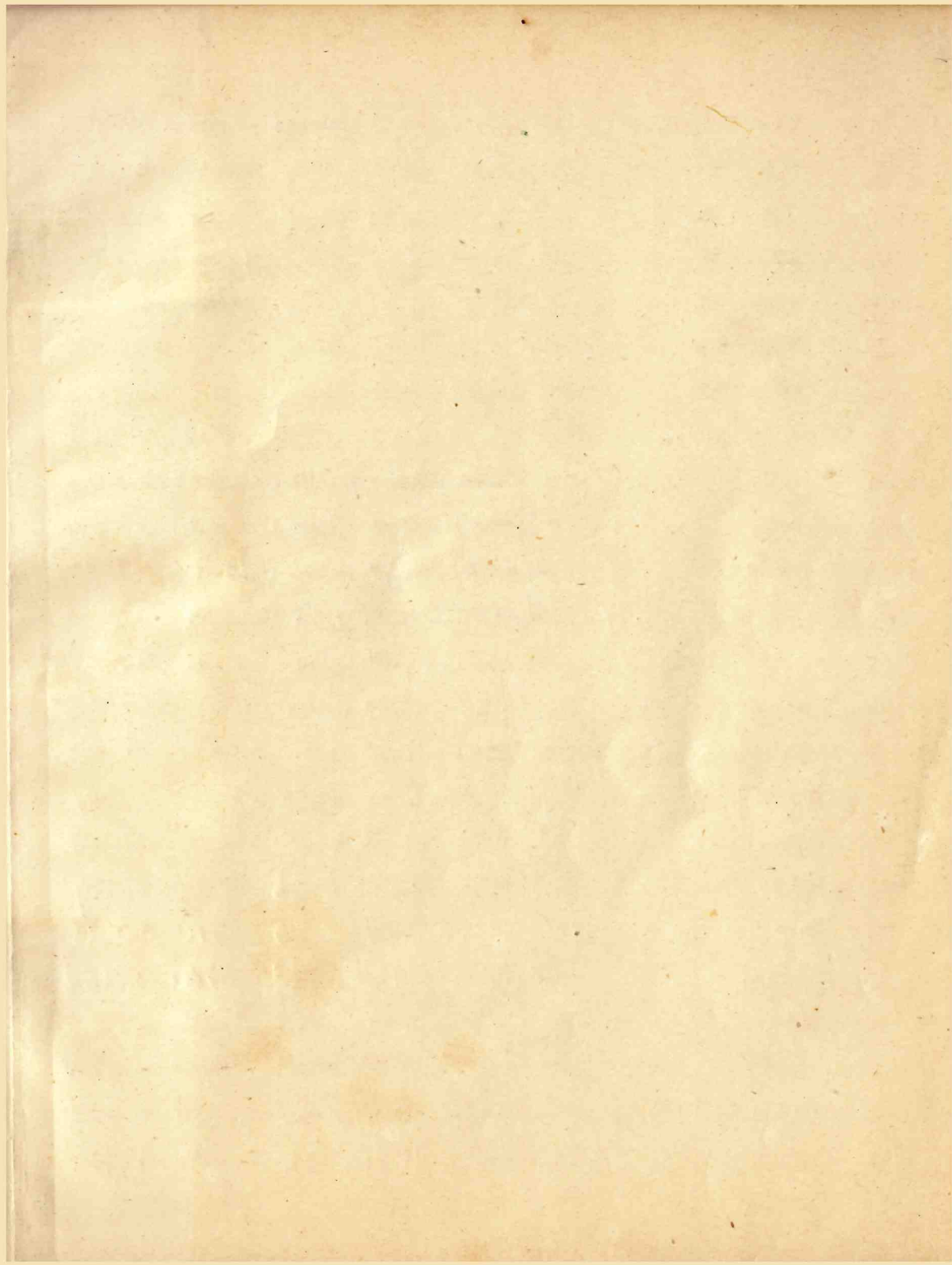


REFLECTOR 4

2925 - 3524





Estado de las imágenes:

p = pulsante

m = móvil

d = difusa

i = irregular

D	-19
14°	7.4
16	6.4
18	5.8
20	5.0
22	4.4
24	3.9

Diapragmas de aluminio:

A d = 11 cm $m_A = 0.8 + mf$

B 19 $m_B = 1.63 + mf$

C 21.5 $m_C = 2 + mf$

2

H ₀	9-10/III/64	K.		T. S.	T. U.	A. h. m
x 2925	5	(3571)	103a-F (8)	10:10 10:18	2:50 2:58	+ 1:22
x 2926	6	(3630)	" (40)	10:40 11:20	3:20 4:00	+ 1:55
x 2927	7	(4205)	" (20)	11:35 11:55	4:15 4:35	+ 1:03
x 2928	8	(4537)	" (13)	12:06 12:19	4:45 4:58	+ 0:26
x 2929	9	(4674)	" (24)	12:27 12:51	5:06 5:30	+ 0:23
x 2930	10	(4993)	" (24)	13:16 13:40	5:55 6:19	+ 0:17

	13-14/III/64	K.		T. S.	T. U.	
x 2931	1	(2746)	103a-E ₍₆₁₎ (10)	7:51 8:01	0:14 0:24	+ 0:45
x 2932	2	"	103a-E ₍₆₃₎ (10)	8:02 8:12	0:25 0:35	+ 0:56
x 2933	3	(2691)	" (24)	8:23 8:47	0:46 1:10	+ 1:30
x 2934	4	(3571)	103a-F (6)	9:25 9:31	1:48 1:54	+ 0:35
x 2935	5	"	103a-E ₆₃ (3)	9:51 9:54	2:14 2:17	+ 0:59.5
x 2936	6	"	" (3)	9:57 10:00	2:20 2:23	+ 1:05.5
x 2937	7	(3611)	" (48)	10:37 11:25	3:00 3:48	+ 2:01
x 2938	8	(4205)	" (8)	11:35 11:43	3:58 4:06	+ 0:57
x 2939	9	(4537)	" (4)	11:52 11:56	4:15 4:19	+ 0:07
x 2940	10	(4674)	" (3)	12:43 12:46	5:06 5:09	+ 0:29
x 2941	11	(4944)	" (30)	13:17 13:47	5:40 6:10	+ 0:28
x 2942	12	(4993)	" (7)	14:00 14:07	6:23 6:30	+ 0:52

	14-15/III/64	K.		T. S.	T. U.	
x 2943	1	(3536)	103a-E (20)	10:21 10:41	2:40 3:00	+ 1:42
x 2944	2	(3656)	" (32)	10:54 11:26	3:12 3:44	+ 2:01
	3	(4571)	" (40)			

Ranura:

$$F_c = 25.5; \rho_{H_1} = 40 \frac{\text{Å}}{\text{mm}}$$

a &

25-7

5

B

de 60°

22.2

22.2

+1"

"

C

"

22.0

21.9

+4"

"

A

"

21.8

21.8

"

B

"

21.6

21.6

"

C

"

21.4

21.3

"

A

"

21.2

21.1

25-7

5

A

de 40°

22.8

22.8

"

B

"

22.8

22.8

"

C

"

22.4

22.3

"

A

de 60°

21.9

21.9

+2"

"

B

de 40°

21.6

21.6

"

C

de 40°

21.5

21.5

"

A

"

21.1

20.9

"

B

"

20.8

20.8

-1"

"

C

"

20.6

20.6

e

"

A

"

20.1

20.1

"

B

"

20.1

20.0

"

C

"

19.9

19.9

25-7

40

A

de 40°

21.8

21.8

5

B

"

21.6

21.4

se mltb

2

15-16/III/64 K.

T. S.

T. V.

x 2945	1	(2182)	103a-E ₆₃	(36)	7:12	7:48	23:27	0:03	+1:24
x 2946	2	(2504)	" ₆₁	(11)	8:03	8:14	0:18	0:29	+1:24
x 2947	3	(2812)	"	(8)	8:34	8:42	0:49	0:57	+1:18,5
x 2948	4	(2912)	"	(48)	9:01	9:49	1:16	2:04	+1:53
x 2949	5	(2922)	"	(6)	10:00	10:06	2:15	2:21	+2:30
x 2950	6	(3435)	"	(48)	10:29	11:17	2:44	3:32	+2:16,5
x 2951	7	(4571)	"	(40)	12:03	12:43	4:45	4:57,5	+0:29
x 2952	8	(4724)	"	(22)	12:54	13:16	5:08,5	5:30,5	+0:43

16-17/III/64 K.

T. S.

T. V.

x 2953	1	(2295)	103a-E ₆₁	(45)	8:01	8:46	0:12	0:57	+2:02
x 2954	2	(3174)	"	(26)	9:05	9:31	1:16	1:42	+1:15
x 2955	3	(3500)	103a-F	(30)	9:45	10:15	1:56	2:26	+1:14
x 2956	4	(3638)	"	(52)	10:36	11:28	2:47	3:39	+1:56
x 2957	5	(4604)	"	(40)	12:40	13:20	4:51	5:31	+0:58

17-18/III/64 K.

T. S.

T. V.

x 2958	1	(2195)	103a-E ₆₃	(30)	8:06	8:36	0:13	0:43	+2:13
x 2959	2	(2947)	"	(42)	8:52	9:34	0:59	1:41	+1:37
x 2960	3	(3463)	"	(40)	9:44	10:24	1:51	2:31	+1:24
x 2961	4	(3479)	"	(21)	10:35	10:56	2:42	3:03	+2:03,5
x 2962	6	(3646)	"	(48)	11:14	12:02	3:21	4:09	+2:31
x 2963	7	(4603)	"	(8)	12:26	12:34	4:33	4:41	+0:29
	8	(4656)	"	(58)	12:48	12:48,50	4:55	4:55:50	+0:36
x 2964	9	(4656)	"	(70)	13:00	13:11,10	5:07	5:08:10	+0:48

t_{avant} $t_{\text{en. de esp. ch}}$

25-7	5	A	$\sqrt{e} 40^\Delta$	21.2	21.1	+2
"	"	B	$\sqrt{e} 50^\Delta$	20.8	20.7	
"	"	C	"	20.4	20.4	
"	"	A	"	20.0	19.6	
"	"	B	"	19.4	19.4	
"	"	C	"	18.8	18.5	+3
"	"	A	"	17.3	17.1	
"	"	B	"	16.8	16.7	

25-7	5	A	$\sqrt{e} 50^\Delta$	18.8	18.7	
"	"	B	"	17.5	18.3	
"	"	C	$\sqrt{e} 60^\Delta$	16.4	17.9	
"	"	A	"	15.9	17.4	+6 ^m
"	"	B	"	15.5	16.4	

25-7	5	A	$\sqrt{e} 40^\Delta$	18.2	19.7	19.5
"	"	B	"	18.0	19.4	19.3
"	"	C	"	"	19.0	18.9
"	"	A	"	"	18.8	18.8
"	"	B	"	"	18.8	18.7
"	"	C	"	17.7	18.6	18.6
"	"	A	"	18.5	18.5	
"	"	B	"	"	"	"

Defects en la emulsión

29-30/II/64 K.

T. S.

T. U.

Correc. $\Delta = + 3^m$

x2965	1	(4552)	103A-E	(5)	1341	1346	1 00.5	1 05.5	+1:54
-------	---	--------	--------	-----	------	------	--------	--------	-------

x2966	2	"	"	(8)	1351	1359	1 10.5	1 18.5	+2:06
-------	---	---	---	-----	------	------	--------	--------	-------

cor. $+3^m$

31/II - I/III/64 K.

T. S.

T. U.

x2967	1	(4221)	103A-E	(16)	1130	1146	22 41	22 57	+0:54
-------	---	--------	--------	------	------	------	-------	-------	-------

x2968	2	(4262)	"	(32)	1201	1223	23 12	23 44	+1:25.5
-------	---	--------	---	------	------	------	-------	-------	---------

x2969	3	(4556)	"	(38)	1255	1333	0 06	0 44	+1:23
-------	---	--------	---	------	------	------	------	------	-------

x2970	4	(4944)	"	(30)	1351	1421	1 02	1 32	+1:02
-------	---	--------	---	------	------	------	------	------	-------

x2971	5	(5121)	"	(29)	1442	1511	1 53	2 22	+1:23
-------	---	--------	---	------	------	------	------	------	-------

	6	(5412)	"	(16)	1529	1545	2 40	2 56	+1:11
--	---	--------	---	------	------	------	------	------	-------

x2972	7	(5557)	"	(28)	1609	1637	3 20	3 48	+1:20
-------	---	--------	---	------	------	------	------	------	-------

cor. $+3^m$

4-5/III/64 K.

T. S.

T. U.

x2973	1	(4781)	103A-E	(16)	1330	1346	0 25	0 41	+1:07.5
-------	---	--------	--------	------	------	------	------	------	---------

x2974	2	(4799)	"	(26)	1405	1431	1 00	1 26	+1:49.5
-------	---	--------	---	------	------	------	------	------	---------

x2975	3	(5049)	"	(24)	1503	1524	1 58	2 22	+1:53
-------	---	--------	---	------	------	------	------	------	-------

x2976	4	(5555)	"	(38)	1558	1636	2 53	3 31	+1:22.5
-------	---	--------	---	------	------	------	------	------	---------

x2977	5	(6172)	"	(26)	1752	1818	4:47	5 13	+1:26
-------	---	--------	---	------	------	------	------	------	-------

5-6/III/64 K.

T. S.

T. U.

x2978	1	(4781)	103A-E	(24)	1304	1328	23:58	0:22	+0:45.5
-------	---	--------	--------	------	------	------	-------	------	---------

x2979	2	(4799)	"	(40)	1340	1420	0:34	1 14	+1:26.5
-------	---	--------	---	------	------	------	------	------	---------

x2980	3	(5049)	"	(36)	14:54	15:30	1 48	2 24	+1:50
-------	---	--------	---	------	-------	-------	------	------	-------

x2981	4	(5554)	"	(42)	1548	1630	2 42	3 24	+1:07
-------	---	--------	---	------	------	------	------	------	-------

x2982	6	(6174)	"	(40)	1648	1728	3 42	4 22	+0:34
-------	---	--------	---	------	------	------	------	------	-------

$$T.U. = T.A. + 4^{\circ}$$

7

25-7	5	A № 40	12.1	13.0	13.0		
"	"	B "	12.1	12.9	12.9	rep. 4"	
25-7	5	A № 50	14.9	15.8	15.8	+2	[e]
"	"	B "	14.5	15.7	15.6	+6	rep. (44")
"	"	C "	14.7	15.6	15.5	+4	
"	"	A "	14.9	15.5	15.5	+4	
"	"	B "	15.3	15.5	15.5	+4	
"	"	C "	15.4	15.5	15.6	+4	placa manchada
"	"	A "	15.4	15.6	15.6	+10	
25-7	5 d	A № 50	10.1	11.7	11.7	+4	rep. can (24") E
"	"	B "	9.6	11.5	11.4	+6	" (40") E
"	5 "	C "	9.0	10.9	10.8	+4	" (36") E
"	"	A "	8.6	10.2	10.1	+10+10	
"	"	B "	7.9	9.4	9.3	+15	e
25-7	5	A № 50	10.4	11.5	11.5		
"	"	B "	10.1	11.3	11.3		
"	"	C "	9.6	10.9	10.8		
"	"	A "	9.4	10.6	10.4		
"	"	B "	8.8	10.3	10.1		

8

5-6/VI/64

K.

T. S.

T. U.

x 2983	7	(6214)	103A-E (24)	1740	18 04	434	4 58	+1:11
x 2984	8	(6320)	" (30)	1823	18 53	516	5 46	+1:38
x 2985	9	(6960)	" (14)	1913	19 30	606	6 23	+0:51

6-7/VI/64

K.

T. S.

T. U.

x 2986	1	(4669)	103A-E (54)	1324	14 18	014	1 08	+1:37.5
x 2987	2	(5140)	" (40)	1441	15 21	131	2 11	+1:23
x 2988	3	(5498)	" (54)	1535	16 24	225	3 19	+1:19
x 2989	4	(6274)	" (60)	1644	17 44	334	4 34	+0:23
x 2990	5	(6347)	" (46)	1755	18 41	445	5 31	+1:16

8-9/VI/64

K.

T. S.

T. U.

x 2991	1	(4696)	103A-E (20)	1325	13 45	007	0 27	+1:18
x 2992	2	(4735)	" (17)	1359	14 16	041	0 58	+1:44
x 2993	3	(5412)	" (24)	1507	15 31	148	2:12	+0:52

19-20/VI/64

K.

T. S.

T. U.

2994	1	(4947)	103A-E (30)	1400	14 30	000	0 30	+1:11
2995	2	(5294)	" (60)	1444	15 44	044	1 44	+1:08
2996	3	(5786)	" (48)	1559	16 47	159	2 47	+1:01
2997	4	(6172)	" (40)	1705	17 45	305	3 45	+0:59
2998	5	(6340)	" (42)	1802	18 44	402	4 44	+1:22
2999	6	(6353)	" (24)	1900	19 24	500	5 24	+2:10
3000	7	(6601)	" (46)	1949	20 35	549	6 35	+2:32
3001	8	(6960)	" (18)	2055	21 13	655	7 13	+2:35

25-7	5	C No 50	8.6	10.0	10.0	
"	"	A "	8.2	9.7	9.6	
"	"	B "	7.5	9.4	9.4	up. (17)E

25-7	5	A No 50	12.1	12.2	12.2	+6
"	"	B "	11.8	12.2	12.2	
"	"	C "	11.7	12.2	12.2	
"	"	A "	11.2	12.2	12.1	e
"	"	B "	10.9	12.1	12.0	up. (40)E
"	"	C				

25-7	5	A No 50	11.3	13.0	12.9	+2 e
"	3 d	B "	11.1	12.7	12.7	+4 debr. up.
"	2 "	C "	10.7	12.2	12.2	+20 lin

25-7	5	A No 50	8.4	10.2	10.1	
"	"	B "	8.1	9.8	9.6	
"	1 d	C "	8.1	9.2	9.2	+6
"	"	A "	7.9	9.0	9.0	e
"	"	B "	7.9	8.9	8.8	
"	"	C "	7.7	8.8	8.8	+2
"	"	A "	7.6	8.7	8.5	+2
"	"	B "	7.6	8.3	8.3	

20-21/II/64		K.	T.S.		T.U.	
3002	a	(4871)	103a-E	(66)	13 56 15 02	23 52,5 0 58,5 +1:42
3003	b	(5628)	"	(48)	15 27 16 15	+23,5 2 11,5 +0:44
3004	c	(5869)	"	(42)	16 29 17 11	2 25,5 3 07,5 +1:04
3005	d	(6347)	"	(48)	17 27 18 15	3 23 4 11 +0:49

23-24/II/64		K.	T.S.		T.U.	
3006	1	(4592)	103a-E	(64)	13 05,5 14 09,5	22 50 23 54 +1:39,5
3007	2	(4887)	"	(22)	14 28 14 50	0 12 0 34 +1:48
3008	3	(5327)	"	(60)	15 18 16 18	1 02 2 02 +1:29,5
3009	4	(5873)	"	(30)	16 31 17 01	2 15 2 45 +0:59
3010	5	(6276)	"	(46)	17 13 17 59	2 57 3 43 +0:42
3011	6	(6289)	"	(30)	18 13 18 43	3 57 4 27 +1:34

25-26/II/64		K.	T.S.		T.U.	
3012	1	(5174)	103a-E	(18)	14 26 14 44	0 02 0 20 +0:51
3013	2	(5357)	"	(46)	14 56 15 42	0 32 1 18 +1:03
3014	3	(5623)	"	(58)	15 59 16 57	1 35 2 33 +1:23
3015	4	(6304)	"	(58)	17 23 18 21	2 59 3 57 +0:55

26-27/II/64		K.	T.S.		T.U.	
3016	5	(5514)	103a-E	(30)	15 19 15 49	0 51 1 21 +0:50
3017	6	(5655)	"	(60)	15 59 16 59	1 31 2 31 +1:19
3018	7	(6182)	"	(60)	17 22 18 22	2 54 3 54 +1:14
3019	8	(6274)	"	(60)	18 55 19 55	4 27 5 27 +2:34

25-7	5P	A	Ne 50 ³	5.9	8.6	8.2	
"	"	B	"	5.0	7.5	7.2	+4
"	"	C	"	4.2	6.8	6.5	
"	"	A	"	3.4	6.1	5.8	+6

25-7	5d	A	Ne 50 ³	6.3			
"	"	B	"	5.5			
"	"	C	"	5.3			e
"	"	A	"	4.5			
"	"	B	"	4.0			
"	"	C	"	3.6			

25-7	5d	A	Ne 50 ³	6.1	8.2	8.1	
"	"	B	"	5.8	7.9	7.7	
"	"	C	"	5.5	7.2	7.0	
"	"	A	"	5.0	6.7	6.5	e

25-7	5d	A	Ne 50 ³	7.7	7.9	7.9	
"	"	B	"	7.4	7.9	7.9	
"	"	C	"	6.7	7.9	7.7	
"	"	A	"	6.0	7.4	7.4	e

12

28-29/V/64 K.

T. S.

T. U.

3020	1	(5163)	103a-E (72)	15 09	16 21	0 33	1 45	+2:04
3021	2	(5863)	" (22)	16 45	17 07	2 09	2 31	+1:13,5
3022	3	(5907)	" (17)	17 23	17 40	2 47	3 04	+1:41
3023	4	(6347)	" (36)	18 23	18 59	3 47	4 23	+1:39

6-7/VII/64 K. S. Ensayo de la cámara Meinel:

CM 7	1	K Cn (4890)	103a-0 (5 ^m)	Sin movimiento fono				
CM 8	2	2 Cn (4730-30)	" (6 ^m)	Giro 180° " " "				
CM 9	3	" "	" (15)	" "	" "	" "	" "	" "
CM 10	4	" "	" (15)	Giro 90° " " "				
CM 11	5	Tz 24	" (5 ^m)	Giro 180° con movimiento fono				
CM 12	6	WGL 6530	" (10 ^m)	" "	" "	" "	" "	" "
CM 13	7	" 6611	" (4)	" "	" "	" "	" "	" "
CM 14	8	" 6618	" (3)	" "	" "	" "	" "	" "

correa del camaro abierto una
vez al menos en el campo del
sonido

20-21/VII/64 K.

T. S.

T. U.

3024	1	(6411)	103a-E (28)	19 14	19 42	3 10	3 38	+2:11
------	---	--------	-------------	-------	-------	------	------	-------

26-27/VII/64 K

T. S.

T. U.

3025	1	(5869)	103a-E (12)	16 07	16 49	28 39	0 21	+0:42
3026	2	(6045)	" (19)	17 00	17 19	0 32	0 51	+0:58
3027	3	(6209)	" (48)	17 52	18 40	1 24	2 12	+1:36
3028	4	(6214)	" (29)	18 54	19 18	2 26	2 50	+2:25
3029	5	(7223)	" (48)	19 24	20 17	3 01	3 49	+0:50
3030	6	(7698)	" (58)	20 37	21 35	4 09	5 07	+0:50

a l						
25-7	5 d	A	de 50 ³	6.1	8.0	7.7 + 8
"	5 d	B	"	5.4	7.4	7.3
"	"	C	"	5.2	7.0	7.0
"	"	A	"	4.8	6.6	6.4

a l						
25-7	5	B	de 50 ³	7.2	8.9	8.7
		C				
25-7	5	B	de 50 ³	8.3	10.1	10.2
"	"	B	"	7.7	9.6	9.5
"	"	C	"	7.5	9.2	9.0 + 4"
"	"	A	"	7.4	8.8	8.8
"	"	B	"	7.4	8.5	8.4
"	"	C	"	7.1	8.3	8.0 + 6"

14

		26-27/VII/64	K.		T.S.		T.U.	
3031	7	(8286)	103a-E	(48)	21 57	22 45	5 29	6 17 +0:40,5
3032	8	(8540)	"	(12)	23 00	23 12	6 32	6 44 +0:43

		27-28/VII/64	K.		T.S.		T.U.	
3033	1	(5646)	103a-E	(6)	15 47	15 53	23 15,5	23 21,5 +0:42,5
3034	2	(5647)	"	(45)	16 05	16 50	23 33,5	0 12,5 +1:20
3035	3	(6253)	"	(52)	17 14	18 06	0 42,5	1 34,5 +0:50
3036	4	(6759)	"	(60)	18 27	19 27	1 55,5	2 55,5 +0:53
3037	5	(7435)	"	(64)	19 41	20 45	3 09	4 13 +0:38
3038	6	(7691)	"	(72)	20 57	22 09	4 25	5 37 +1:27
3039	7	(8381)	"	(54)	22 27	23 21	5 55	6 49 +0:58
3040	8	(8540)	II a-E	(10)	23 32	23 42	7 00	7 10 +1:14

		28-29/VII/64	K.		T.S.		T.U.	
3041	1	(5846)	II a-E	(75)	16 08	17 23	23 33	0 48 +1:05,5
3042	2	(6422)	"	(60)	17 44	18 44	1 09	2 09 +1:00
3043	3	(6990)	"	(23)	19 15	19 38	2 40	3 03 +0:53
3044	4	(7440)	"	(10)	19 49	19 59	3 14	3 24 +0:22
3045	5	(7416)	"	(40)	20 10	20 50	3 35	4 15 +1:01
3046	6	(7881)	"	(21)	21 03	21 24	4 28	4 49 +0:37
3047	7	(8125)	"	(60)	21 40	22 40	5 05	6 05 +0:57
3048	8	(8616)	"	(27)	22 55	23 22	6 20	6 47 +0:34

		29-30/VII/64	K.		T.S.		T.U.	
3049	1	(6381)	II a-E	(30)	17 45	18 15	1 05	1 35 +0:52

25-7 5 d A $\sqrt{e} 50^\circ$ 6.7 7.9 7.8 +4^m

" " B " 6.7 7.7 7.7

25-7 5 d A $\sqrt{e} 50^\circ$ 11.3 12.2 12.2 [2]

" " B " 10.9 12.2 12.1

" " C " 10.3 11.9 11.7 +4^m

" " A " 9.8 11.4 11.3

" " B " 9.4 11.1 10.8 +2^m

" " C " 8.8 10.5 10.4 +2^m

" " A 65° 8.5 10.0 9.8

" " B 50° 8.2 9.6 9.6

25-7 5 d A $\sqrt{e} 50^\circ$ 11.4 11.9 11.8

" " B " 11.3 11.7 11.6 No log 11.2, repetitive

" " C " 11.2 11.6 11.6

" " A " 11.1 11.4 11.4

" " B " 10.8 11.4 11.4

" " C " 10.6 11.4 11.4 +3^m

" " A " 10.4 11.2 11.2

" " B " 10.1 11.1 11.1

25-7 5 d A $\sqrt{e} 50^\circ$ 10.5 11.8 11.8 +4

30-31/VII/64 K.

T.S.

T.U.

3050	1	(5624)	II _{A-E}	(46)	15 42	16 28	22 59	23 45	+1:08
3051	2	(6100)	"	(22)	16 48	17 10	0 05	0 27	+0:39

1-2/VIII/64 K.

T.S.

T.U.

3052	1	(5724)	II _{A-E}	(11)	16 06	16 17	23 14	23 25	+0:50
3053	2	(5719)	"	(22)	16 25	16 47	23 33	23 55	+1:15
3054	3	(6178)	"	(50)	16 57	17 47	0 05	0 55	+0:46,5
3055	4	(6613)	"	(54)	18 03	18 57	1 11	2 05	+0:47
3056	6	(7128)	"	(36)	19 09	19 45	2 17	2 53	+0:35
3057	7	(7480)	"	(26)	19 58	20 24	3 06	3 32	+0:34
3058	8	(7775)	"	(52)	20 50	21 42	3 58	4 50	+0:59
3059	9	(8075)	"	(6)	21 58	22 04	5 06	5 12	+0:59

19-20/VIII/64 K.

T.S.

T.U.

3060	1	(6446)	II _{A-E}	(8)	18 36	18 44	0 34	0 42	+1:22
3061	2	(7024)	"	(52)	18 59	19 51	0 57	1 49	+0:41
3062	3	(7590)	"	(6)	20 06	20 12	2 04	2 10	+0:13
3063	4	(7587)	"	(22)	20 22	20 44	2 20	2 42	+0:40
3064	5	(7779)	"	(30)	20 55	21 25	2 53	3 23	+0:51
3065	6	(7992)	"	(72)	21 40	22 52	3 38	4 50	+1:25
3066	7	(8597)	"	(6)	23 18	23 24	5 16	5 22	+0:49
3067	8	(8816)	"	(54)	23 38	0 32	5 36	6 30	+0:59

20-21/VIII/64 K.

T.S.

T.U.

3068	1	(6500)	II _{A-E}	(3)	17 58	18 01	23 52	23 55	+0:32
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25-7	3-4	A	NE 50°	11.9	13.9	13.7	+6	kilo
"	3	B	"	11.1	13.5	13.4	+2	"
25-7	5	A	NE 50°	8.7	10.4	10.4		
"	"	B	"	8.3	10.3	10.1		
"	"	C	"	8.0	9.9	9.7	+4	
"	"	A	"	7.3	9.4	9.1		
"	"	B	"	6.7	8.8	8.6		
"	"	C	"	6.4	8.4	8.2	+6	
"	"	A	"	5.7	7.9	7.6	+6	
"	"	B	"	5.2	7.3	7.3		

Duke repetitor HR 7480 : kay 1 linia dudusan.
 Repeti : HV 3098 no kane eta linia.

