REFLECTOR 5

Estado de las imágenes:

P	pulsante
m	móvil
d	difusa
i	irregular

K	Kucewicz
f	ferrer
G	Gomez Ana Elvira
J	Jaschik
M	Malaroda
B	Brandi
L	García Lia
H	Hernández
A	Arnal
Gr	Gerhardt
LG	Lopez García
HL	Lerato Hugo

El enfoque:

$F_{colimador} = 23.5$

$D_{Hg} = 20 \frac{Å}{mm}$, $F_{cám.} = 28.5$

$D_{Hg} = 40 \frac{Å}{mm}$, $F_{cám.} = 25.5$

$D_{Hg} = 110 \frac{Å}{mm}$, $F_{cám} = 7.5$

El tiempo de la revelación:

D-19

14°	7.m4
16	6.4
18	5.8
20	5.0
22	4.4
24	3.9

Diafragmas de aluminio:

A	d = 11 cm	$m_A = 0.8 + m_f$
B	19	$m_B = 1.63 + m_f$
C	21.5	$m_C = 2 + m_f$

					T. S.		T. U.		A. h. m.
HX 3524	8	HR 7150	103a-O	2	19 14	19 16	2 30	2 32	+0 19.5
	9	"	"	3.5	19 16	19 19.5	2 32	2 35.5	+0 22.5
	10	"	"	6	19 20	19 26	2 36	2 42	+0 27.5
	11	HR 7446	"	8.5	19 38	19 46.5	2 54	3 02.5	+0 07.5
	12	"	"	14.5	19 46.5	20 01	3 02.5	3 17	+0 19
	13	"	"	24	20 01	20 25	3 17	3 41	+0 38.5
	14	"	"	18	20 25	20 43	3 41	3 59	+0 59.5

HX 3525 30-31/VII/68 Ver la p. 150 del cuaderno 4.

HX 3525A

1-2/VIII/68 J.

ε Sco	HR 6241	103a-O	1	18 13	18 14	1 22	1.23	+1 26
	"	"	2	18 15	18 17	1-24	1.26	+1 28.5
	"	"	4	18 19	18 23	1-28	1.32	+1 33.5
μ' Sco	HR 6247	"	1	18 30	18 31	1.39	1.40	+1 41.5
	"	"	1.5	18 32	18 33.5	1.41	1.42.5	+1 43.5
	"	"	2	18 34	18 36	1.43	1.45	+1 46
ν Sco	HR 6446	"	4	18 43	18 47	1.52	1.56	+1 26.5
	"	"	13	18 49	19 02	1.58	2.11	+1 37
	"	"	7	19 03	19 10	2.12	2.19	+1 48
HX 3526	HR 6879	"	0.5	19 34	19 34.5	2.43	2.43.5	+1 12.5
ε Sgr	"	"	1	19 35	19 36	2.44	2.45	+1 14
α Tel	HR 6897	"	1	19 39	19 40	2.48	2.49	+1 15.5
	"	"	2	19 41	19 43	2.50	2.52	+1 18
	"	"	4	19 44	19 48	2.53	2.57	+1 22
σ Sgr	HR 7121	"	0.5	19 56	19 56.5	3.05	3.05.5	+1 03.5

Ramicci:
A L $A = 1^R + 5$; $L = 11^R + 12$; $F_c = 7.5$; $D_{Hg} = 110 \frac{A}{m\,m}$

5-1	5	B		
"	"			
"	"		t esp. = 14.1	t amb. = 13.0
"	"			
"	3			
"	"			
"	2		t esp. = 13.7	t amb. = 12.6
		Fe 8 1		
5-1	5	A		
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"	Fe 8 1		
"	"			
"	4			
"	"			
"	"			
"	"			
"	"			

				T. S.		T. U.		A. p. m.
	1-2/VIII/68 T.							
HX 3526	HR 7121	II a-0	1	19 58	19 59	3:07	3:08	+1 05.5
ζ Sgr	HR 7194	"	1	20 04	20 05	3:13	3:14	+1 04.5
	"		2	20 06	20 08	3:15	3:17	+1 07
	2-3/VIII/68 F; G							
3527	HR 5260	II a-0	8	15 10	15 18	22 15,5	22 23,5	+1 15
	"	"	16	15 21.5	15 37.5	22 27	22 43	+1 30.5
	"	"	25	15 39.5	16 04.5	22 45	23 10	+1 53
	HR 5961	"	12	16 40.5	16 52.5	23 46	23 58	+0 46
	"	"	15	16 54.5	17 09.5	0 00	0 15	+1 01.5
	"	"	15	17 12.5	17 27.5	0 18	0 33	+1 19.5
	HR 6095	"	2	17 49.5	17 51.5	0 55	0 57	+1 30.5
	"	"	5	17 54.5	17 59.5	1 00	1 05	+1 37
	"	"	10	18 03.5	18 13.5	1 09	1 19	+1 48.5
3528	HR 6556	"	1.5	19 28	19 29.5	2 33,5	2 35	+1 55.5
	"	"	20^s	19 31	19 31.3	2 36 30	2 36 50	+1 58
	"	"	30^s	19 32.5	19 33	2 38	2 38,5	+1 59.5
	"	"	1^{mn}	19 39.5	19 40.5	2 45	2 46	+2 07
	HR 6446	"	4	20 00.5	20 04.5	3 06	3 10	+2 44
	"	"	8	20 10.5	20 18.5	3 16	3 24	+2 56
	9-10/VIII/68 K.							
3529	1 HR 6453	103a-0	1	18 31	18 32	1 07	1 08	+1 12
	2 "	"	1.5	18 32	18 33.5	1 08	1 09.5	+1 13
	3 "	"	3	18 34	18 37	1 10	1 13	+1 16

5-1	3	A		
"	3			
"	3		T_{esp} 14.5	T_{cup} 14.8
		Fe 7 ‰		
5-1		A		
"				
"				
"				
"				
"				
"				
"				
"		Fe 7 ‰		
"				
"				
"				
"				
"				
"			T_{esp} = 12°5	T_{amb} = 11°5
5-1	5	B	Fe 10 ‰	
"	"			
"	"		$t_{esp.}$ = 11.7	$t_{amb.}$ = 10,5

		9-10/VIII/68 K.			T. S.		T. U		
HX 3529	17	HR 7264	103a-O	1.2	19 46	19 47.2	2 22	2 23.2	+0 39
	18	"	"	2	19 48	19 50	2 24	2 26	+0 41.5
	19	"	"	3.5	19 50	19 53.5	2 26	2 29.5	+0 44.5
	10	HR 7623	"	3.5	20 02	20 05.5	2 38	2 41.5	+0 06.5
	11	"	"	6	20 06	20 12	2 42	2 48	+0 12
	12	"	"	10.5	20 12	20 22.5	2 48	2 58.5	+0 20
	13	HR 7869	"	3	20 35	20 38	3 11	3 14	+0 02
	14	"	"	5.5	20 38	20 43.5	3 14	3 19.5	+0 06.
3530	21	HR 7869	"	10	21 37	21 47	4 13	4 23	+1 07.5
	2	HR 7913	"	1.5	21 54	21 55.5	4 21.5	4 31	+1 13,5
	3	"	"	3	21 56	21 59	4 31.5	4 34.5	+1 16
	4	"	"	5	21 59	22 04	4 34.5	4 39.5	+1 20
	5	HR 7920	"	7	22 16	22 23	4 51.5	4 58.5	+1 38.5
	6	"	"	12	22 23	22 35	4 58.5	5 10.5	+1 48
	7	"	"	20	22 35	22 55	5 10.5	5 30.5	+2 04
		10-11/VIII/68 K							
3530	28	HR 6462	103a-O	1.2	17 54	17 55.2	0 25	0 26.2	+0 32.5
	9	"	"	2	17 56	17 58	0 27	0 29	+0 35
	10	"	"	3.5	17 58	18 01.5	0 29	0 32,5	+0 37.5
	11	HR 6698	"	4	18 04	18 16	0 35	0 39	+0 09
	12	"	"	7.5	18 16	18 23.5	0 39	0 46.5	+0 22.5
	13	"	"	13	18 24	18 37	0 47	1 00	+0 33.5
3531	31	HR 6746	"	3	19 09	19 12	1 40	1 43	+1 07
	2	"	"	5	19 12	19 17	1 43	1 48	+1 11

5-1	5 B			
"	"			
"	"		t esp. = 11.2	t amb. = 10.1
"	"			
"	"			
"	"		t esp. = 11.0	t amb. = 10.0
"	"			
"	"		t esp. = 10.8	t amb. = 10.0
"	"	Fe 8^{1}	t esp. = 10.5	t amb = 9.9
"	"			
"	"			
"	"		t esp = 10.4	t amb = 9.8
"	"			
"	"			
"	"		t esp. = 10.3	t amb. = 9.5
5-1	5 B			
"	"			
"	"		t esp. = 13.4	t amb = 12.7
"	"			
"	"			
"	"		t esp. = 13.4	t amb. = 12.9
"	"	Fe 8^{1}		
"	"			

					T.S.		T.U.		A.h.m.
	10-11/VIII/68	k.							
HX 3531	3 2 HR 6746	103a-O	8	19 17	19 25	1 48	1 56	+1 17.5	
	4 HR 7063	"	12	19 41	19 53	2 12	2 24	+1 02	
	5 "	"	21	19 53	20 14	2 24	2 45	+1 18.5	
	6 "	"	36	20 14	20 50	2 45	3 21	+1 47	
	7 HR 7340	"	3.5	21 05	21 08.5	3 36	3 39.5	+1 47.5	
	8 "	"	6	21 09	21 15	3 40	3 46	+1 52.5	
	9 "	"	10.5	21 15	21 25.5	3 46	3 56.5	+2 01	
	10 HR 7747	"	12	21 37	21 49	4 08	4 20	+1 27.5	
	11 "	"	21	21 49	22 10	4 20	4 41	+1 44	
	12 "	"	36	22 10	22 46	4 41	5 17	+2 12.5	
	11-12/VIII/68	k.							
3531	3 13 HR 6527	103a-O	1.2	18 04	18 05.2	0 31	0 32.2	+0 33.5	
	14 "	"	1.8	18 06	18 07.8	0 33	0 34.8	+0 36	
3532	4 1 HR 6527	"	2.5	18 18	18 20.5	0 45	0 47.5	+0 48.5	
	2 HR 6859	"	3	18 35	18 38	1 02	1 05	+0 18	
	3 "	"	5	18 38	18 43	1 05	1 10	+0 22	
	4 "	"	10	18 43	18 53	1 10	1 20	+0 29.5	
	5 HR 7134	"	9	19 07	19 16	1 34	1 43	+0 16	
	6 "	"	16	19 16	19 32	1 43	1 59	+0 28.5	
	7 "	"	26	19 32	19 58	1 59	2 25	+0 49.5	
	8 HR 7234	"	1.6	20 06	20 07.6	2 33	2 34.6	+1 02.5	
	9 "	"	2.8	20 08	20 10.8	2 35	2 37.8	+1 05	
	10 "	"	4.8	20 11	20 15.8	2 38	2 42.8	+1 09	
	11 "	"	1.6	20 16	20 17.6	2 43	2 44.6	+1 12.5	

5-1	5	B	$t_{esp.} = 13.2$	$t_{amb.} = 12.7$
"	"			
"	"			
"	"		$t_{esp.} = 13.2$	$t_{amb.} = 12.5$
"	"			
"	"			
"	"		$t_{esp.} = 13.0$	$t_{amb.} = 12.3$
"	"			
"	"			
"	"		$t_{esp.} = 12.8$	$t_{amb.} = 12.0$
5-1	5	B Con Diaf. $\bar{X}1$		
"	"	" "	$t_{esp.} = 14.5$	$t_{amb.} = 13.9$
"	"	Fe $8^{\frac{1}{2}}$ Con Diaf. $\bar{X}1$		
"	"			
"	"			
"	"		$t_{esp.} = 14.5$	$t_{amb.} = 13.6$
"	"			
"	"			
"	"		$t_{esp} = 14.4$	$t_{amb.} = 13.6$
"	"			
"	"			
"	"		$t_{esp.} = 14.3$	$t_{amb.} = 13.7$
"	"			

				T.S.		T.U.		A.h.m.
	11-12/VIII/68 K.							
HX 3532	12 HR 7236	103a-0	1.4	20 32	20 33.2	2 59	3 00.4	+1 28.5
	13 "	"	2.5	20 34	20 36.5	3 01	3 03.5	+1 31
	14 "	"	4	20 37	20 41	3 04	3 08	+1 35
	2-3/IX/68 J.; Ma.							
3533	HR 5941	IIIa-0	12	18 13	18 25	23 16	23 28	+2 23
	HR 7074	"	2	18 50	18 52	23 53	23 55	+0 02.5
	"	"	4	18 53	18 57	23 56	0 00	+0 06.5
	"	"	11	19 00	19 11	0 03	0 14	+0 17
	2-3/IX/68 K							
3534	1 HR 7665	103a-0	4	21 24	21 28	2 27	2 31	+1 21
	2 "	"	7	21 28	21 35	2 31	2 38	+1 26.5
	3 "	"	12	21 35	21 47	2 38	2 50	+1 36
	4 HR 8140	"	5	21 57	22 02	3 00	3 05	+0 42.5
	5 "	"	9.2	22 02	22 11.2	3 05	3 14.2	+0 49.5
	6 "	"	16	22 12	22 28	3 15	3 31	+1 03
	7 HR 8425	"	1.2	22 44	22 45.2	3 47	3 48.2	+0 39
	8 "	"	2.1	22 46	22 48.1	3 49	3 51.1	+0 41.5
	9 "	"	3.6	22 48.1	22 51.7	3 51.1	3 54.7	+0 44
	10 HR 8636	"	2.4	23 06	23 08.4	4 09	4 11.4	+0 27
	11 "	"	4.1	23 09	23 13.1	4 12	4 16.1	+0 30.5
	12 "	"	7.1	23 14	23 21.1	4 17	4 24.1	+0 37
	13 HR 8787	"	6	23 33	23 39	4 36	4 42	+0 31.5
	14 "	"	11	23 39	23 50	4 42	4 53	+0 40

5×1	5	B		
"	"			
"	"		t exp. = 14.3	t amb. = 13.8
5-1	5	A		
"	"			
"	"			
"	"			
5-1	5	B	Fe 8	
"	"			
"	"			t amb. = 8.1
"	"			
"	"			
"	"			t amb. = 8.2
"			Con Dial. B	
"	"		" "	
"	"			t amb. = 8.2
"	"			
"	"			
"	"			t amb. = 8.2
"	"			
"	"			t amb. = 8.2

	3-4/IX/68	J.; Ma.; Br.		T. S.		T. U.		A.P.m.
HX 3535	HR 6081	IIa-0	13	17 22	17 35	22 21	22 34	+1 10.5
	"	"	22	17 36	17 58	22 35	22 57	+1 29
	HR 6581	"	4	18 09	18 13	23 08	23 12	+0 32
	"	"	8	18 14	18 22	23 13	23 21	+0 39
	HR 6745	"	5	18 38	18 43	23 37	23 42	+0 36
	"	"	12	18 45	18 57	23 44	23 56	+0 46.5
	HR 6714	"	5	19 08	19 13	0 07	0 12	+1 12
	"	"	6	19 13	19 19	0 12	0 18	+1 17.5
	"	"	9	19 19	19 28	0 18	0 27	+1 25
	4-5/IX/68	J.; G.; F.						
HX 3536	HR 6175	IIa-0	0.6	17 10.7	17 11.3	22 05.8	22 06.4	+0 36
	"	"	1	17 12.4	17 13.4	22 07.5	22 08.5	+0 38
	"	"	2	17 15.5	17 17.5	22 10.6	22 12.6	+0 41.5
	HR 6285	"	7.2	17 40.7	17 47.9	22 35.8	22 43	+0 49
	"	"	11	17 50.4	18 01.4	22 45.5	22 56.5	+1 00.5
	"	"	19	18 04.5	18 23.5	22 59.6	23 18.6	+1 18.5
	HR 6510	"	0.8	18 36.6	18 37.4	23 31.7	23 32.5	+1 08.5
	"	"	1.3	18 40.9	18 42.2	23 36	23 37.3	+1 13
	"	"	2	18 43.4	18 45.4	23 38.5	23 40.5	+1 15.5
	HR 6879	"	0.2	18 59.3	18 59.5	23 54.4	23 54.6	+0 38
	"	"	0.4	19 00.9	19 01.3	23 56	23 56.4	+0 39.5

5-1	5	A		
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
5-1	5	A	Fe 8.1	
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			t amb. = 16

14

				T.S.		T.U.		A.h.m.
HX3537	5-6/IX/68 HR 6027	J, Br, Ca IIa-O	4	17 27	17 31	22 18	22 22	+1 19
	"	"	6	17 33	17 39	22 24	22 30	+1 26
	"	"	12	17 41	17 53	22 32	22 44	+1 37
	HR 6486	"	7	18 14	18 21	23 05	23 12	+0 54
	"	"	10	18 23	18 33	23 14	23 24	+1 04
	7-8/IX/68	F						
HX3538	HR 6582	IIaO	9	17 49	17 58	22 32	22 41	+0 12
			15	18 03	18 18	22 46	23 01	+0 28
			21	18 21	18 42	23 04	23 25	+0 50
	8-9/IX/68	J, Ma, Br						
Hx3539	HR 6217	IIa-O	5	17:40	17:45	22 18	22:23	+0 58
	"	"	6	17:46	17:52	22:24	22:30	+1 04
	"	"	6	17:53	17:59	22:31	22:37	+1 12
	HR 6445	"	9	18:18	18:24	22 56	23:05	+1 04
	"	"	15	18:28	18:43	23:06	23:21	+1 17
	HR 6905	"	11	18:52	19:03	23:30	23:41	+0 32
	"	"	20	19:06	19 26	23 44	0 04	+0 50
	HR 7337	"	4	19 36	19 40	0 14	0 18	+0 18
	"		5	19:42	19:47	0 20	0:25	+0 24
	"		10	19 50	20:00	0 28	0 38	+0 35

Ranura	Cielo (5 despej. 0 nublado)	arco	Temper amb.
5-1	5	A-Fe 8^5	+16°
"	"		
"	"		
"	"		
"	"		Intens x mot. fuio en α.
5-1		A-Fe 10^5	+ 23°
"			relo.
5-1	4	A-Fe 10^5	+22°8
"	"		
"	"		
"	"		
"	"		
"	"		
"	"		
"	"		
"	"		

				TS		TU		A.h.m.
	11-12/IX/68	Ba-Na						
HX 3540	HR 5523	IIa-0	18	18:37	18:55	23:05	23:23	+3 59
	"	"	30	18:56	19:26	23:24	23:54	+4h 24
	"	"	58	19:27	20:25	23:55	0:53	+5h 09m
HX 3541	12-13/IX/68	Ba-Na						
	HR 6561	IIa-0	2	19:01	19:03	23:25	23:27	+1h 27m
	"	"	6	19:04	19:10	23:28	23:34	+1 32
	"	"	8	19:10	19:18	23:34	23:42	+1 39
	HR 6556	"	0,5	19:34	19:34,5	23 58	23 58,5	+2 01
	"	"	0.8	19:34,5	19:35,3	23 58,5	23 59,3	+2 02
	"	"	1.4	19:37,5	19:38,9	0 01.5	0 02,9	+2 05
	2-3/IX/68	K.						
HX 3542	1 HR 8787	103a-0	18	0 25	0 43	5 28	5 46	+2 29.5
	2 HR 9098	"	5	1 02	1 07	6 05	6 10	+1 03
	3 "	"	8	1 07	1 15	6 10	6 18	+1 09.5
	4 "	"	14	1 15	1 29	6 18	6 32	+1 20.5
	3-4/IX/68	K.						
HX 3542	5 HR 7074	103a-0	3	20 44	20 47	1 43	1 46	+1 57
	6 "	"	5	20 47	20 52	1 46	1 51	+2 01
	7 "	"	10	20 52	21 02	1 51	2 01	+2 08.5
	4-5/IX/68	K.						
HX 3542	8 HR 7254	103a-0	4	20 19	20 23	1 13	1 17	+1 14

5-1	3	A	Fe 8^5	$+9.6^\circ$	
"	"				
"	"				
5-1	5	A	Fe 8^5	$+9.6^\circ$	
"	"				
"	"				
"	"				
5-1	5	B	Fe 8^1		$t_{amb} = 8.2$ Ver : HX 3534 HR 8787
"	"				
"	"				
"	"				$t_{amb} = 8.2$
5-1	5	B			
"	"				
"	"				$t_{amb} = 12.0$. Se nubla
5-1	4	B			