25-7	5	A	NE 50°	6.5	9.2	9.2		
"	"	B	"	6.1	8.7	8.3	+4	
"	"	C	"	5.6	8.0	8.0		
"	"	A	"	5.2	7.8	7.6	+2	
"	"	B	"	5.0	7.4	7.2	+4	
"	"	C	"	5.0	6.8	6.5	+8	
"	"	A	"	4.4	6.2	6.2		
"	"	B	"	4.1	5.8	5.7	+6	

25-7	5	A	NE 50°	8.4	9.6	9.6		
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18

20-21/VIII/64		K.		T.S.	T.U.	
3069	2	(6505)	IIa-E	(54)	18 22	19 16 0 16 1 10 +1:22
3070	3	(7134)	"	(14)	19 45	19 59 1 39 1 53 +0:58
3071	4	(7329)	"	(18)	20 08	20 26 2 02 2 20 +0:58
3072	5	(7392)	"	(36)	20 40	21 16 2 34 3 10 +1:32

21-22/VIII/64		K.		T.S.	T.U.	
3073	1	(6447)	IIa-E	(40)	17 40	18 20 23 30 0 10 +0:40
3074	2	(6460)	"	(16)	18 40	18 56 0 30 0 46 +1:27
3075	3	(6808)	"	(54)	19 06	20 00 0 56 1 50 +1:19.5
3076	4	(7092)	"	(60)	20 26	21 26 2 16 3 16 +2:06
3077	5	(8019)	"	(72)	21 53	23 05 3 43 4 55 +1:31.5
3078	6	(8910)	"	(60)	23 28	0 28 5 17 6 17 +0:34
3079	7	(9076)	"	(12)	0 45	0 57 6 34 6 46 +0:54
3080	8	(9108)	"	(28)	1 12	1 40 7 01 7 29 +1:23.5

22-23/VIII/64		K.		T.S.	T.U.	
3081	1	(6373)	IIa-E	(64)	18 11	19 15 23 57 1 01 +1:33.5
3082	2	(7134)	"	(14)	19 33	19 47 1 18 1 32 +0:45
3083	3	(7188)	"	(12)	19 56	20 08 1 41 1 53 +1:02
3084	4	(7337)	"	(6)	20 21	20 27 2 06 2 12 +1:04.5

24-25/VIII/64		K.		T.S.	T.U.	
3085	1	(6525)	IIa-E	(66)	18 25	19 31 0 03 1 09 +1:26.5
3086	2	(6829)	"	(28)	20 04	20 32 1 42 2 10 +1:59
3087	3	(7710)	"	(15)	20 52	20 53 2 30 2 31.5 +0:44

25-7	5	B	$\sqrt{e} 50^3$	7.9	9.5	9.3	+6
"	"	"	"	7.7	9.1	9.0	
"	"	A	"	7.5	8.9	8.9	
"	"	B	"	7.5	8.8	8.8	3c mulls'

25-7	5	A	$\sqrt{e} 50^3$	10.8	11.4	11.2	+4
"	"	B	"	10.3	11.2	11.2	
"	"	C	"	9.7	11.1	11.0	
"	"	A	"	8.6	10.5	10.3	+6 +10
"	"	B	"	7.7	9.6	9.4	+6
"	"	C	"	7.0	8.9	8.6	
"	"	A	"	6.4	8.3	8.3	2c mulls (10)
"	"	B	"	6.3	8.0	8.0	+2

25-7	5	A	$\sqrt{e} 50^3$	9.2	11.1	10.9	+4
"	"	B	"	8.9	10.5	10.5	
"	"	C	"	8.8	10.4	10.4	
"	"	A	"	8.5	10.3	10.3	

25-7	5	A	$\sqrt{e} 50^3$	9.9	11.9	11.7	
"	"	B	"	9.3	11.2	11.1	
"	"	C	"	9.1	11.1	11.1	

20

24-25/VIII/64 K.

T. S.

T. V.

3088	5	(7821)	IIa-E	(46)	2133	2219	310	356	+1:30

25-26/VIII/64 K.

T. S.

T. V.

3089	1	(6544)	IIa-E	(24)	1814	1838	2347	011	+0:54
3090	2	(6567)	"	(10)	1849	1859	022	032	+1:19
3091	3	(6932)	"	(92)	1911	1953	044	126	+1:05
3092	4	(7596)	"	(28)	2010	2038	142	210	+0:32
3093	6	(7614)	"	(16)	2057	2113	229	245	+1:10
3094	7	(7985)	"	(24)	2136	2200	308	332	+0:59
3095	8	(8141)	"	(28)	2213	2241	345	413	+1:11.5

27-28/VIII/64 K.

T. S.

T. V.

3096	1	(7507)	IIa-E	(24)	2056	2120	220	244	+1:25
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2-3/IX/64 K.

T. S.

T. V.

3097	2	(6422)	IIa-E	(60)	1858	1958	2358	058	+2:12.5
3098	3	(7480)	"	(26)	2016	2042	116	142	+0:51
3099	4	(7890)	"	(54)	2110	2204	210	304	+1:00
3100	5	(8451)	"	(50)	2232	2322	332	422	+0:49
3101	6	(8704)	"	(40)	2342	022	441	521	+1:11
3102	7	(11)	"	(58)	050	148	549	647	+1:14

3-4/IX/64 K.

T. S.

T. V.

3103	8	(6700)	IIa-E	(11)	1831	1842	2327	2338	+0:39.5
3104	9	(6755)	"	(32)	1855	1927	2351	023	+1:07.5

25-7 5 A Ne 50³ 8.7 10.8 10.6

25-7 5 A Ne 50³ 10.7 13.2 13.1 +2"

" " B " 10.5 12.9 12.9

" " C " 10.2 12.7 12.5 +4

" " D " 10.0 12.2 12.1 +2 +6

" " B " 9.8 11.9 11.8 +2

" " C " 9.6 11.5 11.4 +4

" " A " 9.6 11.3 11.2 +2

25-7 5 A Ne 50³ 12.7 14.8 14.7

25-7 5 A Ne 50³ 6.8 8.9 8.8

" " B " 6.1 8.5 8.3 +6

" " C " 6.0 7.9 7.6 +8 e

" " A " 6.2 7.3 7.2 +8

" " B " 6.2 7.1 7.0 +10

" " B-2 C " 6.2 6.8 6.8 +30 Velo

Se observa que las prismas se han movidas: Ver
Hu 3057 y Hu 3098

25-7 5 A Ne 50³ 10.9 11.1 11.1

" " B " 10.9 11.1 11.1 +15 Velo

22

9-10/IX/64 K.

T. S.

T. U.

3105	1	8 Cap	Π_{a-0}	(8)	22 00	22 08	2 35	2 43	+0:20
3106	2	"	"	(12)	22 49	23 01	3 24	3 36	+1:11

10-11/IX/64 K.

T. S.

T. U.

3107	1	(6879)	Π_{a-E}	(20)	18 34	18 34 20	23 06	23 06 20	+0:13.5
3108	2	(6893)	"	(60)	18 49	19 49	23 21	0 21	+0:56
3109	3	(7230)	"	(42)	20 04	20 46	2 36	1 18	+1:22
3110	4	(7239)	"	(40)	21 03	21 43	1 35	2 15	+2:19
3111	5	(8337)	"	(50)	22 26	23 16	2 58	3 48	+1:04
3112	6	(8856)	"	(60)	23 39	0 39	4 10	5 10	+0:54
3113	7	(51)	"	(34)	1 11	1 45	5 42	6 16	+1:16
3114	8	(444)	"	(80)	2 05	3 25	6 36	7 56	+1:15

11-12/IX/64 K.

T. S.

T. U.

3115	1	(8087)	Π_{a-E}	(20)	21 37	21 57	2 05	2 25	+0:41.5
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12-13/IX/64 K.

T. S.

T. U.

3116	2	(7143)	Π_{a-E}	(54)	19 22	20 16	23 46	0 40	+0:55.5
3117	3	(7575)	"	(42)	20 35	21 17	0 59	1 41	+1:05.5
3118	4	(8054)	"	(54)	21 37	22 31	2 01	2 55	+1:04
3119	5	(8533)	"	(36)	22 48	23 27	3 11	3 47	+0:44
3120	6	(8647)	"	(58)	23 48	0 46	4 11	5 09	+1:36.5
3121	7	(12)	"	(40)	1 06	1 46	5 29	6 09	+1:21
3122	8	(474)	"	(60)	2 03	3 03	6 26	7 26	+0:57
3123	9	(899)	"	(24)	3 46	4 10	8 08.5	8 32.5	+1:01

$$F_c = 28,5 ; \sigma = 20 \frac{A}{mm^2}$$

con vidrio
esmerilado:

23

10-5	5	1	Fe: 2+2	8,3	10,5	10,4
"	"	2	3+3	8,0	10,0	9,9

25-7	5	A	Ne 50	10,3	11,3	11,3
"	"	B	"	9,8	11,2	11,0
"	"	C	"	9,2	10,8	10,6 +4 ^m
"	"	A	"	8,8	10,5	10,3 +10 ^m
"	"	B	"	8,1	9,9	9,6 +6 ^m
"	"	C	"	7,5	9,4	9,0 +10 ^m
"	"	A	"	6,9	8,6	8,5
"	"	B	"	6,3	8,2	7,8 +16 ^m

25-7	4	A	Ne 50	8,9	10,4	10,4 +2 ^m
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25-7	5	A	Ne 50	15,2	13,9	14,2 +8 ^m
"	"	B	"	14,7	14,4	14,6 +6 ^m
"	"	C	"	14,0	14,3	14,6 +6 ^m
"	"	A	"	13,1	14,4	14,3 +4 ^m
"	"	B	"	12,2	14,2	13,9 +10 ^m
"	"	C	"	11,8	13,7	13,4 +4 ^m
"	"	A	"	11,6	13,3	13,0 +8 ^m
"	"	B	"	11,1	12,6	12,6 +4 ^m

24

21-22/IX/64. K.

T.U = T.A. + 4^h
T.S. $\Delta T = +1^m$
T.A. = H.L. *Duration*

3124	1	(7552)	IIa-E	(22)	21 06	21 28	20 53	21 15	+1:28
3125	2	(7933)	"	(24)	21 42	22 06	21 29	21 53	+1:11
3126	3	(8305)	"	(8)	22 32	22 40	22 19	22 27	+0:54
3127	4	(8790)	"	(28)	23 09	23 37	22 56	23 24	+0:19
3128	5	(8919)	"	(34)	22 55	0 29	23 42	0 16	+0:46
3129	6	(191)	"	(10)	0 59	1 09	0 46	0 56	+0:23
3130	7	(338)	"	(14)	1 35	1 49	1 22	1 36	+0:36
3131	8	(380)	"	(60)	2 06	3 06	1 53	2 53	+1:21
3132	9	(939)	"	(24)	3 38	4 02	3 24	3 48	+0:49
3133	10	(1212)	"	(14)	4 29	4 43	4 15	4 29	+0:45

 $\Delta T = -1^m$

25-26/IX/64 K.

T.S.

T.A.

3134	1	(8319)	IIa-E	(22)	22 22	22 44	21 55	22 17	+0:49
3135	2	(8512)	"	(22)	23 05	23 27	22 38	23 00	+0:59
3136	3	(8567)	"	(58)	23 41	0 39	23 14	0 12	+1:43
3137	4	(323)	"	(76)	1 31	2 47	1 04	2 20	+1:05

 $\Delta T = +1^m$

1-2/X/64 K.

T.S.

T.A.

3138	1	(8573)	IIa-E	(12)	23 59	0 11	23 07	23 19	+1:37
3139	2	(61)	"	(66)	0 25	1 31	0 33	1 39	+0:44
3140	3	(338)	"	(6)	1 59	2 05	2 07	2 13	+0:56
3141	4	(443)	"	(58)	2 22	3 20	2 30	3 28	+1:22
3142	5	(9831)	"	(46)	4 02	4 48	4 10	4 56	+1:12

25-7	5	A	N $\bar{E}$ 50°	12.9	14.6	14.6 +4	T. U. 0 54 ^m → 120 ^m ✓
"	"	B	"	12.6	14.4	14.3 +4	1 30 1 58 ✓
"	"	C	"	12.3	14.0	14.0 +2	2 20 2 30 ✓
"	"	A	"	11.6	13.7	13.5 +4	2 57 3 29
"	"	B	"	11.2	13.2	13.0 +6	3 43 4 28
"	"	C	"	11.2	12.7	12.7 +2	4 44 4 59
"	"	A	"	11.1	12.4	12.4 +2	5 25 5 39
"	"	B	"	10.7	12.2	12.0 +16	5 54 7 10
"	"	C	"	9.8	11.5	11.4 +6	7 25 8 55
"	"	A	"	9.9	11.2	11.2 +2	8 16 8 32

T. U.

25-7	5	A	N $\bar{E}$ 50°	16.7	17.4	17.4 +4	1 54 2 20
"	"	B	"	16.7	17.3	17.3 +2 +2	2 37 3 03
"	"	C	"	16.3	17.2	17.1 +20	3 13 4 31
"	5	A	"	15.7	16.9	16.7 +10	5 03 6 29

T. U.

25-7	5	A	N $\bar{E}$ 50°	9.9	12.5	12.5 +2	3 08 3 22
"	"	B	"	9.5	12.2	11.8 +12	4 34 5 52
"	"	C	"	9.0	11.2	11.2	6 08 6 14
"	"	A	"	8.2	10.9	10.8 +12	6 31 7 41
"	"	B	"	7.9	9.7	9.5 +10 +16	8 11 9 23

26

5-6/X/64 K.

T.S.

T.A.

3143	6	(18134)	Π_{A-E}	(54)	21 50	22 44	20 43	21 37	+1:03
3144	7	(185)	"	(48)	0 59	1 47	23 51	0 39	+0:44
3145	8	(498)	"	(30)	2 08	2 38	1 00	1 30	+0:44
3146	9	(674)	"	(3)	2 53	2 56	1 45	1 48	+0:40,5
3147	10	(658)	"	(88)	3 20	4 48	2 12	3 40	+1:51
3148	11	(1617)	"	(12)	5 21	5 41	4 21	4 33	+0:36

6-7/X/64 K.

T.S.

T.A.

3149	1	(7961)	Π_{A-E}	(34)	21 15	21 49	20 04	20 28	+0:46
3150	2	(8083)	"	(46)	22 08	22 54	20 57	21 43	+1:26

T.U. = T.A. + 3^R desde 14.X.64

23-24/X/64 K.

T.S.

T.U.

3151	1	(7937)	Π_{A-E}	(40)	21 49	22 29	23 34	0 14	+1:27
3152	2	(8542)	"	(52)	23 03	23 55	0 48	1 40	+1:08,5

24-25/X/64 K.

T.S.

T.U.

3153	1	(8033)	Π_{A-E}	(54)	22 24	23 18	0 04	0 58	+1:56
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30-31/X/64 K.

T.S.

T.U.

3154	1	(8014)	Π_{A-E}	(68)	22 29	23 37	23 45	0 53	+2:11
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31/X-1/XI/64 K.

T.S.

T.U.

3155	1	(7878)	Π_{A-E}	(50)	22 39	23 24	23 51	0 41	+2:31
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T.O. 27

25-7	5 d	A Ne 50 ^Δ	11.0 13.7	13.5 + 16	0 43 miles	1 53
"	" "	B "	9.6 11.7	11.5 + 10	3 51	4 49
"	" "	C "	9.0 11.1	11.0 + 6	5 00	5 36
"	" "	A "	8.8 10.5	10.5	5 45	5 48
"	" "	B "	8.3 10.3	9.9 + 20	6 12	8 00
"	" "	C "	7.8 9.4	9.4 + 2	8 21 Rep.	8 35

T.U.

25-7	5 d	A Ne 50 ^Δ	11.9 13.5	13.4 + 4	0 04	0 42
"	" d	B "	11.5 13.1	12.9 + 10	0 54 Si miles	1 53

25-7	5 d	A Ne 50 ^Δ	14.6 16.3	16.2 + 6		
"	" d	B "	14.0 15.9	15.6 + 10		

25-7 5 m A Ne 50^Δ 18.5 19.0 19.0 16

25-7 5 d A Ne 50^Δ 13.9 17.6 17.1 + 20

25-7 5 d A Ne 50^Δ 14.5 16.2 16.0 + 30

28

6-7 $\sqrt{x}$ / 64. k.

T.S

T. U.

3156 (8663) + Γ_{a-F} (30) 23 31 0 01 0 14 0 47 + 1:00

9-10/51/64 K.

T. S.

T. O.

3157 1 (7842) Π_{A-E} / (66) 23 11 0 17 23 45 0 51 +3:14

3158 2 (8663) " (30) 057 127 131 201 +2:25

3159 3 (708) 16 235 251 308,5 324,5 + 0:20

3160 4 (845) " (26) 259 325 3325 3585 +0:25

3161 5 1980 " 162 350 452 423 525+1:09.5

3162 6 $\begin{pmatrix} 11 & 21 \end{pmatrix}$ n.s. $\begin{pmatrix} 30 \end{pmatrix}$ 510 540 543 613 +1:47

10-11/21/64 K.

T. S.

T. U.

3163 1 (1146) IIa-E (18) 455 513 524 542 +1:22

3/64 2 (16/17) " (19) 522 534 551 603 +0:29

31653 (1657) " (18) 547 605616 634 +0:52

3166 4 (2109) 34. (72) 631 743 700 812 +1:10

25-7	5	A Ne 50 ³	20.2	21.0	20.8 +10
------	---	----------------------	------	------	----------

25-7	5	A Ne 50 ⁴	14.6	17.4	16.9
"	"	B "	13.0	15.9	15.5
"	"	A "	12.5	14.6	14.6
"	"	B "	12.4	14.5	14.2
"	"	A "	12.0	14.0	13.6
"	"	B "	11.7	13.4	13.2

25-7	5	A Ne 50 ⁵	14.2	15.0	14.9
"	"	B "	14.0	14.8	14.8
"	"	C "	14.0	14.8	14.8
"	"	A "	13.9	14.6	14.5 -6 ^m

Espectrógrafo de red.

1. Ancho de ranura.

Ranura se abre moviendo el cilindro graduado (en 24 divisiones) en la dirección del movimiento de aguja de reloj. Como mejor ancho de ranura fue elegido el ancho que corresponde a la lectura 21 sobre el cilindro graduado y que sobre la película equivale al ancho de la línea espectral en 22 μ .

Lectura	Disco atmosférico diámetro de imagen	Equivalente en la película	
15	2" = 160 μ	16 μ	
19	2,5	20 μ	} mejor ancho
21 $\longleftrightarrow$	2,75 $\longleftrightarrow$	22 μ	
23	3" = 240 μ	24 μ	

2. Largo de ranura.

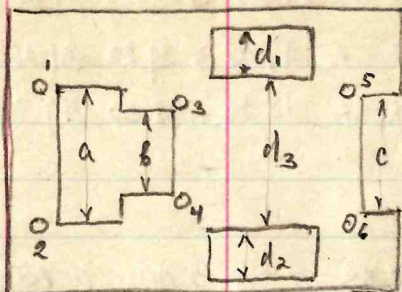
La máscara tiene 3 ventanas para distintos largos: a, b, c; 2 ventanas para el espectro de comparación: d_1 y d_2 ; y, además, 6 orificios.

$$a = 7 \text{ mm}; b = 4,5 \text{ mm}; c = 6 \text{ mm}; d_1 = d_2 = 2,4 \text{ mm}$$

La distancia entre ventanas d_1 y d_2 es $d_3 = 7,9 \text{ mm}$

$$d_1 + d_3 + d_2 = 12,7 \text{ mm}$$

máscara.



3. Microscopias.

Para observar la imagen de estrella sobre ranura hay 2 microscopios que dan imagen invertida.

4. Buscador II.

El buscador II tiene aumento 44 y la pupila de salida de diámetro $d = 2,7 \text{ mm}$.

26-27/VI/65 J.

T. S.

T. U.

A. h. m.

1	23 Sco (6165)	II a-D	(1 ^m 30 ^s)	17 ^h 34 ^m	35 ^m 30 ^s	3 ^h 05 ^m 30 ^s	07 ^m 00 ^s	+ 1 03
2	α Ara (6510)	"	(1 ^m 40 ^s)	17 58	59 40	3 29 30	31 10	+ 0 32
3	34 Sco (6508)	"	(1 ^m 20 ^s)	18 17	18 20	3 48 30	49 50	+ 0 51

10-11/VII/65 K.

1	α Cir (5463)	II a-D	(6 ^m)	15 33	15 39	0 09	0 15	+ 0 57
2	β Aps (6163)	"	(19 ^m)	16 45	17 04	1 21	1 40	+ 0 17
3	β Ara (6461)	"	(6 ^m , 5)	17 51	17 57,5	2 27	2 33,5	+ 0 34

12-13/VIII/65 K.

1	γ Cen (5231)	II a-D	(4 ^m)	14 46	14 50	23 14	23 18	+ 0 57
---	---------------------	--------	-------------------	-------	-------	-------	-------	--------

14-15/IX/65 K.

1	19 Sge (6859)	II a-D	(7 ^m)	19 32	19 39	3 53	4 00	+ 1 17,5
2	46 Sge (7342)	"	(11 ^m)	20 18	20 29	4 38	4 49	+ 1 04,5

16-17/X/65 K.

1	χ Cen (5285)	II a-D	(9 ^m)	14 58	15 07	23 06	23 15	+ 0 59,5
2	β Cen (5267)	"	(30 ^s)	15 28	15 28,5	0 12	0 12,5	+ 1:58:15

17-18/XI/65 K.

1	μ Cen (5193)	II a-D	(3 ^m)	14 44	14 47	22 54	22 57	+ 0 59,5
2	δ Cet (5339)	"	(28 ^s)	15 21	15 49	23 31	23 59	+ 1 14
3	β TrA (5897)	"	(3 ^m , 5)	16 24	16 27,5	0 34	0 37,5	+ 0 36
4	γ Aps (6102)	"	(20 ^s)	17 00	17 20	1 04	1 24	+ 0 43

temp. am

21a	5		I = 21	Subexp.
"	"		"	
"	4		"	
21a	5	4.6	"	
"	"	4.1	"	
"	"	3.5	"	
21a	3	8.7	"	Pasan los umbes
21a	4	4.3	"	
"	"	3.9	"	
21a	5	5.4	"	
"	"	4.9	"	
21a	5	7.1	"	
"	"	6.7	"	
"	"	6.3	"	
"	"	6.1	"	se muello

25-26/VII/65 K.

T.S.

T.V.

A.h.m.

✓	1	206 Sco (6084) II a-0	(2 ^m)	16 48	16 50	0 27	0 29	+ 0 31
✓	2	35 η Oph (6378) "	(1,5)	17 17	17 18,5	0 56	0 57,5	+ 0 11

30-31/VII/65 K.

✓	1	20 ε Sgr (6879) II a-0	(4 ^m)	18 36	18 40	1 54	1 58	+ 0 18
✓	2	35 α Sco (6527) "	(3 ^m)	19 14	19 17	2 32	2 35	+ 1 44,5
✓	3	34 G Sgr (7121) "	(4 ^m)	20 01	20 05	3 19	3 23	+ 1 11,5
✓	4	38 ζ Sgr (7194) "	(3 ^m)	20 23	20 26	4 01	4 04	+ 1 25,5
✓	5	65 B Aql (7710) "	(3 ^m)	21 22	21 25	4 40	4 43	+ 1 16
✓	6	22 β Aql (8232) "	(5 ^m)	21 54	21 59	5 12	5 17	+ 0 28
✓	7	22 β Aql (8232) "	(6 ^m)	22 31	22 37	5 49	5 55	+ 1 05,5

5-6/VIII/65 K.

En el espectrógrafo de red fué cambiado el espejo mayor diámetro: $d_2 = 27.5 \text{ mm}$. En la consecuencia de anterior $I_1 = 21$ se cambió por el actual $I_2 = 18,5$.

16-17/VIII/65 K.

✓	1	8 β Sco (5984) II a-0	(2 ^m)	16 45	16 47	22 56	22 58	+ 0 44
✓	2	μ Sco (6247) "	(2 ^m)	17 38	17 40	23 49	23 51	+ 0 51
✓	3	μ ² Sco (6252) "	(3 ^m)	18 03	18 06	0 14	0 17	+ 1 15,5
✓	4	10 γ Sgr (6746) "	(6,5)	18 31	18 37,5	0 42	0 48,5	+ 0 32
✓	5	α Sco (6973) "	(24 ^m)	18 56	19 20	1 11	1 35	+ 0 41
✓	6	41 ε Aql (7447) "	(14 ^m)	20 09	20 23	2 19	2 33	+ 0 42

21a	5	20.0	I = 21
"	"	18.0	" se nubló

21a	5	16.5	"
"	"	16.2	"
"	"	15.8	"
"	"	15.5	"
"	"	15.2	"
"	"	15.2	"
"	"	15.8	" se nubló

jo secundario de diametro $d_s = 15 \text{ mm}$ por el otro de que fue' cambio en el enfoque del espectrógrafo:

21a	5	12.7	I = 18.5
"	"	11.8	"
"	"	11.8	"
"	"	11.6	"
"	"	11.5	"
"	3	11.2	" Veto se nubló

18-19/VIII/65 K.

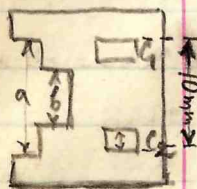
T.S.

T.V.

A.h.m.

✓	1	58 η Sex (6869) IIa-0	(14 ^m)	18 40	18 54	0 42	0 56	+ 0 30
✓	2	α Sgr (7348) "	(8 ^m)	20 03	20 11	2 05	2 13	+ 0 47
✓	3	α Pav (7790) "	(4 ^m)	20 33	20 37	2 35	2 39	+ 0 14

Fueron puestas la lente pupilar sobre la



$$a = 10 \text{ mm}$$

$$b = 6.8 \text{ mm}$$

$$c_1 = c_2 = 1.5 \text{ mm}$$

Al principio del
(concurso) del día

11-12/XI/65 K.

T.S.

T.V.

A.h.m.

✓	1	732 Aqr (8698) IIa-0	(12)	1:00	1:12	1 32	1 44	+ 2 11.5
✓	2	ε Phe (25) "	(6)	1 33	1 39	2 05	2 11	+ 1 30
✓	3	γ Eri (674) "	(1)	2 29	2 30	3 00	3 01	+ 0 15.5
✓	4	δ Hyi (705) "	(3)	2 55	2 58	3 28	3 31	+ 0 36.5
✓	5	HR 1106 "	(13)	4 31	4 44	5 03	5 16	+ 1 02.5
✓	6	57 μ Eri (1520) "	(2)	5 17	5 19	5 48	5 50	+ 0 36

12-13/XI/65 H.K.

el enfoque del espejo-cámara:

✓	1	α Phe (99) IIa-0	(1.5)	1 20.5	1 22.0	1 41 45	1 43.15	+ 0:58:45
✓	2	"	"	1 37.5	1 39.0	1 58 45	2:00:15	1:15:45
✓	3	"	"	2 20.0	2 21.5	2 41 15	2 42 45	1:58:15
✓	4	"	"	2 29.5	2 31.0	2 50 45	2 52 15	2:07:45

$F = 380$ (enfoque del telescopio) 37

	C			
21a	4-3		7.5	$I = 18.5$ se nubló por 0.5
"	4		7.1	"
"	5		6.8	"
				se nubló

ramera y una muela más cara;

en septiembre fue cambiado el espejo secundario
nuevo $\varnothing = 27.5 \text{ mm}$ por el espejo de $\varnothing = 15 \text{ mm}$.

	C		$F_{\text{amb.}}$	I^1
21b	5	$F_c = 5^A$	13.2	$I = 17.0$
"	"	"	13.0	"
"	"	"	12.0	"
"	4	"	11.1	" se veló
"	4	"	10.9	"
"	3	"	10.7	"

16b	5	6^A	13.1	$I = 15.5$
"	"	"		$I = 16.5$
"	"	"		$I = 15.25$
"	"	"		$I = 15.75$

¹⁾ I es el índice del enfoque del espejo-cámara del espectroscopio.

14-15/XI/65 K.

T.S.

T.V.

A.h.m

✓	1	732 Apr (8698)	IIa-0	(14)	1 18	1 32	1 35	1 49	+2 35
✗	2	37 Cet (366)	"	(12)	2 00	2 12	2 16	2 28	+0 54
✓	3	765 Cet (740)	"	(8)	2 58	3 06	3 15	3 23	+0 32
✓	4	828 Cet (779)	"	(1,5)	3 33	3 34,5	3 50	3 57,5	+0 57

15-16/XI/65 K.

✓	1	525 Cet (509)	IIa-0	(3)	2 00	2 03	2 14	2 17	+0 20,5
✗	2	595 Cet (585)	"	(12)	2 21	2 33	2 35	2 47	+0 30
✓	3	595 Cet (585)	"	(12)	2 42	2 54	2 55	3 07	+0 51
✗	4	(997)	"	(16)	3 42	3 58	3 56	4 12	+0 34
✓	5	24 Eri (1146)	"	(15)	4 28	4 33	4 41	4 46	+0 49
✓	6	48 V Eri (1463)	"	(1,5)	4 57	4 58,5	5 10	5 11,5	+0 24

16-17/XI/65 K.

✓	1	46 Cet (412)	IIa-0	(20)	1 54	2 14	2 03	2 23	+0 42
✗	2	34 γ Eri (1231)	"	(3)	4 17,5	4 20,5	4 26,5	4 29,5	+0 24

17-18/XI/65 K.

✓	1	135 Eri (984)	IIa-0	(6)	4 00	4 06	4 06	4 12	+0 50
✗	2	222 γ Eri (1181)	"	(7)	4 29,5	4 36,5	4 35,5	4 42,5	+0 48
✓	3	53 Eri (1481)	"	(15)	5 13	5 18	5 20	5 25	+0 40
✓	4	485 Ori (1931)	"	(1)	6 02,5	6 03,5	6 08,5	6 09,5	+0 27

18-19/XI/65 K.

✓	1	16 β Cet (188)	IIa-0	(0,5)	1 31 45	1 32 15	1 33 45	1 34 15	+0 52
---	---	----------------	-------	-------	---------	---------	---------	---------	-------

	C		$t^{\circ}\text{C}$	
166	5	$F_c = 6^{\Delta}$	14.4	$I = 15.75$
"	"	"	14.3	"
"	"	"	13.9	"
"	"	"	13.7	"
166	5	$F_c = 6^{\Delta}$	16.7	"
"	"	"	16.4	" con * gueta sobre rama
"	"	"	16.2	"
"	"	"	15.8	" Es doble: $m = 9.1$
"	"	"	15.2	"
"	"	"	15.7	"
166	4	$F_c = 6^{\Delta}$	19.6	"
"	3	"	19.2	"
166	5	$F_c = 6^{\Delta}$	22.1	"
"	"	"	21.9	"
"	"	"	21.5	"
"	"	"	21.3	"
166	5	$F_c = 6^{\Delta}$	23.3	"

40

18-19/XI/65 K.

T. S.

T. U.

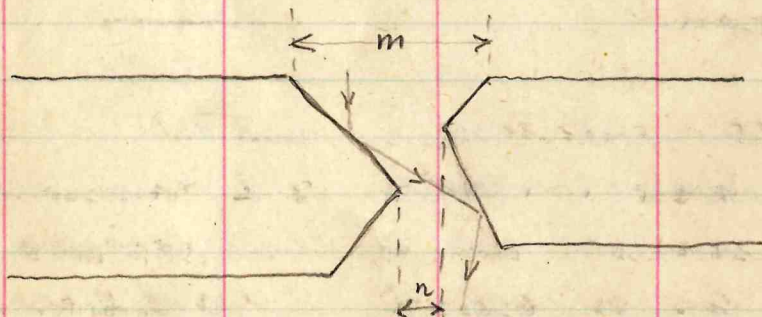
A.h.m.

✓	2 x 3cl (280) IIa-0	(2)	1 51	1 53	1 53	1 55	+0 57
✓	3 450 Clt (402) "	(3,5)	2 15	2 18,5	2 17	2 20,5	+0 56
✓	4 22p Clt (708) "	(4,5)	2 58	3 02,5	2 59	3 03,5	+0 37
✓	5 50 r'Ezi (1453) "	(8,5)	4 55	5 03,5	4 57	5 05,5	+0 29
✓	6 (1621) "	(4,5)	5 23	5 27,5	5 25	5 29,5	+0 27
✓	7 9p Lep (1829) "	(2)	5 42	5 44	5 44	5 46	+0 18

20-21/XI/65 K.

✓	1 12'Ezi (818) IIa-0	(5)	3 23,5	3 28,5	3 19,5	3 24,5	+0 44
✓	2 12'Ezi (818) "	(6,2)	3 44,5	3 50,7	3 37,5	3 43,7	+1 05
✓	3 16E*Ezi (1003) "	(5)	4 12,5	4 17,5	4 05,5	4 10,5	+0 58

Con el fin de mejorar el enfoque del espectro-
grafo fue estudiada la ranura bajo microscopio
y se encontró que los labios de ella tiene tal
posición que no definen bien el ancho de ranura



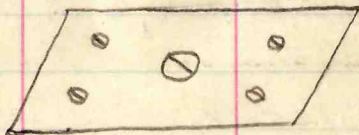
La vista del costado de los labios de ranura
de este dibujo vemos que es difícil decir
que ancho tiene la ranura: m ó n, ó cual-

	C		t°	
166	5	$Fe 6^3$	22.9	$I = 15.75$
"	"	"	22.5	"
"	"	"	22.3	"
"	"	"	22.2	"
"	"	"	22.0	"
"	"	"	22.0	"

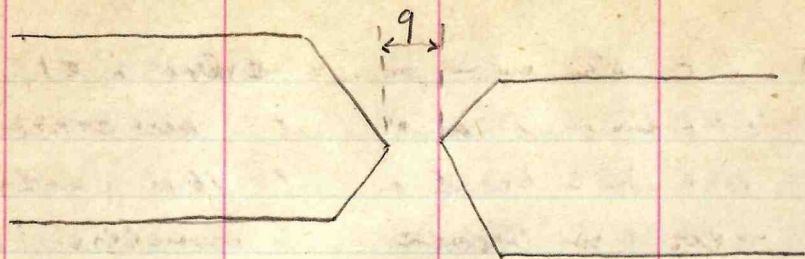
166	5	$Fe 6^3$	23.7	"
16a	"	—	23.4	"
166	"	$Fe 6^3$	23.2	"

quier otro. Para definir este ancho bien en el soporte metálico, sobre cual está pegado uno de los labios del vidrio aluminizado, fueron agregados 4 tornillos más alrededor del tornillo central grande.

Mirando el reflejo del tubo fluorescente

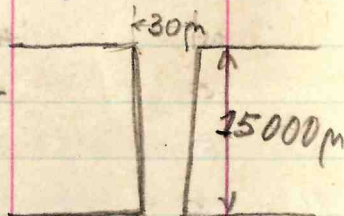


prendido sobre dos labios de la ramra y usando cinco tornillos fue conseguida la posición paralela de las superficies de los labios de ramra con el ancho "g" bien definido como muestra el dibujo en la pag. 42. Cuando las superficies de los labios no estaban paralelas,



el imagen del tubo fluorescente no presentaba una línea recta sino doblada.

En vista de arriba de la ranura bajo del microscopio tiene aspecto así:



Después de armar la ranura, la relación entre la lectura sobre el cilindro graduado y el ancho de ranura se cambió. La tabla dada en este cuaderno de observación en la pag. 30 desde ahora ya no es válida. La ranura comienza abrirse con el índice sobre tambor i, e 5. Después, pasando por

1-2 / XII / 65 K.

T.S.

T.V.

A.h.m

✓	1 λ Tuc (77)	IIa-0	(4 ^m)	1 20	1 24	0 30	0 34	+1 04,5
✓	2 β Phe (322)	"	(2 ^m)	2 00	2 02	1 05	1 07	+0 57,5
✓	3 γ^2 Hyi (570)	"	(10 ^m)	2 23	2 33	1 33	1 43	+0 34,5
✓	4 β Hor (909)	"	(5,5 ^m)	3 21	3 26,5	2 31	2 36,5	+0 26
✓	5 β Ret (1175)	"	(5 ^m)	4 01	4 06	3 11	3 16	+0 20
✓	6 γ Dor (1338)	"	(3 ^m)	5 10	5 13	4 20	4 23	+0 57,5

10, 15, 20 y 0 debemos parar sobre $i_2 = 1$, cuando el ancho de ranura es igual a 160μ que corresponde al ancho de la línea sobre la película 16μ y está próximo al poder resolvente de la emulsión de la película (15-16 μ). La nueva tabla de la relación entre el índice ó lectura sobre tambores y el ancho de ranura

Lectura	Ancho	Equivalente en la película
0	150 μ	15 μ
1 $\longleftrightarrow$ 2	$2'' = 160 \mu$	16 μ
2	170	17
3	180	18
4	190	19
5	200	20
6	210	21
7	$2,5'' = 220 \mu$	22 μ

16	5	18.7	$I = 15.75$
"	"	18.1	"
"	"	17.9	"
"	"	17.5	"
"	"	18.3	"
"	"	19.1	"

	1-2/XII/65	K.		T. S.	T. U.	A. h. m.
✓	7 348 Ori (1852)	IIa-0	(1 ^m)	5 44	5 45	4 54 4 55 +0 15,5
✓	8 348 Ori (1852)	"	(1 ^m)	6 22	6 23	5 32 5 33 +0 53

3-4/XII/65 K. enfoque del espejo - cámara

✓	1 ϵ Phe (338)	IIa-0	(1 ^m)	1 38	1 39,5	0 40 0 41,5 +0 32
✓	2 ϵ Phe (338)	"	(1 ^m)	1 56	1 57,5	0 58 0 59,5 +0 50
✓	3 ϵ Phe (338)	"	(1 ^m)	2 06	2 07,5	1 08 1 09,5 +1 00
✓	4 ϵ Phe (338)	"	(1 ^m)	2 12	2 13,5	1 14 1 15,5 +1 06

4-5/XII/65 K. enfoque del espejo - cámara

✓	1 41 Eri (1347)	IIa-0	(1 ^m)	4 51,5	4 52,5	3 48,5 3 49,5 +0 36
✓	2 41 Eri (1347)	"	(1 ^m)	5 02,5	5 03,5	3 59,5 4 00,5 +0 47
✓	3 41 Eri (1347)	"	(1 ^m)	5 11,5	5 12,5	4 08,5 4 09,5 +0 56
✓	4 41 Eri (1347)	"	(1 ^m)	5 20,5	5 21,5	4 17,5 4 18,5 +1 05
✓	5 41 Eri (1347)	"	(1 ^m)	5 28,5	5 29,5	4 25,5 4 26,5 +1 13

5-6/XII/65 K. enfoque del espejo - cámara

✓	1 β Ret (1175)	IIa-0	(6 ^m)	4 09	4 15	3 04 3 10 +0 28
✓	2 β Ret (1175)	"	(6 ^m)	4 26	4 32	3 21 3 27 +0 45
✓	3 β Ret (1175)	"	(6 ^m)	4 40	4 46	3 35 3 41 +0 59

6-7/XII/65 K. enfoque del espejo - cámara

✓	1 β Ret (1175)	IIa-0	(6 ^m)	4 12,5	4 23,5	3 08,5 3 14,5 +0 38
✓	2 β Ret (1175)	"	(6 ^m)	4 39	4 45	3 30 3 36 +0 59,5
✓	3 β Ret (1175)	"	(6 ^m)	4 58	5 04	3 49 3 55 +1 18,5

$\phi = 14''$ es diámetro de la
imagen de la *

$$I = 15.75 \quad \phi = 14''$$

$$I = 15.75 \quad \phi = 14''$$

$$26 \quad 5 \quad 24.7$$

$$I = 15.75$$

$$26 \quad 4 \quad 24.6$$

$$I = 17.0$$

$$26 \quad 4 \quad 24.5$$

$$I = \boxed{18.0} \text{ mejor de todos}$$

$$26 \quad 3 \quad 24.5$$

$$I = 15.0 \text{ se nubla'}$$

$$26 \quad 5 \quad 21.3$$

$$I = 17.5$$

$$26 \quad 4 \quad 21.2$$

$$I = 18.5$$

$$26 \quad 4 \quad 21.1$$

$$I = 19.0$$

$$26 \quad 4 \quad 21.1$$

$$I = 19.5$$

$$26 \quad 3 \quad 21.0$$

$$I = \boxed{20.0} \text{ se selo'}$$

$$26 \quad 4 \quad 21.1$$

$$I = 20.0$$

$$26 \quad 4 \quad 20.9$$

$$I = 21.0$$

$$26 \quad 4 \quad 20.7$$

$$I = \boxed{22.0}$$

$$16 \quad 4 \quad 19.5$$

$$I = \boxed{22.0}$$

$$16 \quad 4 \quad 19.4$$

$$I = 22.5$$

$$16 \quad 4 \quad 19.3$$

$$I = 23.0$$

46

6-7/ $\overline{XII}$ /65 K.

T.S.

T.O.

A.h.m

✓	4	β Ret (1175)	$\overline{IIa-0}$	(6 ^m)	5 13	5 19	4 04	4 10	+1 33,5
✓	5	β Ret (1175)	"	(6 ^m)	5 28	5 34	4 19	4 25	+1 48,5
✓	6	β Ret (1175)	"	(6 ^m)	5 46	5 52	4 37	4 43	+2 06,5

8-9/ $\overline{XII}$ /65 K.

✓	1	ψ Phe (555)	$\overline{IIa-0}$	(16 ^m)	2 27,5	2 43,5	2 11	2 27	+0 36
✓	2	ϵ Hgi (806)	"	(2 ^m)	2 54	2 56	1 37	1 39	+0 15
✓	3	θ ' Eri (897)	"	(1 ^m)	3 15,5	3 16,5	1 58,5	1 59,5	+0 20

11-12/ $\overline{XII}$ /65 K.

Ensayo con el ancho de zarrucha.

✓	1	3 η Eri (874)	$\overline{IIa-0}$	(5 ^m)	3 36,5	3 41,5	2 06,5	2 11,5	+0 45
✓	2	3 η Eri (874)	"	(3,5 ^m)	3 57	4 00,5	2 27	2 30,5	+1 05
✓	3	(1288)	"	(4,5 ^m)	4 31	4 35,5	3 01	3 05,5	+0 27
✓	4	(1288)	"	(6,5 ^m)	4 44	4 50,5	3 14	3 20,5	+0 40

13-14/ $\overline{XII}$ /65 K.

✓	1	5 Eri (899)	$\overline{IIa-0}$	(8,3 ^m)	3 23	3 31,3	1 46	1 54,3	+0 30,5
✓	2	17 Eri (1070)	"	(4 ^m)	3 48	3 52	2 12	2 16	+0 23
✓	3	32 Eri (1212)	"	(15 ^m)	4 19	4 34	2 41,5	2 56,5	+0 35
✓	4	(1483)	"	(6 ^m)	5 13	5 19	3 35,5	3 41,5	+0 40
✓	5	28 η Ori (1788)	"	(40 ^s)	5:30:10	5:30:50	3:52:40	3:53:20	+0 09
✓	6	44 ζ Ori (1899)	"	(20 ^s)	5:47:20	5:47:40	4:09:50	4:10:10	+0 15

14-15/ $\overline{XII}$ /65 K.

✓	1	680 Cet (681)	$\overline{IIa-0}$	(2 ^m)	3 03	3 05	1 22	1 24	+0 48
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16	4		19.3	$I = 23.5$
"	"		19.2	$I = 0.0$
"	"		19.1	$I = 0.5$ se feló
16	5		16.7	$I = 22.0$
"	4		16.7	"
"	3		16.6	" Pusan los nubes
16	5	$Fe=6^S$	17.8	$I = 22.0$
76	"	"	17.6	"
76	"	"	17.4	"
16	"	"	17.3	" mejor 16
16	5		15.3	$I = 22.0$
"	"		15.0	"
"	"		14.8	"
"	"		14.3	"
"	"		14.1	"
"	"		14.0	"
16	5		18.0	$I = 22.0$

14-15/XII/65 K.

T. S.

T. V.

A. h. m.

✓	2	680 Cet (681)	II a-0	(2 ^m)	3 11	3 13	1 30	1 32	+0 55
✓	3	238 Eri (1136)	"	(3 ^m)	4 00	4 03	2 19	2 21	+0 21
✓	4	505 Eri (1453)	"	(9 ^m)	4 46	4 55	3 05	3 14	+0 20
✓	5	654 Eri (1617)	"	(3 ^m)	5 20	5 23,5	3 39	3 42,5	+0 32
✓	6	287 Ori (1788)	"	(1,3)	5:41:30	5:42:48	4:00:30	4:01:48	+0 21
✓	7	446 Ori (1899)	"	(40 ^s)	5:53:40	5:54:20	4:12:40	4:13:20	+0 22
✓ F.	8	✓ 4 (3017)	"	(8 ^m)	8 25	8 33	6 44	6 52	+0 46

15-16/XII/65 K.

✓	1	195 Eri (1088)	II a-0	(2 ^m)	3:48.5	3:50,7	2:05	2:07,2	+0 19
✓	2	182 Eri (1084)	"	(4 ^m)	4 07,5	4 11,5	2 24	2 28	+0 40
✓	3	20 Eri (1100)	"	(6 ^m)	4 28	4 34	2 44,5	2 50,5	+0 58
✓	4	525 Eri (1464)	"	(4 ^m)	4 56	5 00	3 12,5	3 16,5	+0 25
✓	5	287 Ori (1788)	"	(3 ^m)	5 44,5	5 47,5	4 01	4 04	+0 25
✓	6	446 Ori (1899)	"	(1,3)	6 03,5	6 04,8	4 20	4 21,3	+0 32
✓	7	58 Mon (2227)	"	(8 ^m)	6 28	6 36	4 44,5	4 52,5	+0 20
✓ F.	8	(2616)	"	(10 ^m)	7 16.5	7 26,5	5 33	5 43	+0 26

16	5	17.9	I = 22.0
"	"	16.8	"
"	"	16.3	"
"	"	15.8	"
"	"	15.4	"
"	"	15.3	"
"	"	14.2	"

16	5	20.7	I = 22.0
"	"	20.5	"
"	"	20.5	"
"	"	20.5	"
"	"	20.4	"
"	"	20.4	"
"	"	20.2	"
"	4	20.0	" Viento fuerte

3-4/III/66

K.

T. S.

T. V.

HW 3167	1	HR 3703	IIA-E	(14)	10 54	11 08	4 03	4 17	+1 46
3168	2	4355	"	(17)	12 07	12 24	5 15	5 32	+1 06
3169	3	4706	"	(18)	12 57	13 15	6 06	6 24	+0 47
3170	4	5115	"	(44)	14 06	14 50	7 15	7 59	+0 53

5-6/III/66

K.

3171	1	HR 2148	IIA-E	(15)	7 10	7 25	0 08,5	0 23,5	+1 17
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8-9/III/66

K.

3172	1	HR 2148	IIA-E	(25)	8 48	9 03	1 37	1 52	+2 54
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9-10/III/66

K.

3173	1	HR 3970	IIA-E	(14)	10 31	10 45	3 16	3 30	+0 38,5
3174	2	HR 3981	"	(12)	11 01	11 13	3 47	3 59	+1 04,5
3175	3	HR 4220	"	(32)	11 41	12 13	4 27	4 59	+1 15,5
3176	4	HR 4185	"	(40)	12 30	13 10	5 16	5 56	+2 15
3177	5	HR 4823	"	(18)	13 26	13 44	6 12	6 30	+0 59
3178	6	HR 5069	"	(60)	14 00	15 00	6 45	7 45	+1 07

11-12/III/66

K.

3179	1	HR 3983	IIA-E	(34)	11 00	11 34	3 35	4 09	+1 15
3180	2	HR 4338	"	(26)	11 51	12 17	4 26	4 52	+0 58
3181	3	HR 4620	"	(34)	12 31	13 05	5 06	5 40	+0 43
3182	4	HR 4933	"	(18)	13 17	13 35	5 52	6 10	+0 26
3183	5	HR 4977	"	(54)	13 57	14 51	6 32	7 26	+1 15
3184	6	HR 5494	"	(48)	15 05	15 53	7 40	8 28	+0 47

12-13/III/66

K.

3185	1	HR 2863	IIA-E	(30)	8 41	9 11	1 14	1 44	+1 32,5
3186	2	HR 3665	"	(51)	9 25	9 30	1 58	2 03	+0 18

$F_{rel.} = 30\%, 8; F_{cám.} = 25.0$ de $\Phi_{H_2} = 40 \frac{h}{m}$.

a	↓				
25-7	5	A	Ne 50 ³	20.5	+6 m
"	"	C	Ne 50 ³	19.6	+7
"	"	A	"	19.2	+8 { Rep. Interc. estrella hay cerca de H ₂ una lín. de abs.
"	"	C	"	18.6	+20 { Pasan las nubes. Repet.
25-7	5	A	Ne 60 ³	18.1	e
25-7	4	A	Ne 60 ³	21.0	se nubla e
25-7	5	A	Ne 60 ³	21.1	
"	"	B	"	20.9	
"	"	C	"	20.7	
"	"	A	"	20.4	
"	"	B	"	20.1	e
"	"	C	"	19.7	
25-7	5	A	Ne 60 ³	18.9	
"	"	B	"	18.1	{ casi no tiene H ₂ . +2 m Interc. estrella: sacar una placa más.
"	"	C	"	17.5	
"	"	A	"	17.3	
"	"	B	"	17.0	Casi no tiene H ₂
"	"	C	"	16.7	
25-7	5	A	Ne 60 ³	22.1	
"	"	B	"	21.7	

12-13/III/66

K.

T.S.

T.U.

H03187	3	HR 3665	IIa-E	(5)	9 48	9 53	2 21	2 26	+0 41
3188	4	HR 3683	"	(30)	10 24	10 54	2 57	3 27	+1 27
3189	5	HR 4317	"	(34)	11 12	11 46	3 45	4 19	+0 28

13-14/IV/66

K.

3190	1	HR 4975	IIa-E	(12)	13 43	13 55	4 08	4 20	+0 40
3191	2	HR 5367	"	(8)	14 51	14 59	5 17	5 25	+0 38
3192	3	HR 5543	"	(20)	15 22	15 42	5 47	6 07	+0 43

A fines del mes abril del año 1966 hubo modificación
 tiene bajo del microscopio aspecto así: 
 Estando frente al tambor al momento en el que
 abrirse. Pero la luz aún no llega a la cámara
 Para la lectura 15 en la cámara fotográfica
 no aumentar el tiempo de la exposición en
 caídas. Con la abertura de la cámara 25 de
 La abertura de la cámara 32 es equivalente
 mas hasta este tiempo.

2-3/V/66

K.

T.S.

T.U.

3193	2	HR 6204	IIa-E	(36)	17 50	18 26	6 59	7 35	+1 26
3194	3	HR 6916	"	(20)	18 45	19 05	7 54	8 14	+0 23

3-4/V/66

K.

3195	6	HR 6628	IIa-E	(14)	18 46	19 00	7 53	8 07	+1 10
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25-7 5 c de 60" 21.6

" " A " 21.5

" " B " 21.3

+4^m, Velo25-7 5d A de 1^m 14.7 16.1" " " A 2^m 14.4 15.6+1^m

" " d,d B " 14.3 15.4

Velado

cranes en la ranura. Ahora, cuando está socada, que corresponde al coro de la lectura del tambor. Todo de la aguja del reloj, la ranura comienza fotográfica cuando las lecturas del son de 0 hasta 10. Hay luz, pero para sacar un espectro es necesario 5 veces con respecto a la ranura antes de modificarlo aumentar el tiempo de la exposición en 3 veces a la abertura 25 de la ranura anterior que usa-

25-7 5d B de 2^m,5 13.3 15.1 14.9

" " " C 3 12.9 14.8 14.6

30-7 5d C de 2 14.4 15.7 15.7

54

7-8/V/66 K.

T. S.

T. U.

403196 1	HR 4689	<u>II</u> a-E	(7)	13 26	13 33	2 15	2 22	+1 13
3197 2	HR 4963	"	(12)	13 52	14 04	2 41	2 53	+0 51
3198 3	HR 5332	"	(36)	15 00	15 36	3 49	4 25	+1 06
3199 4	HR 5355	"	(44)	15 52	16 36	4 41	5 25	+2 00.5

10-11/V/66 K.

3200 1	HR 5033	<u>II</u> a-E	(72)	13 48	15 00	2 25	3 37	+1 05
3201 2	HR 5522	"	(64)	15 22	16 26	3 59	5 03	+1 09
3202 3	HR 6070	"	(16)	16 44	17 00	5 21	5 37	+0 38
3203 4	HR 6291	"	(36)	17 16	17 52	5 53	6 29	+0 41
3204 5	HR 6647	"	(54)	18 13	19 07	6 50	7 44	+0 52

11-12/V/66 K.

3205 7	HR 5485	<u>II</u> a-E	(18)	14 33	14 51	3 11	3 29	+0 02
3206 8	HR 5558	"	(28)	15 09	15 37	3 42	4 10	+0 31
3207 9	HR 5753	"	(96)	15 56	17 32	4 29	6 05	+1 16
3208 10	HR 5489	"	(18)	17 53	18 11	6 26	6 44	+3 21
3209 11	HR 6652	"	(92)	18 29	20 01	7 02	8 34	+1 26

2-3/VI/66 K.

3210 1	HR 5230	<u>II</u> a-E	(44)	16 03	16 47	3 10	3 53	+2 33
3211 2	HR 6139	"	(66)	17 56	19 02	5 02	6 08	+1 38
3212 3	HR 6912	"	(80)	19 27	20 47	6 33	7 53	+1 31

3-4/VI/66 K.

3213 1	HR 5240	<u>II</u> a-E	(68)	15 45	16 53	2 48	3 56	+2 23
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32-7	5	A	We 2 ^m	15.0	17.0	17.0
"	"	B	"	14.8	16.8	16.8
"	"	C	"	13.9	16.2	15.8
"	"	A	"	13.5	15.7	15.4

32-7	5	A	We 2 ^m , 3 ^m	9.8	12.3	11.8
"	"	B	"	9.2	11.4	10.9
"	"	C	"	9.0	10.7	10.6
"	"	A	"	8.6	10.4	10.3
"	"	B	"	8.4	10.0	9.7

32-7	3	A	We 2 ^m	11.1	12.5	12.5 + 4 ^m
"	4	B	"	11.1	12.4	12.4
"	5	C	"	10.5	12.1	11.9
"	"	A	"	10.2	11.6	11.6
"	"	B	"	10.1	11.4	11.2

32-7	5	A	We 2 ^m	13.3	15.2	14.6
"	"	B	"	13.3	14.1	13.9
"	"	C	"	12.7	13.4	13.3

32-7	5	A	We 2 ^m	13.4	14.6	14.5
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6-7/VI/66 K.

T. S.

T. V.

3214 2	HR 6134	Π a-E	(12)	17 47	17 49	4 37	4 39	+1 22
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7-8/VI/66 K.

3215 3	HR 4712	Π a-E	(50)	13 39	14 29	0 26	1 16	+1 43
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11-12/VI/66 K.

3216 1	HR 6134	Π a-E	(1)	16 50	16 51	3 21	3 22	+0 25
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3217 2	HR 5998	"	(68)	17 14	18 22	3 45	4 53	+1 44
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3218 3	HR 6657	"	(70)	19 06	20 16	5 37	6 47	+1 52
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29-30/VI/66 K., Lop.

3219	HR 6812	Π a-E	(3)	18 46	18 49	4 05,5	4 08,5	+0 37
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3-4/VII/66 K.

3220 1	HR 6662	Π a-E	(60)	19 30	20 30	4 33	5 33	+2 09,5
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16-17/VII/66 K.

3221 1	HR 5883	Π a-E	(12)	15 57	16 09	0 12	0 24	+0 16
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3222 2	HR 6029	"	(42)	16 22	17 04	0 37	1 19	+0 34,5
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3223 3	HR 6354	"	(86)	17 22	18 48	1 37	3 03	+1 02
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3224 4	HR 6660	"	(100)	19 05	20 45	3 20	5 00	+2 05
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17-18/VII/66 K.

3225 1	HR 6007	Π a-E	(44)	16 28	17 12	0 39	1 23	+0 44
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3226 2	HR 6353	"	(56)	17 27	18 23	1 37	2 33	+0 53
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32-7 4 A Ne 2^m 12.7 14.0 14.0 Rep. can temp = 1^m.

32-7 3 A Ne 2^m 12.0 14.0 13.8

32-7 5 d.m A Ne 2^m 10.3 11.9 11.9

" 5 B " 10.1 11.8 11.4 + 8^m

" 4 C " 9.0 10.7 10.3 nubes

32-7 5 A Ne 2^m 5.1 7.3 7.3

32-7 5 A Ne 2^m 9.2 10.4 10.4 + 10^m

32-7 5 A Ne 2^m 9.6 11.2 11.2

" " B " 9.3 11.1 10.9

" 4 C " 8.7 10.6 10.3 Pasaron las nubes

" " A " 7.9 9.6 9.4 " " "

32-7 4 A Ne 2^m 8.9 10.6 10.4

" 3 d.m B " 8.6 10.3 10.1

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17-18/VII/66 K.

T. S.

T. U.

HV 32273	HR 6663	$\Pi a-E$ (100)	18 42	20 22	2 52	4 32	+1 42
3228 4	HR 6668	" (70)	22 44	21 54	4 54	6 04	+3 28

5-6/VIII/66 K.

3229 1	HR 7039	$\Pi a-E$ (2)	19 20	19 22	2 14	2 16	+0 39
3230 2	HR 6663	" (100)	19 43	21 23	2 37	4 17	+2 43
3231 3	HR 7817	" (82)	21 38	23 00	4 32	5 54	+1 54

6-7/VIII/66 K.

3232 1	HR 6134	$\Pi a-E$ (0,5)	17 02	17 02,5	23 52	23 52,5	+0 36
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7-8/VIII/66 K.

3233 1	HR 6210	$\Pi a-E$ (68)	17 17	18 25	0 04	1 12	+1 11
3234 2	HR 6494	" (56)	18 37	19 33	1 24	2 20	+1 41

8-9/VIII/66 K.

3235 1	HR 6003	$\Pi a-E$ (54)	16 33	17 27	23 16	0 10	+0 55
3236 2	HR 5988	" (62)	17 48	18 50	0 31	1 33	+2 17
3237 3	HR 6316	" (26)	19 17	19 43	1 59	2 25	+2 32
3238 4	HR 7035	" (50)	20 02	20 52	2 44	3 34	+1 46

23-24/VIII/66 K.

3239 1	HR 6114	$\Pi a-E$ (44)	18 15	18 59	23 57	0 41	+2 13
3240 2	HR 7095	" (96)	19 20	20 56	1 02	2 38	+1 19
3241 3	HR 7668	" (96)	21 31	23 07	3 13	4 49	+2 17

32-7	4-5	C	Ne 2 ^m	8.2	9.8	9.6
"	5	A	"	7.8	9.1	9.0

32-7	5	A	Ne 2 ^m	6.5	8.2	8.2
"	"	B	"	6.1	8.0	7.5
"	"	C	"	5.5	7.1	6.9

32-7	3	A	Ne 2 ^m	7.5	8.8	8.8
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32-7	5	A	Ne 2 ^m	7.5	9.4	9.1
"	"	B	"	6.8	8.8	8.6

32-7	4	A	Ne 2 ^m	7.7	9.4	9.3
"	"	B	"	6.9	8.8	8.6
"	"	C	"	6.6	8.3	8.2
"	4-3	A	"	6.4	8.0	7.9

32-7	5	A	Ne 2 ^m	10.6	12.7	12.4
"	"	B	"	9.8	12.0	11.6
"	"	C	"	8.6	10.9	10.4

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23-24/VIII/66 K.

T.S.

T.O.

HV3242 4	HR 280	IIa-D (36)	0 20	0 56	6 01	6 37	-0 18
3243 5	HR 280	" (26)	2 02	2 28	7 43	8 09	+1 20
3244 6	HR 612	" (40)	2 44	3 24	8 25	9 05	+1 03

24-25/VIII/66 K.

3245 1	HR 6475	IIa-E (84)	18 01	19 25	23 40	1 04	+1 20,5
3246 2	HR 6934	" (18)	20 00	20 18	1 38	1 56	+1 41,5
3247 3	HR 7348	" (8)	20 34	20 42	2 12	2 20	+1 18

1-2/IX/66 K.

3248 1	HR 7156	IIa-E (102)	19 48	21 30	0 57	2 39	+1 43,5
3249 2	HR 7491	" (74)	21 57	23 11	3 06	4 20	+2 54,5
3250 3	HR 8919	IIa-D (114)	0 22	2 16	5 30	7 24	+1 53

2-3/IX/66 K.

3251 5	HR 7380	IIa-E (38)	20 57	21 35	2 02	2 40	+1 53
3252 6	HR 8137	IIa-D (90)	22 15	23 45	3 20	4 50	+1 45,5
3253 7	HR 9031	" (70)	0 11	1 21	5 16	6 26	+0 58

6-7/IX/66 K.