					T. S.	T. O.	A. h. m.
	4-5/IX/68	K.					
HX 3542	9 HR 7254	103a-0	6	20 23	20 29	1 17	1 23	+1 19
	10 "	"	10	20 29	20 39	1 23	1 33	+1 27
	9-10/IX/68	K					
HX 3542	11 HR 7217	103a-0	7	19 19.5	19 26.5	23 55	0 02	+0 20.5
	12 "	"	12	19 26.5	19 38.5	0 02	0 14	+0 30
	13 "	"	20	19 38.5	19 58.5	0 14	0 34	+0 46
HX 3543	3 1 HR 7763	"	12	20 37.5	20 49.5	1 13	1 25	+0 26.5
	2 "	"	20	20 49.5	21 09.5	1 25	1 45	+0 42.5
	3 "	"	34	21 09.5	21 43.5	1 45	2 19	+1 09.5
	4 HR 7950	"	2	22 01	22 03	2 36.5	2 38.5	+1 16.5
	5 "	"	5	22 03	22 08	2 38.5	2 43.5	+1 20
	6 "	"	7	22 08	22 15	2 43.5	2 50.5	+1 26
	7 HR 8305	"	4	22 25.5	22 29.5	3 01	3 05	+0 45
	8 "	"	7	22 29.5	22 36.5	3 05	3 12	+0 50.5
	9 "	"	12	22 36.5	22 48.5	3 12	3 24	+1 00
	10 HR 8322	"	6	23 04.5	23 10.5	3 40	3 46	+1 22.5
	11 "	"	10	23 10.5	23 20.5	3 46	3 56	+1 30.5
	12 "	"	18	23 20.5	23 38.5	3 56	4 14	+1 44.5
	13 HR 8353	"	5	23 50.5	23 55.5	4 26	4 31	+2 01.5
	14 "	"	8.5	23 55.5	0 04	4 31	4 39.5	+2 08
HX 3544	1 HR 8353	"	15	0 10	0 25	4 45.5	5 00.5	+2 26
	10-11/IX/68	K					
HX 3544	2 HR 8075	103a-0	3	21 44	21 47	2 16	2 19	+0 42

5-1	4			
"	"		t amb. = 15.2	Se nubló
5-1	5			
"	"			
"	"		t amb. = 14.8	
"	"			
"	"			
"	"		t amb = 13.5	
"	"			
"	"			
"	"		t amb. = 13.1	
"	"			
"	"			
"	"		t amb. = 13.0	
"	"	Con Diaf. B		
"	"	"		
"	"	"	t amb. = 12.2	
"	"	"		
"	"	"		
"	"	Fe 8 1 "	t amb. = 11.0	
5-1	5			

					T. S.		T. U.		A. h. m
	10-11/IX/68	K.							
HX3544	4 3	HR 8075	103a-0	5	21 47	21 52	2 19	2 24	+0 46
	4	"	"	9	21 52	22 01	2 24	2 33	+0 53
	5	HR 8402	"	6	22 12	22 18	2 44	2 50	+0 14
	6	"	"	11	22 18	22 29	2 50	3 01	+0 22.5
	7	"	"	18	22 29	22 47	3 01	3 19	+0 37
	8	HR 8709	"	8	22 59	23 07	3 31	3 39	+0 10.5
	9	"	"	14	23 07	23 21	3 39	3 53	+0 21.5
	10	"	"	24	23 21	23 45	3 53	4 17	+0 40.5
	11	HR 9016	"	6	23 59	0 05	4 31	4 37	+0 15
	12	"	"	11	0 05	0 16	4 37	4 48	+0 23.5
	13	"	"	16	0 16	0 32	4 48	5 04	+0 37
	11-12/IX/68	K.							
HX3545	5 1	HR 8260	103a-0	5	21 59	22 04	2 29	2 34	+0 26.5
	2	"	"	8	22 04	22 12	2 34	2 42	+0 33
	3	"	"	14	22 12	22 26	2 42	2 56	+0 44
	4	HR 8278	"	3	22 37	22 40	3 06.5	3 09.5	+1 00.5
	5	"	"	5	22 40	22 45	3 09.5	3 14.5	+1 04.5
	6	"	"	8	22 45	22 53	3 14.5	3 22.5	+1 11
	7	HR 8576	"	4	23 03	23 07	3 32.5	3 36.5	+0 36
	8	"	"	7	23 07	23 14	3 36.5	3 43.5	+0 41.5
	9	"	"	12	23 14	23 26	3 43.5	3 55.5	+0 51
	10	HR 8937	"	4	23 39.5	23 43.5	4 09	4 13	+0 10.5
	11	"	"	7	23 43.5	23 50.5	4 13	4 20	+0 16
	12	"	"	12	23 50.5	0 02.5	4 20	4 32	+0 25.5

5-1	5		
"	"		t amb. = 12.5
"	"		
"	"		
"	"		t amb. = 12.0
"	"	Con Diaf. B	
"	"	"	
"	"		t amb. = 11.5
"	"		
"	"		
"	"		t amb = 10.4
5-1	5	Fe 9	
"	"		
"	"		t amb.= 8.4
"	"		
"	"		
"	"		t amb. = 8.3
"	"		
"	"		
"	"		t amb. = 8.1
"	"		
"	"		
"	"		t amb. = 7.5

					T. S.		T. U.		A. l. m.
	11-12/IX/68	k.							
HX3545	13 HR 8959 ·	103a-0	7	0 11	0 18	4 40.5	4 47.5	+0 39	
	14 "	"	12	0 18	0 30	4 47.5	4 59.5	+0 48.5	
HX-3546	16-17/IX/68	Bn. g.							
	HR 5466	IIa-0	21	18 49	19 10	22 57	23 18	+4 21	
	"	"	48	19 11	19 59	23 19	0 07	+4 56	
	"	"	72	20 00	21 12	0 08	1 20	+5 58	
	17-18/IX/68								
HX3546A	HR 5466	IIa-0	21	18 38	18 59	22 42	23 03	+4 10	
	"	"	54	19 00	19 54	23 04	23 58	+4 48	
	13-14/IX/68	k.							
HX 3547	1 HR 7337 ·	103a-0	2.5	20 57	20 59.5	1 18	1 20.5	+1 38.5	
	2 "	"	4	21 00	21 04	1 21	1 25	+1 42	
	3 "	"	7	21 04	21 11	1 25	1 32	+1 47.5	
	4 HR 7343 ·	"	6	21 18	21 24	1 39	1 45	+2 00.5	
	5 "	"	10	21 24	21 34	1 45	1 55	+2 08.5	
	6 "	"	16	21 34	21 50	1 55	2 11	+2 21.5	
	7 HR 7790 ·	"	2	22 04	22 06	2 25	2 27	+1 42.5	
	8 "	"	2.5	22 06	22 08.5	2 27	2 29.5	+1 45	
	9 "	"	4.2	22 08.5	22 12.7	2 29.5	2 33.7	+1 48	
	10 HR 8254 ·	"	7	22 22	22 29	2 43	2 50	+0 48.5	
	11 "	"	12	22 29	22 41	2 50	3 02	+0 58	
	12 "	"	20	22 41	23 01	3 02	3 22	+1 14	
	13 HR 8368 ·	"	6	23 11	23 17	3 31.5	3 37.5	+1 19	
	14 "	"	11	23 17	23 28	3 37.5	3 48.5	+1 27.5	
HX 3548	2 1 HR 8368 ·	"	18	23 54	0 12	3 48.5	4 06.5	+2 08	

5-1	5				
"	"			+ amb. = 6.7	Se nubló
5-1	5	A	Fe=8^{5}	+10°.5	
5-1	5	A	Fe=8^{4}	+12.2	
"	"			velo	
5-1	4		Fe 8^{4}	"	
"	"				
"	"			+ amb. = 10.6	
"	"				
"	"				
"	"			+ amb = 10.6	
"	3		Con Diaf. B	Pasan las nubes	
"	"		"		
"	"		"	+ amb = 10.7	
"	"			Pasan las nubes	
"	"				
"	"			+ amb. = 10.6	
"	"				
"	"			Pasan las nubes	
"	"		Fe 8^{4}	+ amb = 10.4	Se nubló

					T. S.		T. V.		A.h.m.
	15-16/IX/68	K.							
HX 3548	2	HR 8865	103a-O	8	23 25	23 33	3 37	3 45	+0 12
	3	"	"	14	23 33	23 47	3 45	3 59	+0 23
	4	"	"	24	23 47	0 11	3 59	4 23	+0 42.
	5	HR 8812	"	8	0 23	0 31	4 35	4 43	+1 19.5
	6	"	"	13	0 31	0 44	4 43	4 56	+1 30
	7	"	"	23	0 44	1 07	4 56	5 19	+1 48
	8	HR 8939	"	6	1 17	1 23	5 29	5 35	+1 49
	9	"	"	11	1 23	1 34	5 35	5 46	+1 57.5
	10	"	"	18	1 34	1 52	5 46	6 04	+2 12
	11	HR 8988	"	5	2 01	2 06	6 12	6 18	+2 23
	12	"	"	8	2 06	2 14	6 18	6 26	+2 29.5
	13	"	"	14	2 14	2 28	6 26	6 40	+2 40.5
	16-17/IX/68	K.							
HX 3549	1	HR 8431	103a-O	5	22 46	22 51	2 54.5	2 59.5	+0 42.5
	2	"	"	10	22 51	23 01	2 59.5	3 09.5	+0 50
	3	"	"	15	23 01	23 16	3 09.5	3 24.5	+1 02.5
	4	HR 8447	"	13	23 30	23 43	3 38.5	3 51.5	+1 28.5
	5	"	"	23	23 43	0 06	3 51.5	4 14.5	+1 46.5
	6	"	"	40	0 06	0 46	4 14.5	4 54.5	+2 18
	7	HR 8858	"	11	0 56	1 00	5 04.5	5 08.5	+1 42
	8	"	"	7	1 00	1 07	5 08.5	5 15.5	+1 47.5
	9	"	"	12	1 07	1 19	5 15.5	5 27.5	+1 57
	10	HR 8949	"	7	1 35	1 42	5 44	5 51	+2 05.5
	11	"	"	12	1 42	1 54	5 51	6 03	+2 15
	12	"	"	20	1 54	2 14	6 03	6 23	+2 31

5-1	5			
"	"			
"	"			t amb = 9.3
"	"			
"	"			
"	"			t amb. = 8.6
"	"			
"	"			
"	"			t amb. = 8.2
"	"			
"	"			
"	"			t amb. = 7.8
5-1	5	Fe^{8^1}		
"	"			
"	"			t amb. = 9.9
"	"			
"	"			
"	"			t amb = 9.7
"	"			
"	"			t amb. = 9.7
"	"			
"	"			
"	"			t amb. = 9.5

Deside 6.X.68 T.U. = T.A. + 3h

				T.S.		T.U.		A.h.m.
	7-8/X/68	K.						
1 HX 3550	1 HR 7342	103a-0	9	20 08	20 17	22 53	23 02	+0 53
	2 "	"	15	20 17	20 32	23 02	23 17	+1 05
	3 "	"	25	20 32	20 57	23 17	23 42	+1 25
	4 HR 7754	"	5	21 10	21 15	23 55	0 00	+0 56.5
	5 "	"	9	21 15	21 24	0 00	0 09	+1 03.5
	6 "	"	15	21 24	21 39	0 09	0 24	+1 15.5
	7 HR 7747	"	5	21 45	21 50	0 30	0 35	+1 32
	8 "	"	9	21 50	21 59	0 35	0 44	+1 39
	9 "	"	15	21 59	22 14	0 44	0 59	+1 51
	10 HR 8232	"	2	22 26	22 28	1 11	1 13	+0 57.5
	11 "	"	4	22 28	22 32	1 13	1 17	+1 02.5
	12 "	"	6	22 32	22 38	1 17	1 23	+1 05.5
	13 HR 8679	"	16	22 50	23 06	1 35	1 51	+0 10.5
	14 "	"	28	23 06	23 34	1 51	2 19	+0 32.5
2 HX 3551	1 HR 8679	"	48	23 42	0 30	2 27	3 15	+1 18.5
	2 HR 8597	"	3	0 40	0 43	3 25	3 28	+2 08
	3 "	"	5	0 43	0 48	3 28	3 33	+2 12
	4 "	"	8	0 48	0 56	3 33	3 41	+2 18.5
	12-13/X/68	K.						
	5 HR 7342	103a-0	10	21 41	21 51	0 07	0 17	+2 26.5
	6 "	"	15	21 51	22 06	0 17	0 32	+2 39
	7 "	"	8	22 06	22 14	0 32	0 40	+2 50.5

T.U. = T.A. + 3h

5-1	5	Fe 8 1	
"	"		
"	"		t amb = 14.9
"	"		
"	"		
"	"		t amb. = 14.5
"	"		
"	"		
"	"		t amb = 14.0
"	"		
"	"		
"	"		t amb. = 13.8
"	"		
"	"		t amb. = 13.5
"	"	Fe 8 1	t amb = 13.2
"	"		
"	"		
"	"		t amb. = 13.0
5-1	5 d		
"	"		
"	"		t amb. = 16 — de muflo

				T. S.		T. U.		A. h. m.
14-15/X/68 K.								
2 HX 3551 8	HR 8418	103a-O	4	22 24	22 28	0 41	0 45	+0 22
9	"	"	6	22 28	22 34	0 45	0 51	+0 27
10	"	"	11	22 34	22 45	0 51	1 02	+0 35.5
11	HR 8502	"	4	22 54	22 58	1 11	1 15	+0 40
12	"	"	6.5	22 58	23 04.5	1 15	1 21.5	+0 45.5
13	"	"	12	23 05	23 17	1 22	1 34	+0 55
3 HX 3552 1	HR 472	"	1	0 41	0 42	2 58	2 59	-0 55.5
2	"	"	1.5	0 42	0 43.5	2 59	3 00.5	-0 54
3	"	"	2	0 44	0 46	3 01	3 03	-0 52
4	"	"	2.5	0 46	0 48.5	3 03	3 05.5	-0 49.5
5	"	"	3	0 50	0 53	3 07	3 10	-0 45.5
6	"	"	3.5	0 53	0 56.5	3 10	3 13.5	-0 42
16-17/X/68 K.								
1 HX 3553 1	HR 8556	103a-O	9	22 46	22 55	0 55	1 04	+0 23.5
2	"	"	15	22 55	23 10	1 04	1 19	+0 35.5
3	"	"	25	23 10	23 35	1 19	1 44	+0 55.5
4	HR 8560	"	64	23 41	0 45	1 50	2 54	+1 45.5
5	HR 191	"	4	1 10	1 14	3 19	3 23	+0 30.5
6	"	"	7	1 14	1 21	3 23	3 30	+0 36
7	"	"	12	1 21	1 33	3 30	3 42	+0 45.5
8	HR 472	"	24[1]	1 48	1 48 24	3 57	3 57 24	+0 11.5
9	"	"	42[1]	1 49	1 49 42	3 58	3 58 42	+0 12.5
10	"	"	72[2]	1 51	1 52 12	4 00	4 01 12	+0 15

5-1	5	B			
"	"				
"	"				t amb. = 16.3
"	"				
"	"				
"	4	Pasan las nubes. Viento.			t amb. = 16.3
"	5	B	Fc 8	Con Diaf. C	(d = 21.5 cm)
"	"		"	"	"
"	"		"	"	"
"	"		"	"	"
"	"		"	"	"
"	"	Viento fuerte.			t amb. = 15.2
5-1	5	B	Fc 7		
"	"				
"	"				t amb = 14.9
"	4	Pasan las nubes.			t amb. = 14.1
"	5				
"	"				
"	"				t amb. = 13.8
"	"	Con Diaf. C (d = 21.5 cm).			
"	"		"	"	"
"	"		"	"	t amb. = 13.7
					Se nubló.

					T. S.		T. V.		A. h. m.
	17-18/X/68	K.							
1 HX 3553	11 HR 7342	103a-O	8	21 42	21 50	23 46.5	23 54.5	+2 26.5
	12 "	"	15	21 50	22 05	23 54.5	0 09.5	+2 38
	13 "	"	25	22 05	22 30	0 09.5	0 34.5	+2 58
	19-20/X/68	K.							
1 HX 3554	1 HR 8521	103a-O	90	22 20	23 50	0 16	1 46	+0 44.5
	2 HR 8524	"	45	23 57	0 42	1 53	2 38	+1 59
	3 HR 74	"	7	0 52	0 59	2 48	2 55	+0 38
	4 "	"	12	0 59	1 11	2 55	3 07	+0 47.5
	5 "	"	21	1 11	1 32	3 07	3 28	+1 04
	6 HR 99	"	2	1 40	1 42	3 36	3 38	+1 16.5
	7 "	"	3	1 42	1 45	3 38	3 41	+1 19
	8 "	"	5	1 45	1 50	3 41	3 46	+1 23
	9 HR 100	"	3	2 05	2 08	4 01	4 04	+1 42
	10 "	"	6	2 08	2 14	4 04	4 10	+1 46.5
	11 "	"	10	2 14	2 24	4 10	4 20	+1 54.5
	12 HR 566	"	5	2 34	2 39	4 30	4 35	+0 42
	13 "	"	9	2 39	2 48	4 35	4 44	+0 49
	14 "	"	15	2 48	3 03	4 44	4 59	+1 01
	20-21/X/68	K.							
2 HX 3555	1 HR 8204	103a-O	7	22 22.5	22 29.5	0 15	0 22	+1 01.5
	2 "	"	12	22 29.5	22 41.5	0 22	0 34	+1 11
	3 "	"	19	22 41.5	23 00.5	0 34	0 53	+1 26.5
	4 HR 8414	"	3	23 10.5	23 13.5	1 03	1 06	+1 08.5

5-1	5	B			
"	"				
"	"			t amb. = 13.8	
					Se nubló
5-1	5		Fe 7 1	t amb. = 17.3	
"	"			" 16.5	
"	"				
"	"				
"	"			" 16.0	
"	"				
"	"				
"	"			" 16.0	
"	"				
"	"				
"	"			" 15.8	
"	"				
"	"				
"	"			" 15.7	
5-1	5	B	Fe 7 1		
"	"				
"	"			t amb. = 19.1	
"	"				

				T. S.	T. V.	A. R. m.
	20-21/X/68	K.				
2HX3555	5 HR 8414 ·	103a-0	5	23 13.5 23 18.5	1 06 1 11	+1 12.5
	6 "	"	8	23 18.5 23 26.5	1 11 1 19	+1 19
	7 HR 8906 ·	"	38	23 36 0 14	1 28.5 2 06.5	+0 31
	8 HR 8789 ·	"	15	0 26.5 0 41.5	2 19 2 34	+1 29.5
	9 "	"	23	0 41.5 1 04.5	2 34 2 57	+1 48.5
	10 "	"	40	1 04.5 1 44.5	2 57 3 37	+2 20
	11 HR 402 ·	"	6	1 58 2 04	3 50 3 56	+0 39
	12 "	"	11	2 04 2 15	3 56 4 07	+0 47.5
	13 "	"	17	2 15 2 32	4 07 4 24	+1 01.5
	2-3/XI/68	L+F				
HX3556	HR 8181 ·	IIa-0	7	22 5 04	23 5 34	+0 44
	"		14	22 19 30	23 20 00	+1 02
	"		24	22 37 45	23 38 15	+1 25
	HR 8675 ·		2.5	23 23 00	0 23 38	+0 37
	"		4.	23 27 00	0 27 34	+0 42
	"		8	23 31 30	0 32 20	+0 48
	HR 77 :		9	0 11 10	1 11 55	−0 03
	"		16	0 24 30	1 24 25	+0 14
	3-XI-68	M-B				
Hx3557	HR 8151 ·	IIa-0	8	22h 48m 53	23:38 23:50	+1 36
	"		17	22:55 23:16	23:52 0:13	+1 46
	"		24	23:17 23:44	0:14 0:40	+2 11
	HR 8949 ·		8	23:56 0:04	0:52 1:00	+0 26
	"		17	0:05 0:27	1:02 1:24	+0 42

5-1	5			
"	"			$t_{amb.} = 18.8$
"	5d			" 18.4
"	" "			
"	" "			
"	" "			" 18.2
"	" "			
"	" "			
"	" "			" 18.0
5-1	5			$t_{amb} = 18°5$
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	4			$T_{amb} = 16°8$
"	"			"
"	"			"
"	"			"
"	"			"

					T. S.		T. U.		A. R. m.
	2-3/XI/68	K.							
HX3558	1 HR 370	103a-O	15	1 56	2 11	2 56	3 11	+0 49.5	
	2 "	"	26	2 11	2 37	3 11	3 37	+1 10	
	3 "	"	43	2 37	3 20	3 37	4 20	+1 44.5	
	4-5/XI-68	K							
	4 HR 8425	103a-O	2.5	2 06	2 08.5	2 58	3 00.5	+4 00.5	
	5 "	"	3.6	2 09	2 12.6	3 01	3 04.6	+4 04	
	6 "	"	6	2 13	2 19	3 05	3 11	+4 09.5	
	6-7/XI/68	L+F							
HX 3559	HR 8728	103a-O	10^{sec}	0 36	0 36 10	1 18	1 18 10	+1 40.	
	HR 8675		$2^{m}20$	0 47	0 49 20	1 29	1 31 20	+2 01	
			$1^{m}10$	0 54	0 55 10	1 36	1 37 10	+2 08	
			6^{m}	0 57	0 63 00	1 39	1 45 00	+2 14	
	4-5/XI/68	K.							
2 HX 3560	1 HR 1008	103a-O	8	3 49	3 57	4 41	4 49	+0 34	
	2 "	"	14	3 57	4 11	4 49	5 03	+0 45	
	3 "	"	24	4 11	4 35	5 03	5 27	+1 04	
	4 HR 1247	"	52	4 46	5 38	5 38	6 30	+1 13.5	
	6-7/XI/68	K.							
2 HX 3560	5 HR 98	103a-O	9	2 00	2 09	2 46	2 55	+1 40	
	6 "	"	15	2 09	2 24	2 55	3 10	+1 52	
	7 "	"	26	2 24	2 50	3 10	3 36	+2 12.5	
	8 HR 778	"	28	3 09	3 37	3 55	4 23	+0 46.5	
	9 HR 1264	"	50	4 00	4 50	4 46	5 36	+0 24.5	