3254 1	HR 7337	IIa-D (18)	20 28	20 46	1 17	1 35	+1 18
3255 2	HR 7590	" (20)	21 03	21 23	1 52	2 12	+1 17
3256 3	HR 8425	" (15)	22 16	22 17,5	3 05	3 06,5	+0 11,5

32-7	5	A	Fe 6 ¹	7.6	9.5	9.4	} Area de Fe con el Sidris esmerilado
"	"	B	"	6.8	8.7	8.5	
"	"	C	"	6.7	8.3	8.1	

32-7	5	A	Ne 2 ^m	9.8	11.5	11.2	
"	"	B	"	8.9	10.8	10.8	
"	"	C	"	8.8	10.6	10.6	Feto

32-7	5	A	Ne 2 ^m	7.4	11.2	9.7	
"	"	B	"	6.0	9.2	8.4	
"	"	C	Fe 6 ¹	5.5	7.2	6.9	con el bid. esmeril.

32-7	5	B	Ne 2 ^m	9.1	10.2	10.2	
"	"	C	Fe 6 ¹	8.9	9.9	9.8	} Area de Fe con el vidrio esmerilado
"	"	A	"	8.2	9.7	9.6	

32-7	5	A	Fe 6 ¹	12.5	14.5	14.5	} Area de Fe con el sidris esmerilado
"	"	B	"	12.3	14.3	14.2	
"	"	C	"	12.1	13.8	13.8	

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9-10/X/66

K.

T. S.

T. U.

HR 32571	HR 7236	IIa-E (4)	21 08	21 12	145,5	149,5 + 2 07,5
32582	HR 7694	" (88)	21 38	23 06	215,5	343,5 + 2 17,5

6-7/X/66

K.

32591	HR 7738	IIa-E (140)	21 48	0 08	0 37	2 57 + 2 45
32602	HR 9087	IIa-O (80)	0 54	2 14	3 43	5 03 + 1 36
32613	HR 612	" (40)	2 41	3 21	5 30	6 10 + 1 00
32624	HR 1100	" (80)	3 40	5 00	6 28,5	7 48,5 + 0 47

8-9/X/66

K.

32635	HR 7675	IIa-E (120)	22 18	0 18	101,5	301,5 + 3 16,5
32646	HR 51	IIa-O (128)	0 48	2 56	3 31,5	5 39,5 + 1 41

11-12/X/66

K.

32651	HR 9108	IIa-O (122)	0 55	2 57	3 26	5 28 + 1 54
32662	HR 280	" (24)	3 18	3 42	5 48	6 12 + 2 34
32673	HR 939	" (92)	4 10	5 42	6 40	8 12 + 1 55

Beside 15. X. 66

T. U. = T. A. + 3^h

26-27/X/66

K.

32681	HR 8386	IIa-E (30)	23 41	0 11	111,5	141,5 + 1 58
32692	HR 8628	" (10)	0 35	0 45	2 06	2 16 + 2 02
32703	HR 280	" (15)	1 45	2 00	3 16	3 31 + 0 56,5
32714	HR 734	" (120)	2 48	4 48	4 18	6 18 + 1 21,5

32-7	4	A	Ne 2 ^m	14.5	15.5	15.5
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"	"	B	"	14.1	15.4	15.2
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32-7	5	A	Ne 2 ^m	14.4	16.0	15.7
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"	"	B	Fe 6 ^s	14.8	15.7	15.7
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"	"	C	"	14.5	15.5	15.4
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"	"	A	"	13.9	15.2	15.2
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32-7	5	A	Ne 2 ^m	16.1	18.3	17.6
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"	"	B	Fe 6 ^s	15.6	17.1	16.5
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32-7	5	A	Fe 6 ^s	8.7	12.8	11.3
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"	"	B	"	8.6	10.6	10.4
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"	"	C	"	7.8	9.7	9.2
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32-7	5	A	Ne 2 ^m	12.4	15.1	14.8	e
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"	"	B	"	11.5	14.5	14.4	e
---	---	---	---	------	------	------	---

"	"	C	"	10.9	13.2	13.2	
---	---	---	---	------	------	------	--

"	"	A	"	9.5	12.2	11.0	
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64

27-28/ $\bar{X}$ /66 K.

T. S.

T. V.

HR 32725	HR 8919	$\bar{\Pi}a-O$ (120)	0 45	2 45	2 07	4 07	+2 19
32736	HR 852	$\bar{\Pi}a-E$ (40)	3 03	3 43	4 29,5	5 09,5	+0 36
32747	HR 1240	" (20)	4 17	4 37	5 43,5	6 03,5	+0 30

29-30/ $\bar{X}$ /66 K.

32751	HR 8402	$\bar{\Pi}a-E$ (40)	23 07	23 47	0 31,5	1 11,5	+1 27
32762	HR 8260	" (46)	0 07	0 53	1 26	2 12	+2 56
32773	HR 817	" (100)	2 47	4 27	4 06	5 46	+0 55,5

30-31/ $\bar{X}$ /66 K.

32784	HR 9087	$\bar{\Pi}a-O$ (120)	1 01	3 01	2 16	4 16	+2 02,5
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31/ $\bar{X}$ -1/ $\bar{X}$ /66 K.

32795	HR 9031	$\bar{\Pi}a-O$ (124)	0 07	2 11	1 18,5	3 29,5	+1 21
32806	HR 814	$\bar{\Pi}a-E$ (120)	3 02	5 02	4 13	6 13	+1 22

1-2/ $\bar{X}$ /66 K.

32817	HR 8408	$\bar{\Pi}a-E$ (60)	23 38	0 38	0 46	1 46	+2 07
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25-26/ $\bar{X}$ /66 K.

32821	HR 1713	$\bar{\Pi}a-E$ (8 ¹)	5 43	5 43	0 515	5 15 08	+0 31
32832	HR 1713	" (10 ¹)	6 20	6 20	10 552	5 52 10	+1 08

20/ $\bar{X}$ -1/ $\bar{X}$ /66 K.

32841	HR 838	$\bar{\Pi}a-O$ (30)	3 06	3 36	2 18	2 48	+0 34
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Ramsay

A X

32-7 5 B 11.0 13.3 12.4

" " C Ne 2^m 9.7 12.0 11.6

" " A " 9.2 11.3 11.2

32-7 5 A Ne 2^m 14.9 18.0 17.6 e

" " B " 14.0 17.2 16.4 e

" " C " 12.3 15.0 14.0

32-0 5 A 14.3 16.0 15.4

32-0 5 A 15.8 18.2 17.4

32-7 " B Ne 2^m 15.3 16.8 16.232-7 5 A Ne 2^m 17.0 19.2 18.8 e32-7 4 A Ne 2^m 19.7 21.0 21.0 e

" " C " 19.6 20.8 20.8 e

32-0 5 A 21.0 24.1 23.9

66

30/XI-1/XII/66 K.

T.S.

T.V

4032852 HR 1121 IIa-D (160) 3 55 6 35 3 07 5 47 +1 37

2-3/XII/66 K.

32861 HR 674 IIa-D (24) 2 37 3 01 1 41 2 05 +0 34

32872 HR 939 " (76) 3 21 4 37 2 25 3 41 +0 57

4-5/XII/66 K.

32882 HR 1139 IIa-E (42) 4 25 5 07 3 21 4 03 +1 04 30

5-6/XII/66 K.

32893 HR 674 IIa-D (12) 2 18 2 30 1 10 1 22 +0 10

32904 HR 798 IIa-E (124) 2 41 4 45 1 33 3 37 +1 05

32915 HR 1312 " (72) 5 19 6 31 4 11 5 23 +1 44

32927 HR 2324 " (40) 7 14 7 54 6 05,5 6 45,5 +1 10

6-7/XII/66 K.

32931 HR 853 IIa-E (82) 3 14 4 36 2 02 3 24 +1 06 30

32942 HR 1347 " (4) 4 49 4 53 3 37 3 41 +0 36

32953 HR 1559 " (68) 5 14 6 22 4 02 5 10 +0 58 30

32964 HR 2502 " (44) 7 09 7 53 5 57 6 41 +0 47

32975 HR 2714 " (10) 8 08 8 18 6 56 7 06 +1 04

19-20/XII/66 K.

32981 HR 721 IIa-E (10) 2 54 3 04 0 55 1 05 +0 34

32992 HR 893 " (80) 3 31 4 51 1 30 2 50 +1 16

Rangetta
A Z

32-0 4 B 20.9 23.4 22.1

32-0 5 A 22.1 25.4 25.2

" " B 21.8 24.2 23.9

32-7 5 B Ne 2^m 16.7 18.8 18.6

32-0 5 A 19.9 22.1 22.0

" " B Ne 2^m 18.7 21.8 20.9

32-7 " C " 19.1 20.0 19.7

" " B " 19.4 19.5 19.4

32-7 4 A Ne 2^m 20.8 22.4 22.1

" " B " 20.5 21.8 21.8

" 3 C " 20.1 21.8 21.4

" 4 A " 19.7 21.0 20.8

" 3 B " 19.5 20.6 20.6

32-7 5 A Ne 2^m 19.2 22.0 21.6

" 4 B " 18.6 21.2 20.4 1c mello'

22-23 / $\overline{XII}$ / 66

K.

T. S.

T. U.

HU3300 1	HR 1357	$\overline{II}$ a-E	(96)	4 35	6 11	2 21,5	3 57,5	+ 1 08
3301 2	HR 2210	"	(126)	6 25	8 31	4 11	6 17	+ 1 18,5
3302 3	HR 3314	"	(8)	8 54	9 02	6 40	6 48	+ 0 35,5

23-24 / $\overline{XII}$ / 66

K.

3303 4	HR 1372	$\overline{II}$ a-E	(90)	5 57	7 27	3 39,5	5 09,5	+ 2 26
3304 6	HR 3486	"	(30)	9 02	9 32	6 44	7 14	+ 0 33

26-27 / $\overline{XII}$ / 66

K.

3305 1	HR 903	$\overline{II}$ a-E	(100)	3 22	5 02	0 52,5	2 32,5	+ 1 15
3306 2	HR 1476	"	(96)	5 23	6 59	2 53	4 29	+ 1 37

27-28 / $\overline{XII}$ / 66

K.

3307 a	HR 970	$\overline{II}$ a-E	(94)	3 46	5 20	1 12,5	2 46,5	+ 1 22,5
3308 b	HR 2345	"	(70)	6 46	7 56	4 12	5 22	+ 0 58,5
3309 c	HR 2683	"	(30)	8 26	8 56	5 52	6 22	+ 1 39

17-18 / $\overline{II}$ / 67

K.

3310 1	HR 2320	$\overline{II}$ a-E	(40)	7 30	8 10	1 34	2 14	+ 1 29
3311 2	HR 4172	"	(50)	11 01	11 51	5 05	5 55	+ 0 50

18-19 / $\overline{II}$ / 67

K.

3312 3	HR 2138	$\overline{II}$ a-E	(44)	6 26	7 10	0 26	1 10	+ 0 49
3313 4	HR 2602	"	(32)	7 21	7 53	1 21	1 53	+ 0 45
3314 5	HR 3038	"	(72)	8 05	9 17	2 05	3 17	+ 0 57

32-7	5	A	Ne 2 ^m	16.3	19.2	18.2
"	"	B	"	15.1	17.8	16.8
"	"	C	"	14.2	15.8	15.8

32-7	5	A	Ne 2 ^m	16.0	18.2	17.7
"	"	C	"	14.8	16.7	16.5

32-7	5	A	Ne 2 ^m	22.1	24.5	23.6
"	"	B	"	21.2	23.1	22.6

32-7	5	A	Ne 2 ^m	22.6	25.0	24.2	Pasan las ondas.
"	4	B	"	22.7	23.5	23.2	
"	5	C	"	22.2	23.2	23.1	

32-7	5	A	Ne 2 ^m	17.8	20.3	19.9
"	"	B	"	17.5	18.7	18.4

32-7	5	A	Ne 2 ^m	21.5	23.3	23.0
"	"	B	"	21.1	22.8	22.5
"	"	C	"	20.7	22.3	22.1

18-19/II/67 K.

T. S.

T. U.

33 15 6	HR 3661	IIa-E	(48)	9 42	10 30	3 41	4 29	+0 56
3316 7	HR 3856	"	(16)	10 50	11 06	4 49	5 05	+1 20

19-20/II/67 K.

3317 8	HR 2674	IIa-E	(42)	7 32	8 14	1 27	2 09	+0 51
3318 9	HR 2925	"	(92)	8 29	10 01	2 24	3 56	+1 42
3319 10	HR 3927	"	(52)	10 15	11 07	4 10	5 02	+0 48

20-21/II/67 K.

3320 a	HR 2194	IIa-E	(48)	7 09	7 57	1 00	1 48	+1 27
3321 b	HR 3440	"	(40)	9 20	10 00	3 11	3 51	+1 02
3322 c	HR 3883	"	(98)	10 14	11 52	4 05	5 43	+1 19

22-23/II/67 K.

3323 1	HR 2221	IIa-E	(24)	6 34	6 58	0 17	0 41	+0 36,5
3324 2	HR 2446	"	(40)	7 12	7 52	0 55	1 35	+0 56

24-25/II/67 K.

3325 3	HR 2762	IIa-E	(16)	8 13	8 29	1 47	2 03	+1 07
3326 4	HR 3139	"	(60)	8 45	9 45	2 19	3 19	+1 17,5
3327 5	HR 3875	"	(58)	10 00	10 58	3 34	4 32	+0 46

25-26/II/67 K.

3328 6	HR 2518	IIa-E	(28)	7 36	8 04	1 06	1 34	+1 03
3329 7	HR 3359	"	(20)	9 39	9 59	3 09	3 29	+1 20

U.T

2 T

32-7 5 A Ne 2^m 19.7 21.8 21.5

" " B " 19.4 21.2 21.0

32-7 5 A Ne 2^m 22.0 24.2 24.0

" " B " 21.8 23.5 23.1

" " C " 21.8 22.6 22.5

32-7 5 A Ne 2^m 23.4 25.6 25.2

" " B " 23.0 24.3 24.2

" " C " 22.8 24.1 23.7

32-7 5 A Ne 2^m 24.1 26.6 26.3

" " B " 23.8 26.1 25.6 Se nublo

32-7 5 A Ne 2^m 21.0 23.7 23.4

" " B " 20.5 23.2 22.6

" " C " 19.8 22.2 21.6

32-7 5 A Ne 2^m 23.0 25.0 24.8

" " B " 22.0 23.8 23.6 Pasan los nubes.

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28/II-1/III/67 K.

T. S.

T. V.

3330 1	HR 2678	IIA-E	(20)	8 05	8 25	1 22	1 42	+1 08,5
3331 2	HR 3189	"	(72)	8 38	9 50	1 55	3 07	+1 05
3332 3	HR 3822	"	(72)	10 08	11 20	3 25	4 37	+1 08.5
3333 4	HR 4214	"	(36)	11 55	12 31	5 11	5 47	+1 26
3334 5	HR 4567	"	(22)	12 53	13 15	6 09	6 31	+1 08

1-2/III/67 K.

3335 7	HR 2461	IIA-E	(40)	8 36	9 16	1 49	2 29	+2 15
3336 8	HR 3675	"	(132)	10 11	12 23	3 23,5	5 35,5	+2 02,5

2-3/III/67 K.

3337 1	HR 2456	IIA-E	(10)	8 30	8 40	1 39	1 49	+1 54
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3-4/III/67 K.

3338 1	HR 3189	IIA-E	(90)	9 07	10 37	2 13	3 43	+1 42,5
3339 2	HR 4214	"	(40)	11 06	11 46	4 13	4 53	+0 41,5
3340 3	HR 4428	"	(40)	12 00	12 40	5 07	5 47	+0 53
3341 4	HR 4757	"	(2)	12 58	13 00	6 05	6 07	+0 31

4-5/III/67 K.

3342 5	HR 3670	IIA-E	(30)	9 55	10 25	2 58	3 28	+0 58
3343 6	HR 3674	"	(24)	10 39	11 03	3 42	4 06	+1 38
3344 7	HR 4118	"	(36)	11 31	12 07	4 33.5	5 09,5	+1 21

6-7/III/67 K.

32-7	5	A	Ne 2 ^m	19.9	22.8	22.6	e?
"	"	B	"	19.3	22.2	21.4	
"	"	C	"	18.3	20.9	20.3	
"	"	A	"	17.1	19.5	19.0	
"	"	B	"	16.7	18.8	18.6	

32-7	3	B	Ne 2 ^m	18.6	21.0	20.6	Velo
"	4	C	"	17.8	20.0	19.4	

32-7	5	A	Ne 2 ^m	20.2	22.5	22.3	Se nubló
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32-7	5	A	Ne 2 ^m	19.2	21.8	21.2	
"	"	B	"	18.1	20.4	20.0	
"	"	C	"	17.5	19.9	19.5	
"	"	A	"	17.3	19.2	19.2	

32-7	5	A	Ne 2 ^m	19.3	22.1	21.6	e
"	"	B	"	18.7	21.4	21.2	
"	"	C	"	18.5	20.8	20.5	

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6-7/III/67 K.

T. S.

T. U.

H033458	HR 2678	IIa-E	(34)	8 51	9 25	1 46	2 20	+ 2 03
3346 9	HR 3745	"	(80)	9 55	11 15	2 50	4 10	+ 1 10
3347 10	HR 4238	"	(54)	11 30	12 24	4 24.5	5 18.5	+ 1 09
3348 1	HR 4817	"	(16)	12 44	13 00	5 38	5 54	+ 0 14
3349 2	HR 4819	"	(32)	13 20	13 20.5	6 14	6 14.5	+ 0 41

16-17/III/67 K.

3350 1	HR 3487	IIa-E	(8)	9 24	9 32	1 38	1 46	+ 0 44
3351 2	HR 3496	"	(64)	9 48	10 52	2 02	3 06	+ 1 34.5
3352 3	HR 4316	"	(104)	11 12	12 56	3 26	5 10	+ 1 01
3353 4	HR 4662	"	(2)	13 10	13 12	5 24	5 26	+ 0 58

18-19/III/67 K.

3354 5	HR 3670	IIa-E	(60)	9 36	10 36	1 42	2 42	+ 0 54.5
3355 6	HR 4049	"	(60)	10 55	11 55	3 01	4 01	+ 1 09.5
3356 7	HR 4423	"	(40)	12 10	12 50	4 16	4 56	+ 1 04.5

20-21/III/67 K.

3357 1	HR 3745	IIa-E	(100)	9 33	11 13	1 32	3 12	+ 0 59
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21-22/III/67 K.

3358 1	HR 3294	IIa-E	(24)	9 16	9 40	1 11	1 35	+ 1 08
3359 3	HR 3685	"	(34)	9 53	9 53.34	1 48	1 48.34	+ 0 41
3360 4	HR 3708	"	(70)	10 08	11 18	2 04	3 14	+ 1 27
3361 5	HR 4460	"	(20)	11 49	12 09	3 44	4 04	+ 0 28

32-7	5	A	Ne 2 ^m	22.3	24.2	24.0
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"	3	B	"	21.8	23.7	23.3	[e]
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"	4	C	"	21.7	22.8	22.6
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"	5	A	"	21.5	22.5	22.4
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"	"	B	"	21.5	22.4	22.4
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32-7	5	A	Ne 2 ^m	16.0	17.5	17.4
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"	"	B	"	16.2	17.2	17.1
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"	"	C	"	16.1	17.0	16.8
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"	"	A	"	16.2	16.7	16.7
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32-7	5	A	Ne 2 ^m	20.7	22.7	22.4	[e]
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"	"	B	"	20.3	22.1	21.8
---	---	---	---	------	------	------

"	"	C	"	20.0	21.6	21.4
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32-7	5	A	Ne 2 ^m	17.8	20.0	19.4	e
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32-7	5	A	Ne 2 ^m	18.1	20.3	20.0
------	---	---	-------------------	------	------	------

"	"	B	"	18.0	19.8	19.8
---	---	---	---	------	------	------

"	"	C	"	16.9	19.5	19.1	e
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"	"	A	"	15.7	18.2	17.9	[e]
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21-22/III/67 K.

T. S.

T. V.

HU3362 6	HR 4467	IIa-E	(2)	12 31	12 33	4 26	4 28	+0 59,5
3363 7	HR 4913	"	(36)	13 29	14 05	5 24	6 00	+0 54

22-23/III/67 K.

3364 3	HR 4908	IIa-E	(20)	12 30	13 50	5 22	5 42	+0 49
3365 4	HR 5190	"	(2)	14 21	14 23	6 13	6 15	+0 38

25-26/III/67 K.

3366 1	HR 3439	IIa-E	(36)	9 13	9 49	0 53,5	1 29,5	+0 52,5
3367 2	HR 3708	"	(68)	10 03	11 11	1 43	2 51	+1 20
3368 3	HR 4312	"	(120)	11 33	13 33	3 13	5 13	+1 29

27-28/III/67 K.

3369 4	HR 2456	IIa-E	(26)	8 11	8 37	23 44	0 10	+1 46
3370 5	HR 3383	"	(70)	8 56	10 06	0 29	1 39	+1 00
3371 6	HR 3963	"	(60)	10 41	11 41	2 13	3 13	+1 10
3372 7	HR 4468	"	(30)	12 28	12 58	4 00	4 30	+1 09

28-29/III/67 K.

3373 8	HR 3389	IIa-E	(80)	9 00	10 20	0 29,5	1 49,5	+1 09
3374 9	HR 4037	"	(4)	10 37	10 41	2 06	2 10	+0 27
3375 10	HR 4194	"	(70)	11 02	12 12	2 31	3 41	+0 57,5
3376 11	HR 4735	"	(40)	12 38	13 18	4 07	4 47	+0 35
3377 12	HR 4748	"	(70)	13 53	15 03	5 22	6 32	+2 03,5

32-7	5	B	Ne 2 ^m	15.4	17.6	17.6
"	"	C	"	14.7	17.0	16.7
32-7	4	C	Ne 2 ^m	15.0	17.0	16.8 e
"	5	A	"	14.7	16.5	16.5
32-7	5	A	Ne 2 ^m	20.6	22.7	22.5
"	"	B	"	20.4	22.5	22.1 e
"	"	C	"	19.8	21.4	20.9
32-7	5	A	Ne 2 ^m	21.6	23.8	23.5
"	"	B	"	21.0	23.3	22.8
"	"	C	"	20.5	22.2	21.9
"	"	A	"	20.0	21.4	21.3
32-7	5	A	Ne 2 ^m	19.5	22.7	21.9
"	"	B	"	18.9	21.3	21.3 e
"	"	C	"	18.7	21.0	20.5
"	"	A	"	18.6	20.1	19.9
"	"	B	"	18.5	19.6	19.4

78

30-31/III/67 K.

T. S.

T. U.

Hu3378	1	HR 3720	IIa-E	(50)	9 55	10 45	1 15	2 05	+1 01
3379	2	HR 3721	"	(90)	10 49	12 19	2 05	3 39	+2 15
3380	3	HR 4460	"	(20)	12 34,5	12 54,5	3 54	4 14	+1 11
3381	4	HR 4908	"	(20)	13 23	13 43	4 42,5	5 02,5	+0 39
3382	5	HR 5190	"	(4)	14 05	14 09	5 24	5 28	+0 20

31/III - 1/IV/67 K.

3383	6	HR 3810	IIa-E	(100)	10 37	12 17	1 54	3 34	+1 56
3384	7	HR 4583	"	(38)	13 12	13 50	4 28	5 06	+1 32,5
3385	8	HR 4952	"	(40)	14 06	14 46	5 42	6 22	+1 21

18-19/IV/67 K.

Reside 2. IV. 67 T. U. = T. A. + 4^h

3386	1	HR 4618	IIa-E	(10)	12 22	12 32	2 28	2 38	+0 21
3387	2	HR 4887	"	(48)	13 33	14 21	3 39	4 27	+1 06
3388	3	HR 4876	"	(56)	14 36	15 32	4 42	5 38	+2 13
3389	4	HR 5680	"	(16)	16 00	16 16	6 06	6 22	+0 52,5
3390	5	HR 6002	"	(36)	17 00	17 36	7 06	7 42	+1 13,5

20-21/IV/67 K.

3391	1	HR 4065	IIa-E	(34)	10 51	11 25	0 50	1 24	+0 50,5
3392	2	HR 4188	"	(72)	12 00	13 12	1 58	3 10	+1 56,5
3393	3	HR 5190	"	(3)	14 34	14 37	4 32	4 35	+0 44,5
3394	4	HR 5449	"	(40)	15 00	15 40	4 58	5 38	+0 46,5
3395	6	HR 5907	"	(22)	16 03	16 25	6 01	6 23	+0 23
3396	7	HR 6096	"	(54)	16 56	17 50	6 54	7 48	+1 03,5

32-7	5	A	Ne 2 ^m	15.8	18.7	18.2
"	"	B	"	14.8	18.0	17.2
"	"	C	"	14.2	16.7	16.5 e
"	"	A	"	14.1	16.1	16.0 e
"	"	B	"	13.8	15.7	15.6

32-7	5	A	Ne 2 ^m	16.5	18.8	18.2
"	"	B	"	16.1	17.5	17.3
"	"	C	"	16.0	17.1	17.0 e

32-7	5	A	Ne 1,5 ^m	13.1	15.4	15.2	T.U. = T.A. + 4 ^R
"	"	B	"	12.2	14.5	14.2	
"	"	C	"	11.6	14.0	13.4	[e]
"	"	A	"	11.3	13.2	13.0	
"	"	B	"	11.0	12.6	12.5	

32-7	5	A	Ne 1,5 ^m	13.7	15.5	15.3	
"	"	B	"	12.8	15.0	14.4	e
"	"	A	Ne 2 ^m	11.9	13.7	13.7	
"	"	C	Ne 1,5 ^m	11.7	13.3	13.2	
"	"	A	"	11.3	13.1	13.0	
"	"	B	"	10.9	12.7	12.4	

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21-22/IV/67 K.

T.S.

T.V.

HU3397	8	HR 3708	IIa-E	(50)	10 40	11 30	0 35	1 25	+1	48,5
3398	9	HR 5440	"	(1)	14 54	14 55	4 48	4 49	+0	22,5
3399	10	HR 5559	"	(28)	15 13	15 41	5 07	5 35	+0	34
3400	11	HR 5440	"	(1)	16 13	16 14	6 07	6 08	+1	41,5

24-25/IV/67 K.

3401	1	HR 4116	IIa-E	(20)	11 06	11 26	0 48	1 08	+0	49,5
3402	2	HR 4356	"	(22)	11 40	12 02	1 22	1 44	+0	40
3403	3	HR 4604	"	(22)	12 20	12 42	2 02	2 24	+0	28
3404	4	HR 4876	"	(40)	13 10	13 50	2 52	3 32	+0	39
3405	5	HR 4887	"	(58)	14 08	15 06	3 50	4 48	+1	45,5

25-26/IV/67 K.

3406	1	HR 3989	IIa-E	(52)	10 51	11 43	0 29	1 21	+1	10
3407	2	HR 4519	"	(18)	12 10	12 28	1 49	2 07	+0	36
3408	3	HR 4611	"	(90)	12 50	14 20	2 28	3 58	+1	31
3409	4	HR 5296	"	(42)	14 34	15 16	4 12	4 54	+0	48,5
3410	5	HR 5782	"	(30)	15 56	16 26	5 34	6 04	+0	34
3411	6	HR 5994	"	(36)	16 45	17 21	6 23	6 59	+0	57

26-27/IV/67 K.

3412	1	HR 4347	IIa-E	(50)	11 43	12 33	1 17	2 07	+0	58,5
3413	2	HR 4722	"	(42)	13 13	13 55	2 47	3 29	+1	12
3414	3	HR 5170	"	(52)	14 30	15 22	4 04	4 56	+1	13,5
3415	4	HR 5798	"	(24)	16 27	16 51	6 01	6 25	+1	04

32-7	5	A	Ne 2 ^m	14.3	15.7	15.6	e
"	"	A	"	13.5	14.6	14.6	
"	"	B	Ne 1,5 ^m	13.5	14.5	14.5	
"	"	A	Ne 2 ^m	13.5	14.5	14.5	

32-7	5	A	Ne 1,5 ^m	10.9	13.6	13.2	
"	"	B	"	10.4	13.0	12.8	
"	"	C	"	10.1	12.5	12.2	
"	"	A	"	10.1	12.0	11.7	
"	3	B	"	10.1	11.6	11.4	Nebo

32-7	4	A	Ne 1,5 ^m	12.6	14.4	14.2	
"	5	B	"	12.4	14.0	13.8	
"	"	C	"	12.0	13.6	13.3	
"	"	A	"	11.7	13.1	13.0	
"	"	B	"	11.4	12.7	12.6	
"	"	C	"	11.3	12.5	12.4	

32-7	5	A	Ne 1,5 ^m	13.4	15.0	15.0	
"	"	B	"	12.7	14.6	14.4	
"	"	C	"	12.7	14.2	14.0	
"	"	A	"	12.2	13.6	13.4	

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27-28/IV/67 K.

T. S.

T. V.

HR 3416	5	HR 3189	IIa-E	(80)	10 12	11 32	23 42	1 02	+2	45,5
3417	6	HR 4372	"	(60)	11 52	12 52	1 22	2 22	+1	07
3418	7	HR 4744	"	(50)	13 24	14 14	2 54	3 44	+1	23

20-21/V/67 K.

3419	1	HR 4401	IIa-E	(16)	11 42	11 58	23 41	23 57	+0	28
3420	2	HR 4611	"	(80)	12 16	13 36	0 15	1 35	+0	51,5
3421	3	HR 4952	"	(50)	14 20	15 10	2 19	3 09	+1	38,5
3422	4	HR 5671	"	(2)	15 47	15 49	3 46	3 48	+0	31,5
3423	5	HR 5683	"	(10)	16 12	16 22	4 10	4 20	+1	01

16-17/VI/67 K.

3424	1	HR 5141	IIa-E	(30)	15 00	15 30	1 13	1 43	+1	36
3425	2	HR 6187	"	(50)	17 00	17 50	3 13	4 03	+0	47

24-25/VI/67 K.

3426	1	HR 4952	IIa-E	(60)	14 09	15 09	23 51	0 51	+1	33
3427	2	HR 5683	"	(10)	15 44	15 54	1 26	1 36	+0	33,5
3428	3	HR 6002	"	(50)	16 18	17 08	2 00	2 50	+0	38
3429	4	HR 6519	"	(20)	17 48	18 08	3 29	3 49	+0	29

27-28/VI/67 K.

3430	1	HR 5141	IIa-E	(50)	14 46	15 36	0 15	1 05	+1	31,5
3431	2	HR 6007	"	(40)	16 40	17 20	2 09	2 49	+0	52,5

32-7	5	A	Ne ^m 1.5	13.2	16.1	15.6
"	"	B	"	13.1	15.1	14.7
"	"	C	"	12.8	14.5	14.8

32-7	5	A	Ne ^m 1.5	15.8	16.8	16.6
"	"	B	"	15.4	16.5	16.4
"	"	C	"	15.4	16.3	16.0 e
"	"	A	"	15.3	16.0	16.0
"	"	B	"	15.1	15.9	15.9 [e]

32-7	4	A	Ne ^m 1.5	6.2	7.7	7.7
"	3	B	"	5.9	7.4	7.3 se unblo'

32-7	4	A	Ne ^m 1.5	8.1	9.7	9.5 e
"	"	B	"	7.8	9.1	9.1 e
"	"	C	"	7.7	8.8	8.7
"	"	A	"	7.5	8.5	8.5 se unblo' [e]

32-7	5	A	Ne ^m 2	8.8	8.6	
"	4	B	"	8.2	8.0	se unblo'

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1-2/VII/67

K.

T. S.

T. V.

H034321	HR 5485	IIa-E	(12)	14 42	14 54	23 55	0 07	+0 07
34332	HR 5652	"	(12)	15 52	16 04	1 05	1 17	+0 48,5
34343	HR 6187	"	(40)	16 55	17 35	2 08	2 48	+0 37

2-3/VII/67

K.

34354	HR 6340	IIa-E	(60)	17 30	18 30	2 39	3 39	+0 58
34365	HR 6825	"	(64)	19 03	20 07	4 12	5 16	+1 22,5
34376	HR 7763	"	(30)	20 43	21 13	5 51	6 21	+0 42

26-27/VII/67

K.

34381	HR 6537	IIa-E	(12)	18 25	18 37	2 00	2 12	+0 58
34392	HR 6870	"	(30)	18 56	19 26	2 31	3 01	+0 50,5
34403	HR 6960	"	(14)	20 03	20 17	3 38	3 52	+1 41

29-30/VII/67

K.

34411	HR 6736	IIa-E	(67)	18 38	19 45	2 01	3 08	+1 09,5
34422	HR 7342	"	(20)	20 02	20 22	3 24,5	3 44,5	+0 54
34433	HR 7378	"	(40)	20 50	21 30	4 12,5	4 52,5	+1 46

1-2/IX/67

K.

34442	HR 7378	IIa-E	(40)	19 42	20 22	0 51	1 31	+0 38
34453	HR 7379	"	(110)	20 39	22 29	1 48	3 38	+2 10
34464	HR 8151	"	(16)	22 56	23 12	4 05	4 21	+1 46
34475	HR 8180	"	(40)	23 24	0 04	4 32	5 12	+2 22

32-7	5	A	Ne 2 ^m	9.4	9.4	
"	4	B	"	9.3	9.3	
"	2	C	"	9.2	9.2	

32-7	5	A	Ne 2 ^m	10.8	10.6	
"	"	B	"	10.2	10.1	
"	"	C	"	9.8	9.7	e

32-7	5	A	Ne 2 ^m	10.0	11.6	11.6	
"	"	B	"	9.5	11.5	11.4	
"	4	C	"	9.1	10.9	10.8	se mbló'

32-7	5	A	Ne 2 ^m	8.5	10.7	10.2	
"	"	B	"	8.0	10.0	9.9	e
"	4	C	"	7.6	9.6	9.4	se mbló'

32-7	5	A	Ne 2 ^m	12.0	13.6	13.5	
"	"	C	"	11.7	13.3	13.0	
"	"	A	"	11.4	12.7	12.7	
"	"	B	"	11.5	12.7	12.5	

5-6/IX/67

K.

T. S.

T. U.

H₀ 34481

HR 8244

IIa-E (130) 22 10 0 20 3 04 5 14 + 1 43

6-7/IX/67

K.

3449 2

HR 7336

IIa-E (28) 19 47 20 15 0 37 1 05 + 0 42,5

3450 3

HR 7594

" (90) 21 03 22 33 1 53 3 23 + 1 55,5

15-16/IX/67

K.

3451 1

HR 7856

IIa-E (100) 22 14 23 54 2 28 4 08 + 2 32,5

3452 2

HR 9102

" (90) 0 27 1 57 4 40 5 10 + 1 11

19-20/IX/67

K.

3453 3

HR 8118

IIa-E (120) 21 36 23 36 1 34 3 34 + 1 25,5

3454 4

HR 8695

" (12) 0 40 0 52 4 38 4 50 + 1 57

3455 5

HR 125

" (16) 1 38 1 54 5 36 5 52 + 1 18

20-21/IX/67

K.

3456 6

HR 7574

IIa-E (90) 20 57 22 27 0 51,5 2 21,5 + 1 53

3457 7

HR 8355

" (120) 23 23 1 23 3 17 5 17 + 2 33

Desde 1.X.67 T. U. = T. A. + 3^h

5-6/XII/67

K.

Cámara de $D=110 \frac{A}{mm}$ con $F_0=7$.

HX

3458 1

HR 1983

IIa-0 (15) 4 45 5 00 3 40 3 55 - 0 50,5

"

"

(30)

5 00

5 30

3 55

4 25

- 0 28

HX

3459 2

HR 2282

" (15) 6 12 6 17 5 07 5 12 - 0 04,5

Ramach

A L

32-7

4

A Ne 2^mt^{amb} t^o de espesura

11.3

12.8

12.5

32-7

5

A Ne 2^m

15.4

16.4

16.3

"

"

B "

13.5

16.1

15.6

32-7

5

A Ne 2^m

16.6

18.2

17.8

"

"

B "

16.0

17.5

17.1

32-7

5

A Ne 2^m

9.4

12.0

11.3

"

"

B "

8.0

10.2

10.1

"

"

A "

7.4

9.5

9.5

32-7

5

A Ne 2^m

10.9

13.5

13.1

"

"

B "

10.0

12.2

11.7

$$T.V. = T.A. + 3^P$$

Ramach: Ancho, A, se abre con el aumento de la lectura del tambor.

A=0 está cerrado, A=5 es $1^R + 5$. Largo, L, se abre con disminución

5-1

5

B Fe 15⁴

con 2 vidrios

de la lectura del tambor

"

"

"

esmerilados

L=13 está cerrado,

"

"

" Fe 15³L=1 es $11^R + 12$.

88

5-6/XII/67

K Placas nuevas T. S.

T. V.

HX34592	HR 2282	IIa-0	(10)	6 17	6 27	5 12	5 22	+ 0 03
"	"	"	(20)	6 27	6 47	5 22	5 42	+ 0 18

20-21/XII/67

K Placas nuevas $F_c = 7$

Corr. de T.V. = +3"

34601	HR 591	103a-0	(5)	4 02	4 07	1 55	2 00	+ 2 07
"	"	"	(8)	4 07	4 15	2 00	2 08	+ 2 13,5
"	"	"	(14)	4 15	4 29	2 08	2 22	+ 2 23,5
HR 1347	"	"	(7)	4 47	4 54	2 40	2 47	+ 0 34
"	"	"	(12)	4 54	5 06	2 47	2 59	+ 0 44
"	"	"	(21)	5 06	5 27	2 59	3 20	+ 1 00
34612	HR 2020	"	(6)	6 35	6 41	4 28	4 34	+ 0 52
"	"	"	(8)	6 41	6 49	4 34	4 42	+ 0 59
"	"	"	(14)	6 49	7 03	4 42	4 56	+ 1 10
HR 2106	"	"	(6)	7 14	7 20	5 07	5 13	+ 1 21
"	"	"	(10)	7 20	7 30	5 13	5 23	+ 1 29
"	"	"	(20)	7 30	7 50	5 23	5 43	+ 1 44

21-22/XII/67

K $F_c = 7,5$

34623	HR 591	103a-0	(0,5)	4 24,5	4 25	2 13,5	2 14	+ 2 27
"	"	"	(2)	4 25	4 27	2 14	2 16	+ 2 28,5
"	"	"	(5)	4 27	4 33	2 16	2 21	+ 2 32
HR 1347	"	"	(1)	4 54	4 55	2 42	2 43	+ 0 38
"	"	"	(3)	4 55	4 58	2 43	2 46	+ 0 40
"	"	"	(8)	4 58	5 06	2 46	2 54	+ 0 45,5

Corr. de T.V. = +3"

Ranura:

89

A L

5 - 1

5

B

Placas ligas

4

"

5 - 1

5

B Fe 20⁴

Placas medidas.

"

"

" En la serie de placas HX para cada estrella.

"

"

" Ha hay tres espectros sacados con la

"

"

" distinta exposición: una exposición

"

"

" normal que corresponde a la

"

"

" $t_{exp}^0 = 23^{\circ}C$; $t_{rev} = 6^{m}$

"

"

" Fe 10⁴

"

"

" magnitud de la estrella y 2

"

"

" espectros más que corresponden

"

"

" a 0,5 magnitud menor y a 0,5

"

"

" magnitud mayor de la normal.

"

"

" Fe 10⁴ con $F_{cámara} = 7,5$

"

"

" Fe 10⁴ " " = 8 $t_{exp}^0 = 20^{\circ}C$; $t_{rev} = 6^{m}$

5 - 1

5

B Fe 10⁴

"

"

"

"

"

"

"

"

"

"

"

"

"

4

"

$t_{exp}^0 = 20,6$

$t_{exp}^0 = 22^{\circ}C$; $t_{rev} = 5^{m}$

90

28-29/XII/67

K

 $F_c = 7.5$ T.S.

T.V.

HX3463

HR 1865

103a-0

(1)

6 14

6 15

3 35

3 36

+0

43,5

"

"

(2)

6 15

6 17

3 36

3 38

+0

45

"

"

(4)

6 17

6 21

3 38

3 42

+0

48

30-31/XII/67

K.

 $F_c = 7.5$

3464 1

HR 889

103a-0

(6)

4 43

4 49

1 55

2 01

+1

51

"

"

(11)

4 49

5 00

2 01

2 12

+1

59,5

"

"

(19)

5 00

5 19

2 12

2 31

+2

14,5

HR 1666

"

(1)

5 37

5 38

2 49

2 50

+0

31,5

"

"

(2)

5 38

5 40

2 50

2 52

+0

33

"

"

(3)

5 40

5 43

2 52

2 55

+0

35,5

HR 1756

"

(4)

5 58

6 02

3 10

3 14

+0

42

"

"

(8)

6 02

6 10

3 14

3 22

+0

48

"

"

(14)

6 10

6 24

3 22

3 36

+0

59

3465 2

HR 2361

"

(7)

7 01

7 08

4 12,5

4 19,5

+0

37,5

"

"

(12)

7 08

7 20

4 19,5

4 31,5

+0

47

"

"

(19)

7 20

7 39

4 31,5

4 50,5

+1

02,5

HR 2657

"

(4)

7 48,5

7 52,5

5 00

5 04

+0

48,5

"

"

(8)

7 52,5

8 00,5

5 04

5 12

+0

54,5

"

"

14

8 00,5

8 14,5

5 12

5 26

+1

05,5

2-3/I/68

K.

 $F_c = 7.5$

3466 3

HR 1088

103a-0

(2)

4 33

4 35

1 40

1 42

+1

02

"

"

(7)

4 35

4 42

1 42

1 49

+1

06,5

"

"

(10)

4 42

4 52

1 49

1 59

+1

15

	2-3/I/68	K.		T. S.		T. U.	
HX3466	HR 1088	103a-0	(16)	4 52	5 08	1 59	2 15 +1 28
	HR 1520	"	(4)	5 40	5 44	2 46	2 50 +0 58
	"	"	(8)	5 44	5 52	2 50	2 58 +1 04
	"	"	(14)	5 52	6 06	2 58	3 12 +1 15
	HR 1788	"	(1)	6 27	6 28	3 33	3 34 +1 05
	"	"	(3)	6 28	6 31	3 34	3 37 +1 07
	"	"	(5)	6 31	6 36	3 37	3 42 +1 11

Después de aluminizar el espejo

3-4/I/68 K. *gritud en la exposición de*

34671	HR 1338	103a-0	(5)	4 33	4 38	1 35	1 40 +0 20.5
	"	"	(9)	4 38	4 47	1 40	1 49 +0 27.5
	"	"	(15)	4 47	5 02	1 49	2 04 +0 39.5
	HR 1338	"	(5)	5 06	5 11	2 08	2 13 +0 53.5
	"	"	(9)	5 11	5 20	2 13	2 22 +1 00.5
	"	"	(15)	5 20	5 35	2 22	2 37 +1 12.5
	HR 1735	"	(3)	5 47	5 50	2 49	2 52 +0 33
	"	"	(5)	5 50	5 55	2 52	2 57 +0 37
	"	"	(1)	5 55	5 56	2 57	2 58 +0 40

4-5/I/68 K.

34682	HR 721	103a-0	(3)	4 09	4 12	1 07	1 10 +1 44.5
	"	"	(5)	4 12	4 17	1 10	1 15 +1 48.5
	"	"	(9)	4 17	4 26	1 15	1 24 +1 55.5
	HR 1758	"	(25)	5 20	5 45	2 18	2 43 +0 14.5
	"	"	(43)	5 45	6 28	2 43	3 26 +0 48.5

5-1 5 B $t_{exp} = 18.1^{\circ}C$ $t_{amb} = 17.8^{\circ}C$

" " "

" " "

" " "

" " "

" " "

" " "

$t_{exp} = 17.2^{\circ}C$ $t_{amb} = 17.0^{\circ}C$

$t_{exp} = 16.8^{\circ}C$ $t_{amb} = 16.5^{\circ}C$ $t_{ext} = 18^{\circ}C$
 $t_{ext} = 6^{\circ}m$

del reflector hay ganancia de 0,5 de una
 la placa.

5-1 5 B Fe 10^4 Rampa: $L = 10^R + 12$

" " "

$t_{exp} = 20.3^{\circ}C$ $t_{amb} = 20.1^{\circ}C$

" " "

Rampa: $L = 11^R + 12$

" " "

" " "

" " "

" " "

" " "

$t_{exp} = 20.0^{\circ}C$ $t_{amb} = 19.6^{\circ}C$ Se midió

5-1 5 B Fe 10^4

" " "

" " "

" " "

" " "

$t_{exp} = 21.7^{\circ}C$ $t_{amb} = 21.6^{\circ}C$ ya placa
 está ya
 yado.
 Repetirle

94

4-5/I/68 K.

T. S.

T. U.

HX 3468 HR 1758 103a-0 (74) 6 28 7 42 3 26 4 40 + 1 47

5-6/I/68 K.

3469 ³	HR 919	103a-0	(4 ^m)	4 55	4 59	1 48	1 52	+ 1 56
"	"	"	(7)	4 59	5 06	1 52	1 59	+ 2 01,5
"	"	"	(11)	5 06	5 17	1 59	2 10	+ 2 10,5
	HR 2326	"	(1 ¹)	6 56		3 49		+ 0 33
"	"	"	(2 ¹)					
"	"	"	(3 ¹)					
	HR 2387	"	(3 ^m)	7 10	7 13	4 03	4 06	+ 0 41,5
"	"	"	(5)	7 13	7 18	4 06	4 11	+ 0 45,5
"	"	"	(9)	7 18	7 27	4 11	4 20	+ 0 52,5

11-12/I/68 K

3470 ¹	HR 919	103a-0	(4)	4 35	4 39	0 59	1 03	+ 1 36
"	"	"	(7)	4 39	4 46	1 03	1 10	+ 1 41,5
"	"	"	(11)	4 46	4 57	1 10	1 21	+ 1 50,5
	HR 889	"	(6)	5 02	5 08	1 30	1 36	+ 2 09
"	"	"	(11)	5 08	5 19	1 36	1 47	+ 2 17,5
"	"	"	(19)	5 19	5 38	1 47	2 06	+ 2 32,5
	HR 2326	"	(15 ¹)	6 20		2 48		- 0 03
"	"	"	(1 ¹)					
"	"	"	(2 ¹)					
"	"	"	(4 ¹)					
3471 ²	HR 2326	"	(3 ¹)	6 50		3 18		+ 0 27

5-1 3 B $t_{exp.} = 20.7^{\circ}C$ $t_{amb.} = 20.6^{\circ}C$

5-1 5 B Fe 10^1

" " " "

" " " " $t_{exp.} = 23.8^{\circ}C$ $t_{amb.} = 23.7^{\circ}C$

" " " "

" " " "

" " " "

" " " "

" " " "

" " " " $t_{exp.} = 23.2$ $t_{amb.} = 23.1$

5-1 5 B Fe 10^1

" " " "

" " " "

" " " "

" " " "

" " " " $t_{exp.} = 22.7$ $t_{amb.} = 22.8$

5-1 1 + 5 B Fe 10^0 con el imagen desenfocada, el aparece la toda zarraca:  imagen zarraca

Se debe el comportamiento de HR 919 con la temperatura en el espectro de HR 23.26.

Rep.

96

11-12/I/68.

K.

T. S.

T. U.

HX3471

HR 2326

103a-0 (40³)

6 51

3 19

+ 0 28,5

HR 2387

"

(3^m)

7 13

7 16

3 41

3 44

+ 0 44,5

"

"

(5)

7 16

7 21

3 44

3 49

+ 0 48,5

"

"

(9)

7 21

7 30

3 49

3 58

+ 0 55,5

HR 3117

"

(1)

7 52

7 53

4 20

4 21

- 0 03

"

"

(3)

7 53

7 56

4 21

4 24

- 0 01

"

"

(5)

7 56

8 01

4 24

4 29

+ 0 03

12-13/I/68.

K.

3472 3

HR 1175

103a-0 (8)

4 23

4 31

0 47

0 55

+ 0 43

"

"

(15)

4 31

4 46

0 55

1 10

+ 0 54,5

"

"

(25)

4 46

5 11

1 10

1 35

+ 1 14,5

HR 1208

"

(8)

5 29

5 32

1 53

2 01

+ 1 45

"

"

(15)

5 37

5 52

2 01

2 16

+ 1 56,5

"

"

(25)

5 52

6 17

2 16

2 41

+ 2 16,5

3473 4

HR 2553

"

(3)

7 15

7 18

3 38,5

3 41,5

+ 0 27,5

"

"

(5)

7 18

7 23

3 41,5

3 46,5

+ 0 31,5

"

"

(9)

7 23

7 32

3 46,5

3 55,5

+ 0 38,5

HR 2736

"

(9)

7 43,5

7 52,5

4 07

4 16

+ 0 39

"

"

(15)

7 52,5

8 07,5

4 16

4 31

+ 0 51

"

"

(25)

8 07,5

8 32,5

4 31

4 56

+ 1 11

13-14/I/68

K.

3474 5

HR 1083

103a-0 (9)

4 22

4 31

0 41,5

0 50,5

+ 0 58

"

"

(15)

4 31

4 46

0 50,5

1 05,5

+ 1 10

5-1 1 + 5 12 16 2 10 4 30 7-8.5.01 2001 411 Rep.

4.5 1 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 1 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

$t_{amb} = 22.6^{\circ}C$

5-1 0 + 5 1 1 B Fe 10⁴ 30 7 $t_{exp} = 22.7^{\circ}C$ $t_{amb} = 22.9^{\circ}C$

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

$t_{exp} = 22.5^{\circ}C$ $t_{amb} = 22.7^{\circ}C$

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

Pasan los nubes. $\leftarrow$ Esde entre el esp. de comp. Fe

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

4.5 0 + 4 1 1 2 4 20 12 20 2 12 1405 34

$t_{exp} = 21.6^{\circ}C$ $t_{amb} = 21.4^{\circ}C$ Se nubló

5-1 1 + 5 1 1 B Fe 10⁴ 30 7

		13-14/I/68 K.		T. S.		T. V.	
HX 3474	HR 1083	103a-0	(25)	4 46	5 11	1 05.5	1 39.5 + 1 30
	HR 1336	"	(4)	5 30.5	5 34.5	1 50	1 54 + 1 18.5
	"	"	(16)	5 34.5	5 50.5	1 54	2 10 + 1 28.5
	HR 2120	"	(9)	6 40.5	6 49.5	3 00	3 09 + 0 47
	"	"	(15)	6 49.5	7 04.5	3 09	3 24 + 0 59
	"	"	(26)	7 04.5	7 30.5	3 24	3 50 + 1 19.5

		15-16/I/68 K.		$F_c = 7.5$			
HX 34756	HR 2451	103a-0	(1)	7 04	7 05	3 17.5	3 18.5 + 0 28
	"	"	(2)	7 05	7 07	3 18.5	3 20.5 + 0 29.5
	"	"	(3)	7 07	7 10	3 20.5	3 23.5 + 0 32
	HR 2803	"	(7)	7 22	7 29	3 35.5	3 42.5 + 0 08.5
	"	"	(12)	7 29	7 41	3 42.5	3 54.5 + 0 18
	"	"	(24)	7 41	8 05	3 54.5	4 18.5 + 0 36
	HR 3318	"	(5)	8 39	8 44	4 52.5	4 57.5 + 0 22.5
	"	"	(9)	8 44	8 53	4 57.5	5 06.5 + 0 29.5
	"	"	(15)	8 53	9 08	5 06.5	5 21.5 + 0 41.5

		18-19/I/68 K.		$F_c = 7.5$			
34767	HR 1463	103a-0	(3)	5 06	5 09	1 07	1 10 + 1 33
	"	"	(5)	5 09	5 14	1 10	1 15 + 1 37
	"	"	(8)	5 14	5 22	1 15	1 23 + 1 43.5
	HR 1758	"	(25)	5 33	5 58	1 34	1 59 + 0 27.5
	"	"	(43)	5 58	6 41	1 59	2 42 + 1 01.5

5-1 5 B $t_{exp} = 22.9$ $t_{amb} = 22.7^{\circ}C$

$t_{exp} = 22.5$ $t_{amb} = 22.3^{\circ}C$

$t_{exp} = 22.1$ $t_{amb} = 22.0^{\circ}C$

5-1 4 B $Fe 10^3$

$t_{exp} = 22.5$ $t_{amb} = 22.5^{\circ}C$

$t_{exp} = 22.1$ $t_{amb} = 22.2$ Veto

$t_{exp} = 21.6$ $t_{amb} = 21.9^{\circ}C$

5-1 5 B $Fe 10^3$

$t_{exp} = 23.8$ $t_{amb} = 23.6^{\circ}C$

$t_{exp} = 23.7$ $t_{amb} = 23.7^{\circ}C$

se. nullo.

20-21/I/68 K. $F_c = 7.5$ T. S. T. U.

HK 3477	1	HR 1560	103a-0	(5 ^m)	5 29	5 34	1 21	1 26	+ 0	40.5
	2	"	"	(9)	5 34	5 43	1 26	1 35	+ 0	47.5
	3	"	"	(15)	5 43	5 58	1 35	1 50	+ 0	59.5
	4	HR 1892	"	(5)	6 14	6 19	2 06	2 11	+ 0	43
	5	"	"	(9)	6 19	6 28	2 11	2 20	+ 0	50
	6	"	"	(15)	6 28	6 43	2 20	2 35	+ 1	02
	7	HR 1983	"	(3)	6 52	6 55	2 44.5	2 47.5	+ 1	10.5
	8	"	"	(5)	6 55	7 00	2 47.5	2 52.5	+ 1	14.5
	9	"	"	(9)	7 00	7 09	2 52.5	3 01.5	+ 1	21.5
	10	HR 2714	"	(3)	7 20	7 21	3 12.5	3 15.5	+ 0	11.5
	11	"	"	(5)	7 21	7 26	3 15.5	3 20.5	+ 0	13.5
	12, 14	"	"	(9)	7 26	7 35	3 20.5	3 29.5	+ 0	20.5

23-24/I/68 K. $F_c = 7.5$

3478	1	HR 2538	103a-0	(2)	7 42	7 44	3 23	3 25	+ 0	54.5
	2	"	"	(3)	7 44	7 47	3 25	3 28	+ 0	57
	3	"	"	(6)	7 47	7 53	3 28	3 34	+ 1	01.5
	4	HR 2749	"	(2)	8 06	8 08	3 47	3 49	+ 0	54
	5	"	"	(3)	8 08	8 11	3 49	3 52	+ 0	56.5
	6	"	"	(6)	8 11	8 17	3 52	3 58	+ 1	01
	7	HR 2996	"	(3)	8 24	8 27	4 06	4 09	+ 0	43.5
	8	"	"	(5)	8 27	8 32	4 09	4 14	+ 0	47.5
	9	"	"	(9)	8 32	8 41	4 14	4 23	+ 0	54.5
	10	HR 3314	"	(3)	8 49	8 52	4 31	4 34	+ 0	27
	11	"	"	(4)	8 52	8 56	4 34	4 38	+ 0	30.5
	12	"	"	(8)	8 56	9 04	4 38	4 46	+ 0	36.5

5-10	5	18	$Fe 10^3$			
"	"	"	"	$t_{exp.} = 23.6$	$t_{amb.} = 23.4^{\circ}C$	
"	"	"	"			
"	"	"	"			
"	"	"	"			
"	"	"	"			
"	"	"	"			
"	"	"	"			
"	"	"	"	$t_{exp.} = 22.5$	$t_{amb.} = 22.6$	
"	"	"	"			
"	"	"	"			
"	"	"	$Fe 10^4$	$t_{exp.} = 22.5$	$t_{amb.} = 22.4$	

5-10	5	18	$Fe 10^3$			H_2O
"	"	"	"			"
"	"	"	"	$t_{exp.} = 22.9$	$t_{amb.} = 22.7$	"
"	"	"	"			
"	"	"	"	$t_{exp.} = 22.9$		
"	"	"	"			
"	"	"	"	$t_{exp.} = 22.7$	$t_{amb.} = 22.5$	
"	3	"	"			Viento fuerte
"	2	"	"	$t_{exp.} = 22.4$	$t_{amb.} = 22.2$	

29-30/I/68 K.

T. S.

T. U.

HX 3479	1	HR 721	103a-0 (3)	4 56	4 59	0 14	0 17	+2	31.5
	2	"	" (5)	4 59	5 04	0 17	0 22	+2	35.5
	3	"	" (9)	5 04	5 13	0 22	0 31	+2	42.5
	4	HR 1325	" (11)	5 31	5 42	0 49	1 00	+1	23
	5	"	" (19)	5 42	6 01	1 00	1 19	+1	38
	6	"	" (33)	6 01	6 34	1 19	1 52	+2	04
	7	HR 1790	" (36 ³)	6 42		2 00		+1	19
	8	"	" (57 ³)	6 43		2 01			
	9	"	" (96 ³)	6 45	6 46,6	2 03	2 04,6		
	10	HR 1852	" (57 ³)	7 01		2 19		+1	31.5
	11	"	" (96 ³)	7 02		2 20			
	12	"	" (156 ³)	7 04	7 06,6	2 22	2 24,6		
	13	HR 1899	" (60 ³)	7 24	7 25	2 41.5	2 42.5	+1	51
	14	"	" (102 ³)	7 25	7 26,7	2 42.5	2 44,2		
HX 3480	1	HR 1899	" (124 ³)	7 36	7 38,9	2 53.5	2 56,4	+2	04
	2	HR 2970	" (8 ³)	8 23	8 31	3 40.5	3 42.5	+0	48
	3	"	" (14)	8 31	8 45	3 48.5	4 02.5	+0	59
	4	"	" (24)	8 45	9 09	4 02.5	4 26.5	+1	18
	5	HR 3438	" (8)	9 40	9 48	4 57.5	5 05.5	+1	05
	6	"	" (14)	9 48	10 02	5 05.5	5 19.5	+1	16
	7	"	" (25)	10 02	10 27	5 19.5	5 44.5	+1	36

1-2/II/68 K.

HX 3480	8	HR 3045	103a-0 (5)	8 56	9 01	4 00.5	4 05.5	+1	11
	9	"	" (9)	9 01	9 10	4 05.5	4 14.5	+1	18
	10	"	" (16)	9 10	9 26	4 14.5	4 30.5	+1	30.5

5-1	5-1	B Fe 10 ¹			
4-2	4-2				
4-3	4-3				
4-4	4-4				
4-5	4-5				
4-6	4-6				
4-7	4-7				
4-8	4-8				
4-9	4-9				
4-10	4-10				
4-11	4-11				
4-12	4-12				
4-13	4-13				
4-14	4-14				
4-15	4-15				
4-16	4-16				
4-17	4-17				
4-18	4-18				
4-19	4-19				
4-20	4-20				
4-21	4-21				
4-22	4-22				
4-23	4-23				
4-24	4-24				
4-25	4-25				
4-26	4-26				
4-27	4-27				
4-28	4-28				
4-29	4-29				
4-30	4-30				
4-31	4-31				
4-32	4-32				
4-33	4-33				
4-34	4-34				
4-35	4-35				
4-36	4-36				
4-37	4-37				
4-38	4-38				
4-39	4-39				
4-40	4-40				
4-41	4-41				
4-42	4-42				
4-43	4-43				
4-44	4-44				
4-45	4-45				
4-46	4-46				
4-47	4-47				
4-48	4-48				
4-49	4-49				
4-50	4-50				
4-51	4-51				
4-52	4-52				
4-53	4-53				
4-54	4-54				
4-55	4-55				
4-56	4-56				
4-57	4-57				
4-58	4-58				
4-59	4-59				
4-60	4-60				
4-61	4-61				
4-62	4-62				
4-63	4-63				
4-64	4-64				
4-65	4-65				
4-66	4-66				
4-67	4-67				
4-68	4-68				
4-69	4-69				
4-70	4-70				
4-71	4-71				
4-72	4-72				
4-73	4-73				
4-74	4-74				
4-75	4-75				
4-76	4-76				
4-77	4-77				
4-78	4-78				
4-79	4-79				
4-80	4-80				
4-81	4-81				
4-82	4-82				
4-83	4-83				
4-84	4-84				
4-85	4-85				
4-86	4-86				
4-87	4-87				
4-88	4-88				
4-89	4-89				
4-90	4-90				
4-91	4-91				
4-92	4-92				
4-93	4-93				
4-94	4-94				
4-95	4-95				
4-96	4-96				
4-97	4-97				
4-98	4-98				
4-99	4-99				
4-100	4-100				

$t_{exp} = 20.8$ $t_{amb} = 20.6$

$t_{exp} = 19.9$ $t_{amb} = 19.7$

$t_{exp} = 19.1$ $t_{amb} = 19.2$

$t_{exp} = 18.6$ $t_{amb} = 18.8$

$t_{exp} = 18.5$ $t_{amb} = 18.5$

$t_{exp} = 17.3$ $t_{amb} = 17.4$

$t_{exp} = 25.1$ $t_{amb} = 22.9$ (kilo deveso)

24-25/II/68 K.