5-1	5	Fe 7		
"	"			
"	"		t esp. = 16.7	t amb = 16.8
5-1	5	Con Diaf. B		
"	"	" "		
"	"	" "	t esp = 17.8	t amb = 18.0
5-1			t esp = 18°	t amb = 21.2
"				
"				
5-1	5	Fe 7		
"	"			
"	"		t esp. = 18.1	t amb. = 18.2
"	"		" = 18.0	" = 18.1 t emb 6
5-1	5	Con Diaf. B		
"	"	"		
"	"	" "	t esp. = 18.1	t amb = 18.1
"	"		" = 17.8	" = 17.8
"	"		" = 17.4	" = 17.3

				T.S.		T.V.		A.R.m.
	6-7/XI/68	K.						
2 HX3560	10 HR 1465 ·	103a-0	7	5 08	5 15	5 53,5	6 00,5	+0 38
	11 "	"	12	5 15	5 27	6 00,5	6 12,5	+0 47,5
	12 "	"	20	5 27	5 47	6 12,5	6 32,5	+1 03,5
	7-8/XI/68	B.						
Hx 3561	HR 8949 ·	II a-0	8	0 38	0 47	1 27	1 36	+1 09
	"	"	17	0 48	1 06	1 37	1 55	+1 23
	"	"	24	1 12	1 46	2 00	2 24	+1 55
Hx 3562	10-11/XI/68	L+F						
	HR 8151 ·	103a-0	13	23 48	0 01	0 20	0 33	+2 35,5
	HR 8278 ·	"	2	0 24	0 26	0 56	0 58	+2 46
	"	"	5	0 27	0 32	0 59	1 04	+2 50
	"	"	9	0 33	0 42	1 05	1 14	+2 58
	HR 8410 ·	"	35	0 55	1 30	1 27	2 02	+2 09
	8-9/XI/68	K.						
3 HX 3563	1 HR 8425 ·	103a-0	1	1 26	1 27	2 05	2 06	+3 20
	2 "	"	2	1 27	1 29	2 06	2 08	+3 21,5
	3 "	"	3	1 29	1 32	2 08	2 11	+3 24
	4 HR 98 ·	"	5	1 48	1 53	2 27	2 32	+1 26
	5 "	"	8	1 53	2 01	2 32	2 40	+1 32,5
	6 "	"	13	2 01	2 14	2 40	2 53	+1 43
	7 HR 674 ·	"	9	2 35	2 44	3 14	3 23	+0 24
	8 "	"	16	2 44	3 00	3 23	3 39	+0 36,5
	9 "	"	26	3 00	3 26	3 39	4 05	+0 57,5
	10 HR 1025 ·	"	42	3 40	4 22	4 19	5 01	+0 44,5

5-1	5	Con Diaf. B		
"	"	" "		
"	"	" "	t esp. = 17.0	t amb. = 17.0
				te mblo'
"	ovelo			T. amb. = 25°
5-1				t amb 19°.0
"				
"				
"				
"				t amb 17.5
5-1	5	Fe 7 Con Diaf. B		
"	"	"		
"	"	"	t esp = 20.6	t amb. = 20.5
"	"	"		
"	"	"		
"	"	"	t esp = 20.1	t amb. = 20.0
"	"	"		
"	"	"		
"	"	"	t esp. = 19.5	t amb. = 19.4
"	"		t esp. = 18.6	t amb. = 18.8

				T. S.		T. V.		A. h. m.
	8-9/XI/68	K.						
HX3563	HR 1326	103a-0	8	4 38	4 46	5 17	5 25	+0 29
	12 "	"	14	4 46	5 00	5 25	5 39	+0 40
	10 "	"	24	5 00	5 24	5 39	6 03	+0 59
	12-13/XI/68	H, J						
HX3564	HR 8244		2	22 50	22 52	23 15	23 17	+1 18
	"		4	22 53	22 57	23 18	23 22	+1 22
	HR 8521		2	23 02	23 04	23 27	23 29	+0 42
	"		4	23 05	23 09	23 30	23 34	+0 46
	13-14/XII/68	M-B						
Hx3565	HR 8728	Ia-0	30s	23h 25m 00s	- 23 25 45	23:45	-23 45.5	+0 29
	"	"	1m	23 26	- 23h 27m 25	23 47	-23 48.25	+0 30
	HR 8848	"	11m	23 46	23 58	0 05	0 18	+0 35.5
	HR 100	"	7m	0 17	0 25	0 37	0 45	-0 04
Hx3566	HR 8949	"	7m	0 55	1 02	1 15	1 22	+1 25.5
	"	"	13m	1 03	1 16	1 23	1 36	+1 36.5
	"	"	20m	1 17	1 37	1 37	1 57	+1 54
	14-15/XI/68	L+F						
HX 3567	HR 8722	103a-0	12m	0 33	0 45	0 49	1 01	+1 44
	HR 8919	"	4m	1 03	1 07	1 19	1 23	+1 38
	"	"	6m	1 08	1 14	1 24	1 30	+1 44
	HR 183	"	6m	1 36	1 42	1 52	1 58	+0 58 0 58
	"	"	12m	1 44	1 56	2 00	2 12	+1 09

5-1	5				
"	"				
"	3		t exp. = 18.7	t amb. = 18.8	se nubló
5-1	5				
"	"				
"	"				
"	"				
"	3	Fe = 8^s			
"	"	"			
"	"	"			
"	"	"			
"	rebo	"			
"	"	"			
"	"	"			+ 1 54
5-1		Fe 5 seg.		t amb = 23.5	
"		"			
"		"			
"		"			
"		"		t amb = 20.3	

	10-11/XI/68	K.		T. S.		T. V.		A. h. m
HX 3568	1 HR 779	103a-0	2.5	3 26	3 28.5	3 54	3 56.5	+0 49
	2 "	"	4	3 29	3 33	3 57	4 01	+0 52.5
	3 "	"	7	3 33	3 40	4 01	4 08	+0 58
	4 HR 1070	"	6	4 04	4 10	4 32	4 38	+0 37.5
	5 "	"	11	4 10	4 21	4 38	4 49	+0 46
	6 "	"	17	4 21	4 38	4 49	5 06	+1 00
	7 HR 1298	"	4	4 48	4 52	5 16	5 20	+0 39.5
	8 "	"	8	4 52	5 00	5 20	5 28	+0 45.5
	9 "	"	13	5 00	5 13	5 28	5 41	+0 56
	10 HR 1617	"	6	5 30	5 36	5 58	6 04	+0 33
	11 "	"	10	5 36	5 46	6 04	6 14	+0 41
	12 "	"	16	5 46	6 02	6 14	6 30	+0 54
	14-15/XI/68	K.						
2 HX 3569	4 HR 1143	103a-0 gr.	6	4 32	4 38	4 44	4 50	+0 53
	5 "	"	11	4 38	4 49	4 50	5 01	+1 01.5
	6 "	"	18	4 49	5 07	5 01	5 19	+1 16
	7 HR 1492	"	11	5 20	5 31	5 32	5 43	+0 49
	8 "	"	18	5 31	5 49	5 43	6 01	+1 03.5
	9 "	"	32	5 49	6 21	6 01	6 33	+1 28.5
	10 HR 1862	"	2	6 33	6 35	6 45	6 47	+1 04
	11 "	"	4	6 35	6 39	6 47	6 51	+1 07
	12 "	"	7	6 39	6 46	6 51	6 58	+1 12.5

5-1	5	Fcám = 7.5	Fe 7^{1}	
"	"			
"	"		t esp. = 16.0	t amb. = 16.0
"	"			
"	"		" 15.5	" 15.4
"	"			
"	"			
"	"		" 15.2	" 15.2
"	"			
"	"			
"	"		" 14.6	" 14.7
			—	
5-1	5	Fcám = 7	Fe 5^{1} con 3 vidrios esmerilados	
"	"			
"	"		t esp. = 17.3	t amb. = 17.5
"	"			
"	"			
"	"		" 15.7	" 16.3
"	"			
"	"			
"	"		" 15.9	" 16.1

42

				T. ⊿.	T. U.	A. h. m.
3HX3570	15-16/XI/68 K.					
	1 HR 1318 ·	103a-0 gr.	7	4 58.5 5 05.5	5 06 5 13	+0 49
	2 "	"	13	5 05.5 5 18.5	5 13 5 26	+0 59
	3 "	"	22	5 18.5 5 40.5	5 26 5 48	+1 16.5
	4 HR 1483 ·	"	25	5 50.5 5 53	5 58 6 00.5	+1 14
	5 "	"	4	5 53 5 57	6 00.5 6 04.5	+1 17.5
	6 "	"	7	5 57 6 04	6 04.5 6 11.5	+1 23
	7 HR 2227 ·	"	3.5	6 28.5 6 32	6 36 6 39.5	+0 16.5
	8 "	"	6	6 32 6 38	6 39.5 6 45.5	+0 21.5
	9 "	"	10	6 38 6 48	6 45.5 6 55.5	+0 29.5
	17-18/XI/68 K.					
	10 HR 749 ·	103a-0 gr.	2	2 55.5 2 57.5	2 56 2 58	+0 24
	11 "	"	4	2 57.5 3 01.5	2 58 3 02	+0 27
	12 "	"	6	3 01.5 3 07.5	3 02 3 08	+0 32
	13 HR 984 ·	"	2,3	3 24.5 3 26.8	3 25 3 27.3	+0 11
	14 "	"	4	3 27 3 31	3 27.5 3 31.5	+0 14.5
~~HX3571~~	15-16/XI/68 A.					
HX 3571	1 HR 8137 ·	103a-0 gr	4	23 30.5 23 34.5	23.38 - 23.42	+2 16
	2 "	"	6	23 41.5 23 47.5	23.49 - 23.55	+2 28
	3 "	"	8	23 51.5 23 59.5	23.59 - 0.07	+2 39
	1 HR 8919 ·	103a-0 gr	9	1 32.5 1 41.5	1 40 - 1.49	+2 09.5
	2 "	"	13	1 47.5 2 00.5	1 55 - 2.08	+2 26.5
	3 "	"	17	2 02.5 2 19.5	2.10 - 2.27	+2 43.5

5-1	5			
"	"	Fe 5²		
"	"		t_{exp} = 18.3	$t_{amb.}$ = 18.7
"	"			
"	"			
"	"		" 18.3	" 18.6
"	"			
"	"			
"	"		" 18.3	" 18.6
5-1	4			
"	"			
"	"		" 22.1	" 22.3
"	"			
"	"		" 22.1	" 22.2
5-1	5	Fe 5⊥		
"	"			
"	"			
"	"			
"	"			
"	"			

	16-17/XI/68	M+B		T.S.		T.U.		A.h.m
Hx 3572	HR 8135	103 a-0	4m	23 40	23 45	23 45	23 50	+2 26
	"	"	9	23 46	23 54	23 51	24 00	+2 34
	HR 8151	"	4	0 08	0 15	0 14	0 21	+2 52.5
	"	"	6	0 16	0 25	0 22	0 31	+3 01.5
	HR 8949	"	6	0 34	0 41	0 39	0 46	+1 04
	"	"	4	0 42	0 47	0 47	0 52	+1 11
Hx 3573	HR 8848	"	5	1 03	1 09	1 04	1 10	+1 50
	"	"	3	1 13	1 16	1 18	1 21	+1 58.5
	HR 100	"	1	1 25	1 26	1 30	1 31	+1 00.5
	"	"	2	1 29	1 31	1 34	1 36	+1 05
	HR 118	"	5.4m	1 42	1 48 40	1 42	1 49	+1 16.5
	"	"	9.4	1 50 13	1 59 50	1 55	2 05	+1 26
	HR 331	"	5.4	2 11 45	2 17 10	2 16	2 22	+1 08.5
	"	"	9.4	2 17 50	2 28 45	2 23	2 34	+1 17

30/XI – 1/XII/68

	30/XI/68	M+B	30/XI – 11/XII/68				
Hx 3574	HR 8135	103 a-0	4	0 26	0 31	23 38	23 44	+3 13
	"	"	6	0 32	0 39	23 45	23 52	+3 19
	HR 8151	"	4	0 48	0 52	24 00	24 04	+3 31
	"	"	6	0 54	1 01	24 06	24 13	+3 38.5
	HR 8949	"	4	1 10	1 14	24 22	24 26	+1 38
	"	"	6	1 16	1 23	24 28	24 35	+1 46
Hx 3575	HR 12	"	9	1 43	1 53	0 55	1 05	+1 41.5
	"	"	15	1 54	2 09	1 06	1 21	+1 55

5-1	5	Fc=5^5		
"	"			
"	"			Tamb = 23°
"	"			
"	"			
"	"			
5-1	5	Fc = 5^5		
"	"			T. amb: 23°
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
5-1	5	Fc=5^5		
"	"			
"	"			T. amb = 22°
"	"			
"	"			
"	"			

30/XI - 1/XII /68

	30/XI/68	H+B		TS		TU		Δ h.m
Hx 3575	HR 120	103a-O	9	220	229	133	142	+1 55
	"	"	15	231	247	143	159	+2 10
	HR 473	"	6	302	313	214	225	+1 30
	"	"	11	314	326	226	238	+1 42.5
	1-2/XII/68	B+H						
Hx 3576	HR 35	103a-O	6	046	053	2354	001	+0 39
	"	"	10	054	104	003	013	+0 49
	HR 187	"	8	116	124	024	032	+0 39
	"	"	15	126	143	034	051	+0 53
	HR 197	"	9	236	245	144	153	+1 57
	1-2/XII/68	B+M						
Hx 3577	HR 612	103a-O	5	2:59	3:04	2:07	2:12	+0 58
	HR 1240	"	5	3:35	3:41	2:43	2:49	-0 21
	"	"	3	3:42	3:46	2:50	2:54	-0 15
	17-18/XI/68	K.						
HX3578	1 HR 984	103a-O gr	8	341.5	349.5	342	350	+0 31
	29-30/XI/68	K.						
"	2 HR 939	103a-O gr	4	429	433	343.5	347.5	+1 29
	3 "	"	6	433	439	347.5	353.5	+1 34
	4 "	"	11	439	450	353.5	404.5	+1 42.5
	5 HR 1541	"	4	521.5	525.5	436	440	+0 40
	6 "	"	6	525.5	531.5	440	446	+0 45
	7 "	"	11	531.5	542.5	446	457	+0 53.5

5-1	6		Fe 5^5			
"	"				T. amb 22°	
"	"					
"	"					
5-1	5		Fe 5^5			
"	"				T amb. 22°,6	
"	"					
"	"					
"	"					
5-1	5					
"	"					
"	"				T. amb = 22°.6	
5-1	4	B	Fe 5^1	t esp.=21.7	t amb=21.9	Se nubló
5-1	5	B				
"	"					
"	"			t esp= 18.6	t amb.= 18.8	
"	"					
"	"					
"	"			t esp = 18.0	t amb. = 18.3	

				T. S.		T. U.		A. h. m.
	29-30/XI/68	K.						
HX 3578	8 HR 1829	103a-O qz	5	6 00	6 05	5 14.5	5 19.5	+0 35.5
	9 "	"	8	6 05	6 13	5 19.5	5 27.5	+0 42
	10 "	"	13	6 13	6 26	5 27.5	5 40.5	+0 52.5
	11 HR 1998	"	5	6 37	6 42	5 51.5	5 56.5	+0 53.5
	12 "	"	8	6 42	6 50	5 56.5	6 04.5	+1 00
	13 "	"	13	6 50	7 03	6 04.5	6 17.5	+1 10.5
	29-30/XI/68	F+L						
HX 3579	HD 212385	103a-O	60	0 33	1 33	23 46	0 46	+2 35
	HR 8937	"	40^s	1 43 40	1 44 20	0 56	0 57 20	+2 13
	"	"	$1^m 10^s$	1 45	1 46 10	0 58	0 59 10	+2 15
	"	"	4^m	1 47	1 51	1 00	1 04	+2 18
	HR 8949	"	$1^m 10^s$	2 09 30	2 10 40	$1^h 22^m 30^s$	-1 23 40	+2 43
	"	"	$2^m 30^s$	2 11 30	2 14	1 24 30	-1 27	+2 46
	"	"	6^m	2 15	2 21	1 28	1 34	+2 51
	2-3/XII/68	F+L						
HX 3580	HR 8877	103a-O	25	1 13	1 38	0 13	0 38	+2 06
	HR 8969	"	1	2 00	2 01	1 00	1 01	+2 23
		"	2	2 02	2 04	1 02	1 04	+2 26
		"	5	2 05	2 10	1 05	1 10	+2 30
	HR 370	"	13	2 45	2 58	1 45	1 58	+1 37
	5-6/XII/68	F+L						
HX 3581	HR 8787	103a-O	1	1^h 01	1 02	0 51	0 52	+1 56
	"	"	2	1 02	1 04	0 52	0 54	+1 58
	"	"	5	1 05	1 10	0 55	0 00	+2 03

5-1	5	Con Diaf. C			
"		"			
"		"	$t_{esp} = 17.9$	$t_{amb.} = 18.3$	
"		"			
"		"			
"		"	$t_{esp.} = 17.7$	$t_{amb.} = 18.1$	
5-1		Fe 5^s.		$t_{amb} = 22°$	
"					
"					
"					
"			$t_{esp} = 21°$	$t_{amb} = 21°$	
5-1		Fe 5^s.		$t_{amb} = 24°$	
"					
"					
"				$t_{amb} = 22°5$	se nubló.
5-1		Fe 5^s	$t_{esp} =$	$t_{amb} = 24°$	23 57
"					23 [illegible]
"					[illegible]

		F., L.		T.S		T.U.		A.h.m.
	5-6/XII/68							
HX 3581	HD 3580	103 a-O	40	1 37	2 17	0 27	1 07	+ 1 20
	HR 612	"	2	2 36	2 38	1 26	1 28	+ 0 35
	"	"	5	2 39	2 44	1 29	1 34	+ 0 38
	30/XI - 1/XII/68	K.						
HX 3582	1 HR 1121	103 a-O gr.	4	4 30	4 34	3 42	3 46	+ 0 52.5
	2 "	"	6	4 34	4 40	3 46	3 52	+ 0 57.5
	3 "	"	10	4 40	4 50	3 52	4 02	+ 1 05.5
	4 HR 1302	"	5	5 08	5 13	4 20	4 25	+ 1 00.5
	5 HR 1326	"	4	5 24	5 28	4 36	4 40	+ 1 13
	1-2/XII/68	K.						
	6 HR 909	103 a-O gr	5	4 30	4 35	3 37	3 42	+ 1 34
	7 HR 1355	"	7	4 44	4 51	3 51	3 58	+ 0 31.5
	8 HR 1393	"	7	5 05	5 12	4 12	4 19	+ 0 45,5
	9 HR 1502	"	3	5 39	5 42	4 46	4 49	+ 1 01
	4-5/XII/68	K.						
	10 HR 1121	103 a-O gr	4	5 28	5 32	4 23	4 27	+ 1 50.5
	11 "	"	6	5 32	5 38	4 27	4 33	+ 1 55.5
	12 "	"	10	5 38	5 48	4 33	4 43	+ 2 03.5
	13 HR 1648	"	90	6 11	7 41	5 06	6 36	+ 1 52
	9-10/XII/68	B.						
Hx 3583	HR 8137	103 a-O	7	1 11	1 21	23 47	23 57	+ 4 00
Hx 3584	HR 151	"	27	1 51	2 19	0 27	0 55	+ 1 30

5-1	5	B Fe 5^{1}		
"	"			
"	"		t_{exp} = 21.0	t_{amf} = 21.2
"	"		" 20.8	" 21.1
"	3-2		" 20.8	" 21.0
"	5		" 22.7	" 22.8
"	"			
"	2		" 22.5	" 22.6
"	"		" 22.4	" 22.5
"	5			
"	"			
"	"		" 22.5	" 22.4
"	"		" 20.0	" 20.2
5-2	4	Fe = 5^{5}		t_{amb} = 24°.5
"	"			

				T.S.		T.U.		A. h. m.
	9-10/XII/68	B.						
Hx3584	HR 612	103a-0	3	2 67	3 00	1 32	1 35	+0 55
	"	"	5	3 01	3 08	1 37	1 44	+1 01
	HR 1240	"	3	3 22.5	3 26.5	1 59	2 03	−0 35
	"	"	4,5	3 27	3 31,5	2 03.5	2 08	−0 30
	10-11/XII/68	F+L.						
HX 3585	HR 8137	103a-0	11	1 19	1 30	23 49	0 00	+4 08
	HR 100	"	1	1 48	1 49	0 18	0 19	+1 24
	+ " "	"	2	1 50	1 52	0 20	0 22	+1 27
	HR 127	"	2	2 04	2 06	0 34	0 36	+1 35
	"	"	5	2 07	2 12	0 37	0 42	+1 39
	HR 595	"	5	2 25	2 30	0 55	1 00	+0 27
	"	"	10	2 31	2 41	1 01	1 11	+0 36
	9-10/XII/68	K.						
HX 3586	1 HR 1173	103a-0 gr.	3	4 31	4 34	3 06	3 09	+0 47
	10-11/XII/68	K.						
	2 HR 1100	103a-0 gr.	4.5	4 34	4 38.5	3 04	3 08,5	+1 01
	3 HR 1363	"	8,5	4 56	5 04,5	3 26	3 34.5	+0 41
	4 HR 1383	"	5	5 17	5 22	3 47	3 52	+0 57
	5 HR 1784	"	4,5	5 38	5 42,5	4 08	4 12,5	+0 17.5
	6 HR 1496	"	11	5 54	6 05	4 24	4 35	+1 20
	7 HR 1481	"	4	6 25	6 29	4 55	4 59	+1 50
	8 HR 1487	"	21	6 39	7 00	5 09	5 30	+2 11.5
	9 HR 2479	"	7	7 17	7 24	5 47	5 54	+0 38