T. S.

T. U.

HX 34811	1	HR 1899	103a-0 (6 ^h)	6 17	6 18	23 51	23 53	+ 0	44
	2	"	" (10 ^h)	6 18	6 19.7	23 52	23 53.7	+ 0	45.5
	3	"	" (17 ^h)	6 19.7	6 22.6	23 53.7	23 56.6	+ 0	47.5
	4	HR 2282	" (14 ^h)	6 42	6 44.4	0 16	0 18.4	+ 0	24.5
	5	"	" (3 ^h)	6 44.4	6 48.3	0 18.4	0 22.3	+ 0	27.5
	6	"	" (7 ^h)	6 48.3	6 55.8	0 22.3	0 29.5	+ 0	33
	7	HR 2491	" (1 ^h)	7 18		0 53		+ 0	34.5
	8	"	" (2 ^h)						
	9	"	" (4 ^h)						
	10	HR 2618	" (2 ^h)	7 35		1 10		+ 0	37.5
	11	"	" (5 ^h)						
	12	"	" (8 ^h)						
	13	HR 2653	" (2 ^h)	7 59	8 01.7	1 34	1 36.7	+ 0	59
	14	"	" (4 ^h)	8 01.7	8 06.5	1 36.7	1 41.5	+ 1	02.5
HX 34822	1	HR 2653	" (9 ^h)	8 17	8 26	1 52	2 01	+ 1	20
	2	HR 2693	" (1 ^h)	8 45	8 46.8	2 20	2 21.8	+ 1	39
	3	"	" (3 ^h)	8 46.8	8 49.8	2 21.8	2 24.8	+ 1	41.5
	4	"	" (5 ^h)	8 49.8	8 54.9	2 24.8	2 29.9	+ 1	45.5
	5	HR 3685	" (0 ^h)	10 18	10 18.8	3 53	3 53.8	+ 1	05.5
	6	"	" (1 ^h)	10 18.8	10 20.1	3 53.8	3 55.1	+ 1	06.5
	7	"	" (2 ^h)	10 20.1	10 22.1	3 55.1	3 57.1	+ 1	08

28-29/II/68 K.

8	HR 1713	103a-0 (6 ^h)	7 09		0 28.5		+ 1	56.5
9	"	" (12 ^h)						
10	"	" (21 ^h)						

5-1

5

B Fe 10³

Rep.

$$t_{\text{exp}} = 20.4 \quad t_{\text{amb}} = 20.0$$
$$F_e 10^{-1}$$
$$t_{exp} = 20.3 \quad t_{amb} = 20.1$$
$$t_{ap} = 20.3 \quad t_{amb} = 20.1$$

$t_{exp} = 19.9$ $t_{amb} = 19.7$

5

$t_{exp.} = 19.9$ $t_{amb.} = 19.6$

28-29/II/68 K.

T.S.

T.V.

HX 3482	2	11	HR 1903	103a-0	(0.6)	7 22	7 22.6	0 41.5	0 42.1	+1 48
	12	"	"	"	(1 ^m)	7 22.6	7 23.6	0 42.1	0 43.1	+1 49
	13	"	"	"	(1.8)	7 23.6	7 25.4	0 43.1	0 44.9	+1 50.5
	14	HR 1948	"	"	(1 ^m)	7 35	7 36	0 54.5	0 55.5	+1 57
3483	3	1	HR 1948	"	(1.8)	7 49	7 50.8	1 08.5	1 10.3	+2 11
	2	"	"	"	(3)	7 50.8	7 53.8	1 10.3	1 13.3	+2 13.5
	3	HR 2004	"	"	(0.9)	8 08	8 08.9	1 27.5	1 28.4	+2 22.5
	4	"	"	"	(1.5)	8 08.9	8 10.4	1 28.4	1 29.9	+2 24
	5	"	"	"	(2.5)	8 10.4	8 12.9	1 29.9	1 32.4	+2 26
	6	HR 2294	"	"	(0.8)	8 29	8 29.8	1 48.5	1 49.3	+2 08.5
	7	"	"	"	(1.3)	8 29.8	8 31.1	1 49.3	1 50.6	+2 09.5
	8	"	"	"	(2.2)	8 31.1	8 33.3	1 50.6	1 52.8	+2 11.5
	9	HR 2326	"	"	(3 ¹)	8 41		2 03		+2 21
	10	"	"	"	(6 ¹)					
	11	"	"	"	(12 ¹)					
	12	HR 2827	"	"	(1.5)	9 03	9 04.5	2 22	2 23.5	+1 40.5
	13	"	"	"	(2.4)	9 04.5	9 06.9	2 23.5	2 25.9	+1 42.5
	14	"	"	"	(4 ^m)	9 06.9	9 10.9	2 25.9	2 29.9	+1 46

29/II-1/III/68 K.

3484	1	1	HR 1956	103a-0	(1.8)	7 34	7 35.8	0 49	0 50.8	+1 57
	2	"	"	"	(3)	7 35.8	7 38.8	0 50.8	0 53.8	+1 59
	3	"	"	"	(5)	7 38.8	7 43.8	0 53.8	0 58.8	+2 03
	4	HR 3185	"	"	(1.3)	8 41	8 42.3	1 55.5	1 56.8	+0 36
	5	"	"	"	(2)	8 42.3	8 44.3	1 56.8	1 58.8	+0 37.5

5-1

5

B

 $t_{exp} = 19.9$ $t_{amb.} = 19.6$ $Fe 10^4$ $t_{exp} = 19.8$ $t_{amb} = 19.9$ $t_{exp} = 20.0$ $t_{amb} = 19.9$ $t_{exp} = 20.0$ $t_{amb} = 19.9$

Rep.

 $t_{exp} = 20.0$ $t_{amb.} = 19.9$ $t_{exp} = 20.0$ $t_{amb.} = 19.9$

5-1

5

B

 $Fe 10^4$ $t_{exp} = 22.7$ $t_{amb} = 22.3$

108

29/II - 1/III/68 K.

T.S.

T.U.

HX 3484	6	HR 3185	103a-D	(4)	8 44.3	8 48.3	2 58.8	2 02.8	+0 40.5
	7	HR 3468	"	(1.7)	9 04	9 05.7	2 18.5	2 20.2	+0 23
	8	"	"	(3)	9 05.7	9 08.7	2 20.2	2 23.2	+0 25.5
	9	"	"	(5)	9 08.7	9 13.7	2 23.2	2 28.2	+0 28.5
	10	HR 3748	"	(1.5)	9 40	9 41.5	2 54.5	2 56	+0 15
	11	"	"	(3)	9 41.5	9 44.5	2 56	2 59	+0 17.5
	12	"	"	(4)	9 44.5	9 48.5	2 59	3 03	+0 21
	13	HR 3845	"	(11)	10 03	10 14	3 17.5	3 28.5	+0 30.5
	14	"	"	(18)	10 14	10 32	3 28.5	3 46.5	+0 45
3485	2	1	HR 3845	"	(32)	10 44	11 16	3 58.5	4 30.5 +1 22

2-3/III/68 K.

3485	2	2	HR 1931	103a-D	(1.7)	6 48	6 49.7	23 54	23 55.7 +1 12
	3	"	"	"	(3)	6 49.7	6 52.7	23 55.7	23 58.7 +1 14.5
	4	"	"	"	(5)	6 52.7	6 57.7	23 58.7	0 03.7 +1 18.5
	5	HR 2040	"	(4)	7 16	7 20	0 22	0 26	+1 28.5
	6	"	"	(7)	7 20	7 27	0 26	0 33	+1 34
	7	"	"	(12)	7 27	7 39	0 33	0 45	+1 43.5

4-5/III/68 K.

3485	2	8	HR 1702	103a-D	(1.2)	6 45	6 46.2	23 42	23 43.2 +1 34.5
	9	"	"	"	(2)	6 46.2	6 48.2	23 43.2	23 45.2 +1 36
	10	"	"	"	(3)	6 48.2	6 51.2	23 45.2	23 48.2 +1 38.5
	10	HR 2429	"	(2)	7 08	7 10	0 05	0 07	
	11	"	"	(9)	7 10	7 19	0 07	0 16	+0 39.5

5-1 5 B $t_{exp} = 22.4$ $t_{amb} = 22.1$

$t_{exp} = 22.3$ $t_{amb} = 22.0$

$t_{exp} = 22.1$ $t_{amb} = 21.9$

$t_{exp} = 22.0$ $t_{amb} = 21.9$

Fe 10³

5-1 5 B

$t_{exp} = 23.6$ $t_{amb} = 23.1$

$t_{exp} = 22.8$ $t_{amb} = 22.5$ Pasar

las nubes, Nubló.

5-1 5 B

$t_{exp} = 25.2$ $t_{amb} = 24.8$ exp.

Por error expuso 2^{na} HR 2429 en vez de HR 1702

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4-5/III/68 K.

T.S.

T.V.

HX 34852	12	HR 2429	103a-0	(15)	7 19	7 34	0 16	0 31	+0 51.5
	13	"	"	(25)	7 34	7 59	0 31	0 56	+1 11.5
	14	HR 2773	"	(4)	8 22	8 26	1 19	1 23	+1 08.5
HX 34863	1	HR 2773	"	(7)	8 33	8 40	1 30	1 37	+1 21
	2	"	"	(12)	8 40	8 52	1 37	1 49	+1 30.5
	3	HR 3614	"	(8)	9 21	9 29	2 18	2 26	+0 22
	4	"	"	(15)	9 29	9 44	2 26	2 41	+0 33.5
	5	"	"	(25)	9 44	10 09	2 41	3 06	+0 53.5
	6	HR 4023	"	(3)	10 23	10 26	3 19.5	3 28.5	+0 11.5
	7	"	"	(4)	10 26	10 40	3 22.5	3 26.5	+0 15
	8	"	"	(8)	10 40	10 48	3 26.5	3 34.5	+0 31
	9	HR 4094	"	(12)	11 01	11 13	3 47.5	3 54.5	+0 43
	10	"	"	(21)	11 13	11 34	3 59.5	4 20.5	+0 59.5
	11	"	"	(36)	11 34	12 10	4 20.5	4 56.5	+1 28

5-6/III/68 K.

HX 34863	12	HR 2574	103a-0	(15)	7 04	7 19	23 57	0 12	+0 19
	13	"	"	(25)	7 19	7 44	0 12	0 37	+0 39
	14	"	"	(43)	7 44	8 27	0 37	1 20	+1 11
HX 34874	1	HR 3270	"	(6)	8 47	8 53	1 39.5	1 45.5	+0 33
	2	"	"	(11)	8 53	9 04	1 45.5	1 56.5	+0 41.5
	3	"	"	(18)	9 04	9 22	1 56.5	2 14.5	+0 56
	4	HR 3523	"	(16)	9 47	10 03	2 39.5	2 55.5	+1 05.5
	5	"	"	(28)	10 03	10 31	2 55.5	3 23.5	+1 27.5
	6	"	"	(35)	10 31	11 06	3 23.5	3 58.5	+1 59

9-10/III/68 K.

T. S.

T. V.

HX 3487	7	HR 2550	103A-0	(1 ^m)	7 59	8 00	0 34	0 35	+1	11.5
	8	"	"	(3)	8 00	8 03	0 35	0 38	+1	13.5
	9	"	"	(5)	8 03	8 08	0 38	0 43	+1	17.5
	10	HR 3024	"	(8)	8 26	8 34	1 01	1 09	+0	48
	11	"	"	(15)	8 34	8 49	1 09	1 24	+0	59.5
	12	"	"	(25)	8 49	9 14	1 24	1 49	+1	19.5
	13	HR 3615	"	(3.5)	9 26	9 29.5	2 01	2 04.5	+0	26
	14	"	"	(6)	9 29.5	9 35.5	2 04.5	2 10.5	+0	30.5
HX 3488	1	HR 3615	"	(11)	9 44	9 55	2 19	2 30	+0	47.5
	2	HR 3890	"	(1.7)	10 10	10 11.7	2 45	2 46.7	+0	25
	3	"	"	(3)	10 11.7	10 14.7	2 46.7	2 49.7	+0	27.5
	4	"	"	(5)	10 14.7	10 19.7	2 49.7	2 54.7	+0	31.5

12-13/III/68 K.

	5	HR 1702	103A-0	(1.2)	7 29	7 30.2	23 55	23 56.2	+2	18.5
	6	"	"	(2)	7 30.2	7 32.2	23 56.2	23 58.2	+2	20
	7	"	"	(3)	7 32.2	7 35.2	23 58.2	0 01.2	+2	22.5
	8	HR 2491	"	(0.3)	8 08	8 08.2	0 34	0 34.3	+1	25
	9	"	"	(0.5)	8 10	8 10.5	0 36	0 36.5	+1	27
	10	"	"	(1.1)	8 14	8 15.1	0 40	0 41.1	+1	31
	11	HR 2326	"	(0.8)	8 30	8 30.8	0 56	0 56.8	+2	07.5
	12	"	"	(1.6)	8 32	8 33.6	0 58	0 59.6	+2	10
	13	"	"	(3.2)	8 35	8 38.2	1 01	1 04.2	+2	13.5
	14	HR 3307	"	(2)	9 11	9 13	1 37	1 39	+0	50.5
HX 3489	2	HR 3307	"	(3)	9 22	9 25	1 48	1 51	+1	02

5-1

5

B

 $t_{exp} = 23.4$ $t_{amb} = 23.1$ $t_{exp} = 22.9$ $t_{amb} = 22.7$ $F_c 10^4$ $t_{exp.} = 22.5$ $t_{amb} = 22.2$ $t_{exp.} = 22.4$ $t_{amb} = 22.1$ Pasando los
ruidos

5-1

5

 $t_{exp.} = 22.3$ $t_{amb} = 21.8$

con el imagen desenfocado.

Rep.

 $t_{exp.} = 22.3$ $t_{amb} = 21.7$

Rep.

 $t_{exp.} = 21.8$ $t_{amb} = 21.5$ $t_{exp.} = 21.5$ $t_{amb} = 21.0$ $F_c 10^4$

111

12-13/III/68 K.

T. S.

T. V.

HX 3489	2	HR 3307	103a-0	(6)	9 25	9 31	1 51	1 57	+1 06.5
	3	HR 3940	"	(1.6)	10 08	10 09.6	2 34	2 35.6	+0 13.5
	4	"	"	(3)	10 10	10 13	2 36	2 39	+0 16
	5	"	"	(5)	10 13	10 18	2 39	2 44	+0 20
	6	HR 4114	"	(3.5)	10 49	10 52.5	3 15	3 18.5	+0 24.5
	7	"	"	(6)	10 52.5	10 58.5	3 18.5	3 24.5	+0 29
	8	"	"	(11)	10 58.5	11 09.5	3 24.5	3 35.5	+0 37.5
	9	HR 4140	"	(2)	11 25	11 27	3 50.5	3 52.5	+0 55.5
	10	"	"	(3)	11 27	11 30	3 52.5	3 55.5	+0 58
	11	"	"	(5)	11 30	11 35	3 55.5	4 00.5	+1 02
	12	HR 4390	"	(2)	12 15	12 17	4 40.5	4 42.5	+0 57
	13	"	"	(3.5)	12 17	12 20.5	4 42.5	4 46	+1 00
	14	"	"	(6)	12 20.5	12 26.5	4 46	4 52	+1 04.5

13-14/III/68 K

HX 3490	3	HR 2878	103a-0	(7)	8 06	8 13	0 28	0 35	+0 41.5
	2	"	"	(11)	8 13	8 24	0 35	0 46	+0 50.5
	3	"	"	(21)	8 24	8 45	0 46	1 07	+1 06.5
	4	HR 3080	"	(6)	8 53.5	8 59.5	1 15	1 21	+1 05.5
	5	"	"	(11)	8 59.5	9 10.5	1 21	1 32	+1 14
	6	"	"	(19)	9 10.5	9 29.5	1 32	1 51	+1 29
	7	HR 3696	"	(25)	9 41	10 06	2 02.5	2 27.5	+0 38.5
	8	"	"	(43)	10 06	10 49	2 27.5	3 10.5	+1 12.5
	9	"	"	(49)	10 49	11 38	3 10.5	3 59.5	+1 58.5

5-1 5 B $t_{exp} = 21.3$ $t_{amb} = 20.7$

" " " " " "

" " " " " "

" " " " $t_{exp} = 21.2$ $t_{amb} = 20.8$

" " " " " "

" " " " " "

" " " " $t_{exp} = 21.0$ $t_{amb} = 20.7$

" " " " " "

" " " " " "

" " " " $t_{exp} = 21.0$ $t_{amb} = 20.6$

" " " " " "

" " " " " "

" " " " $t_{exp} = 20.8$ $t_{amb} = 20.3$ Nubes

5-1 5 B Fe 10⁴

" " " " " "

" " " " $t_{exp} = 24.1$ $t_{amb} = 23.6$

" " " " " "

" " " " " "

" " " " $t_{exp} = 23.8$ $t_{amb} = 23.4$

" " " " " "

" " " " " "

" " " " $t_{exp} = 22.3$ $t_{amb} = 22.9$

se movió

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15-16/III/68 K.

T. S.

T. U.

HX 3491	1	HR 2874	103a-0	(9)	7 52	8 01	0 05	0 14	+ 0 28
	2	"	"	(15)	8 01	8 16	0 14	0 29	+ 0 40
	3	"	"	(25)	8 16	8 41	0 29	0 54	+ 1 00
	4	HR 3477	"	(8)	9 39	9 47	1 52	2 00	+ 1 00
	5	"	"	(14)	9 47	10 01	2 00	2 14	+ 1 11
	6	"	"	(24)	10 01	10 25	2 14	2 38	+ 1 30
	7	HR 3825	"	(3)	10 57.5	11 00.5	3 10	3 13	+ 1 26
	8	"	"	(6)	11 00.5	11 06.5	3 13	3 19	+ 1 30.5
	9	"	"	(10)	11 06.5	11 16.5	3 19	3 24	+ 1 38.5
	10	HR 4257	"	(6)	11 21	11 27	3 33.5	3 39.5	+ 0 32
	11	"	"	(11)	11 27	11 38	3 39.5	3 50.5	+ 0 40.5
	12	"	"	(19)	11 38	11 57	3 50.5	4 09.5	+ 0 55.5

16-17/III/68 K

HX 3491	13	HR 2035	103a-0	(7)	7 22	7 29	23 31	23 38	+ 1 36
	14	"	"	(12)	7 29	7 41	23 38	23 50	+ 1 45.5
HX 3492	21	HR 2035	"	(21)	7 48	8 09	23 57	0 18	+ 2 09
	2	HR 2296	"	(6)	8 19	8 25	0 28	0 34	+ 2 01.5
	3	"	"	(11)	8 25	8 36	0 34	0 45	+ 2 10
	4	"	"	(18)	8 36	8 54	0 45	1 03	+ 2 24.5
	5	HR 3518	"	(12)	9 09	9 21	1 17.5	1 29.5	+ 0 26
	6	"	"	(21)	9 21	9 42	1 29.5	1 50.5	+ 0 42.5
	7	"	"	(36)	9 42	10 18	1 50.5	2 26.5	+ 1 11
	8	HR 3903	"	(9)	10 37	10 46	2 45	2 54	+ 0 52
	9	"	"	(16)	10 46	11 02	2 54	3 10	+ 1 04.5

5-1 5 B Fe 10⁴ $t_{exp} = 17.6$ $t_{amb} = 17.4$ $t_{exp} = 15.6$ $t_{amb} = 15.5$ $t_{exp} = 15.2$ $t_{amb} = 15.2$ $t_{exp} = 14.9$ $t_{amb} = 14.9$ 5-1 5 B Fe 10⁴ $t_{exp} = 19.0$ $t_{amb} = 18.5$ $t_{exp} = 18.5$ $t_{amb} = 18.2$ $t_{exp} = 18.0$ $t_{amb} = 17.6$ $t_{exp} = 17.1$ $t_{amb} = 16.8$

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16-17/III/68 K.

T.S.

T.U.

HX3492 2 10 HR 3903 103a-0 (26) 1102 1128 310 336 +1 25.5

3-4/IV/68 K.

3493 1 1 HR 2745 103a-0 (4) 946 950 047 051 +2 35.5
 2 " " (7) 950 957 051 058 +2 41
 3 " " (12) 957 1009 058 110 +2 50.5
 4 HR 2749 " (2) 1018 1020 119 121 +3 06
 5 " " (3.5) 1020 1023.5 121 124.5 +3 09
 6 " " (6) 1023.5 1029.5 124.5 130.5 +3 13.5

3494 2 1 HR 4232 " (4) 1143 1147 243.5 247.5 +0 57.5
 2 " " (8) 1147 1155 247.5 255.5 +1 03.5
 3 " " (14) 1155 1209 255.5 309.5 +1 14.5
 4 HR 4287 " (11) 1230 1241 330.5 341.5 +1 37.5
 5 " " (19) 1241 1300 341.5 400.5 +1 52.5
 6 " " (32) 1300 1332 400.5 432.5 +2 18

6-7/IV/68 K.

Desde 7.IV.68

T.U. = T.A. + 4^P

27 HR 3447 103a-0 (1.5) 856 857.5 2345.5 2347 +0 17.5
 8 " " (3) 857.5 900.5 2347 2350 +0 20
 9 " " (4.5) 900.5 905 2350 2354.5 +0 23.5
 10 HR 3571 " (2) 924 926 013.5 015.5 +0 31
 11 " " (4) 926 930 015.5 019.5 +0 34
 12 " " (6.5) 930 936.5 019.5 026 +0 39

9-10/IV/68 K.

2 13 HR 4216 103a-0 (2) 1124 1126 202 204 +0 40.

5-1 5 B

5-1 5 B Fe 10³ $t_{exp} = 12.7$ $t_{amb} = 12.7$ Fe 10³ $t_{exp} = 12.1$ $t_{amb} = 12.0$ $t_{exp} = 11.4$ $t_{amb} = 11.3$

5-1 5

 $t_{exp} = 14.6$ $t_{amb} = 14.1$ T.U. = T.A. + 4^h $t_{exp} = 14.7$ $t_{amb} = 13.9$ Fe 10

5-1 5

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9-10/IV/68 K.

T. S.

T. U.

HX 3494	2	14	HR 4216	103a-0	(3)	11 26	11 29	2 04	2 07	+0 42.5
HX 3495	3	1	HR 4216	"	(6)	11 29	11 35	2 07	2 13	+0 47
		2	HR 4467	"	(62)	12 15	12 16	2 53	2 54	+0 41.5
		3	"	"	(1,5)	12 16	12 17.5	2 54	2 55.5	+0 43
		4	"	"	(3)	12 17.5	12 20.5	2 55.5	2 58.5	+0 45
		5	HR 4638	"	(2.5)	12 43	12 45.5	3 21	3 23.5	+0 35
		6	"	"	(4)	12 45.5	12 49.5	3 23.5	3 27.5	+0 38
		7	"	"	(7)	12 49.5	12 56.5	3 27.5	3 34.5	+0 43.5
		8	HR 4898	"	(2.5)	13 15	13 17.5	3 53	3 55.5	+0 24
		9	"	"	(4)	13 17.5	13 21.5	3 55.5	3 59.5	+0 27
		10	"	"	(7.5)	13 21.5	13 29	3 59.5	4 07	+0 33
		11	HR 5248	"	(1.5)	14 28	14 29.5	5 06	5 07.5	+0 33
		12	"	"	(3)	14 29.5	14 32.5	5 07.5	5 10.5	+0 35
		13	"	"	(5.5)	14 32.5	14 38	5 10.5	5 16	+0 39.5
		14	HR 5249	"	(2)	14 56	14 58	5 33.5	5 35.5	+1 01
3496	4	1	HR 5249	"	(3)	15 07	15 10	5 44.5	5 47.5	+1 12.5
		2	"	"	(6)	15 10	15 16	5 47.5	5 53.5	+1 17

15-16/IV/68 K.

43	HR 3237	103a-0	(6)	10 15	10 21	0 29	0 35	+2 06
4	"	"	(11)	10 21	10 32	0 35	0 46	+2 14.5
5	"	"	(18)	10 32	10 50	0 46	1 04	+2 29
6	HR 4140	"	(1.5)	12 00	12 01.5	2 14	2 15.5	+1 30
7	"	"	(2.5)	12 01.5	12 04	2 15.5	2 18	+1 32
8	"	"	(4)	12 04	12 08	2 18	2 22	+1 35.5

5-1 5 A $t_{exp} = 18.2$ $t_{amb} = 17.7$

" " Fe 10^A

" " " " " "

" " " " " "

" " " " $t_{exp} = 17.9$ $t_{amb} = 17.3$

" " " " " "

" " " " " "

" " " " $t_{exp} = 17.5$ $t_{amb} = 17.0$

" " " " " "

" " " " " "

" " " " $t_{exp} = 17.5$ $t_{amb} = 16.8$

" " " " " "

" " " " " "

" " " " $t_{exp} = 16.9$ $t_{amb} = 16.4$

" " " " " "

" " " " Fe 10^A

" " " " $t_{exp} = 16.8$ $t_{amb} = 16.3$

" " " " " "

" " " " " "

5-1 5 Fe 10^A em: H β , H γ

" " " " " "

" " " " $t_{exp} = 16.5$ $t_{amb} = 16.1$ Pasan los
unles.
em: H β

" " " " " "

" " " " " "

" " " " $t_{exp} = 16.5$ $t_{amb} = 16.0$

122

15-16/IV/68 K.

T.S.

T.V.

HX 34964	9	HR 4689	103a-0 (2.5)	13 01,5	13 04	3 15	3 17,5	+0 45
	10	"	" (4)	13 04	13 08	3 17,5	3 21,5	+0 48
	11	"	" (8)	13 08	13 16	3 21,5	3 24,5	+0 54

16-17/IV/68 K.

4 12	HR 3786	103a-0 (3)	9 30	9 33	23 40	23 43	+0 02,5
13	"	" (4.5)	9 33	9 37,5	23 43	23 47,5	+0 06
14	"	" (8)	9 37,5	9 45,5	23 47,5	23 55,5	+0 12,5

17-18/IV/68 K.

34971	1	HR 3430	103a-0 (25)	9 20	9 45	23 26	23 51	+0 55
	2	"	" (42)	9 45	10 27	23 51	0 33	+1 28,5
	3	"	" (74)	10 27	11 41	0 33	1 47	+2 29,5
	4	HR 4405	" (4)	12 09	12 13	2 15	2 19	+0 48
	5	"	" (7)	12 13	12 20	2 19	2 26	+0 53,5
	6	"	" (12)	12 20	12 32	2 26	2 38	+1 03

30/IV-1/V/68 K.

17	HR 4450	103a-0 (5)	11 40	11 45	0 56	1 01	+0 11,5
8	"	" (8.3)	11 45	11 53,3	1 01	1 09,3	+0 18,5
9	"	" (14.5)	11 53,3	12 07,8	1 09,3	1 23,8	+0 29,5
10	HR 4623	" (4)	12 23	12 27	1 39	1 43	+0 18,5
11	"	" (7.5)	12 27	12 34,5	1 43	1 50,5	+0 24,5
12	"	" (13)	12 34,5	12 47,5	1 50,5	2 03,5	+0 34,5
13	HR 4630	" (4)	12 59	13 03	2 14,5	2 18,5	+0 53

5-1	5	B		
"	"	"		
"	2		$t_{exp} = 16.1$	$t_{amb} = 15.7$ Se nubló
5-12	3	B		
"	"	"		
"	2		$t_{exp} = 16.1$	$t_{amb} = 15.4$ Velo
5-1	5	B Fe 10 ⁴		
"	"	"	$t_{exp} = 17.5$	$t_{amb} = 16.9$
"	"	"	$t_{exp} = 17.3$	$t_{amb} = 16.9$
"	"	"		
"	3			Pasan los
"	2		$t_{exp} = 17.4$	$t_{amb} = 17.1$ umbes.
5-1	5	B		
"	"	"		
"	"	"	$t_{exp} = 10.5$	$t_{amb} = 9.9$
"	"	"		
"	"	"		
"	"	"	$t_{exp} = 10.3$	$t_{amb} = 9.6$
"	"	"		

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30/IV - 1/II/68 K.

T.S.

T.V.

HX 3497	14 HR 4630	103a-D (7,5)	13 03	13 10.5	2 18.5	2 26	+0 58.5
34982	1 HR 4630	" (13)	13 23	13 36	2 38.5	2 51.5	+1 21.5
	2 HR 4786	" (1.7)	13 50	13 51.7	3 05.5	3 07.2	+1 18.5
	3 "	" (3)	13 52	13 55	3 07.5	3 10.5	+1 21
	4 "	" (5)	13 55	14 00	3 10.5	3 15.5	+1 25
	5 HR 5378	" (3.5)	14 45	14 48.5	4 00.5	4 04	+0 26
	6 "	" (6)	14 48.5	14 54.5	4 04	4 10	+0 31
	7 "	" (11)	14 54.5	15 05.5	4 10	4 21	+0 39.5
	8 HR 5288	" (1)	15 17	15 18	4 32.5	4 33.5	+1 13
	9 "	" (1.5)	15 18	15 19.5	4 33.5	4 35	+1 14.5
	10 "	" (3)	15 19.5	15 22.5	4 35	4 38	+1 16.5
	11 HR 5285	" (3)	15 38	15 41	4 53.5	4 56.5	+1 36
	12 "	" (6)	15 41	15 47	4 56.5	5 02.5	+1 40.5
	13 "	" (10)	15 47	15 57	5 02.5	5 12.5	+1 48.5

3-4/II/68 K.