5-1	4				
"	"				
"	"				
"	"			T. amb = 24°.5	
5-1					
"					
"					
"					
"					
"					
"					
5-1	4-3	B	Fe5A	t esp. = 23.8	t amb = 23.7	Se nubla
5-1	4			" 23.3	" 23.6	
"	4			" 23.3	" 23.5	
"	5			" 23.2	" 23.4	
"	4			" 23.2	" 23.4	
"	"			" 23.2	" 23.4	
"	"			" 23.1	" 23.3	
"	"			" 23.0	" 23.1	
"	"			" 22.8	" 23.0	

	10-11/XII/68 K.			T. S.		T. U.		A. R. m.
HX 3586	10 HR 2580	103a-0 gr	7	7 38	7 45	6 08	6 15	+0 48.5
	11 HR 2881	"	7	7 57	8 04	6 27	6 34	+0 31
	12 HR 3034	"	18	8 16	8 34	6 46	7 04	+0 38
	13 HR 2616	"	6	8 47	8 53	7 17	7 23	+1 52.5
	14 "	"	11	8 53	9 04	7 23	7 34	+2 01
	16-17/XII/68 K.							
HX 3587	1 HR 1003	103a-0 gr	5	3 59	4 04	2 05	2 10	+0 43
	2 HR 1084	"	24	4 20	4 44	2 26	2 50	+1 00.5
	3 HR 1202	"	6	4 53	4 59	2 59	3 05	+1 04.5
	4 HR 1453	"	7	5 09	5 16	3 15	3 22	+0 40
	5 HR 1525	"	18	5 23	5 41	3 29	3 47	+0 46.5
	6 HR 1621	"	4	5 53	5 57	3 59	4 03	+0 54.5
	7 HR 2085	"	4	6 09	6 13	4 15	4 19	+0 16
	8 HR 1855	"	5	6 25	6 30	4 31	4 36	+0 57
	9 HR 1654	"	7	6 45	6 52	4 51	4 58	+1 44
	10 HR 2646	"	5	7 20	7 25	5 26	5 31	+0 22
	11 HR 2740	"	3	7 40	7 43	5 46	5 49	+0 30
	12 HR 3055	"	7	7 58	8 05	6 04	6 11	+0 13
	13 HR 3223	"	11	8 22	8 33	6 28	6 39	+0 20
	14 HR 3340	"	7	8 41	8 48	6 47	6 54	+0 23
	28-29/XII/68 A-J.							
HX 3588	1 HR 1441	103a 0 gr	8	3:32 - 3:40		0:58 ~~0:43~~	-1:01	-0:55
	2 " "		78	3:42 - 3:49		1:03 - 1:10		-0:46

Ranura	Cielo				
5-1	5	B		t_{esp} = 22.6	t_{amb} = 22.9
"	"			" 22.5	" 22.8
"	"		Con Diaf. C	" 22.5	" 22.8
"	"			" 22.5	" 22.8
"	"			" 22.5	" 22.8
5-1	5	B	Fe 5^{s}	t_{esp} = 16.7	t_{amb} = 16.8
"	"		Con Diaf C	" 16.6	" 16.8
"	"			" 16.5	" 16.6
"	"			" 16.1	" 16.4
"	"			" 16.0	" 16.2
"	"			" 15.7	" 16.1
"	"		Con Diaf A	" 15.8	" 16.0
"	"		" " A	" 15.9	" 16.1
"	"		" " A	" 15.7	" 15.9
"	"			" 15.6	" 15.8
"	"				
"	"		Con Diaf. B	" 15.3	" 15.5
"	"		" " B	" 15.3	" 15.4
"	"			" 15.3	" 15.4
5-1	5			t_{esp} 21°5	t_{amb} = 21°5
"	"				

				T. S.	T. U.	A. h. m.
HX 3588	3 HR 1582	103a 0 qr	6	4:08 - 4:14	1:29 - 1:35	-0:43
	4 "		6	4:15 - 4:21	1:36 - 1:42	-0:39
	21-22/XII/68 K.					
HX 3589	1 HR 2509	103a-0 qr	12	5 37 5 49	3 25 3 37	-1 03
	27-28/XII/68 K.					
	2 HR 2509	103a-0 qr	11	5 42 5 53	3 05 3 16	-0 58.5
	3 HR 2595	"	4	6 08 6 12	3 31 3 35	-0 44
	4 HR 2603	"	20	6 29 6 49	3 52 4 12	-0 17
	5 HR 2611	"	12	7 07 7 19	4 30 4 42	+0 17
	6 HR 2616	"	6	7 33 7 39	4 56 5 02	+0 39
	7 HR 2621	"	16	7 52 8 08	5 15 5 31	+1 02
	8 HR 2628	"	17	8 25 8 42	5 48 6 05	+1 34
	9 HR 2741	"	17	8 54 9 11	6 17 6 34	+1 50
	10 HR 2743	"	20	9 22 9 42	6 45 7 05	+2 19
	11 HR 2766	"	20	9 55 10 15	7 18 7 38	+2 50
	28-29/XII/68 K.					
HX 3590	1 HR 2826	103a-0 qr	20	5 33 5 53	2 53 3 13	-1 40
	2 HR 2841	"	10	6 09 6 19	3 29 3 39	-1 10
	3 HR 3817	"	4	7 57 8 01	5 17 5 21	-1 34
	4 "	"	8	8 01 8 09	5 21 5 29	-1 28
	5 "	"	12	8 09 8 21	5 29 5 41	-1 18

5-1	5		Fe 6^5	t_{esp}	21°5	t_{emp} 21°5
5-1	5	B	Fe 5^1			
5-1	5	B		t_{esp} =	18.5	t_{emb} = 18.5
"	"			"	18.5	" 18.5
"	"			"	18.1	" 18.3
"	"			"	17.9	" 18.1
"	"			"	17.7	" 17.9
"	"			"	17.5	" 17.7
"	"			"	17.3	" 17.6
"	"			"	17.1	" 17.3
"	"			"	16.7	" 17.0
"	"			"	16.4	" 16.5
5-1	5	B	Fe 6^1	t_{esp} =	21.0	t_{emp} = 21.0
"	"			"	21.0	" 21.0
"	"			"	20.6	" 20.7
"	"			"	20.6	" 20.7
"	"			"	20.6	" 20.6

				T. S.	T. U	A.h.-m.
	2-3/I/69	J+A				
HX3591	1 HR 1100	103a-Oy.	4.5	3:35.5/3:40	0:35 - 0:40	+0:04
	2 "		6"	3:40 - 3:46	0:40 - 0.46	+0.10
	3 HR 1121		7"	4:20 -4:27	1:20 - 1:27	+0 44
	4 "		6.5	4:27 - 4:34	1:27 - 1:34	+0 51
	5 HR 1582		6"	4:46 - 4:52	1:46 - 1:52	-0:03
	"		8"	4:52 - 5:00	1:52 - 2:00	+0:02
	3-4/I/69	J+A				
HX3592	1 HR 1582	103a-Oy.	7	3:28 - 3:35	0:25 - 0:32	-0:50
	2 "		8	3:37.5 - 3:45.5	0:34 - 0:42	-0:40
	3 HR 1449		8	3:55 - 4:03	0:52 - 1:00	-0:21
	4 "		10	4:03 - 4:13	1:01 - 1:11	-0:25
	5 HR 1723		4	4:35 - 4:39	1:23 - 1:27	-0:33
	6 "		5.5	4:41.5 - 4:47	1:29 - 1:35	-0:28
	1-2/I/69	M+B				
Hx3593	HR 612	103a-O	3	3 32	3 39	0 35	0 42	+1 30
	"	"	5	3 45	3 51	0 48	0.54	+1 44
Hx3594	HR 1240	"	3	5 39	5 42	2 42	2 45	+1 38
	"	"	5	5 43	5 48	2 46	2 51	+1 46
	HR 1465	"	40s	6 06	6 07	3 09	3 10	+1 33
	"	"	1	6 08	6 09 20	3 11	3 12 20	+1 35
Hx3595	HR 2761	"	16	8 09	8 25	5 12	5 28	+1 03
	HR 3151	"	20	8 50	9 11	5 53	6 14	+1 01

5-1	5	Fe 5^s	temp. 21°.5	temp. 22°
"	"			
"	"			
"	"			
"	"			
"	"			
5-1	5	Fe 6^s	temp. 23°.5	temp. 24°
"				
"				
"				
"				
"				
5-1	(entre nubes)	Fe: 5^s		T. amb = 21°.7
"	5			
"	"	"		
"	"			
"	"			
"	"			T. amb = 18°.9
"	"	"		
"	"			T. amb = 18°.5

				T. ☉		T. U.		
	1-2/I/69	M+B						
Hx 3596	HR 1981	103a-0	20	6 51	7 11	3 54	4 14	+1 18
	HR 2550	"	40^s	7 29 05	7 30 05	4 33	4 34	+0 41
	"	"	1^m	7 32	7 33 15	4 34	4 35	+0 44
Hx 3597	HR 3183	"	6	9 30	9 37	7 32	7 39	+1 27
	"	"	12	9 39	9 52	7 41	7 55	+1 40
	HR 3270	"	2	10 05	10 07	7 08	7 10	+1 48
	"	"	4	10 09	10 13	7 12	7 16	+1 53
	HR 3426	"	1	10 20	10 21	7 23	7 24	+1 44
	"	"	2	10 22	10 24	7 25	7 27	+1 46
	23/I/69	M+B						
Hx 3598	HR 1465	103a-0	40^s	5 36	5 36 50	2 37	2 37 50	+1 03
	"	"	1^m	5 37	5 38 10	2 38	2 39 10	+1 04
	HR 1240	"	4	5 50	3 54	2 51	2 55	+1 57
	"	"	5	5 55	6 00 30	2 56	3 01 30	+1 59
	HR 3151	"	22	8 41	9 03	5 42	6 04	+0 52
	HR 3466	"	15	9 29	9 44	6 30	6 45	+0 55
	5-6/I/69	A+Gr						
Hx 3599	1 HR 1723	103a-0	150^s	3:17:10 - 3:19		0 07 10	0 09	-1:56
	2 "		4^m	3:22 - 3:26		0 12	0 16	-1:49
	3 "		7^m	3:29 - 3:36		0 19	0 26	-1:41
	4 HR 2177		40^s	3:37:20 - 3:38		0 27 20	0 48	-2:11
	5		3^m	4:03 - 4:06		0 53	0 56	-2:01

5-1	5	Fe 5^s		T.amb = 19°3	
"	"				
"	"				
"	"	Fe 5^s			
"	"				
"	"				
"	"				
"	"				
"	"		T. esp. = 17°8	T. amb = 18°	
5-1	5	Fe = 5^s		T. amb = 22°	
"	"				
"	"				+1 53
"	"			T. amb = 21°5	
"	"				
"					
"	nubes		T. esp = 21°	T. amb = 21°3	
5-1	5	Fe 5^s	T esp = 26°7	T esp = 26°3	
"	"				
"	"				
"	"				
"	"				

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Hx 3599	6HR 2177	103a-0	7 m	4:10 - 4:17		-1:52
	6-7/I/69	A				
Hx 3600	1 HR 1100	103a-0	2 m	3:10 - 3:12	23:56 - 23:58	-0:23
	2 "		5	3:14 - 3:19	24:00 - 0:05	-0:17
	3		9	3:21 - 3:30	0:08 - 0:17	-0:08
	4 HR 1441		5	3:43 - 3:48	0:30 - 0:35	-0:44
	5 "		9	3:50 - 3:59	0:37 - 0:46	-0:34
	6 "		15	4:03 - 4:18	0:50 - 1:05	-0:19
	7 HR 2461		5	4:41 - 4:46	1:27 - 1:32	-1:55
	8 "		9	4:47 - 4:56	1:34 - 1:43	-1:46
	9 "		15	4:58 - 5:13	1:43 - 1:58	-1:34

Hx 3601	2-3/I/69	M+B						
	1 HR 1502	103a-0	2 m	6 36	6 38	3 35	3 37	+1 57
	2 "	"	5	6 39	6 44	3 40	3 45	+2 02
	3 HR 1530	"	4	6 54	7 01	3 55	4 02	+2 14
	4 HR 1649	"	11	7 14	7 25	4 15	4 26	+2 17
	5 HR 2015	"	2	7 40	7 42	4 41	4 43	+1 56
	6 "	"	5	7 44	7 49	4 45	4 50	+2 02
	7 HR 3218	"	12	10 00	10 12	7 01	7 13	+1 57
	8 HR 3445	"	7	10 23	10 30	7 24	7 31	+1 47
	9 HR 3452	"	7	10 38	10 45	7 39	7 46	+2 01

5-1	5			
5-1	5	Fe 5^s	t_{esp} = 26°	t_{esp} = 26°
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
5-1	5			T. amb = 21°.5
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			T. amb = 21°.3
"	nubes			
"		Fe = 6^s	T. esp = 21°	t. amb = 21°.3

		3-4/I/69	M+B		T.S.		T.O.		
Hx 3602	1	HR 1240	103a-0	3m	5 47	5 50	2 44	2 47	+1 50
	2	"	"	5	5 52	5 57,5	2 49	2 54,5	+1 56
	3	HR 1465	"	40s	6 05 20	0 06 20	3 02	3 03	+1 33
	4	"	"	1m	6 08	6 09 25	3 05	3 06 25	+1 35
	6	HR 3151	"	21	8 43	9 04	5 40	6 01	+0 54
	7	HR 3466	"	14	9 16	9 30	6 12	6 26	+0 41
		3-4/I/69	M+B						
Hx 3603	1	HR 1530	103a-0	19	6 32	6 46	3 29	3 43	+1 55
	2	HR 1859	"	18	6 55	7 13	3 52	4 10	+1 37
	3	HR 2094	"	16	7 22	7 38	4 18	4 34	+1 40
	4	HR 2384	"	11	7 48	7 59	4 45	4 56	+1 24
	6	HR 2996	"	1	10 25	10 26 18	7 21	7 22 18	+2 43
	7	"	"	2	10 28	10 30 15	7 24	7 26 15	+2 46
		5-6/I/69	M+B						
Hx 3604	1	HR 710	103a-0	18m	5 47	6 05	2 40	2 58	+3 31
	2	HR 1240	"	4	6 16	6 19 20	3 05	3 08 20	+2 19
	3	"	"	5	6 20	6 25	3 09	3 14	+2 24
	4	HR 1465	"	40s	6 34 40	-6 35 35	3 22 40	-3 23 05	+2 02
	5	"	"	1m	6 36	6 37	3 24	3 25	+2 03
	6	HR 2534	"	22	6 58	7 20	3 46	4 08	+0 20
	7	HR 3151	"	21	9 34	9 55	7 22	7 43	+1 45
	8	HR 3466	"	15	10 07	10 22	7 56	8 11	+1 33

5-1	5		t. esp. = 23.8°	t. amb = 23.5°
"	"			
"	"			
"	"			
"	"			t. amb = 21°
"	"	Fe = 6 s	t. esp. = 22°	t. amb = 21°
"	"			t. amb = 23°
"	"			
"	"			
"	"			
"	"			
"	"	Fe = 6 s	t. esp = 22°	t. amb = 22°
5-1	5			t. amb = 23.2°
"	"			
"	"			
"	"			
"	"			
"	"			
"	"			
"	"	Fe = 6 s	t. esp = 20°	t. amb = 19.7°

	5-6/I/69		M+B		T.S.			T.U.			
Hx 3605	1	HR 1502	103 a-0	2m	7	35	7 37	4 23	4 25	+ 2	56
	2	"	"	6	7	39	7 45	4 27	4 33	+ 3	02
	3	HR 1649	"	11	7	55	8 06	4 44	4 55	+ 2	58
	4	HR 2785	"	29	8	37	9 06	5 26	5 55	+ 1	34
	5	HR 3226	"	8	9	16	9 24	7 05	7 13	+ 1	09
	6	HR 3270	"	3	10	38	10 41	7 27	7 30	+ 2	22
	7	"	"	7	10	43	10 50	7 31	7 38	+ 2	29
	8	HR 3350	"	13	10	59	11 12	7 48	8 01	+ 2	38
	6-7/I/69		M+B								
Hx 3606	1	HR 1240	103 a-0	5m	5	57	6 02	2 42	247	+ 2	01
	2	HR 1465	"	40s	6	11 35	6 12 35	2 56	2 56 50	+ 1	38
	3	"	"	1m	6	13	6 14	2 57	2 58	+ 1	40
	4	HR 2534	"	23	7	58	8 21	4 42	5 05	+ 1	20
	5	HR 3151	"	21	8	31	8 52	5 15	5 36	+ 0	42
	6	HR 3466	"	10	9	00	9 10	5 43	5 53	+ 0	23
	6-7/I/69		M+B								
Hx 3607	1	HR 883	103a-0	9	6	44	6 53	3 27	336	+ 3	52
	2	HR 1882	"	20	7	08	7 28	3 53	4 13	+ 1	48
	3	HR 2092	"	8	7	38	7 36	4 22	4 30	+ 1	42
	4	HR 2909	"	17	9	35	9 52	7 19	7 36	+ 2	10
	5	HR 3183	"	8	10	00	10 08	7 44	7 52	+ 1	58
	6	HR 3426	"	1	10	18	10 19	7 01	7 02	+ 1	42
	7	"	"	2	10	20	10 22	7 03	7 05	+ 1	44
	8	HR 3527	"	10	10	32	10 44	7 15	7 27	+ 1	48

5-1	5		t.amb = 22.5
〃	〃		
〃	〃		
〃	〃		
〃	〃	t.esp = 21°,5	t amb = 21°
〃	〃		
〃	〃		
〃	〃 Fe = 6^s		t amb = 19°.5
5-1	〃	t.esp = 26°,5	t.amb = 25°.8
〃	〃		
〃	〃		
〃	〃		
〃	〃		
〃	〃 Fe = 6^s		t.amb = 22°.8
5-1	5		t amb = 25°.9
〃			
〃			
〃			
〃			
〃			
〃			
〃	〃 Fe = 6^s		t.amb = 22°.7

	20-21/II/69	M+B		TS		TU		
HX3608	1 HR 1275	103a-0	12m	5:52	6:04	23:41	23 53	+1 53
	2 HR 1653	"	27m	6:18	6:45	0:07	0:34	+1 28
	3 HR 1865	"	55m	6:56:20	6:57:15	0:45:20	0:46:15	+1 25
	4 HR 1935	"	11m	7:30	7:41	1:18	1:29	+1 59
	20-21/II/69	M+B						
Hx 3609	1 HR 2534	103a-0	27m	8 00	8 27	1:49	2 16	+1 24
	2 HR 3151	"	26m	8 47	9 13	2 36	3 02	+1 00
	3 HR 3466	"	14m	9 25	9 39	3 13	3 27	+0 50
	20-21/II/69	K.						
HX 3610	1 HR 3994	103a-0	3	10 50	10 53	4 39	4 42	+0 42
	2 HR 4119	"	3,5	11 33	11 36,5	5 22	5 25,5	+1 05.5
	3 HR 4382	"	3	11 50	11 53	5 39	5 42	+0 33.5
	4 HR 4662	"	2	12 25	12 27	6 14	6 16	+0 11.5
	21-22/II/69	K.						
	5 HR 3165	103a-0	2	9 15	9 17	3 00	3 02	+1 13.5
	6 HR 3206	"	2	9 34	9 36	3 19	3 21	+1 26
	7 HR 3207	"	1	9 48	9 49	3 33	3 34	+1 39.5
	8 HR 3426	"	3	10 00	10 03	3 45	3 48	+1 25
	9 HR 3445	"	5	10 18	10 23	4 03	4 08	+1 40.5
	10 HR 3487	"	11	10 40	10 51	4 25	4 36	+2 00.5
	11 HR 4520	"	11	11 57	12 08	5 42	5 53	+0 18
	12 HR 4522	"	4	12 16	12 20	6 01	6 05	+0 33
	13 HR 4537	"	3	12 30	12 33	6 15	6 18	+0 43
	14 HR 4616	"	4	12 46	12 50	6 31	6 35	+0 42.5

5-1	5		t. amb. 22°,7		
"	"	Fe = 7 seg		Tesp. 23°	
"	"				55^1
"	"				
5-1	5	Fe = 7 seg.	t. amb. = 21,9		
"	"				
"	"				
5-1	4	B Fe 5^1	t esp = 20.4	t amb = 20.5	F cam = 7.5
"	"		20.1	20.3	Δδ = +13'
"	"		20.1	20.2	
"	"	Con Diaf. B	20.1	20.3	
5-1	5	Con Diaf. C	22.1	22.1	
"	"		21.8	21.9	
"	"	Con Diaf. C	21.8	21.8	
"	"		21.7	21.6	
"	"	Con Diaf C	21.5	21.4	
"	"	" " "	21.3	21.2	
"	"	" " "	21.0	21.0	
"	"		20.9	20.8	
"	"		20.8	20.7	
"	"		20.8	20.7	