3499	7 HR 5378	103a-D (3,5)	15. 01	15 04.5	4 06.5	4 10	+0 42
	8 "	" (6)	15 04.5	15 10.5	4 10	4 16	+0 47
	9 "	" (11)	15 10.5	15 21.5	4 16	4 27	+0 55.5

4-5/II/68 K.

3500	1 HR 4743	103a-D (2)	13 26	13 28	2 27.5	2 29.5	+1 01
	2 "	" (3.5)	13 28	13 31.5	2 29.5	2 33	+1 04
	3 "	" (6)	13 31.5	13 37.5	2 33	2 39	+1 08.5

5-1 1 5-10 3 B $t_{exp} = 9.2$ $t_{amb} = 9.3$

" 2-1 " 2-10 3 Fe 10³

" 3-1 " 3-10 3 12-10 3

" 4-1 " 4-10 3 15-10 3

" 5-1 " 5-10 3 $t_{exp} = 9.2$ $t_{amb} = 8.7$

" 6-1 " 6-10 3 18-10 3

" 7-1 " 7-10 3 21-10 3

" 8-1 " 8-10 3 $t_{exp} = 8.5$ $t_{amb} = 8.2$

" 9-1 " 9-10 3 24-10 3

" 10-1 " 10-10 3 27-10 3

" 11-1 " 11-10 3 $t_{exp} = 8.3$ $t_{amb} = 7.9$

" 12-1 " 12-10 3 30-10 3

" 13-1 " 13-10 3 33-10 3

" 14-1 " 14-10 3 $t_{exp} = 7.9$ $t_{amb} = 7.4$

" 15-1 " 15-10 3 36-10 3

" 16-1 " 16-10 3 39-10 3

5-1 4 B

" 2-1 " 2-10 3 12-10 3

" 3-1 " 3-10 3 Fe 10³ $t_{exp} = 13.0$ $t_{amb} = 12.2$

" 4-1 " 4-10 3 15-10 3

" 5-1 " 5-10 3 18-10 3

" 6-1 " 6-10 3 21-10 3

5-1 4 B Fe 10³

" 2-1 " 2-10 3 12-10 3

" 3-1 " 3-10 3 15-10 3

" 4-1 " 4-10 3 18-10 3

4-5/V/68

K.

T. S.

T. O.

HX 3500	4	HR 4763	103a-0 (1.2)	13 52	13 53.2	2 53.5	2 54.7	+1 23.5
	5	"	" (2)	13 54	13 56	2 55.5	2 57.5	+1 26
	6	"	" (3.5)	13 56	13 59.5	2 57.5	3 01	+1 29
	7	HR 4802	" (2)	14 10	14 13	3 11.5	3 14.5	+1 36
	8	"	" (4)	14 13	14 17	3 14.5	3 18.5	+1 39.5
	9	"	" (8)	14 17	14 25	3 18.5	3 26.5	+1 45.5
	10	HR 5378	" (3.5)	14 38	14 41.5	3 39.5	3 43	+0 19
	11	"	" (6)	14 41.5	14 47.5	3 43	3 49	+0 24
	12	"	" (11)	14 47.5	14 58.5	3 49	4 00	+0 35.5
	13	"	" (6)	14 58.5	15 04.5	4 00	4 06	+0 41
	14	"	" (11)	15 04.5	15 15.5	4 06	4 17	+0 49.5

6-7/V/68

K.

3501	21	HR 5378	103a-0 (3.5)	16 39	16 42.5	5 29	5 32.5	+2 20
	2	"	" (6)	16 42.5	16 48.5	5 32.5	5 38.5	+2 25
	3	"	" (11)	16 48.5	16 59.5	5 38.5	5 49.5	+2 33.5

7-8/V/68

K.

24	HR 4037	103a-0 (1.2)	11 17	11 18.2	0 04	0 05.2	+1 05
5	"	" (2)	11 19	11 21	0 06	0 08	+1 07.5
6	"	" (3.5)	11 21	11 24.5	0 08	0 11.5	+1 10
7	HR 4050	" (8.5)	11 34	11 42.5	0 21	0 29.5	+1 22.5
8	"	" (14.5)	11 42.5	11 57	0 29.5	0 44	+1 34
9	"	" (25)	11 57	12 22	0 44	1 09	+1 53.5
10	HR 5378	" (4)	13 00	13 04	1 47	1 51	-1 18.5
11	"	" (14)	13 04	13 18	1 51	2 05	-1 09.5

8-9/V/68

K.

T.S

- T. U.

HX 3502

1	HR 3659	103a-D (12)	11 00	11 01.2	23 44	23 45.2	+1 50.5
2	"	" (2)	11 02	11 04	23 46	23 48	+1 53
3	"	" (4)	11 04	11 08	23 48	23 52	+1 56
4	HR 3663	" (2)	11 21	11 23	0 05	0 07	+2 11.5
5	"	" (4)	11 23	11 27	0 07	0 11	+2 14.5
8	HR 5378	" (10)	12 58	13 08	1 41.5	1 51.5	-1 17.5
9	"	" (20)	13 08	13 28	1 51.5	2 11.5	-1 02.5
10	"	" (10)	13 28	13 38	2 11.5	2 21.5	-0 47.5
11	"	" (6)	13 38	13.44	2 21.5	2 27.5	-0 39.5
12	"	" (8)	13 44	13 52	2 27.5	2 35.5	-0 32.5
13	"	" (4)	13 52	13 56	2 35.5	2 39.5	-0 26.5
14	"	" (10)	13 56	14 06	2 39.5	2 49.5	-0 19.5

3503

41	HR 5378	" (3,5)	15 00.5	15 04	3 44	3 47.5	+0 42
2	"	" (6)	15 04	15 10	3 47.5	3 53.5	+0 46.5
3	"	" (11)	15 10	15 21	3 53.5	4 04.5	+0 55
4	HR 5463	" (1,5)	15 49	15 50.5	4 32	4 33.5	+1 10.5
5	"	" (3)	15 51	15 54	4 34	4 37	+1 13
6	"	" (4)	15.54	15 58	4 37	4 41	+1 16.5

10-11/V/68

K.

3503

47	HR 4210	103a-D (25)	11 35	12 00	0 10	0 35	+1 04
8	"	" (43)	12 00	12 43	0 35	1 18	+1 38
9	"	" (25)	12 43	13 08	1 18	1 43	+2 12
10	HR 5378	" (3,5)	15 01	15 04.5	3 36	3 39.5	+0 42
11	"	" (6)	15 05	15 11	3 40	3 46	+0 47.5

5-1	5	B Fe 10 ³		
"	"			
"	"		$t_{exp.} = 17.3$	$t_{amb.} = 16.6$
"	"			
"	"		$t_{exp.} = 17.0$	$t_{amb.} = 16.3$
"	2			
"	1			
"	2			
"	3			
"	"			
"	4			
"	"		$t_{exp.} = 14.4$	$t_{amb.} = 14.0$
"	5			
"	"			
"	"		$t_{exp.} = 13.4$	$t_{amb.} = 12.9$
"	"			
"	"			
"	"		$t_{exp.} = 12.7$	$t_{amb.} = 12.4$ se umbló

5-1	5	Fe 10 ³		
"	4		$t_{exp.} = 16.5$	$t_{amb.} = 16.0$
"	1		$t_{exp.} = 16.3$	$t_{amb.} = 15.8$ se umbló
"	3			
"	"			

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10-11/I/68

K.

T. S.

T. U.

HX 25034	12	HR 5378	103a-0	(11)	15 11	15 22	3 46	3 57	+0 56
	13	"	"	(6)	15 22	15 28	3 57	4 03	+1 04.5
	14	"	"	(11)	15 28	15 39	4 03	4 14	+1 13

11-12/II/68

K.

3504	1	HR 5378	103a-0	(3,5)	14 05	-14 08.5	2 37	2 40.5	-0 14
	2	"	"	(6)	14 08.5	14 14.5	2 40.5	2 46.5	-0 09
	3	"	"	(11)	14 14.5	14 25.5	2 46.5	2 57.5	-0 00.5
	4	HR 6549	"	(8)	14 47	14 55	3 19	3 27	-2 44
	5	"	"	(14)	14 55	15 09	3 27	3 41	-2 33
	6	"	"	(24)	15 09	15 33	3 41	4 05	-2 14
	7	HR 5358	"	(4)	15 56	16 00	4 28	4 32	+1 40.5
	8	"	"	(8)	16 00	16 08	4 32	4 40	+1 46.5
	9	"	"	(14)	16 08	16 22	4 40	4 54	+1 57.5
	10	HR 5354	"	(1,5)	16 34	16 35.5	5 06	5 07.5	+2 18
	11	"	"	(2,5)	16 35.5	16 38	5 07.5	5 10	+2 20
	12	"	"	(4)	16 38	16 42	5 10	5 14	+2 23

12-13/II/68

K.

3504	13	HR 5378	103a-0	(3,5)	14 21.5	14 25	2 50	2 53.5	+0 02.5
	14	"	"	(6)	14 25	14 31	2 53.5	2 59.5	+0 07.5
3505	21	HR 5378	"	(11)	14 38.5	14 49.5	3 07	3 18	+0 23.5

14-15/II/68

K.

3505	22	HR 3207	103a-0	(0.5)	11 48	11 48.5	0 07	0 07.5	+3 40
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5-1	3	B	
"	4		
"	4		$t_{exp} = 14.1$ $t_{amb} = 13.4$

5-1	3	B $F_2 10^{-1}$	
"	4		
"	4		$t_{exp} = 14.0$ $t_{amb} = 13.4$
"	5		
"	"		
"	"		$t_{exp} = 13.4$ $t_{amb} = 12.8$
"	"		
"	"		
"	"		$t_{exp} = 13.3$ $t_{amb} = 12.9$
"	"		
"	"		
"	"		$t_{exp} = 13.4$ $t_{amb} = 13.0$

5-1	4		
"	"		$t_{exp} = 18.1$ $t_{amb} = 17.4$
"	"	B $F_2 10^{-1}$	$t_{exp} = 18.1$ $t_{amb} = 17.6$

sembra

5-1. 5 - Condiapragma del ancho 19cm (B)

14-15/V/68 K.			T. S.	T. U.	A. P. m.
HX 3505	3 HR 3207	103a-0	(1) 11 48,5	11 49,5	0 07,5 0 08,5 + 3 41
	4 "	"	(1,5) 11 49,5	11 51	0 08,5 0 10 + 3 42
	5 "	"	(2) 11 51	11 53	0 10 0 12 + 3 44
	6 "	"	(5,5) 11 53	11 58,5	0 12 0 17,5 + 3 47,5
	8 HR 4674	"	(3) 12 30	12 33	0 49 0 52 + 0 15,5
	9 "	"	(6) 12 33	12 39	0 52 0 58 + 0 20
	10 "	"	(10) 12 39	12 49	0 58 1 08 + 0 28
	11 HR 5378	"	(3,5) 13 07	13 10,5	1 26 1 29,5 - 1 12
	12 "	"	(6) 13 10,5	13 16,5	1 29,5 1 35,5 - 1 07
	13 "	"	(11) 13 16,5	13 27,5	1 35,5 1 46,5 - 0 58,5
	14 "	"	(6) 13 27,5	13 33,5	1 46,5 1 52,5 - 0 50
3506	1 HR 5339	"	(17) 14 50	15 07	3 09 3 26 + 0 38
	2 "	"	(28) 15 07	15 35	3 26 3 54 + 1 00,5
	3 "	"	(46) 15 35	16 21	3 54 4 40 + 1 37,5

20-21/V/68 K					
3506	4 HR 5378	103a-0	(7) 13 23	13 30	1 19 1 26 - 0 54
	5 "	"	(2) 13 30	13 32	1 26 1 28 - 0 49,5
	6 "	"	(3,5) 17 41	17 44,5	5 37 5 40,5 + 3 22
	7 "	"	(6) 17 45	17 51	5 41 5 47 + 3 27,5
	8 "	"	(11) 17 51	18 02	5 47 5 58 + 3 36
	9 "	"			

7-8/VI/68 K.					
3507	1 HR 5378	103a-0	3,5	14 26	- 14 29,5 1 12 1 15,5 + 0 07

5-1 5. B con la drappeggia del anello de 19 cm (B)

$$t_{exp} = 9.9 \quad t_{amb} = 9.6$$

$t_{exp.} = 9.5$ $t_{amb.} = 9.0$

$$E \approx 10^4$$
$$t_{exp} = 8.1 \quad t_{amb.} = 8.2$$
$$f_{exp.} = 7.6 \quad f_{amb} = 7.6$$

5-1 3 B

4 2-1

4 5

h M

4 . 11

$t_{exp.} = 9.7$ $t_{amb.} = 9.2$

Fe 10¹

5-1. 5 B Fe 10^{-4}

Le mulo

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		7-8/VI/68	K		T. S.	T. U.	A. R. m.
HX 3507	2	HR 5378	103a-0	(6)	14 30	14 36	1 16 1 22 + 0 12.5
	3	"	"	(11)	14 36	14 47	1 22 1 33 + 0 21
	4	HR 5576	"	(0.9)	15 10	15 10.9	1 56 1 56.9 + 0 14
	5	"	"	(1.5)	15 11	15 12.5	1 57 1 58.5 + 0 15
	6	"	"	(3)	15 12	15 16	1 59 2 02 + 0 18
	7	HR 5626	"	(2.6)	15 32.5	15 35.1	2 18 2 20.6 + 0 27.5
	8	"	"	(4)	15 36	15 40	2 21.5 2 25.5 + 0 32
	9	"	"	(8)	15 40	15 48	2 25.5 2 33.5 + 0 38
	10	HR 5683	"	(3)	16 06	16 09	2 51.5 2 54.5 + 0 51.5
	11	"	"	(5)	16 09	16 14	2 54.5 2 59.5 + 0 55.5
	12	"	"	(10)	16 14	16 24	2 59.5 3 09.5 + 1 03
3508	2	1 HR 6262	"	(11)	17 41	17 52	4 26.5 4 27.5 + 0 55.5
	2	"	"	(19)	17 52	18 11	4 37.5 4 56.5 + 1 10.5
	3	"	"	(32)	18 11	18 43	4 56.5 5 28.5 + 1 36
		8-9/VI/68	K.				
3508	2	4 HR 5378	103a-0	(5)	15 09	15 14	1 49 1 54 + 0 51
	5	"	"	(8)	15 14	15 22	1 54 2 02 + 0 57.5
	6	"	"	(15)	15 22	15 37	2 02 2 17 + 1 09
		15-16/VI/68	K.				
3508	2	7 HR 3817	103a-0	(14)	13 12	13 26	23 25 23 39 + 3 46.5
	8	"	"	(20)	13 26	13 46	23 39 23 59 + 4 03.5
	9	"	"	(30)	13 46	14 16	23 59 0 29 + 4 28.5
	10	HR 5378	"	(3.5)	14 35	14 38.5	0 48 0 51.5 + 0 16

5-1	5	B Fe 8 ¹		
"	"	Fe 7 ¹	$t_{exp.} = 9.5$	$t_{amb.} = 8.9$
"	"			
"	"			
"	"		$t_{exp.} = 9.2$	$t_{amb.} = 8.7$
"	"			
"	"			
"	"		$t_{exp.} = 9.0$	$t_{amb.} = 8.4$
"	"			
"	"			
"	"		$t_{exp.} = 8.7$	$t_{amb.} = 8.3$
"	"	Fe 7 ¹		
"	"			
"	"		$t_{exp.} = 8.3$	$t_{amb.} = 7.9$

5-1	2	B		
"	"	Fe 7 ¹		
"	3	Fe 7 ¹	$t_{exp.} = 10.6$	$t_{amb.} = 10.0$

5-1	5	B Fe 7 ¹		
"	"		$t_{exp.} = 9.9$	$t_{amb.} = 9.4$
"	"		$t_{exp.} = 9.6$	$t_{amb.} = 9.2$
"	"			

15-16/VI/68 K.

T. S.

T. U.

A. P. m.

HX 35082	11	HR 5378	103a-0	(6)	14 39	14 45	0 52	0 58	+0 21.5
	12	"	"	(11)	14 45	14 56	0 58	1 09	+0 30
35093	1	HR 5671	"	(0.9)	16 24.5	16 25.4	2 37	2 37.9	+1 10
	2	"	"	(1.5)	16 25.5	16 27	2 38	2 39.5	+1 11
	3	"	"	(3)	16 27	16 30	2 39.5	2 42.5	+1 13.5

17-18/VI/68 K.

35093	4	HR 4199	103a-0	(3.5)	13 21	13 24.5	23 26	23 24.5	+2 41
	5	"	"	(6)	13 24.5	13 30.5	23 29.5	23 35.5	+2 46
	6	"	"	(10)	13 30.5	13 40.5	23 35.5	23 45.5	+2 54
	7	HR 5231	"	(3)	14 00	14 03	0 05	0 08	+0 08.5
	8	"	"	(5)	14 03	14 08	0 08	0 13	+0 12.5
	9	"	"	(8)	14 08	14 16	0 13	0 21	+0 19
	10	HR 5378	"	(3.5)	14 29	14 32.5	0 34	0 37.5	+0 10
	11	"	"	(6)	14 33	14 39	0 38	0 44	+0 15.5
	12	"	"	(11)	14 39	14 50	0 44	0 55	+0 24
	13	HR 5210	"	(5)	15 10	15 15	1 15	1 20	+1 23
	14	"	"	(9)	15 15	15 24	1 20	1 29	+1 30
3510	1	HR 5210	"	(16)	15 35	15 51	1 40	1 56	+1 53.5
	2	HR 5883	"	(3)	16 14	16 17	2 18.5	2 21.5	+0 27
	3	"	"	(4)	16 17	16 21	2 21.5	2 25.5	+0 30.5
	4	"	"	(8)	16 21	16 29	2 25.5	2 33.5	+0 36.5
	5	HR 5987	"	(3)	16 46	16 49	2 50.5	2 53.5	+0 43.5
	6	"	"	(5)	16 49	16 54	2 53.5	2 58.5	+0 47.5
	7	"	"	(9)	16 54	17 03	2 58.5	3 07.5	+0 54.5

5-1	5	B Fe 7 ³		
"	"		+ esp. = 9.3	+ amb. = 8.9
"	4	Fe 7 ⁴		
"	"			
"	3		+ esp. = 8.6	+ amb. = 8.4
				se mulló

5-1	5	B Can diafragma: B		
"	"	Fe 7 ³		
"	"		+ esp. = 11.7	+ amb. = 11.0
"	"			
"	4			
"	"			
"	"			
"	"			
"	"	Fe 7 ⁴		
"	"		+ esp. = 11.1	+ amb. = 10.4
"	"			
"	"			
"	"			
"	"	B Fe 7 ³	+ esp. = 10.4	+ amb. = 9.9
"	"			
"	"			
"	"		+ esp. = 10.0	+ amb. = 9.5
"	"			
"	"			
"	"		+ esp. = 9.7	+ amb. = 9.2

17-18/VI/68 K.

T. S.

T. U.

A. P. m.

HX3510	8	HR 6262	103a-0	(11)	17 24	17 35	3 28.5	3 39.5	+0 38.5
	9	"	"	(19)	17 35	17 54	3 39.5	3 58.5	+0 53.5
	10	"	"	(32)	17 54	18 26	3 58.5	4 30.5	+1 19
	11	HR 6973	"	(11)	18 56	19 07	5 00.5	5 11.5	+0 28.5
	12	"	"	(18)	19 07	19 25	5 11.5	5 29.5	+0 43
	13	"	"	(30)	19 25	19 55	5 29.5	5 59.5	+1 07

19-20/VI/68 K.

3511	21	HR 5378	103A-0	(3,5)	14 42	14 45.5	0 40	0 43.5	+0 23
	2	"	"	(6)	14 46	14 52	0 44	0 50	+0 28.5
	3	"	"	(11)	14 52	15 03	0 50	1 01	+0 37

20-21/VI/68 K.

3511	24	HD 96248	103a-0	(90)	13 40.5	15 10.5	23 35	1 05	+3 23
	5	HR 5378	"	(3,5)	15 30	15 33.5	1 24	1 27.5	+1 11
	6	"	"	(6)	15 34	15 40	1 28	1 34	+1 16.5
	7	"	"	(11)	15 40	15 51	1 34	1 45	+1 25
	8	HR 5528	"	(3)	16 06	16 09	2 00	2 03	+1 18.5
	9	"	"	(6)	16 09	16 15	2 03	2 09	+1 23
	10	"	"	(10)	16 15	16 25	2 09	2 19	+1 31
	11	HR 6262	"	(11)	16 51	17 02	2 45	2 56	+0 05.5
	12	"	"	(19)	17 02	17 21	2 56	3 15	+0 20.5
	13	"	"	(32)	17 21	17 53	3 15	3 47	+0 46

5-1 5 B
 " " $t_{exp.} = 9.0$ $t_{amb.} = 8.6$

" "
 " "
 " "
 " " $t_{exp.} = 8.0$ $t_{amb.} = 7.9$

5-1 5 B
 " " Fe 7¹ $t_{exp.} = 10.0$
 " " $t_{exp.} = 10.0$ $t_{amb.} = 9.3$

Se mella

5-1 5 B Fe 7¹ $t_{exp.} = 13.7$ $t_{amb.} = 12.6$

" "
 " " Fe 7¹
 " " $t_{exp.} = 13.2$ $t_{amb.} = 12.4$

" "
 " "
 " "
 " " $t_{exp.} = 13.1$ $t_{amb.} = 12.1$

" "
 " "
 " "
 " " $t_{exp.} = 12.0$ $t_{amb.} = 11.1$

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22-23/VI/68 K.

T.S.

T.U.

A.P.m.

HV35121	HR 5210	103a-0	(35)	14 45	15 20	0 31.5	-1 06.5	+1 14
HV35132	HR 5378	"	(24)	16 18	16 42	2 04.5	2 28.5	+2 10.5

25-26/VII/68 K.

HV35141	HR 5378	103a-0	(24)	15 21	15 45	0 55	1 19	+1 12.5
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17-18/VIII/68 K.

HX35151	HR 5812	103a-0	(1.5)	16 19	16 20.5	0 27	0 28.5	+0 43.5
2	"	"	(3)	16 21	16 24	0 29	0 32	+0 46.5
3	"	"	(5)	16 24	16 29	0 32	0 37	+0 50.5
4	HR 6070	"	(7)	16 54	17 01	1 02	1 09	+0 41.5
5	"	"	(12)	17 01	17 13	1 09	1 21	+0 51
6	"	"	(21)	17 13	17 34	1 21	1 42	+1 07.5
7	HR 6492	"	(6)	17 49	17 55	1 57	2 03	+0 27
8	"	"	(11)	17 55	18 06	2 03	2 14	+0 35.5
9	"	"	(18)	18 06	18 24	2 14	2 32	+0 50
10	HR 6561	"	(2)	18 34	18 36	2 41.5	2 43.5	+0 59.5
11	"	"	(4)	18 36	18 40	2 43.5	2 47.5	+1 02.5
12	"	"	(7)	18 40	18 47	2 47.5	2 54.5	+1 08
13	HR 7039	"	(1.1)	18 58	18 59	3 05.5	3 06.6	+0 15.5
14	"	"	(1.5)	19 00	19 01.5	3 07.5	3 09	+0 17.5

20-21/VII/68 K.

HX35161	HR 5680	103a-0	10	16 05	16 15	0 01	0 11	+0 54.5
2	"	"	18	16 15	16 33	0 11	0 29	+1 08.5

					$t_{exp.}$	$t_{amb.}$
21-5	5	$C Fe 2^+$	$C. IV. e.$		11.7-11.5	10.3-10.2
"	"	"	"	"	11.4-11.2	10.1-10.1

21-5	4	$C Fe 5^+$	$C. IV. e.$			$t_{amb.} = 6.0$
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5-1	5	$B Fe 4^+$	$C. 2. f. e.$			
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					$t_{exp.} = 11.4$	$t_{amb.} = 10.3$
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					$t_{exp.} = 11.0$	$t_{amb.} = 9.9$
--	--	--	--	--	-------------------	------------------

					$t_{exp.} = 10.6$	$t_{amb.} = 9.6$
--	--	--	--	--	-------------------	------------------

					$t_{exp.} = 10.3$	$t_{amb.} = 9.2$
--	--	--	--	--	-------------------	------------------

					$t_{exp.} = 10.2$	$t_{amb.} = 9.2$
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se nullo

5-1	5	$B Fe 8^+$				
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20-21/VII/68 K.

T. S.

T. V.

A. h. m.

HX 35162 3 HR 5680 103a-0 30 16 33 17 03 0 29 0 59 +1 32.5

25-26/VII/68 K.

3516	2	4	HR 5695	103a-0	1	16 12	16 13	23 49	23 50	+0 54
	5		"	"	1.6	16 13	16 14.6	23 50	23 51.6	+0 55
	6		"	"	2.8	16 15	16 17.8	23 52	23 54.8	+0 57.5
	7		HR 6134	"	0.9	16 39	16 39.9	0 16	0 16.9	+0 12.5
	8		"	"	1.5	16 40	16 41.5	0 17	0 18.5	+0 14
	9		"	"	2.5	16 42	16 44.5	0 19	0 21.5	+0 16
	10		HR 6143	"	3	16 58	17 01	0 35	0 38	+0 31
	11		"	"	5	17 01	17 06	0 38	0 43	+0 35
	12		"	"	10	17 06	17 16	0 43	0 53	+0 42.5
	13		HR 6461	"	4	17 27	17 31	1 04	1 08	+0 07
	14		"	"	7	17 31	17 38	1 08	1 15	+0 12.5
3517	3	1	HR 6461	"	12	18 25	18 37	2 02	2 14	+1 09
	2		HR 6508	"	3.6	18 55	18 58.6	2 32	2 35.6	+1 28.5
	3		"	"	6	18 59	19 05	2 36	2 42	+1 34
	4		"	"	10	19 05	19 15	2 42	2 52	+1 42
	5		HR 6553	"	3	19 25	19 28	3 02	3 05	+1 52
	6		"	"	4.8	19 28	19 32.8	3 05	3 09.8	+1 56
	7		"	"	7.8	19 33	19 40.8	3 10	3 17.8	+2 02.5
	8		HR 6580	"	2.4	19 51	19 53.4	3 28	3 30.4	+2 12.5
	9		"	"	4.2	19 54	19 58.2	3 31	3 35.2	+2 16.5
	10		"	"	7.2	19 59	20 06.2	3 36	3 43.2	+2 23
	11		HR 6812	"	3	20 26	20 29	4 03	4 06	+2 16

5-1 5 B

Se mple

5-1 5 A

" "

" " $t_{exp.} = 13.7$ $t_{amb.} = 12.9$

" " " " " " " "

" " " " " " " "

" " " " " " " "

" " " " " " " "

" " " " " " " "

" " " " " " $t_{exp.} = 13.5$ $t_{amb.} = 12.6$

" " " " " " " "

" " " " " " $t_{exp.} = 13.3$ $t_{amb.} = 12.6$ " " " " 3 Fe 8⁴ $t_{exp.} = 13.3$ $t_{amb.} = 12.7$

" " " " Con Dif. B

" " " " " "

" " " " $t_{exp.} = 13.3$ $t_{amb.} = 12.7$

" " " " " "

" " " " " "

" " " " $t_{exp.} = 13.2$ $t_{amb.} = 12.6$

" " " " " "

" " " " " "

" " " " $t_{exp.} = 13.1$ $t_{amb.} = 12.5$

" " " " " "

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25-26/VII/68 K.

T. S.

T. U.

A. R. m.

HX 3517	12	HR 6812	103 a-0	16	20 29	20 45	4 06	4 22	+2	25.5
	13	"	"	10	20 45	20 55	4 22	4 32	+2	38.5
	14	"	"	8	20 55	21 03	4 32	4 40	+2	47.5

26-27/VII/68 K.

3518	1	HR 6102	103 a-0	8	16 39	16 47	0 11.5	0 19.5	+0	16
	2	"	"	14	16 47	17 01	0 19.5	0 32.5	+0	27
	3	"	"	21	17 01	17 22	0 33.5	0 54.5	+0	44
	4	HR 6141	"	7	17 39	17 46	1 11.5	1 18.5	+1	14.5
	5	"	"	11	17 46	17 57	1 18.5	1 29.5	+1	23.5
	6	"	"	18	17 57	18 15	1 29.5	1 47.5	+1	38
	7	HR 6822	"	15	18 37	18 52	2 09.5	2 24.5	+0	31.5
	8	"	"	25	18 52	19 17	2 24.5	2 49.5	+0	51.5
	10	"	"	43	19 17	20 00	2 49.5	3 32.5	+1	25.5
	11	HR 7348	"	2.5	20 23	20 25.5	3 55	3 57.5	+1	03.
	12	"	"	4	20 26	20 30	3 58	4 02	+1	07
	13	"	"	7.5	20 30	20 37.5	4 02	4 09.5	+1	12.5

27-28/VII/68 K.