				T. S		T. U		
HX 3611	1/2-III-69	A+Gr		~~7:02~~ ~~7:03~~				+ 0:56
	1 HR 2177	103a-O	40s	7:02	7:03	0:16	0:17	+1:00 +0 56
	2 "	103a-O	3m	7:04	7:07	0:19	0:22	+1:07 +0 54
	3 "	103a-O	7m	7:10	7:17	0:24	0:31	+1 07
	4 HR 1121	103a-O	3m	7:39	7:42	0:53	0:56	+ 4:02
	5 "	103a-O	6m	7:45	7:51	0:59	1:05	+4:10
	6 "	103a-O	11m	7:54	8:05	1:08	1:19	+ 4:21
	7 HR 1541	103a-O	3m	8:31	8:34	1:45	1:48	+3:49
	8 "	103a-O	7m	8:37	8:44	1:51	1:58	+3:57
	9 "	103a-O	12m	8:46	8:58	2:00	2:12	+4:08
	25-26/II/69 K.							
HX 3612	1 HR 3994	103a-O	3	10 26	10 29	3 54	3 57	+0 18
	2 HR 4119	"	3.5	10 41	10 44.5	4 09	4 12.5	+0 13.5
	3 HR 4133	"	4	11 06	11 10	4 34	4 38	+0 36.5
	4 HR 4382	"	3	11 23	11 26	4 51	4 54	+0 06.5
	5 HR 4520	"	11	11 49	12 00	5 17	5 28	+0 10
	26-27/II/69 K.							
	6 HR 3165	103a-O	2.2	9 55	9 57.2	3 20	3 22.2	+1 53.5
	7 HR 3206	"	3.2	10 09	10 12.2	3 34	3 37.2	+2 02
	8 HR 3206	"	2.2	10 15	10 17.2	3 40	3 42.2	+2 07
	9 HR 3207	"	0.8	10 26	10 26.8	3 51	3 51.8	+2 17.5
	10 HR 3426	"	14	10 38	10 52	4 03	4 17	+2 08.5
	11 HR 3426	"	3	11 06	11 09	4 31	4 34	+2 31
	12 HR 4522	"	4	11 55	11 59	5 20	5 24	+0 12

5-1	5		tamb 23°7		
"	"	Fe 6⁵		tamp. 24°.2	
"	"				
"	"				
"	"				
"	"				
"	"				
"	"				
"	"				
"	"				
"	"				
5-1	4	Fe 5⁵	tamp = 22.6	tamb. = 22.9	Fe cam = 7.0
"	"		22.5	22.7	
"	"	Con Diaf. A	22.3	22.6	
"	"		22.3	22.5	
"	3	Con Diaf. C	21.8	22.1	Fe mobile
5-1	4	Con Diaf. C	22.3	22.5	
"	"		22.3	22.5	
"	"		22.3	22.4	
"	"	Con Diaf. C	22.2	22.4	
"	"	Con Diaf. C	22.1	22.3	
"	"		22.0	22.3	
"	"		21.8	22.1	

				T. S.		T. U.		
	26-27/II/69 K.							
HX 3612	13 HR 4537	103a-O	3	12 07	12 10	5 32	5 35	+0 20
	14 HR 4662	"	2	12 28	12 30	5 53	5 55	+0 14.5
	26-27/II/69 F+L							
HX 3613	HR 1664	103a-O	6	6 25	6 31	23 50	23 56	+1 22
	"	"	11	6 31	6 42	23 56	0 07	+1 31
	HR 1672	"	7	7 03	7 10	0 28	0 35	+2 00
	"	"	16	7 10	7 26	0 35	0 51	+2 08
	HR 2108	"	5	7 44	7 49	1 09	1 14	+1 50
	"	"	10	7 50	8 00	1 15	1 25	+1 58
HX3614	HR 2683	"	7	8 18	8 25	1 43	1 50	+1 17
	"	"	12	8 27	8 39	1 52	2 04	+1 29
	HR 2746	"	3	8 48	8 51	2 13	2 16	+1 38
	"	"	7	8 52	8 59	2 17	2 24	+1 43
	27-28/II/69 F+L							
HX 3615	HR 1465	103aO		6 20	6 20 40	23 41	23 41 40	+1 47
	"	"		6 21	6 22	23 42	23 43	+1 48
	"	"		6 22 40	6 23	23 43 40	23 44	+1 49
	HR 1458	"		6 49	6 50	0 10	0 11	+2 16
	"	"		6 51	6 54	0 12	0 15	+2 19
	HR 2108	"		7 05	7 10	0 26	0 31	+1 11
	"	"		7 10	7 20	0 31	0 41	+1 18
HX 3616	HR 2124	"		7 53	754	1 14	1 15	+1 53
	"	"		7 55	7 58	1 16	1 19	+1 56

5-1	4		t esp. = 21.8	t amb. = 22.0	
"	"	Con Drup. B	21.7	22.0	
5-1	3	Fe 5^5	t esp = 25°	t amb = 25°	F cám 7.^{5}
"	"				
"	"				
"	"				
"	"				F. cám. 7.
"	"				
"	"				
"	"				
"	"				
"	"		t esp = 22°5	t amb = 23°	
5-1	3	Fe 5^5	t esp = 26°7	t amb. 26°5	
"	"				
"	"				
"	"				
"	"				
"	"				
"	"				
"	"				

			TS		TU		
	27-28/II/69	F+L					
HX 3616	HR 2320	103a-0	8 15	8 26	1 36	1 47	+1 58
	"	"	8 27	8 44	1 48	2 05	+2 13
	HR 2727	"	9 02	9 08	2 23	2 29	+1 54
	"	"	9 10	9 21	2 31	2 42	+2 05
	28 II/1 III/1969	F+L					
HX 3617	HR 1458	103a-0	6 19	6 21	23 36	23 38	+1 46
	"	"	6 21	6 25	23 38	23 42	+1 58
	HR 1664	"	6 40	6 49	23 57	0 06	+1 38
	"	"	6 50	7 06	0 07	0 13	+1 52
	HR 2124	"	7 12	7 13	0 19	0 20	+1 12
	"	"	7 13	7 17	0 20	0 24	+1 15
	4-5/III/69	F+L					
HX 3618	HR 2320	103a-0	6 24	6 36	23 26	23 38	+0 08
	HR 2683	"	6 45	6 51	23 47	23 53	-0 15
	HR 2761	"	7 01	7 12	0 03	0 14	-0 06
	"	"	7 22	7 39	0 25	0 41	+0 17
	HR 2768	"	7 54	8 11	0 56	1 13	+0 47
	HR 3398	"	8 27	8 37	1 29	1 39	+0 01
	5-6/III/69	F+L					
HX 3619	HR 2108	103a-0	6 27	6 27	23 18	23 23	+0 27
	"	"	6 29	6 39	23 25	23 35	+0 37

5-1	3				
"	"				
"	"				
"	"	Fe 5^s	$t_{esp} = 24°5$	$t_{amb} = 24°3$	
5-1	5	Fe 5^s	$t_{esp} = 27°5$	$t_{amb} = 27°$	Fou cém. 7
"	"				
"	"				
"	"				
"	"				
"	"		Suspendido por conta de luz.		
5-1	5	Fe 5^s	$t_{esp.} = 28°2$	$t_{amb} = 28°0$	
"					
			$t_{esp.} = 24°3$	$t_{amb} = 24°5$	
5-1	8	Fe 5 seg.	$t_{esp} = 22°5$	$t_{amb} = 23°2$	

	5-6/III/69	F+L	TS		TU		
HX3619	3 HR 2124	103a.0	6 48	6 49	23 44	23 45	+0.48
	4 "	"	6 50	6 53	23 46	23 49	+0 51
	5 HR 2171	"	7 08	7 24	0 04	0 20	+1 11
	6 HR 2683	"	7 35	7 44	0 31	0 40	+0 36
	7 HR 2727	"	7 53	7 59	0 49	0 55	+0 45
HX3620	HR 3151	103a.0	8 42	8 58	1 38	1 54	+0 51
	HR 3413	"	9 08	9 18	2 04	2 14	+0 38
	HR 3398	"	9 28	9 38	2 24	2 34	+1 00
	28/II-1/III/69 K.						
HX3621	1 HR 3445	103a-0 qr	5	9 49	9 54	3 05	3 10	+1 11.5
	2 HR 3487	"	11	10 07	10 18	3 23	3 34	+1 27.5
	3 HR 3494	"	9	10 35	10 44	3 51	4 00	+1 54
	4 HR 4110	"	7	11 08	11 15	4 24	4 31	+0 45
	4-5/III/69 K.							
	5 HR 3165	103a-0 qr	2	9 26	9 28	2 25	2 27	+1 24.5
	6 HR 3206	"	2	9 44	9 46	2 43	2 45	+1 36
	7 HR 3207	"	0.8	9 58	9 58.8	2 57	2 57.8	+1 49.5
	8 HR 3426	"	3	10 11	10 14	3 10	3 13	+1 36
	9 HR 4174	"	13	10 39	10 52	3 38	3 51	+0 10
	10 HR 4180	"	6	11 05	11 11	4 04	4 10	+0 30
	11 HR 4210	"	28	11 21	11 49	4 20	4 48	+0 51
	12 HR 4250	"	6	12 04	12 10	5 03	5 09	+1 15.5

5-1	5				
"	"				
"	"				
"	"				
"	"				
"	"				
"	"				
"	"		$t_{esp} = 20°0$	$t_{amb} = 20°5$	Fcám 7.
5-1	5	Fe5^{-1} C.D.C	$t_{esp} = 25.0$	$t_{amb} = 25.0$	Fcám 7.0
"	"	"	24.9	24.9	
"	"		24.7	24.8	
"	3		24.5	24.6	Velo
5-1	5	C.D.C	22.6	22.8	
"			22.4	22.5	
"		Fe5^{-1} C.D.C	22.1	22.3	
"			21.6	21.9	
"			20.0	20.9	
"			20.1	20.6	
"		Fe5^{-1}	19.1	19.7	
"			18.6	19.3	

	4-5/III/69 K.			T. S.		T. V.		
HX 3621	13 HR 4520	103a-0 gr	12	12 27	12 39	5 26	5 38	+0 48.5
	14 HR 4530	"	20	12 53	13 13	5 52	6 12	+1 16
	5-6/III/69 K.							
HX 3622	1 HR 3994	103a-0 gr	3	10 58	11 01	3 53	3 56	+0 50
	2 HR 4116	"	3,5	11 12	11 15.5	4 07	4 10.5	+0 44.5
	3 HR 4133	"	2	11 30	11 32	4 25	4 27	+0 59.5
	4 HR 4382	"	3	11 44	11 47	4 39	4 42	+0 27.5
	5 HR 4522	"	4	12 09	12 13	5 04	5 08	+0 26
	6 HR 4537	"	3	12 25	12 28	5 20	5 23	+0 38
	7 HR 4616	"	3	12 43	12 46	5 38	5 41	+0 39
	7-8/III/69 K.							
	8 HR 3165	103a-0 gr	1.5	9 39	9 40.5	2 26	2 27.5	+0 37
	9 HR 3485	"	1.5	10 00	10 01.5	2 47	2 48.5	+1 16.5
	10 HR 3634	"	3,1	10 12	10 15.1	2 59	3 02.1	+1 06.5
	11 HR 3699	"	2	10 29	10 31	3 16	3 18	+1 13.5
	12 HR 3734	"	2	10 39	10 41	3 26	3 28	+1 18.5
	13 HR 4102	"	3	10 58	11 01	3 45	3 48	+0 35.5
	14 HR 3849	"	3.5	11 15	11 18.5	4 02	4 05.5	+1 37.5
	10-11/III/69 K.							
HX 3623	1 HR 2781	103a-0 gr	1.5	9 28	9 29.5	2 04	2 05.5	+2 11
	2 HR 2782	"	1.6	9 38	9 39.6	2 14	2 15.6	+2 21
	3 HR 3347	"	3,5	9 50	9 53.5	2 26	2 29.5	+1 26
	4 HR 3682	"	4	10 03	10 07	2 39	2 43	+0 50.5

5-1	5	C.D.C	$t_{exp.}$ = 17.6	t_{amb} = 18.7	
"	"		17.3	18.2	
5-1	5	Fe 5^{A}	$t_{exp.}$ = 19.1	t_{amb} = 19.6	$F_{alm.}$ = 7.0
"	"		19.0	19.6	
"	"		18.9	19.5	
"	"		18.9	19.3	
"	4 d.		18.9	19.1	
"	" "		18.8	19.0	
"	3 "		18.7	18.9	
5-1	4	C.D.C.	22.9	22.8	
"	"	"	22.8	22.8	
"	"	C.D.A	22.7	22.6	
"	"	C.D.C	22.6	22.6	
"	"	"	22.6	22.5	
"	3		22.3	22.4	
"	"		22.1	22.2	
5-1	5	Fe 5^{A}	$t_{exp.}$ = 22.8	$t_{amb.}$ = 22.8	
"	"		22.8	22.8	
"	"		22.8	22.9	
"	"		22.9	22.9	

				T. S.		T. U.		
	10-11/III/69	K.						
HX3623	5 HR 4138	103a-0 gr.	5.5	10 23	10 28.5	2 59	3 04.5	-0 04
	6 HR 4167	"	3.5	10 47	10 50.5	3 23	3 26.5	+0 12.5
	7 HR 4169	"	12	11 00	11 12	3 36	3 48	+0 29.5
	8 HD 96248	"	25	11 41	12 06	4 17	4 42	+0 49.5
	9 HD 96446	"	21	12 27	12 48	5 03	5 24	+1 32.5
	10 HR 4337	"	5	13 00	13 05	5 36	5 41	+1 55
	12-13/III/69	K.						
HX3623	11 HR 3343	103a-0 gr.	30	9 23	9 53	1 51	2 21	+1 11
	12 HR 3359	"	15	10 13	10 28	2 41	2 56	+1 52
	13 HR 3410	"	8	10 49	10 57	3 17	3 25	+2 16.5
	14 HR 3415	"	22	11 11	11 33	3 39	4 01	+2 47.5

HX3623A Ver la ~~pag.~~ 152.

HX3624	29-30/III/69	A+6r.						
	1 HR 3448	103a-0	4m	12:26	-12:33	4:52	-4 56	+3 48
	2 HR 3448	103a-0	8m	12 35	-12 44	4 58	-5 06	+3 58
	3 HR 3448	103a-0	13m	12 45	-12 59	5 08	-5 21	+4 13
	4 HR 4089	103a-0	1m20	13 21	-13 23	5 44	-5 45	+3 00
	5 HR 4089	103a-0	3m	13 26	-13 29	5 48	-5 51	+3 05
	6 HR 4089	103a-0	7m	13 31	-13 38	5 53	-6 00	+3 12
HX3625	6-7/III/69	F+L						
	1 HR 2171	103a-0	20m	6 40	7 00	23 32	-23 52	+0h45m
	2 HR 2746	"	3m	7 06	7 09	23 58	0 01	-0 05
	3 HR "	"	8m	7 10	7 18	0 02	0 10	+0 02

5-1	5		$t_{esp.}$ = 22.9	$t_{amb.}$ = 22.9	$F_{cám.}$ = 7.0
"	"	C.D.A	23.0	22.9	
"	"		22.7	22.8	
"	"		22.5	22.6	
"	"		22.4	22.4	
"	3 d		22.4	22.4	
5-1	4		$t_{esp.}$ = 24.4	$t_{amb.}$ = 24.3	
"	"		24.3	24.2	
"	" d		24.3	24.3	
"	" "		24.5	24.5	
5-1	5	Fe 5^s			
"	"				
"	"				
"	4	"			
"	4				
"	2				
5-1		Fe 5^s	t. esp -	t. amb = 22°8	$F_{cám.}$ = 7.0
"					
"					

6-7/III/69 F+L

HX 3625	4 HR 2768	103a-O	19	7 27	7 46	0 19	0 38	+0 22
	5 HD 66605	"	40	8 07	8 47	0 59	1 39	+0 26.

1-2/IV/69 F+L

HX 3626	1 HR 3413	103a-O	10	7 58	8 08	23 12	23 22	−0 32
	2 HR 3413	"	16	8 12	8 28	23 26	23 42	−0 15
	3 HR 3398	"	10	8 45	8 55	23 59	0 09	+0 16
	4 HR 3831	"	19	9 10	9 29	0 24	0 43	−0 15
	5 HR 4025	"	6	9 38	9 44	0 52	0 58	−0 31

1-2/IV/69 K.

HX 3627	1 HR 4519	103a-Ogr	5	12 07	12 12	3 16	3 21	+0 25
	2 HR 4541	"	12	12 23	12 35	3 32	3 44	+0 40
	3 HR 4563	"	13	13 06	13 19	4 15	4 28	+1 19
	4 HR 5048	"	8	13 41	13 49	4 50	4 58	+0 21.5
	5 HR 5048	"	7	14 03	14 10	5 12	5 19	+0 43
	6 HR 5048	"	7	14 22	14 29	5 31	5 38	+1 02
	7 HR 5048	"	6	14 41	14 47	5 50	5 56	+1 20.5
	8 HR 5048	"	5	14 53	14 58	6 02	6 07	+1 32
	9 HR 5048	"	5	15 09	15 14	6 18	6 23	+1 48
	10 HR 5048	"	4	15 22	15 26	6 31	6 35	+2 00.5
	11 HR 5048	"	3	15 33	15 36	6 42	6 45	+2 11
	12 HR 5048	"	3	15 46	15 49	6 55	6 58	+2 24
	13 HR 5048	"	2	15 57	15 59	7 06	7 08	+2 34.5
	14 HR 5041	"	10	16 15	16 25	7 24	7 34	+2 57.5

Ranura A L					
5-1					
"		Fe 5^s	t_{esp} = 21°.0	t_{amb} = 21.2	F_{calm} = 7.0
5-1		Fe 5^s	t_{esp} = 16.5	t_{amb} = 16°5	F_{calm} = 7.
"					
"					
"		Fe 5^s	t_{esp} = 14°	t_{amb} = 14°	
5-1	5	Fe 5^s	t_{esp}. 13.3	t_{amb} 13.4	
"	"		13.3	13.2	
"	"		13.0	12.9	
$A = 5 \cdot 1 = 11^R + \frac{12}{40}$	"		13.0	12.8	
" $10^R + \frac{12}{40}$	"		13.0	12.8	
" $9^R + \frac{12}{40}$	"		12.9	12.6	
" $8^R + \frac{12}{40}$	"		12.7	12.5	
" $7^R + \frac{12}{40}$	"		12.7	12.5	
" $6^R + \frac{12}{40}$	"		12.7	12.6	
" $5^R + \frac{12}{40}$	"		12.7	12.6	
" $4^R + \frac{12}{40}$	"		12.7	12.7	
" $3^R + \frac{12}{40}$	"		12.6	12.7	
" $2^R + \frac{12}{40}$	"		12.6	12.6	
5-1	"		12.6	12.3	

Desde 6. IV. 69 — T. U. = T. A. + 4h

	9-10/IV/69	L. G	T. S.		T. U.	A. R. m.
HX 3628	1 HR 3241	103a-0 7m	9 05	9 12	$23^{45} - 23^{52}$	+0 55
	2 " "	" 12m	9 14	9 26	$23^{54} - 24^{06}$	+1 07
	3 " "	" 18"	9 30	9 48	$0h^{10} - 0h^{28}$	+1 26
	4 HR 3501	" 9m	10 23	10 32	$1^{03} - 1^{12}$	+1 40
	5 "	" 16m	10 34	10 50	$1^{14} - 1^{30}$	+1 55
	6 "	" 29m	11 00	11 29	1h40 - 2 09	+2 27
	7 HR 4185	" 2 1/2	11 38	11 40	2 18 - 2 20	+1 02
	"	" 6m	11 44	11 50	2 24 - 2 30	+1 10
	"	" 11"	11 54	12 05	2 34 - 2 45	+1 22
	7-8/IV/69	K.				
HX 3629	1 HR 5287	103a-0 qr	2 14 42	14 44	5 28,5 5 30.5	+0 38
	2 HR 5378	"	2 15 03	15 05	5 49,5 5 51.5	+0 42
	3 HR 5396	"	3 15 15	15 18	6 01.5 6 04.5	+0 52
	4 HR 5470	"	8 15 40	15 48	6 26.5 6 34.5	+0 59
	5 HR 5664	"	4 16 01	16 05	6 47,5 6 51.5	+0 48
	6 HR 5661	"	8 16 14	16 22	7 00.5 7 08.5	+1 04
	7 HR 5670	"	14 16 37	16 51	7 23.5 7 37.5	+1 28
	8 HR 5708	"	5 17 05	17 10	7 51.5 7 56.5	+1 47
	9 HR 5649	"	2 17 29	17 31	8 15.5 8 17.5	+2 20
	8-9/IV/69	K.				
	10 HR 4889	103a-0 qr	4 13 28	13 32	4 11 4 15	+0 38
	11 HR 4889	"	3 13 38	13 41	4 21 4 24	+0 47.5
	12 HR 4942	"	2 13 50	13 52	4 33 4 35	+0.45

T.U. = T.A. + 4°

5-1	5	Fe 5		
"	"	"		
"	"	"		
"	"	"		
"	"	"		
"	"	"		
"	"	"		
"	"	"		
"	"	"		
5-1	5	Fe 5	$t_{esp.}$ = 15.2	t_{amb} = 15.3
"	"		15.3	15.3
"	"		15.1	15.1
"	"		15.0	14.9
"	"		15.0	15.0
"	"		15.0	14.9
"	"	CDC	15.0	14.8
"	"	CDC	14.9	14.8
"	"		14.8	14.6
"	4, d, p		17.2	16.9
"	" " "		17.2	16.9
"	" " "		17.1	16.9

				T. S.		T. U.		
	8-9/IV/69 K.							
1 HX 3629	13 HR 4923	103a-Oqr	4	14 10	14 14	4 53	4 57	+1 12
	14 HR 5378	"	2	14 30	13 32	5 13	5 15	+0 09.5
2 HX 3630	1 HR 5771	"	6	15 45	15 51	6 28	6 34	+0 14
	2 HR 5781	"	2	16 01	16 03	6 44	6 46	+0 28
	3 HR 5776	"	3	16 15	16 18	6 58	7 01	+0 43
	4 HR 5961	"	4	16 29	16 33	7 12	7 16	+0 30
	9-10/IV/69 K.							
2 HX 3630	5 HR 4773	103a-Oqr	12	14 00	14 12	4 39	4 51	+1 35
	6 HR 4798	"	4	14 25	14 29	5 04	5 08	+1 51
	7 HR 4844	"	4	14 40	14 44	5 19	5 23	+1 57
	8 HR 5378	"	2	14 58	15 00	5 37	5 39	+0 37.5
	10-11/IV/69 K.							
2 HX 3630	9 HR 4441	103a-Oqr	16	12 01	12 17	2 36	2 52	+0 38
	10 HR 4442	"	8	12 24	12 32	2 59	3 07	+0 57
	11 HR 4578	"	9	12 47	12 56	3 22	3 31	+0 54
	12 HR 4671	"	9	13 09	13 18	3 44	3 53	+0 57
	13 HR 5035	"	2	13 48	13 50	4 23	4 25	+0 28
	14 HR 5378	"	2	14 29	14 31	5 04	5 06	+0 08.5
HX 3631	7-8/IV/69	F+L						
	1 HR 4025	103a-O		10 12	10 18	1 00	1 06	+0 03
	2 HR 4263	"		10 34	10 47	1 22	1 35	-0 13
	3 HR 4327	"		10 55	11 00	1 43	1 48	-0 08

5-1	5		t_{sup} = 17.8	t_{amb} = 16.8	
"	"		17.9	16.7	
"	"	Fe 5	16.6	16.5	
"	"		16.6	16.5	
"	"	CDC	16.5	16.4	
"	"		16.5	16.3	
5-1	4	CDC	17.7	17.4	
"	"	CDC	17.6	17.4	
"	"	CDC	17.5	17.4	
"	2		17.5	17.3	tetto
5-1	4		18.1	18.0	
"	"		18.0	17.9	
"	"		17.9	17.8	
"	"		17.8	17.6	
"	3		17.7	17.5	
"	"		17.5	17.4	
5-1		Fe 5	t_{sup} = 16°	t_{amb} = 16°	

				TS		TU		
	7-8/IV/69	F+L						
HX 3631	HR 4369	103a0		11 14	11 31	2 02	2 19	+ 0 10
	HR 4599	"		11 51	11 53	2 39	2 41	- 0 09
	"	"		11 55	11 59	2 43	2 47	- 0 04
	7-8/IV/69	F+L		TS		TU		
HX 3632	HR 4817	103a0		0 50	0 52	3 38	3 40	+ 0 13
	HR 4817	"		0 54	0 59	3 42	3 47	+ 0 19
	8-9/IV/69	F+L						
	HR 3413	103a0		8 40	8 49	23 24	23 33	+ 0 10
	HR 3831	"		8 58	9 17	23 42	0 01	- 0 27
	HR 4025	"		9 33	9 40	0 17	0 24	- 0 35
HX 3633	HR 4263	103a0		11 02	11 15	1 46	1 59	+ 0 15
	HR 4369	"		12 10	12 27	2 54	3 11	+ 1 03
	22/23 IV 69	F+L						
HX 3634	HR 4025	103a0		10 31	10 37	0 20	0 26	0^h 22
	HR 4025	"		10 39	10 51	0 28	0 40	0^h 33
HX 3635	HR 4369	103a-0		11 25	11 43	1 14	1 32	0^h 19
	HR 4817	"		12 05	12 07	1 54	1 56	-0^h 32
	"	"		12 08	12 13	1 57	2 02	-0^h 28
	Ver pág 152							
HX3635A	HR 5008	"		12 52	13 05	2 41	2 54	-0^h 17
HX 3636	25-26 IV 69	LG						
	HR 3501	103a0	9	10 23	10 32	0 00	0 09	+ 1 40
	"	"	16	10 37	10 53	0 14	0 30	+ 1 58
	"	"	29	10 53	11 22	0 30	0 59	+ 2 20
	HR 4185	103a-0	2	11 34	11 36	1 11	1 13	+ 0 56

5-1		Fe 5^s	t.esp. 16°	t.amb. 16°	
			t.esp. 15°5	t.amb. 15°5	
5-1			t.esp. 18°.5	t.amb: 18°.5	
		Fe 5^s			
		Fe 5^s			
		Fe 5^s	t.esp. 17°5	t.amb: 17°.5	
5-0		Fe 0^s.5 ; 3^s.0	t.esp. 17°	t.amb: 17°	
		Fe 0^s.5			
			t.esp 17°	t.amb. 17°	Ver la p.
5-1	3	Fe 3 ^{s}	t.esp 19°	t.amb 19°	152.
"	"	"			
"	"	"			

				T. S.		T. U.		A. h. m.
	25-26/IV/69 LG							
HX3636	HR 4185.	103a-0	6	11 40	11 46	1.17	1.23	+1 04
	" .	"	11	11 48	11 59	1.25	1.36	+1 14
	HR 4519.		2	12 23	12 25	2.00	2.02	+0 40
	" .		5	12 28	12 33	2.05	2.10	+0 46
	" .		9	12 35	12 44	2.12	2.21	+0 55
	27-28 IV-69 LG					Corr$_n$ = +4^m		
HX3637	HR 3241.	103a-0	7	9.17	9.34	22 42	22 49	+1 07
	" .	"	12	9.26	9.38	22 51	23 03	+1 19
	" .	"	11	9.39	9.57	23 04	23 22	+1 35
	HR 4089.	"	1	11.14	11.12	0 39	0 40	+0 49
	" .	"	3	11.14	11.17	0 42	0 45	+0 53
	" .	"	6	11.19	11.25	0 47	0 53	+1 00
	HR 4185.	"	3	11.33	11.36	1 01	1 04	+0 55
	"	"	6	11.40	11.46	1 08	1 14	+1 04
	"	"	11	11.48	11.59	1 16	1 27	+1 14
	HR 4519.	"	2	12.12	12.14	1 40	1 42	+0 28
	" .	"	4	12.16	12.20	1 44	1 50	+0 34
	" .	"	8	12.22	12.30	1 52	2 00	+0 42
	25-26/IV/69 K.							
HX3638	HR 5378.	103a-0 qz	2	14 52	14 54	4 29	4 31	+0 32
	27-28/IV/69 K.							
	2 HR 5378.	"	2	15 05	15 07	4 34	4 36	+0 45
	5-6/V/69 K.							
	3 HR 5378.	"	2	14 29	14 31	3 26	3 28	+0 09

5-1	3	Fe 35	t_{sup} 19°	t_{amb} 19°	
"	"	"	"	"	
"	"	"	"	"	
"	"	"	"	"	
"	"	"	"	"	
				Corr = 0	Corr = +4^{m}
"	5	Fe 0,5		22 46	22 53 22 42-22 49
"	"	"		22 55	23 07
"	"	"		23 08	23 26
"	"	"		0 43	0 44
"	"	"		0 46	0 49
"	"	"		0 51	0 57
"	"	"		1 05	1 08
"	"	"		1 12	1 18
"	"	"		1 20	1 31
"	"	"		1 44	1 46
"	"	"		1 48	1 54
"	"	"		1 56	2 04
5-1	3	Fe 0,5		t_{amb} = 18.7	F_{chim} = 6.5
"	3			15.0	"
"	3			12.0	"

				T. S.		T. V.		A. h. m.
	5-6/II/1969 L.G							
HX3639	HR 4089	103a-O	1	12.05	12.06	102	103	+1 43
	"	"	3	12.07	12.10	104	107	+1 46
	"	"	6	12.11	12.17	108	114	+1 52
	HR 4185	"	3	12 38	12 41	135	138	+2 00
	"	"	6	12 44	12 50	141	147	+2 08
	"	"	11	12 53	13 04	150	201	+2 19
HU	6-7/V/69	k.						
HU3640	1 HR 5687	103a-E	16	16 30	16 46	5 25	5 41	+1 22
3641	2 HR 6420	"	22	17 38	18 00	6 33	6 55	+0 33
3642	3 HR 6788	"	30	18 38	19 08	7 33	8 03	+0 45
	28-29/IV/69	B+M						
HU3643	HR 4327	103a-O	60m	12 32	13 36	1 56	3 00	+1 56
3644	HR 5049	"	162	13 56	16 43	3 21	6 10	+1 53
	6-7/V/69	B+M						
HU3645	HR 3605	103a-O	33m	9 31	10 06	22 25	22 59	+0 46
3646	HR 4185	" "	126	11 06	13 17	23 59	2 10	+1 32
3647	HR 5049	" "	99m	13 31	15 12	2 24	4 05	+0 58
	8-9/V/69	B+M						
HU3648	HR 4185	103a-O	126	12 46	14 53	1 37	3 44	+3 10
	11-12/II/69	F+L						
HX3649	HR 4599	103a-O	2	11 55	11 57	0 28	0 30	+0 06

F-1	5	Fe 0,5	t_{sup} = 11°	t_{amb}
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
$A=\frac{25}{40}$; $L=R+\frac{32}{40}$	5	Ne 1^m		t_{amb} = 14,7
25-7	"	"		14,5 L: 40-33=7
"	5 d	"		14,1
$A=\frac{17}{40}$, $L=2^R$	5	Fe = 3^s		t_{amb} = 18°5
"	"	"		
"	5	Fe = 3^s		t_{amb} = 15°1
"	"	"		
"	"	"		
"	5	Fe = 3^s		t_{amb} = 16°4 HR 4185
		Fe 2^s		t_{amb} = 17°5

	11-12/II/69	F+L		TS		TU		km.
HX 3649	2 HR 4599	103a-O	4"	11 59	12 03	0 32	0 36	−0 01
	3 HR 4847	"	8	12 27	12 35	1 00	1 08	−0 03
	4 HR 5008	"	13	12 50	13 03	1 23	1 36	−0 19
	5 HR 5105	"	4	13 13	13 17	1 46	1 50	−0 18
HX 3650	1 HR 5260	103a-O	4	13 47	13 51	2 20	2 24	−0 11
	2 HR 5260	"	8	13 54	14 02	2 27	2 35	−0 02
	3 HR 5355	"	12	14 54	15 06	3 27	3 39	+0 43
	4 HR 5359	"	2	15 20	15 22	3 53	3 55	+1 03
	5 HR 5624	"	9	15 34	15 43	4 07	4 16	+0 32
	6 HR 5892	"	0.5	15 58	15 58.5	4 31	4 31.5	+0 09
	7 HR 5892	"	1	15 59	16 00	4 32	4 33	+0 10
HX 3651	12-13/II/69	A+L						
	1 HR 3241	103a-O	9"	10 22	10 31	22 52	23 01	+1 13
	2 HR 3241	"	14"	10 32	10 46	23 02	23 16	+1 26
	3 HR 3241	"	21.5	10 56.5	11 18	23 22	23 48	+1 54
	4 HR 3448	"	5.0	11 34	11 39	0 04	0 09	+2 57
	5 HR 3448	"	11"	11 40	11 51	0 10	0 21	+3 06
	6 HR 3448	"	16"	11 53	12 09	0 23	0 39	+3 22
	7 HR 4897	"	40"	12 23	12 34	0 53	0 54	−0 30
	8 HR 4897	"	11.8	12 25	12 27	0 55	0 57	−0 27
	9 HR 4897	"	4"	12 28	12 32	0 58	1 02	−0 23
	7-8/V/69	K.						
HU 3652	4 HR 6153	103a-E	6	17 28	17 34	6 16	6 22	+1 01

Fe 2s

Fe 2s

Fe 2s

tamb. 14°2

Fe 1s

tamb = 16°8

tamb = 14°7

Fe 1s

25-7 3

Ne 1m

tamb = 13.9

				T.S.		T.U.		
	7-8/V/69	K.						
Hu 3653	5 HR 6027	103a-E	(4)	18 25	18 29	7 13	7 17	+2 17
	8-9/V/69	K.						
Hu 3654	1 HR 6112	103a-E	(10)	18 26	18 36	7 13	7 23	+2 08
3655	2 HR 6944	"	(11)	19 06	19 17	7 53	8 04	+0 43
	9-10/V/69	K.						
Hu 3656	3 HR 5685	103a-E	(6)	16 12	16 18	4 56	5 02	+1 00
3657	4 HR 6179	"	(30)	17 25	17 55	6 09	6 39	+1 04
3658	5 HR 6545	"	(50)	18 11	19 01	6 55	7 45	+1 03
3659	6 HR 7145	"	(10)	19 31	19 41	8 15	8 25	+0 41
	11-12/V/69	K.						
Hu 3660	8 HR 6477	103a-E	(12)	18 28	18 40	7 02	7 14	+1 10
3661	1 HR 6953	"	(30)	19 18	19 48	7 52	8 22	+1 02
	12-13/V/69	K.						
Hu 3662	2 HR 6002	103a-E	(24)	17 40	18 04	6 07	6 31	+1h 02m
3663	3 HR 6952	"	(48)	19 03	19 51	7 30	8 18	+0 57
3664	4 HR 7021	"	(11)	20 17	20 28	8 44	8 55	+1 42
	13-14/II/69	M+B						
Hu 3665	HR 4185	103a-O	128	11 24	13 32	23 49	1 59	+1 49
Hu 3666	HR 5049	"	167	13 51	16 38	2 16	5 03	+1 50

25-7	3	Ne 1m		t amb = 13.7	
25-7	3	Ne 7m		t amb. = 15.8	
"	"	"		15.6	
25-7	4	Ne 1m	con diaf. C	t amb. = 16.4	
	5	"		15.5	
"	"	"		15.0	
	"			15.1	
25-7	5d.	Ne 1m		t amb. = 12.5	
	"	"		12.0	
25-7	5	Ne 1m		t amb. = 12.5	
"	"	"		12.6	
"	"	"		12.6	
A = 17/40 , L = 2 + 20/40	5	Fe = 3s		T. amb = 14°.4	128m
"	"	"			167m.

	20-21/V/69 K.			T.S.		T.U.		A.h.m.
HU3667	1 HR 5167	103a-E	(30)	14 57	15 27	2 56	3 26	+1 29
3668	2 HR 5250	"	(12)	15 46	15 58	2 45	3 57	+1 56
3669	3 HR 5407	"	(10)	16 12	16 22	4 11	4 21	+1 51
3670	4 HR 5413	"	(18)	16 42	17 00	4 41	4 59	+2 23
	5-6/V/69 K.							
HX 3671	1 HR 5378	103a-Ogr.	2	15 05	15 07	4 02	4 04	+0 45
	7-8/V/69 K.							
	2 HR 5378	"	2	15 49	15 51	4 40	4 42	+1 29
	8-9/V/69 K.							
	3 HR 5378	"	4	16 53	16 57	5 40	5 44	+2 34
	9-10/V/69 K.							
	4 HR 5378	"	2	15 00	15 02	3 44	3 46	+0 40
	11-12/V/69 K.							
	5 HR 5378	"	3	17 04	17 07	5 37	5 40	+2 44
	12-13/V/69 K.							
	6 HR 5378	"	2	16 30	16 32	4 57	4 59	+2 10
	13-14/V/69 K.							
	7 HR 5378	"	3	17 18	17 21	5 41	5 44	+2 58
	16-17/V/69 K.							
	8 HR 5378	"	10	16 18	16 28	4 32	4 42	+2 02
	20-21/V/69 K.							
	10 HR 5378	"	2	13 52	13 54	1 51	1 53	-0 28

25-7	4d	Ne 20^{1}		+ amb. = 11.4	
	5d	30		11.3	
"	"	30		11.3	
"	"	35		10.6	Fe nubb
5-1	3	Fe 0.5		+ amb. = 11.2	
	2			16.0	
	4			17.3	
	4d			13.4	
	5			13.7	
	5d			14.4	
"	1			18.7	
	5d			12.0	

	13-14/V/69	M+B		T.S		T.U		
HX3672	HR 5961	103a-O	5m	17 40	17 45	6 03	6 08	+ 1 41
	HR 6366	"	20m	17 55	18 15	6 18	6 38	+ 0 58
	HR 6486	"	5	18 26	18 31	6 50	6 55	+ 1 04
	HR 6653	"	25	18 41	19 09	7 12	7 37	+ 1 05
	HR 6988	"	23m	19 30	19 53	7 54	8 17	+ 1 05
HX3673	HR 7510	"	17	20 23	20 40	8 46	9 03	+ 0 46
	15-16/VI/69	K.						
HU3674	HR 6897	103a-E	2	19 14	19 16	5 28	5 30	+0 51
HU3675	HR 7256	"	60	20 00	21 00	6 14	7 14	+ 1 23
HX3676	17-18/VI/69	A				Cor. = -3m		
	1) HR 4089	103a-O	2h 15s	12 50	12 52	23 01	23 03	+ 2 29
	2) "	"	3h 30s	12 53	12 57	23 04	23 08	+ 2 33
	3 "	"	8h 15s	12 57	13 05	23 08	23 16	+ 2 39
	4 HR 4406	"	3h 15s	13 21	13 24	23 33	23 36	+ 1 01
	5 "	"	7h 30s	13 25	13 33	23 37	23 45	+ 1 08
	6 "	"	12h 15s	13 33	13 45	23 45	23 58	+ 1 18
	7 HR 4897	"	1m	13 57	13 58	0 09	0 10	+ 1 04
	8 "	"	1m 55s	13 58	14 00	0 10	0 12	+ 1 06
	9 "	"	3h 45s	14 01	14 05	0 13	0 17	+ 1 10
	17-18/VI/69	A						
HX3677	1 HR 5624	103a-O	6m 15s	14 47	14 53	0 59	1 05	- 0 18
	"	"	11m	14 55	15 06	1 07	1 18	- 0 06
	"	"	-	-		-		
	HR 5269	"	9h 10s	15 44	15 53	1 57	2 06	+ 1 46

5-1	5	Fe-3^5	Tamb 14,2		
"	"	"			
"	"	"	Tamb 13,1		
			"		
"	"	"	"		HQ 7510
25-7	5 p		tamf = 7.3		
"	"		7.4		
				Corr = 0	
5-1	5	Fe-3^5	Tamb 8°	22 58	23 00
"	"	"		23 01	23 05
"	"	"		23 05	23 13
"	"	"	Tamb 7°5	23 29	23 32
"	"	"		23 33	23 41
"	"	"		23 41	23 53
"	"	"	Tamb 7°3	0 05	0 06
"	"	"		0 06	0 08
"	"	"	Tamb 7°3	009	0 13
"	"	"			
"	"	"	Tamb 6°4	0 55	1 01
"	"	"		1 03	1 14
"	"	"	Tamb 6°1		
"	"	"	Tamb 5°6	1 52	2 01

				T. S		T. U Corr.=-5		
HX 3677	17-18/III/69	A						
	NR 5269	103a-O	14h.5	15 54	16 08	2 07	2 21	+1 59
	"	"	23h	16 09	16 32	2 19	2 41	+2 18
	9-10/V/69	A						
HX 3678	HR 4519	103a-O	2h 15s	23 52	23 54	0 34	0 36	+0 10
	"	"	5h 45s	23 55	0 01	0 37	0 43	+0 15
	"	"	10h 30s	0 02	0 13	0 44	0 55	+0 24
HX 3679	9-10/II/69	A						
	HR 2944	103a-O	1h 40s	21 38	21 40	22 20	22 22	+2 03
	"	"	3h	21 41	21 44	22 23	22 26	+2 06
	"	"	5h	21 45	21 50	22 27	22 32	+2 11
	HR 2994	"	3h 40s	22 15	22 19	22 57	23 01	+2 36
	"	"	8h	22 21	22 29	23 03	23 11	+2 44
	"	"	14h	22 30	22 44	23 12	23 26	+2 56
	HR 4089	"	2h 10s	23 00	23 02	23 42	23 44	+0 40
	"	"	3h 40s	23 03	23 07	23 45	23 49	+0 44
	"	"	8h	23 08	23 15	23 50	23 58	+0 51
	6-7/IV/69							
	7/III/69	A						
HX 3680	HR 2956	103a-O	8h	9 53	10 02	23 48	23 55	+1 22
	"	"	16h	10 04	10 23	0 00	0 16	+1 40
	"	"	35h	10 24	10 59	0 24	0 59	+2 13
	HR 4519	"	2h	11 14	11 16	1 06	1h 08	−1 28
	"	"	6h	11 18	11 25	1 11	1 17	−1 20
	"	"	8h.0	11 28	11 36	1 20	1 28	−1 10