3519	21	HR 6252	103 a-0	1.4	17 42	17 43.4	1 09.5	1 10.4	+0	53
	2	"	"	2.5	17 44	17 46.5	1 11.5	1 14	+0	55.5
	3	"	"	4	17 47	17 51	1 14.5	1 18.5	+0	59.5
	4	HR 6615	"	1.6	18 21	18 22.6	1 48.5	1 50.1	+0	37
	5	"	"	3	18 23	18 26	1 50.5	1 53.5	+0	39.5
	6	"	"	5	18 26	18 31	1 53.5	1 58.5	+0	43.5

145

5-1	2.01.2	2.02.2	B	2.03.2	2.04.2	2.05.2	2.06.2	2.07.2	2.08.2	2.09.2	2.10.2	2.11.2	2.12.2	2.13.2	2.14.2	2.15.2	2.16.2	2.17.2	2.18.2	2.19.2	2.20.2	2.21.2	2.22.2	2.23.2	2.24.2	2.25.2	2.26.2	2.27.2	2.28.2	2.29.2	2.30.2	2.31.2	2.32.2	2.33.2	2.34.2	2.35.2	2.36.2	2.37.2	2.38.2	2.39.2	2.40.2	2.41.2	2.42.2	2.43.2	2.44.2	2.45.2	2.46.2	2.47.2	2.48.2	2.49.2	2.50.2	2.51.2	2.52.2	2.53.2	2.54.2	2.55.2	2.56.2	2.57.2	2.58.2	2.59.2	2.60.2	2.61.2	2.62.2	2.63.2	2.64.2	2.65.2	2.66.2	2.67.2	2.68.2	2.69.2	2.70.2	2.71.2	2.72.2	2.73.2	2.74.2	2.75.2	2.76.2	2.77.2	2.78.2	2.79.2	2.80.2	2.81.2	2.82.2	2.83.2	2.84.2	2.85.2	2.86.2	2.87.2	2.88.2	2.89.2	2.90.2	2.91.2	2.92.2	2.93.2	2.94.2	2.95.2	2.96.2	2.97.2	2.98.2	2.99.2	3.00.2	3.01.2	3.02.2	3.03.2	3.04.2	3.05.2	3.06.2	3.07.2	3.08.2	3.09.2	3.10.2	3.11.2	3.12.2	3.13.2	3.14.2	3.15.2	3.16.2	3.17.2	3.18.2	3.19.2	3.20.2	3.21.2	3.22.2	3.23.2	3.24.2	3.25.2	3.26.2	3.27.2	3.28.2	3.29.2	3.30.2	3.31.2	3.32.2	3.33.2	3.34.2	3.35.2	3.36.2	3.37.2	3.38.2	3.39.2	3.40.2	3.41.2	3.42.2	3.43.2	3.44.2	3.45.2	3.46.2	3.47.2	3.48.2	3.49.2	3.50.2	3.51.2	3.52.2	3.53.2	3.54.2	3.55.2	3.56.2	3.57.2	3.58.2	3.59.2	3.60.2	3.61.2	3.62.2	3.63.2	3.64.2	3.65.2	3.66.2	3.67.2	3.68.2	3.69.2	3.70.2	3.71.2	3.72.2	3.73.2	3.74.2	3.75.2	3.76.2	3.77.2	3.78.2	3.79.2	3.80.2	3.81.2	3.82.2	3.83.2	3.84.2	3.85.2	3.86.2	3.87.2	3.88.2	3.89.2	3.90.2	3.91.2	3.92.2	3.93.2	3.94.2	3.95.2	3.96.2	3.97.2	3.98.2	3.99.2	4.00.2	4.01.2	4.02.2	4.03.2	4.04.2	4.05.2	4.06.2	4.07.2	4.08.2	4.09.2	4.10.2	4.11.2	4.12.2	4.13.2	4.14.2	4.15.2	4.16.2	4.17.2	4.18.2	4.19.2	4.20.2	4.21.2	4.22.2	4.23.2	4.24.2	4.25.2	4.26.2	4.27.2	4.28.2	4.29.2	4.30.2	4.31.2	4.32.2	4.33.2	4.34.2	4.35.2	4.36.2	4.37.2	4.38.2	4.39.2	4.40.2	4.41.2	4.42.2	4.43.2	4.44.2	4.45.2	4.46.2	4.47.2	4.48.2	4.49.2	4.50.2	4.51.2	4.52.2	4.53.2	4.54.2	4.55.2	4.56.2	4.57.2	4.58.2	4.59.2	4.60.2	4.61.2	4.62.2	4.63.2	4.64.2	4.65.2	4.66.2	4.67.2	4.68.2	4.69.2	4.70.2	4.71.2	4.72.2	4.73.2	4.74.2	4.75.2	4.76.2	4.77.2	4.78.2	4.79.2	4.80.2	4.81.2	4.82.2	4.83.2	4.84.2	4.85.2	4.86.2	4.87.2	4.88.2	4.89.2	4.90.2	4.91.2	4.92.2	4.93.2	4.94.2	4.95.2	4.96.2	4.97.2	4.98.2	4.99.2	5.00.2	5.01.2	5.02.2	5.03.2	5.04.2	5.05.2	5.06.2	5.07.2	5.08.2	5.09.2	5.10.2	5.11.2	5.12.2	5.13.2	5.14.2	5.15.2	5.16.2	5.17.2	5.18.2	5.19.2	5.20.2	5.21.2	5.22.2	5.23.2	5.24.2	5.25.2	5.26.2	5.27.2	5.28.2	5.29.2	5.30.2	5.31.2	5.32.2	5.33.2	5.34.2	5.35.2	5.36.2	5.37.2	5.38.2	5.39.2	5.40.2	5.41.2	5.42.2	5.43.2	5.44.2	5.45.2	5.46.2	5.47.2	5.48.2	5.49.2	5.50.2	5.51.2	5.52.2	5.53.2	5.54.2	5.55.2	5.56.2	5.57.2	5.58.2	5.59.2	5.60.2	5.61.2	5.62.2	5.63.2	5.64.2	5.65.2	5.66.2	5.67.2	5.68.2	5.69.2	5.70.2	5.71.2	5.72.2	5.73.2	5.74.2	5.75.2	5.76.2	5.77.2	5.78.2	5.79.2	5.80.2	5.81.2	5.82.2	5.83.2	5.84.2	5.85.2	5.86.2	5.87.2	5.88.2	5.89.2	5.90.2	5.91.2	5.92.2	5.93.2	5.94.2	5.95.2	5.96.2	5.97.2	5.98.2	5.99.2	6.00.2	6.01.2	6.02.2	6.03.2	6.04.2	6.05.2	6.06.2	6.07.2	6.08.2	6.09.2	6.10.2	6.11.2	6.12.2	6.13.2	6.14.2	6.15.2	6.16.2	6.17.2	6.18.2	6.19.2	6.20.2	6.21.2	6.22.2	6.23.2	6.24.2	6.25.2	6.26.2	6.27.2	6.28.2	6.29.2	6.30.2	6.31.2	6.32.2	6.33.2	6.34.2	6.35.2	6.36.2	6.37.2	6.38.2	6.39.2	6.40.2	6.41.2	6.42.2	6.43.2	6.44.2	6.45.2	6.46.2	6.47.2	6.48.2	6.49.2	6.50.2	6.51.2	6.52.2	6.53.2	6.54.2	6.55.2	6.56.2	6.57.2	6.58.2	6.59.2	6.60.2	6.61.2	6.62.2	6.63.2	6.64.2	6.65.2	6.66.2	6.67.2	6.68.2	6.69.2	6.70.2	6.71.2	6.72.2	6.73.2	6.74.2	6.75.2	6.76.2	6.77.2	6.78.2	6.79.2	6.80.2	6.81.2	6.82.2	6.83.2	6.84.2	6.85.2	6.86.2	6.87.2	6.88.2	6.89.2	6.90.2	6.91.2	6.92.2	6.93.2	6.94.2	6.95.2	6.96.2	6.97.2	6.98.2	6.99.2	7.00.2	7.01.2	7.02.2	7.03.2	7.04.2	7.05.2	7.06.2	7.07.2	7.08.2	7.09.2	7.10.2	7.11.2	7.12.2	7.13.2	7.14.2	7.15.2	7.16.2	7.17.2	7.18.2	7.19.2	7.20.2	7.21.2	7.22.2	7.23.2	7.24.2	7.25.2	7.26.2	7.27.2	7.28.2	7.29.2	7.30.2	7.31.2	7.32.2	7.33.2	7.34.2	7.35.2	7.36.2	7.37.2	7.38.2	7.39.2	7.40.2	7.41.2	7.42.2	7.43.2	7.44.2	7.45.2	7.46.2	7.47.2	7.48.2	7.49.2	7.50.2	7.51.2	7.52.2	7.53.2	7.54.2	7.55.2	7.56.2	7.57.2	7.58.2	7.59.2	7.60.2	7.61.2	7.62.2	7.63.2	7.64.2	7.65.2	7.66.2	7.67.2	7.68.2	7.69.2	7.70.2	7.71.2	7.72.2	7.73.2	7.74.2	7.75.2	7.76.2	7.77.2	7.78.2	7.79.2	7.80.2	7.81.2	7.82.2	7.83.2	7.84.2	7.85.2	7.86.2	7.87.2	7.88.2	7.89.2	7.90.2	7.91.2	7.92.2	7.93.2	7.94.2	7.95.2	7.96.2	7.97.2	7.98.2	7.99.2	8.00.2	8.01.2	8.02.2	8.03.2	8.04.2	8.05.2	8.06.2	8.07.2	8.08.2	8.09.2	8.10.2	8.11.2	8.12.2	8.13.2	8.14.2	8.15.2	8.16.2	8.17.2	8.18.2	8.19.2	8.20.2	8.21.2	8.22.2	8.23.2	8.24.2	8.25.2	8.26.2	8.27.2	8.28.2	8.29.2	8.30.2	8.31.2	8.32.2	8.33.2	8.34.2	8.35.2	8.36.2	8.37.2	8.38.2	8.39.2	8.40.2	8.41.2	8.42.2	8.43.2	8.44.2	8.45.2	8.46.2	8.47.2	8.48.2	8.49.2	8.50.2	8.51.2	8.52.2	8.53.2	8.54.2	8.55.2	8.56.2	8.57.2	8.58.2	8.59.2	8.60.2	8.61.2	8.62.2	8.63.2	8.64.2	8.65.2	8.66.2	8.67.2	8.68.2	8.69.2	8.70.2	8.71.2	8.72.2	8.73.2	8.74.2	8.75.2	8.76.2	8.77.2	8.78.2	8.79.2	8.80.2	8.81.2	8.82.2	8.83.2	8.84.2	8.85.2	8.86.2	8.87.2	8.88.2	8.89.2	8.90.2	8.91.2	8.92.2	8.93.2	8.94.2	8.95.2	8.96.2	8.97.2	8.98.2	8.99.2	9.00.2	9.01.2	9.02.2	9.03.2	9.04.2	9.05.2	9.06.2	9.07.2	9.08.2	9.09.2	9.10.2	9.11.2	9.12.2	9.13.2	9.14.2	9.15.2	9.16.2	9.17.2	9.18.2	9.19.2	9.20.2	9.21.2	9.22.2	9.23.2	9.24.2	9.25.2	9.26.2	9.27.2	9.28.2	9.29.2	9.30.2	9.31.2	9.32.2	9.33.2	9.34.2	9.35.2	9.36.2	9.37.2	9.38.2	9.39.2	9.40.2	9.41.2	9.42.2	9.43.2	9.44.2	9.45.2	9.46.2	9.47.2	9.48.2	9.49.2	9.50.2	9.51.2	9.52.2	9.53.2	9.54.2	9.55.2	9.56.2	9.57.2	9.58.2	9.59.2	9.60.2	9.61.2	9.62.2	9.63.2	9.64.2	9.65.2	9.66.2	9.67.2	9.68.2	9.69.2	9.70.2	9.71.2	9.72.2	9.73.2	9.74.2	9.75.2	9.76.2	9.77.2	9.78.2	9.79.2	9.80.2	9.81.2	9.82.2	9.83.2	9.84.2	9.85.2	9.86.2	9.87.2	9.88.2	9.89.2	9.90.2	9.91.2	9.92.2	9.93.2	9.94.2	9.95.2	9.96.2	9.97.2	9.98.2	9.99.2	10.00.2	10.01.2	10.02.2	10.03.2	10.04.2	10.05.2	10.06.2	10.07.2	10.08.2	10.09.2	10.10.2	10.11.2	10.12.2	10.13.2	10.14.2	10.15.2	10.16.2	10.17.2	10.18.2	10.19.2	10.20.2	10.21.2	10.22.2	10.23.2	10.24.2	10.25.2	10.26.2	10.27.2	10.28.2	10.29.2	10.30.2	10.31.2	10.32.2	10.33.2	10.34.2	10.35.2	10.36.2	10.37.2	10.38.2	10.39.2	10.40.2	10.41.2	10.42.2	10.43.2	10.44.2	10.45.2	10.46.2	10.47.2	10.48.2	10.49.2	10.50.2	10.51.2	10.52.2	10.53.2	10.54.2	10.55.2	10.56.2	10.57.2	10.58.2	10.59.2	10.60.2	10.61.2	10.62.2	10.63.2	10.64.2	10.65.2	10.66.2	10.67.2	10.68.2	10.69.2	10.70.2	10.71.2	10.72.2	10.73.2	10.74.2	10.75.2	10.76.2	10.77.2	10.78.2	10.79.2	10.80.2	10.81.2	10.82.2	10.83.2	10.84.2	10.85.2	10.86.2	10.87.2	10.88.2	10.89.2	10.90.2	10.91.2	10.92.2	10.93.2	10.94.2	10.95.2	10.96.2	10.97.2	10.98.2	10.99.2	11.00.2	11.01.2	11.02.2	11.03.2	11.04.2	11.05.2	11.06.2	11.07.2	11.08.2	11.09.2	11.10.2	11.11.2	11.12.2	11.13.2	11.14.2	11.15.2	11.16.2	11.17.2	11.18.2	11.19.2	11.20.2	11.21.2	11.22.2	11.23.2	11.24.2	11.25.2	11.26.2	11.27.2	11.28.2	11.29.2	11.30.2	11.31.2	11.32.2	11.33.2	11.34.2	11.35.2	11.36.2	11.37.2	11.38.2	11.39.2	11.40.2	11.41.2	11.42.2	11.43.2	11.44.2	11.45.2	11.46.2	11.47.2	11.48.2	11.49.2	11.50.2	11.51.2	11.52.2	11.53.2	11.54.2	11.55.2	11.56.2	11.57.2	11.58.2	11.59.2	11.60.2	11.61.2	11.62.2	11.63.2	11.64.2	11.65.2	11.66.2	11.67.2	11.68.2	11.69.2	11.70.2	11.71.2	11.72.2	11.73.2	11.74.2	11.75.2	11.76.2	11.77.2	11.78.2	11.79.2	11.80.2	11.81.2	11.82.2	11.83.2	11.84.2	11.85.2	11.86.2	11.87.2	11.88.2	11.89.2	11.90.2	11.91.2	11.92.2	11.93.2	11.94.2	11.95.2	11.96.2	11.97.2	11.98.2	11.99.2	12.00.2	12.01.2	12.02.2	12.03.2	12.04.2	12.05.2	12.06.2	12.07.2	12.08.2	12.09.2	12.10.2	12.11.2	12.12.2	12.13.2	12.14.2	12.15.2	12.16.2	12.17.2	12.18.2	12.19.2	12.20.2	12.21.2	12.22.2	12.23.2	12.24.2	12.25.2	12.26.2	12.27.2	12.28.2	12.29.2	12.30.2	12.31.2	12.32.2	12.33.2	12.34.2	12.35.2	12.36.2	12.37.2	12.38.2	12.39.2	12.40.2	12.41.2	12.42.2	12.43.2	12.44.2	12.45.2	12.46.2	12.47.2	12.48.2	12.49.2	12.50.2	12.51.2	12.52.2	12.53.2	12.54.2	12.55.2	12.56.2	12.57.2	12.58.2	12.59.2	12.60.2	12.61.2	12.62.2	12.63.2	12.64.2	12.65.2	12.66.2	12.67.2	12.68.2	12.69.2	12.70.2	12.71.2	12.72.2	12.73.2	12.74.2	12.75.2	12.76.2	12.77.2	12.78.2	12.79.2	12.80.2	12.81.2	12.82.2	12.83.2	12.84.2	12.85.2	12.86.2	12.87.2	12.88.2	12.89.2	12.90.2	12.91.2	12.92.2	1
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27-28/VII/68 K.

T. S.

T. U.

A. P. m.

HX 35192	7	HR 6743	103A-0	2	18 41	18 43	2 08.5	2 10.5	+0 38.5
	8	"	"	3	18 43	18 46	2 10.5	2 13.5	+0 41
	9	"	"	5.5	18 46	18 51.5	2 13.5	2 19	+0 45
	10	HR 6832	"	6	19 15	19 21	2 42.5	2 48.5	+1 03
	11	"	"	11	19 21	19 32	2 48.5	2 59.5	+1 11.5
	12	"	"	18	19 32	19 50	2 59.5	3 17.5	+1 26

28-29/VII/68 J.

3520		HR 5193	103A-0	1	16 17	16 18	23 42	23 43	+2 30.5
		"	"	3	16 18	16 21	23 43	23 46	+2 32.5
		"	"	5	16 21	16 26	23 46	23 51	+2 36.5
		"	"	1	16 26	16 27	23 51	23 52	+2 39.5

28-29/VII/68 K.

35192	13	HR 5469	103A-0	2.4	16 42	16 44.4	0 07	0 09.4	+2 04
	14	"	"	3.6	16 44.4	16 48	0 09.4	0 13	+2 07
3521	3	HR 5469	"	6.6	17 08	17 14.6	0 38	0 39.6	+2 32
	2	HR 5395	"	5	17 33	17 38	0 58	1 03	+3 12
	3	"	"	8	17 38	17 46	1 03	1 11	+3 18.5
	4	"	"	14	17 46	18 00	1 14	1 25	+3 29.5
	5	HR 6262	"	11	18 18	18 29	1 43	1 54	+1 32.5
	6	"	"	19	18 29	18 48	1 54	2 13	+1 47.5
	7	"	"	32	18 48	19 20	2 13	2 45	+2 13
	8	HR 6165	"	1.1	19 29	19 30.1	2 54	2 55.1	+2 56
	9	"	"	2	19 31	19 33	2 56	2 58	+2 59

28-29/VII/68 K.

T. S.

T. U.

A. P. m.

HX 35213	10	HR 6165	103a-0	3	19 33	19 36	2 58	3 01	+3 01.5
	11	HR 6084	"	1	19 45	19 46	3 09.5	3 10.5	+3 27
	12	"	"	1.5	19 46	19 47.5	3 10.5	3 12	+3 28
	13	"	"	2	19 48	19 50	3 12.5	3 14.5	+3 30.5
	14	"	"	3	19 50	19 53	3 14.5	3 17.5	+3 33

29-30/VII/68 J., Feb.

3522

HR 4899	103a-0	20	14 34	14 54	21 55	22 15	+1 52
HR 4898	"	2	14 54.5	14 56.5	22 15.5	22 17.5	+2 03.5
"	"	4	14 59	15 03	22 20	22 24	+2 09
"	"	7	15 03	15 10	22 24	22 31	+2 14.5
HR 4897	"	6	15 15	15 21	22 36	22 42	+2 25.5
"	"	9	15 21	15 30	22 42	22 51	+2 33
"	"	12	15 30	15 42	22 51	23 03	+2 43.5
HR 5440	"	1	15 50	15 51	23 11	23 12	+1 17.5
"	"	2	15 51.5	15 53.5	23 12.5	23 14.5	+1 19.5
"	"	3	15 54	15 57	23 15	23 18	+1 22.5
HR 6243	"	20	16 08	16 28	23 29	23 49	-0 29.5

29-30/VII/68 K.

3523

41	HR 6056	103a-0	4	17 19	17 23	0 40	0 44	+1 09
2	"	"	7	17 23	17 30	0 44	0 51	+1 14.5
3	"	"	12	17 30	17 42	0 51	1 03	+1 24
4	HR 6378	"	3.6	17 58	18 01.6	1 19	1 22.6	+0 52
5	"	"	6	18 02	18 08	1 23	1 29	+0 57
6	"	"	9.6	18 08	18 17.6	1 29	1 38.6	+1 05

54.1 ± 5.88 B $\pm_{\text{avg}} = 16.2$ $f_{\text{amb}} = 15.3$

1904 11 22 182 1904 11 22 182

2014 11 23 2014 11 23

2.32	9 + 4	2008-2009	10/10/08	10/10/08	10/10/08
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$t_{exp.} = 16.2$ $t_{amb.} = 15.3$

[illegible]

2.60	17	2.80 V	2.10 V	3092	11905	V		2MMH SH	21
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5-1 5.91 V 0.3 A 23.78 20.02 5 0 0 0

[illegible][illegible]

4	h		ms 5 8.1115-03
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0.001 - 0.002 10.12.1932 14.11.33 13.12.34

0.4 0.5 0.6 0.7 0.8 0.9 1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0 2.1 2.2 2.3 2.4 2.5 2.6 2.7 2.8 2.9 3.0 3.1 3.2 3.3 3.4 3.5 3.6 3.7 3.8 3.9 4.0 4.1 4.2 4.3 4.4 4.5 4.6 4.7 4.8 4.9 5.0 5.1 5.2 5.3 5.4 5.5 5.6 5.7 5.8 5.9 6.0 6.1 6.2 6.3 6.4 6.5 6.6 6.7 6.8 6.9 7.0 7.1 7.2 7.3 7.4 7.5 7.6 7.7 7.8 7.9 8.0 8.1 8.2 8.3 8.4 8.5 8.6 8.7 8.8 8.9 9.0 9.1 9.2 9.3 9.4 9.5 9.6 9.7 9.8 9.9 10.0 10.1 10.2 10.3 10.4 10.5 10.6 10.7 10.8 10.9 11.0 11.1 11.2 11.3 11.4 11.5 11.6 11.7 11.8 11.9 12.0 12.1 12.2 12.3 12.4 12.5 12.6 12.7 12.8 12.9 13.0 13.1 13.2 13.3 13.4 13.5 13.6 13.7 13.8 13.9 14.0 14.1 14.2 14.3 14.4 14.5 14.6 14.7 14.8 14.9 15.0 15.1 15.2 15.3 15.4 15.5 15.6 15.7 15.8 15.9 16.0 16.1 16.2 16.3 16.4 16.5 16.6 16.7 16.8 16.9 17.0 17.1 17.2 17.3 17.4 17.5 17.6 17.7 17.8 17.9 18.0 18.1 18.2 18.3 18.4 18.5 18.6 18.7 18.8 18.9 19.0 19.1 19.2 19.3 19.4 19.5 19.6 19.7 19.8 19.9 20.0 20.1 20.2 20.3 20.4 20.5 20.6 20.7 20.8 20.9 21.0 21.1 21.2 21.3 21.4 21.5 21.6 21.7 21.8 21.9 22.0 22.1 22.2 22.3 22.4 22.5 22.6 22.7 22.8 22.9 23.0 23.1 23.2 23.3 23.4 23.5 23.6 23.7 23.8 23.9 24.0 24.1 24.2 24.3 24.4 24.5 24.6 24.7 24.8 24.9 25.0 25.1 25.2 25.3 25.4 25.5 25.6 25.7 25.8 25.9 26.0 26.1 26.2 26.3 26.4 26.5 26.6 26.7 26.8 26.9 27.0 27.1 27.2 27.3 27.4 27.5 27.6 27.7 27.8 27.9 28.0 28.1 28.2 28.3 28.4 28.5 28.6 28.7 28.8 28.9 29.0 29.1 29.2 29.3 29.4 29.5 29.6 29.7 29.8 29.9 30.0 30.1 30.2 30.3 30.4 30.5 30.6 30.7 30.8 30.9 31.0 31.1 31.2 31.3 31.4 31.5 31.6 31.7 31.8 31.9 32.0 32.1 32.2 32.3 32.4 32.5 32.6 32.7 32.8 32.9 33.0 33.1 33.2 33.3 33.4 33.5 33.6 33.7 33.8 33.9 34.0 34.1 34.2 34.3 34.4 34.5 34.6 34.7 34.8 34.9 35.0 35.1 35.2 35.3 35.4 35.5 35.6 35.7 35.8 35.9 36.0 36.1 36.2 36.3 36.4 36.5 36.6 36.7 36.8 36.9 37.0 37.1 37.2 37.3 37.4 37.5 37.6 37.7 37.8 37.9 38.0 38.1 38.2 38.3 38.4 38.5 38.6 38.7 38.8 38.9 39.0 39.1 39.2 39.3 39.4 39.5 39.6 39.7 39.8 39.9 40.0 40.1 40.2 40.3 40.4 40.5 40.6 40.7 40.8 40.9 41.0 41.1 41.2 41.3 41.4 41.5 41.6 41.7 41.8 41.9 42.0 42.1 42.2 42.3 42.4 42.5 42.6 42.7 42.8 42.9 43.0 43.1 43.2 43.3 43.4 43.5 43.6 43.7 43.8 43.9 44.0 44.1 44.2 44.3 44.4 44.5 44.6 44.7 44.8 44.9 45.0 45.1 45.2 45.3 45.4 45.5 45.6 45.7 45.8 45.9 46.0 46.1 46.2 46.3 46.4 46.5 46.6 46.7 46.8 46.9 47.0 47.1 47.2 47.3 47.4 47.5 47.6 47.7 47.8 47.9 48.0 48.1 48.2 48.3 48.4 48.5 48.6 48.7 48.8 48.9 49.0 49.1 49.2 49.3 49.4 49.5 49.6 49.7 49.8 49.9 50.0 50.1 50.2 50.3 50.4 50.5 50.6 50.7 50.8 50.9 51.0 51.1 51.2 51.3 51.4 51.5 51.6 51.7 51.8 51.9 52.0 52.1 52.2 52.3 52.4 52.5 52.6 52.7 52.8 52.9 53.0 53.1 53.2 53.3 53.4 53.5 53.6 53.7 53.8 53.9 54.0 54.1 54.2 54.3 54.4 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3 55.4 55.5 55.6 55.7 55.8 55.9 56.0 56.1 56.2 56.3 56.4 56.5 56.6 56.7 56.8 56.9 57.0 57.1 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0 58.1 58.2 58.3 58.4 58.5 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.4 59.5 59.6 59.7 59.8 59.9 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.7 60.8 60.9 61.0 61.1 61.2 61.3 61.4 61.5 61.6 61.7 61.8 61.9 62.0 62.1 62.2 62.3 62.4 62.5 62.6 62.7 62.8 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.6 63.7 63.8 63.9 64.0 64.1 64.2 64.3 64.4 64.5 64.6 64.7 64.8 64.9 65.0 65.1 65.2 65.3 65.4 65.5 65.6 65.7 65.8 65.9 66.0 66.1 66.2 66.3 66.4 66.5 66.6 66.7 66.8 66.9 67.0 67.1 67.2 67.3 67.4 67.5 67.6 67.7 67.8 67.9 68.0 68.1 68.2 68.3 68.4 68.5 68.6 68.7 68.8 68.9 69.0 69.1 69.2 69.3 69.4 69.5 69.6 69.7 69.8 69.9 70.0 70.1 70.2 70.3 70.4 70.5 70.6 70.7 70.8 70.9 71.0 71.1 71.2 71.3 71.4 71.5 71.6 71.7 71.8 71.9 72.0 72.1 72.2 72.3 72.4 72.5 72.6 72.7 72.8 72.9 73.0 73.1 73.2 73.3 73.4 73.5 73.6 73.7 73.8 73.9 74.0 74.1 74.2 74.3 74.4 74.5 74.6 74.7 74.8 74.9 75.0 75.1 75.2 75.3 75.4 75.5 75.6 75.7 75.8 75.9 76.0 76.1 76.2 76.3 76.4 76.5 76.6 76.7 76.8 76.9 77.0 77.1 77.2 77.3 77.4 77.5 77.6 77.7 77.8 77.9 78.0 78.1 78.2 78.3 78.4 78.5 78.6 78.7 78.8 78.9 79.0 79.1 79.2 79.3 79.4 79.5 79.6 79.7 79.8 79.9 80.0 80.1 80.2 80.3 80.4 80.5 80.6 80.7 80.8 80.9 81.0 81.1 81.2 81.3 81.4 81.5 81.6 81.7 81.8 81.9 82.0 82.1 82.2 82.3 82.4 82.5 82.6 82.7 82.8 82.9 83.0 83.1 83.2 83.3 83.4 83.5 83.6 83.7 83.8 83.9 84.0 84.1

3.2)	7	22	25	28	31	1	2	3	4
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2011	14	43.82	28.22	15.31	28.22	1	14
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A	17				
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nr(1) - nr 22	23 24 25 26 27 28 29 30 31	32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100
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$t_{exp} = 16.5$ $t_{amb.} = 15.5$

5-1 5-1 11 B Fe⁹⁺

[illegible]
$$t_{exp} = 16.1 \text{ } t_{amb.} = 14.9$$

Can. Diap. B

10-1-82 11:11 AM

$t_{exp} = 15.9$ $t_{amb} = 14.6$

29-30/VII/68 K.

T. S.

T. U.

A. h. m.

HX 3523	7 HR 6869	103a-0	3.5	18 59	19 02.5	2 20	2 23.5	+0 41
48	"	"	6	19 02	19 09	2 24	2 30	+0 47
9	"	"	11	19 09	19 20	2 30	2 41	+0 55.5
4 10	HR 7193	"	10	19 30	19 40	2 50.5	3 00.5	+0 35.5
11	"	"	17	19 40	19 57	3 00.5	3 17.5	+0 49
12	"	"	28	19 57	20 25	3 17.5	3 45.5	+1 11.5
4 13	HR 7447	"	4	20 41	20 45	4 01.5	4 05.5	+1 08.5
14	"	"	7	20 45	20 52	4 05.5	4 12.5	+1 14
HX 3524	5 1 HR 7447	"	12	21 27	21 39	4 47.5	4 59.5	+1 58.5

30-31/VII/68 J. Ger.

3525	HR 5551	103a-0	20	14 40	15 00	21 56	22 16	-0 03.5
	HR 5683	"	3	15 15	15 18	22 31	22 34	+0 00.5
	"	"	5	15 19	15 24	22 35	22 40	+0 05.5
	"	"	7	15 27	15 34	22 43	22 50	+0 14.5
	"	"						
	HR 5941	"	12	15 49	16 01	23 05	23 17	-0 01
	HR 6142	"	32	16 22	16 54	23 38	0 10	+0 09

30-31/VII/68 K.

3524	5 2 HR 6630	103a-0	4	18 01	18 05	1 17	1 21	+0 16
3	"	"	7.5	18 05	18 12.5	1 21	1 28.5	+0 21.5
4	"	"	13	18 13	18 26	1 29	1 42	+0 32.5
5	HR 6380	"	2	18 40	18 42	1 56	1 58	+1 31.5
6	"	"	3.5	18 42	18 45.5	1 58	2 01.5	+1 34
7	"	"	6	18 46	18 52	2 02	2 08	+1 39.5

5-1

5

B

u

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 $t_{exp.} = 15.3$ $t_{amb.} = 14.2$

u

u

u

u

u

u

 $t_{exp.} = 15.0$ $t_{amb.} = 13.8$

u

u

u

u

 $t_{exp.} = 14.9$ $t_{amb.} = 13.7$

u

u

5-1

4

A

u

u

u

u

u

u

u

Fe

u

u

u

u

5-1

4

B Fe = 9³

u

u

u

u

 $t_{exp.} = 14.7$ $t_{amb.} = 13.5$

u

u

u

u

u

u

 $t_{exp.} = 14.5$ $t_{amb.} = 13.3$