5-1	5			Corr. = 0
"	"			2 02 2 16
"	"	Fe 3°	Tank 5°.2	2 17 2 40
			T. S.	
5-1	5	Fe 3°	11 53 11 55	
"	"		11 56 12 02	
			12 03 12 14	
5-1	5	Fe 3°	T. S.	
"			9 39 9 41	
"			9 42 9 45	
"			9 46 9 51	
			10 16 10 20	
			10 22 10 30	
			10 31 10 45	
			11 01 11 03	
			11 04 11 08	
			11 09 11 17	
			T. S.	
5-1	5	Fe 5°	8 57 9 05	
"	"		9 10 9 26	
"	"		9 34 10 09	
"	"		10 16 10 18	
"	"		10 21 10 27	
"	"		10 30 10 38	

				T-S		T-U		
HX 3680	6-7/VI/69	A						
	HR 3241	103a-O	7.5	11 59	12 06	1 52	1 59	+2 52
	"	"	13.5	12 07	12 20	2 00	2 13	+3 03
	"	"	20	12 21	12 41	2 14	2 34	+3 21
	17-18/VI/69	K.						
HU 3681	HR 6471	103a-E	(44)	18 31	19 15	4 44	5 28	+1 29
HU 3682	HR 6897	"	2	19 42	19 44	5 55	5 57	+1 19
HU 3683	HR 7059	"	28	20 04	20 32	6 17	6 45	+1 34
HU 3684	HR 7470	"	42	20 58	21 40	7 11	7 53	+1 42
HU 3684A	HR 6153	103a-O	29-30/6/69	B				
	29-30/VI/69	K.						
HU 3685	HR 7710	103a-E	4	20 20	20 24	5 41	5 45	+0 12
HU 3686	HR 8865	"	28	21 38	22 06	6 59	7 27	-1 25
HU 3687	HR 8988	"	16	22 22	22 38	7 43	7 59	-1 10
HU 3688	HR 9016	"	18	22 58	23 16	8 19	8 37	-0 40
	1-2/VII/69	M+HL						
HX 3689	HR 4405	103a-O	6	12 46	12 52	22 01	22 07	+1 26
	"	"	11	12 57	13 08	22 12	22 23	+1 40
	HR 4703	"	17	13 34	13 52	22 48	23 06	+1 22
	HR 4981	"	25	14 05	14 30	23 18	23 43	+1 18
HX 3690	HR 5482	"	27	15 46	16 13	0 59	1 26	+1 17
	HR 5723	"	23	16 52	17 15	2 05	2 28	+1 42
	HR 6109	"	20	17 29	17 49	2 40	3 00	+1 14
	HR 6745	"	10	17 58	18 08	3 09	3 19	-0 03

5-1	5		Fe 5s	T. 1.
"	"			11 02 11 09
"	"			11 10 11 23
"	"			11 24 11 44
25-7	4d	1	Ne 27s	t amb. = 3,5
"	" "	2	"	3,3
"	" "	3	"	2,9
"	" "	4	"	2,6
25-7	5	1	Ne 27s	t amb. = 4,9
"	"	2	"	5,4
"	"	3	"	5,4
"	"	4	"	5,7
5-1	4		Fe 3s	t amb 11,4
"	"			
"	"			
"	"		Fe 3s	
"	4		Fe 3s	
"	"			
"	"			t amb. 10,5
"	"		Fe 3s	

HR 5482
5723
6109
6745

				T. Δ.		T. U.		
	15-16/7/69	H + HL						
HX 3691	HR 4520	103a-0	2m	13 56	13 58	22 17	22 19	+2 13
	"	"	4m	13 59	14 03	22 20	22 24	+2 17
HX 3692	HR 5345	"	20m	16 17	16 38	0 38	0 59	+2 10
	27-28/7/69	H + HL						
HX 3693	HR 5531	103a-0	3m	15 35	15 38	23 05	23 08	+0h 48m
HX 3694	HR 6492	"	20m	18 41	19 04	02 11	02 34	1h 28
	HR 6745	"	18m	19 16	19 34	02 45	03 03	1h 19
	HR 6913	"	50m	19 55	20 45	03 23	04 13	1h 54
	3/4-8-69	F						
HX 3695	HR 6129	103a-0	3	16 39	16 42	23 24	23 27	+0 14
	"	"	6	16 44	16 51	23 29	23 36	+0 21
	HR 6153	"	2	17 01	17 03	23 46	23 48	+0 31
	"	"	5	17 05	17 10	23 50	23 55	+0 37
	HR 6234	"	5	17 18	17 23	0 03	0 08	+0 34
	"	"	12	17 24	17 36	0 09	0 21	+0 43
	HR 6561	"	30s	18 14	18 14.5	0 59	0 59.5	+0 38
	"	"	1	18 15	18 16	1 00	1 01	+0 39
HX 3696	HR 6879	103a-0	15s	18 46	18 46.2	1 31	1 31 15	+0 24
	"	"	15s	18 47	18 47.2	1 32	1 32 15	+0 25
	HR 7059	"	10	19 05	19 15	1 50	1 00	+0 25
	"	"	18	19 17	19 35	2 02	2 20	+0 41
	HR 7431	"	10	19 50	20 00	2 35	2 45	+0 21
	"	"	20	20 01	20 21	2 46	2 06	+0 37

Anotar cámara junto con ranura

120 Å/mm	5-1	3	Fe 3^S		f cam
"	"	"		taub 8°	6.5
"	"	f	"		"
120 Å/mm	5-1		Fe 2^S	taub 18.5	"
"	"			taub 17.5	"
"	"				"
"	"				"
120 Å/mm	5-1		Fe 3^S		
					HR 6561
	"		Fe 3^S	taub = 11°5	
120 Å/mm	"				

				TS		TU		Δh medio
	16-17/VIII/69	F						
HX 3697	HR 6234	103a-O	7m	17 49	17 56	23 59	0 06	+ 1 07
	HR 6802	"	30m	18 13	18 43	0 23	0 53	+ 0 18
	HR 7059	"	20m	18 55	19 15	1 05	1 25	+ 0 21
	HR 7431	"	22m	19 23	19 45	1 33	1 55	− 0 05
	HR 8097	"	4m	20 50	20 54	3 00	3 04	− 0 16
	"	"	7m	20 54	21 01	3 04	3 11	− 0 10
	17-18/VIII/69	H+HL						
HX 3698	HR 5825	103a-O	8m	16 18	16 26	22 25	22 33	+ 0h 43
	"	"	4m	16 27	16 31	22 34	22 38	+ 0h 50
HX 3699	HR 5663	"	27m	17 18	17 51	23 25	23 58	+ 2 21
	HR 6273	"	33m	18 23	18 57	0 29	1 05	+ 1 47
	HR 7292	"	12m	20 44	21 01	2 50	3 10	+ 1 39
	HR 7990	"	8m	21 21	21 30	3 30	3 39	+ 0 35
HX 3700	HR 8060	"	10m	22 36	22 46	4 44	4 54	+ 1 38
	19-20/VIII/69	H+HL						
HX 3701	HR 6380	103a-O	1m	19 41	19 43	1 38	1 40	+ 2 32
	HR 6965	"	37m	20 10	20 47	2 08	2 45	+ 1 56
HX 3702	HR 7707	103a-O	50m	22 10	23 00	4 07	4 57	+ 2 25
HX 3703	HR 8740	"	17m	0 40	1 00	6 38	6 58	+ 1 53
	HR 8907	"	17m	1 17	1 34	7 15	7 32	+ 2 00
	HR 8984	"	8m	1 52	2 01	7 50	7 58	+ 2 17
	21-22/VIII/69	F						
HX 3704	HR 6802	103a-O	20m	18 30	18 50	0 25	0 45	+ 0 30
	HR 7059	"	10m	19 05	19 15	1 00	1 10	+ 0 25
	HR 7431	"	10m	19 25	19 35	1 20	1 30	− 0 04

120 Å/mm	5-1	5	Fe 3s	t amb 10°	F. cám 6.5
"	"	"	"	"	"
"	"	"	"	"	"
"	"	"	"	"	"
"	"	"	"	"	"
"	"	5	Fe 3s		"
120 Å/mm	5-1	5	Fe 2s	t amb 11°.6	"
"	"	"	"	"	"
"	"	"	"	t amb 10°	"
"	"	"	"	"	"
"	"	"	"	"	"
"	"	"	"	"	"
"	"	5		t amb 9°.4	"
"	5-1	3		t amb 8°.9	"
"	"	"	"	"	"
"	"	"	"	t amb 7.5	"
"	"	"	"	t amb 6.3	"
"	"	"	"	"	"
"	"	"	"	"	"
120 Å/mm	5-1	5	Fe 2s	t amb 9°.2	F. cám. 6.5
"	"	"	"	"	"
"	"	"	"	"	-0^h04^m

			TS		TU		Δ h medio
HX 3704	21-22/VIII/69	F					
	4 HR 7552	103 a-0	19 45	19 52	1 40	1 47	0 00
	5 HR 7575	"	20 00	20 18	1 55	2 13	+ 0 18
HX 3705	1 HR 8097	103 a-0	21 18	21 21	3 13	3 16	+ 0 12
	2 "	"	21 22	21 30	3 17	3 25	+ 0 18
	3 HR 8151	"	21 40	21 45	3 35	3 40	+ 0 23
	4 HR 8278	"	21 51	21 54	3 46	3 49	+ 0 14
	5 HR 8322	"	22 00	22 01	3 55	3 56	+ 0 15
	6 HR 8322	"	22 01	22 03	3 56	3 58	+ 0 16
	7 HR 8728	"	22 20	22 20.3	4 15	4 15.3	- 0 25
	8 "	"	22 21	22 20.2	4 16	4.16.2	- 0 24
	9 "	"	22 22	22 20.5	4 17	4 17.5	- 0 23
HX 3706	1 HR 8911	103 a-0	23 20	23 24	5 15	5 19	- 0 03

				T.A.		T.S.		
	2-3/VIII/69	L G						
HX 3707	1 HR 5941	103 a-0	4	21 12	21.16	18 05	18 09	+ 2 l 12
	2 "	"	7	21 19	21 26	18 12	18 19	+ 2 l 21
	3 "	"	12	21 28	21 40	18 21	18 33	+ 2 l 32
				T.S.		T.A.		
	4 HR 6916	"	3	20 02	20 05	23 10	23 13	+ 1 l 37
	5 "	"	6	20 08	20 14	23 15	23 21	+ 1 l 44
	6 "	"	11	20 15	20 26	23 25	23 36	+ 1 l 53

120 Å/mm 5-1 t. amb. 9°. Foco 6.5

120 Å/mm 5-1 4 Fe 2^5

4 Fe 2^5 t amb 9°.0

120 Å/mm – Fe 2^5 se nubló – Foco 6.5

	T. U.		A. h. m.
120 Å/mm	Fe 1/2 S	1 12	1 16	+ 2 10
		1 19	1 26	+ 2 19
		1 28	1 40	+ 2 30
		3 09	3 12	+ 1 34
		3 15	3 21	+ 1 42
		3 22	3 33	+ 1 52

				T.S.		T.U.		A. h m
Hu 3708	26-27/8/69	B.						
	HR 6153	103a-O	60	18 20	19 20	23 52	0 52	+ 2 19
Hu 3709	HR 7552	"	126	20 20	22 26	1 50	3 56	+ 1 33
Hu 3710	HR 8151	"	72	23 15	23 55	4 50	5 30	+ 2 32
	30-31/8/69	L. G				T.A. Corr. = +4m		
Hx 3711	HR 5941	103a-O	1	18 14	18 15	19 30	19 31	+ 2h 18m
		"	2	18 17	18 19	19 33	19 35	+ 2h 21
		"	3.5	18 21	18 24.5	19 37	19 40.5	+ 2h 26
	HR 6204	"	1.5	19 00	19 01.5	20 15	20 16.5	+ 2h 15
		"	3.5	19 05	19 08.5	20 20	20 23.5	+ 2h 23
		"	7.5	19 28	19 35.5	20 43	20 50.5	+ 2h 48
	HR 6916	"	1	19 45	19 46	21 00	21 01	+ 1h 17
		"	3	19 47	19 50	21 02	21 05	+ 1h 19
		"	6	19 52	19 58	21 07	21 13	+ 1h 26
	HR 8137	"	3	21 31	21 34	22 47	22 50	+ 0h 16
	28-29/VIII/69	F				T.U.		
Hx 3712	HR 5892	103a-O	30s	16 45	16 45.5	22 10	22 10.5	+ 0h 56
	"	"	2m	16 46	16 48	22 11	22 13	+ 0h 58
	"	"	1m	16 55	16 56	22 20	22 21	+ 1h 05
	"	"	3m	17 03	17 06	22 28	22 31	+ 1h 15
	HR 6129	"	5m	17 15	17 20	22 40	22 45	+ 0 51
	4-5/IX/69	F						
Hx 3713	HR 8410	103a-O	17m	22 18	22 35	3 18	3 35	+ 0h 23m
	HR 8722	"	18m	22 54	23 12	3 54	4 12	+ 0h 09m
Hx 3714	HR 8137	"	15m	23 24	23 39	4 24	4 39	+ 2h 16m

40 Å/mm		4	Fe : 5^s	t. amb	10°	f. cam.
"	17/40 – 2^R + 20/40	"	" "	"	9°	12.5
"		"	" "			"
"	" "	se nubló	" "		7°.5	"
					T. U.	
120 Å/mm			Fe : ½ s		12°.5	23 34 23 35
						23 37 23 39
						23 41 23 44,5
						0 20 0 21.5
						0 25 0 28.5
						0 48 0 55,5
						1 05 1 06
						1 07 1 10
						1 12 1 18
						2 51 2 54
120 Å/mm	5-1	3	Fe 1^s	t amb –	11°	Fcám: 6.5
		se nubló –	Nota: en esta placa los tiempos de exposición son estimativos, por fallas en el movimiento fino.			
120 Å/mm	5-1	4	Fe 1^s	t amb –	11°.4	Fcám: 6.5
			Fe 1^s			

Desde 5.X.69 T.U. = T.A. + 3h

	16/17-X-69	B		T.S.		T.U.		A h m.
Hu 3715	HR 596	103a-0	36m	2 01	2 37	4 13	4 49	+0 18
Hu 3716	HR 612	"	45m	3 12	3 57	5 18	6 03	+1 31
Hu 3717	HR 1240	"	40m	4 36	5 16	6 44	7 27	+0 57
Hu 3718	HR 1465	"	1m	5 43	5 44	7 55	7 56	+1 10
	21-22-X-69	LG				T.A. corr. -2m		
Hx 3719	HR 8137	103a-0	3	21 49	21 52	20 42	20 45	+0h 34m
	"	"	6	21 56	22 02	20 49	20 55	+0h 42m
	"	"	11	22 05	22 16	20 58	21 09	+0h 54m
	HR 8353	"	} fueron dadas tiempos de exposición demasiado cortos					
	"	"						
	"	"						
	HR 8386	"	3	22 42	22 45	21 35	21 38	+0h 44m
	"	"	5	22 46	22 51	21 39	21 44	+0h 49m
	"	"	11	22 52	23 03	21 45	21 56	+0h 58m
Hx 3720	HR 8919	"	4	23 51	23 55	22 44	22 48	+0h 25m
	"	"	9	23 58	0h 7	22 51	23 00	+0h 35m
	"	"	14	0h 08	0h 22	23 01	23 15	+0h 47m
	HR 9031	"	1.5	0h 31	0h 33	23 24	23 26	+0h 42m
	"	"	4	0h 34	0h 38	23 27	23 31	+0h 46m
	"	"	7.5	0h 39	0h 43	23 32	23 40	+0h 53m
	HR 9108	"	4	0h 52	0h 56	23 46	23 50	+0h 50m
	"	"	8	0h 57	1h 05	23 51	23 59	+0h 58
	"	"	13	1h 06	1h 19	24 00	0h 13	+1h 09m

T. V. = T. A. + 3'

					T.V.		f.cam.
40 A/mm²	5	Fe : 6s	t. amb	9°4C	4 11	4 47	12,5
17/40 ; 2R + 20/40	"						
" "	"	"		9°C	5 22	6 07	"
" "	"	"		8°9	6 46	7 26	"
" "	"	"		9°C	7 53	7 54	"
					T.V.		
110 A/mm²	5	Fe 1s	tamb	15°C	23 40	23 43	
"	"	"			23 47	23 53	
"	"	"			23 56	07 + 0 54	
					T.V.		
"	3 (alcp selected)				0 33	0 36	
"	"				0 37	0 42	
"	"				0 43	0 54	
"	5				1 42	1 46	
"	"				1 49	1 58	
"	"				1 59	2 13	
"	3				2 22	2 24	
"	"				2 25	2 29	
"	"				2 30	2 38	
"	"				2 43	2 47	
"	"				2 47	2 55	
"	"				2 56	3 09	

	23-24/x/69	Z.L.G		T.S.		T.A.		A.hm.
HX 3721	HR 8137	103a-0	3	21h30	21h33	20h13	20h16	+ 0h15
	"		6	21h35	21h41	20h17	20h23	+ 0h21
	"		11	21h42	21h53	20h24	20h35	+ 0h31
	HR 8353	"	1	22h01	22h02	20h44	20h45	+ 0h09
	"	"	2	22h03	22h05	20h46	20h48	+ 0h12
	HR 8386	"	3	22h12	22h15	20h55	20h58	+ 0h14
	"	"	6	22h16	22h22	20h59	21h05	+ 0h19
	"	"	11	22h24	22h35	21h07	21h18	+ 0h30
	HR 8478	"	3	22h41	22h44	21h24	21h27	+ 0h30
	"	"	7	22h46	22h53	21h29	21h36	+ 0h37
	"	"	12	22h55	23h07	21h38	21h50	+ 0h48
	HR 8919	"	4.5	23h38	23h43	22h20	22h24	+ 0h13
	"	"	9	23h45	23h54	22h27	22h36	+ 0h29
	"	"	14	23h56	0h10	22h39	22h53	+ 0h35
HX 3722	HR 9031	"	1.5	0h34	0h36	23h17	23h19	+ 0h45
	"	"	4	0h37	0h41	23h20	23h24	+ 0h49
	"	"	7.5	0h42	0h50	23h25	23h33	+ 0h56
	HR 9108	"	4	0h58	1h02	23h41	23h45	+ 0h56
	"	"	8	1h04	1h12	23h47	23h55	+ 1h04
	"	"	13	1h13	1h26	23h56	0h09	+ 1h16
	28-29/x/69	B.				T.U. corr.=-3m		
Hu 3723	HR 8151	103a-0	66	22 14	23 20	23 40	0 46	+ 1 28
Hu 3724	HR 8949	"	62	0 10	1 12	1 36	2 38	+ 1 07
Hu 3725	HR 596	"	37	2 54	3 31	4 20	4 57	+ 1 12

				T.U.	
110 A/mm	5	Fe 3S	t amb 17°C	23 13	23 16
"	5	"		23 18	23 24
"	5	"		23 25	23 36
				23 44	23 45
				23 46	23 48
				23 55	23 58
				23 59	0 05
				0 07	0 18
				0 24	0 27
				0 29	0 36
				0 38	0 50
				1 21	1 26
				1 28	1 37
				1 39	1 53
				2 17	2 19
				2 20	2 24
				2 25	2 33
				2 41	2 45
				2 47	2 55
				2 56	3 09
				T.U. corr. = 0	
40 Å/mm	5	Fe 6S		23 37	0 43 t. amb. 19.4°C
$A = \frac{17}{40} \cdot L = 2^R + \frac{25}{40}$	"	"		1 33	2 35 " 17,3°C
"	"	"		4 17	4 54 " 15.6°C

	28-29/X/69	B.		T.S.		T.U. Corr. = -3m		A.h.m
Hu 3726	HR 612	103a-0	37m	3 58	4 35	5 24	6 01	+2 13
Hu 3727	HR 1240	"	35m	4.59	5 34	6 20	6 55	+1 18
Hu 3728	HR 1465	"	4m	5 55	5 59	7 22	7 26	+1 24
	2-3/XI/69	B				Corr. = -2		
Hu 3729	HR 8151	103a-0	65m	22 44	23 49	23 49	0 54	+1 57
Hu 3730	HR 8949	"	61m	0 17	1 18	1 22	2 23	+1 14
Hu 3731	HR 596	"	31m	2 35	3 06	3 40	4 11	+0 50
Hu 3732	HR 612	"	40m	3 33	4 13	4 37	5 17	+1 50
Hu 3733	HR 1240	"	40m	4 35	5 15	5 40	6 20	+0 56
Hu 3734	HR 1465	"	5m	5.36	5 41	6 42.	6 47	+1 05
	19-20/IX/69							
Hx 3735	19-20/IX/69	A+6						
	HR 8137	103a-0	4m	20 04.5	20 08	0 01	0 05	1h:07m E.
	"	"	8m 55s	20 12	20 19	0 09	0 16	1:01 E.
	"	15 "	13m.3	20 19	20 34	0 16	0 31	0:50 E.
	HD 173370	"	8m	20 47	20 55	0 44	0 52	2:07 0.
	HD 177756	"	1m	21 15	21 16	1 12	1 13	2:13 0.
X	HR 7437	"	2m	21 32	21 34	1 29	1 31	2:02 0.
	"	"	4m.8	21 37	21 42	1 34	1 39	2:06 0.
	9-10/XI/69	"	8m.8	21 42	21 51	1 39	1 48	2:15 0.
Hx 3736	9/10-XI-69	A						
	HR 1313	103 a-0	3m	13 30	13 33	0 09	0 12	0:37 E
	"	"	4m.8	13 34	13 39	0 13	0 18	0:33 E
	"	"	9m.3	13 40	13 50	0 19	0 29	0:24 E.

40 Å/mm	5	Fe = 6^S		T. U.	
A = 17/40 , L = 2^R + 25/40	"	"		5 21 5 58	t amb. 14°2
" "	"	"		6 22 6 57	t. amb = 13°9
" "	"	"		7 18 7 22	" 13°6C
40 Å/mm				T. U.	
A = 17/40 , L = 2^R + 30/40	5	Fe = 7^S		23 47 0 52	t.a. = 15,8°C
" "	"	"		1 20 2 21	= 14,5°
" "	"	"		3 38 4 09	13°C
" "	"	"		4 36 5 16	= 12,5°C
" "	"	"		5 38 6 18	12,4
" "	"	"		6 39 6 44	12.1°C
				h. m.	
110 Å/mm	5	Fe = 2^S		− 1 11	Tamb = 13°4
	"			− 1 01	
	"			− 0 50	
	"		= HR 7040	+ 2 07	Tamb = 13°2
	"		= HR 7236	+ 2 11	Tamb 13°2
	"			+ 2 00	" 13°0
	"			+ 2 06	" 12°7
	"			+ 2 13	
				h. m.	Tamb. 13°6
110 Å/mm	5	Fe 2^S		− 0 39	Tamb = 12°8
	"			− 0 34	
	4			− 0 26	Tamb = 13°0

20-21/VIII/69

				T. S		T. U.		Δ h m
HX 3737	HR 5967	1032-0	1m.10s	17 41	17 42	23 36	23 37	+ 1 40
	"	"	3m	17 45	17 48	23 40	23 43	+ 1 45
	"	"	7m	17 49	17 56	23 44	23 51	+ 1 51
	HR 8137	"	3m	18 34	18 37	0 29	0 32	− 2 41
	"	"	6m	18 39	18 45	0 34	0 40	− 2 35
	"	"	13m	19 05	19 18	1 00	1 13	− 2 05
HX 3738	HR 6912	"	13m	20 19	20 32	2 14	2 27	+ 1 50
	"	"	19m	20 32	20 51	2 27	2 46	+ 2 06
	"	"	35m	20 53	21 28	2 48	3 23	+ 2 35
	HR 8141	"	6m	22 32	22 38	4 27	4 33	+ 1 18
	"	"	9m.5	22 46	22 55	4 41	4 50	+ 1 34
	"	"	16m.5	22 57	23 13	4 52	5 08	+ 1 48
	HR 9031	"	1m.5	01 57	01 59	7 52	7 54	+ 2 08
	"	"	4m.5	02 00	02 05	7 55	8 00	+ 2 12
	"	"	7m.6	02 08	02 16	8 03	8 11	+ 2 22
HX 3739	HR 9108	"	4m.5	02 51	02 56	8 46	8 51	+ 2 50
	"	"	9m	02 57	03 06	8 52	9 01	+ 2 58
	"	"	14m	03 06	03 20	9 01	9 15	+ 3 09

31/VIII − 1/IX /69

31-1/VIII/69

HX 3740	HR 5931	1032-0	12m	18 35	18 47	23 47	23 59	+ 2 46
	"	"	17m.5	18 55	19 13	0 07	0 25	+ 3 09
	"	"	–	—				
	HD 142250	"	9m	19 25	19 34	0 37	0 46	+ 3 37
	HR "	"	15m	19 35	19 56	0 47	1 02	+ 3 49

110 Å/mm	ν	Fe 25			Tab= 7.7
	"				
	"				Tab 7.6
	"				
	"				Tab 6.9
	"				
	4	"			Tab 6.4
	"	"			Tab. 6.2
	"				
	"				Tab. 6.2
	"				
	"				
	"				
	"				
	"				
	"				
	"	"			Tab. 6.1
	"	"			Tab. 5.9
	"				
110 Å/mm	ν	Fe 25			
	"				Tab= 12.9
	"				
	"				
	"		= HR 5910		Tab 12.7
	"		11		

31/VIII - 1/IX/69

HX 3740	31-1/VIII/69	A+6		T.S		T.U		Δ h. m	
	HD 142250	103a-0	22m	19 51	20 13	103	125	+4 09	
	HR 8141	"	5m.5	21 51	21 57	303	309	+0 37	
	"	"	9m	21 58	22 07	310	319	+0 46	
	"	"	14m	22 08	22 22	320	334	+0 58	
	HR 8137	"	3m.5	22 26	22 30	336	340	+1 11	
	"	"	7m	22 30	22 37	340	347	+1 17	
	"	"	13m	22 38	22 51	348	401	+1 28	

25-26/VIII/69

HX 3741	25-26/VIII/69	A+6		HX 3740 A ; 1-IX-69 ; HR 9087 ; A					
	HR 8313	103a-0	2m.5	17 33	17 36	2308	2311	+3 24	
	"	"	3m.8	17 37	17 42	2312	2317	+3 29	
	"	"	9m.5	17 44	17 54	2319	2329	+3 38	
	HR 7437	"	1m.8	19 00	19 03	0 35	0 38	-0 32	
	"	"	4m	19 04	19 09	039	044	-0 27	
	"	"	7m.6	19 09	19 18	044	053	-0 20	
	HR 7664	"	4m	19 31	19 35	106	110	-0 29	
	"	"	9m.2	19 36	19 45	111	120	-0 22	
	"	"	15m	19 47	20 02	122	137	-0 08	

HX 3741A 14-15/IX/69 HD 34511 · HX 3741B 14-15/IX/69 Ver la

6-7/XI/69 F+L

HX 3742	HR 8202	103a-0	21	22 32	22 53	2319	2340	+1 17	
	HR 8293	"	25	23 05	23 30	2353	017	+1 36	
HX 3743	HR 323	"	41	2 00	2 41	3 47	328	+1 15	
	HR 595	"	1	2 48	2 49	3 35	336	+0 48	
	HR 710	"	13	2 59	3 12	346	359	+0 41	

110 Å/mm	5	Fe 2^5		
	"		= HR 5940	Tau 12°.1
	"			Tau 11°.9
	"			
	"			
	"			Tau 11°.9
	"			
	"			Taus 11°.8
110 Å/mm	5	Fe 2^5		
	"			Taus 10
	"			
	"			
	"			Taus 9°.4
	"			
	"			
	"			Taus = 9°.3
	"			
	"			Taus 9°.1

pag. 152. HX 3741 C; Ver la pag. 152.

110 Å/mm	4	Fe 2^5	
	"		
	"		
	"		
	"		

Hu

Hu 3744	13-14/11/69	B.		T. S.		T. U.		
	HR 8949	103a-0	45m	0 28	1 13	0 48	1 33	+1 17
	17-18/11/69	M+HL						
HX 3745	HR 606	103a-0	37m	2 29	3 10	2 33	3 13	+0 48
	HR 901	"	20m	3 23	3 43	3 26	3 47	+0 35
	HR 980	"	14m	3 58	4 12	4 01	4 15	+0 51
	HR 1456	"	28m	4 59	5 37	5 03	5 41	+0 54
	25-26/11/69	M+HL						
HX 3746	HR 462	103a-0	25m	2 17	2 41	1 50	2 15	+0 54
	HR 652	"	18m	3 10	3 28	2 43	3 01	+1 07
	HR 802	"	19m	4 00	4 16	3 30	3 49	+1h 28
	HR 837	"	8m	4 32	4 40	4 05	4 13	+1h 51
	HR 1557	"	44m	5 00	5 44	4 32	5 16	+0h 32
	30-1°/XI-XII/69	B.						
Hu 3747	HR 596	103a-0	36	3:10	3 46	2 22	2 58	+1 27
Hu 3748	HR 612	"	45	4 00	4 45	3 12	3 57	+2 19
Hu 3749	HR 1240	"	45	5 02	5 47	4 14	4 59	+1 26
Hu 3750	HR 1465	"	7	6 12	6 19	5 25	5 32	+1 42
Hu 3750A	28-29/11/69	M+HL		Vedi pag 152.				
HX 3751	HR 359	103a-0	32	2 12	2 44	1 32	2 04	+1 16
	HR 781	"	10	3 12	3 23	2 32	2 43	+0 39
	4-5/12/69	B						
Hu 3752	HR 596	103a-0	56	2 50	3 46	1 46	2 42	+1 17

40 A/mm					
	4	Fe = 6 s			t. amb: 21.5°C
	se nubló				
110 A/mm	4	Fe 3 s			tamb 19°,9
"	"				18°,2
"	3 nublado				
"	4				16°,7
110 A/mm	4	Fe 3 s			tamb 22,6
	"				
	"				
	"				21.5
40 A/mm	5	Fe = 7 s.			t. amb: 18,7
	"	"			" 17°C
	"	"			" 16°C
	"	"			" 15°C
					Ver p. 152
110 A/mm	3 muchoriento	Fe 3 s			tamb 21,3
"	"				" 19,1
40 A/mm	4	Fe = 7 s			t. amb = 26°C
	se nubló				

				T.S.		T.U.		A.h m.
	11-12/12/69	B						
Hu 3753	HR 596	103a-0	36m	2 31	3 09	1 05	1 43	+0 48
Hu 3754	HR 612	"	51	3 30	4 21	2 04	2 55	+1 52
Hu 3755	HR 1240	"	47m	4 38	5 25	3 13	4 00	+1 03
Hu 3756	HR 1465	"	10m	5 49	5 59	4 23	4 33	+1 21
	13-14/12/69	B.						
Hu 3757	HR 596	103a-0	36m	2 58	3 34	1 19	1 55	+1 15
Hu 3758	HR 612	"	45	3 55	4 40	2 16	3 01	+2 14
Hu 3759	HR 1240	"	46	4 57	5 43	3 19	4 05	+1 21
Hu 3760	HR 1465	"	7	6 05	6 12	4 26	4 33	+1 35
	14-15/12/69	B						
Hu 3761	HR 596	103a-0	42	1 40	2 22	23 58	0 40	+0 00
Hu 3762	HR 612	"	45	2 36	3 27	0 55	1 46	+0 55
Hu 3763	HR 1240	"	52	3 50	4 42	2 08	3 00	+0 17
Hu 3764	HR 1465	"	7	4 59	5 06	3 18	3 25	+0 29
	15-16/12/69	B.						
Hu 3765	HR 596	103a-0	36m	1 51	2 27	0 04	0 40	+0 08
Hu 3766	HR 612	"	45	3 20	4 09	1 33	2 21	+0 39
Hu 3767	HR 1240	"	48	4 34	5 22	2 47	3 35	+0 59
Hu 3768	HR 1465	"	7m	5 36	5 43	3 50	3 57	+1 06
	2-3/XII/69.	F+L						
HX 3769	HR 8969	103a-0	2m	0h 33	0h 35	23 38	23 40	+0 55
	"	"	5m	0 35	0 40	23 40	2345	+0 59
	HR 77	"	4m	0 48	0 52	23 53	2357	+0 31

40 Å/mm	5	Fe . 7^s		t.amb. 24.9
"	"	"		23.5
"	"	"		23.6
"	"	"		22.7
	se nubló			
"	5	"		t.amb.- 22.3
"	"	"		20.6
"	"	"		20.3
"	"	"		19.6
"	4	"		24.5
"	"	"		21.7
"	5	"		21.9
"	5	"		21.5
40 Å/mm	5	Fe = 7^s		t.amb.: 26.8
"	"	"		" 25.5
"	"	"		" 25.5
"	"	"		" 24.7
110 Å/mm	5-1	Fe 1^s	t amb . 22°1	F. cám. 6.5
"				

2-3/XII/69 F+L

				T.S.		T.U.		
Hx 3769	4 HR 77	103a-0	6	0h52	0h58	23 57	0 03	+0 36
	5 HR 370	"	8	1 06	1 14	0 11	0 19	−0 04
	6 "	"	13	1 17	1 30	0 22	0 35	+0 10
Hx 3770	1 HR 595	103a-0	1	2 19	2 20	1 24	1 25	+0 19
	2 "	"	2	2 20	2 22	1 25	1 27	+0 20
	3 HR 963	"	1	2 37	2 38	1 42	1 43	−0 33
	4 "	"	5	2 39	2 44	1 44	1 49	−0 29
	5 HR 1173	"	2	3 15	3 17	2 20	2 22	−0 30
	6 "	"	5	3 18	3 23	2 23	2 28	−0 25
	7 HR 1139	"	15	3 30	3 45	2 35	2 50	−0 05
Hx 3771	1 HR 1423	103a-0	6	4 03	4 09	3 08	3 14	−0 42
	2 HR 1423	"	10	4 10	4 20	3 15	3 25	−0 33
	3 HR 1508	"	10	4 35	4 45	3 40	3 50	−0 03
	4 HR 1772	"	12	4 52	5 04	3 57	4 09	−0 22
	20-31/XII/69	A						
Hx 3772	1 HD 19548	103a-0	8m.7	3 59	4 08	1 14	1 23	+0 55
	2 HD 32990	"	7m.2	4 22	4 30	1 37	1 45	−0 41
	3 HD 32991	"	12m.5	4 48	5 00	2 03	2 15	−0 12
	4 HD 35708	"	2m.3	5 05	5 07	2 20	2 22	−0 20
	5 HD 27742	"	2m.5	5 09	5 11	2 24	2 26	+0 48
	6 HD 37795	"	15m	5 13	5 13	2 28	2 43	[redacted] 0 26
Hx 3773	1 HR 1801	"	16m.0	6 47	7 03	4 02	4 18	+1 33
	2 HR 1960	"	17m.5	7 30	7 47	4 45	5 02	+2 09

110 Å/mm 5-1	4				Fcám. 6.5
		Fe 1ª	t.amb. 19°6		
110 Å/mm 5-1		Fe 1ª.			
		Fe 1ª			
10 Å/mm 5-1	4	Fe 1ª			
		Fe 1ª			Fcám: 6.5
1101 Å/mm	4	Fe 2ª	tamb.		
	4		28°	HR 944	
	4		27°.5	HR 1659	
	5		27° 2	HR 1660	
	5		27° 2	HR 1810	
	5		26° 8	HR 1375	
	5		26° 7	HR 1956	-0 26
	5		26° 7		
	5		26° 5		

6-7/I/70

				TS		TU		
	6-7/1/70	M+HL						
HX 3774	HR 2163 ·	103a-0	16m	7 00	7 16	3 46	4 02	+1 02
HX 3774A	Ver la pag. 152.	B.		HX 3774B Ver la pag. 152.		HX 3774C Ver la p		
	16-17/1/70							
Hu 3775	HR 1240 ·	103a-0	39m	5 09	5 48	1 16	1 55	+1 30
	19-20/1/70	B.						
Hu 3776	HR 1240 ·	103a-0	45m	3 52	4 37	23 49	0 34	+0 16
Hu 3777	HR 1465 ·	"	6m	5.09	5.15	1 05	1 11	+0 39
	17-18/I/70	K.						
Hu 3778 1	HR 2148 ·	103a-E	(12)	6 05	6 17	2 09	2 21	+0 08
	19-20/I/70	K.						
Hu 3779 1	HR 1895 ·	"	(12)	6 03	6 15	1 59	2 11	+0 38
	20-21/I/70	K.						
Hu 3780 4	HR 1911 ·	"	(16)	6 04	6 20	1 56	2 12	+0 37
3781 5	HR 2206 ·	"	(30)	6 54	7 24	2 46	3 16	+0 59
3782 6	HR 2875 ·	"	(12)	8 08	8 20	4 00	4 12	+0 46
3783 7	HR 3301 ·	"	(13)	8 45	8 58	4 37	4 50	+0 32
3784 8	HR 3302 ·	"	(18)	9 12	9 30	5 04	5 22	+1 01
	22-23/I/70	K.						
Hu 3785 1	HR 1788 ·	103a-E	(3)	6 06	6 09	1 51	1 54	+0 45
3786 2	HR 1792 ·	"	(20)	6 26	6 46	2 11	2 31	+1 13
3787 3	HR 1861 ·	"	(11)	7 10	7 21	2 55	3 06	+1 45
3788 4	HR 1868 ·	"	(11)	7 45	7 56	3 30	3 41	+2 19

110 Å/mm	3	Fe 3 seg		t amb 23°	se nubló

pag. 152 . HX 3774 D ver la pag. 152 . HX 3774 E ; HX 3774 F ; HX 3774 G

40 Å/mm	4	Fe 7°			
	se nubló				
4 Å/mm	5	Fe 7°		t. amb 27°C	
"	"	"		" 26°C	
			F col = 25.0		
40 Å/mm 25-7	4	Ne 25°	F cám = 12.5	t amb. = 24.6	e
" "	5	Ne 25°	"	t amb = 25.7	e doble
" "	5	Ne 27°	"	t amb = 24.6	
" "	"	"	"	t amb = 24.4	
" "	"	"	"	t amb = 24.4	
" "	"	"	"	t amb = 24.7	
" "	"	"	"	t amb = 24.6	
" "	5	Ne 25°	"	t amb. = 25.6	
" "	"	"	"	t amb. = 25.4	
" "	"	"	"	t amb. = 25.2	
" "	"	"	"	t amb. = 25.0	

				T. S.		T. U.		
	21-22/I/70	B.						
Hu 3789	HR 612	103a-O	45m	4:32	5:17	0 20	1 05	+2 51
Hu 3790	HR 1240	103a-O	45m	5 33	6 18	1 21	2 06	+1 57
Hu 3791	HR 1465	"	7m	6 36	6 43	2 25	2 32	+2 06
	29-30/I/70	B.						
Hu 3792	HR 1240	103a-O	45m	5 10	5 55	0 30	1 15	+1 34
Hu 3793	HR 1465	"	12	6 18	6 30	1 36	1 48	+1 51
	30-31/I/70	B.						
Hu 3794	HR 1240	103a-O	47m	5:05	6 52	0 16	1 03	+1 30
Hu 3795	HR 1465	"	11m	6 24	6 35	1 36	1 47	+1 56
	27-28/I/70	K.						
Hu 3796	HR 1449	103a-E	18	5 10	5 28	0 34	0 52	+0 47
	29-30/I/70	K						
Hu 3797	HR 2948	103a-E	5	8 17	8 22	3 33	3 38	+0 42
Hu 3798	HR 2956	"	32	8 28	9 00	3 44	4 16	+1 06
	30-31/I/70	K.						
Hu 3799	HR 3420	103a-E	12	9 52	10 04	5 02	5 14	+1 22
Hu 3800	HR 4225	"	28	10 53	11 21	6 03	6 31	+0 21
	31/I-1/II/70	K.						
Hu 3801	HR 1723	103a-E	10	5 38	5 48	0 45	0 55	+0 29
Hu 3802	HR 1849	"	17	6 02	6 19	1 09	1 26	+0 41
Hu 3803	HR 1975	"	20	6 33	6 53	1 40	2 00	+1 01
Hu 3804	HR 1895	"	16	7 18	7 34	2 25	2 41	+1 52
Hu 3805	HR 2128	"	8	8 01	8 09	3 08	3 16	+2 05

40 Å/mm	4	Fe 7^{s}			t. amb. 24.8°
"	"	"			" 24.3
"	"	"			" 24.1
40 Å/mm	4	Fe = 7^{s}			t. amb. 26°C
$A = \frac{18}{40}$; $L = 2^{R} + \frac{20}{40}$	"	"			" 24.9
40 Å/mm	5	Fe = 7^{s}			t. amb. 28.7
$A = \frac{18}{40}$; $L = 2^{R} + \frac{20}{40}$	"	" "			" 27.6
40 $\frac{Å}{mm}$ 32-7	3	Ne 25^{1}		t amb. = 22.2	te nublo
40 $\frac{Å}{mm}$ 32-7	4	Ne 25^{1}		t amb = 23.8	
" " "	4-3	"		" 23.0	te nublo
40 $\frac{Å}{mm}$ 28-7	5	Ne 24^{1}		t amb = 23.9	
"	"	"		" 22.7	
40 $\frac{Å}{mm}$ 28-7	5	Ne 24^{1}		t amb. = 25.9	
"	"	"		" 25.5	
" "	"	"		" 25.3	
" "	"	"		" 25.2	e.
" "	5-4	"		" 25.0	Velo

				TS		TU		Δh medio
	24/3/70	M+HL						
HX3806	HR2163	103a-0	14m	7^h18	7^h34	0^h25	0^h40	+1 20
	HR 2530	"	33m	7^h58	8^h41	1^h10	1^h47	+1 25
	HR 3183	"	19m	9^h10	9^h12	2^h07	2^h18	+1 00
	HR 3588	"	17m	9^h28	9 47	2 34	2 53	+0 38
	25-26/2/70	B.						
Hu 3807	HR1465	103a.0	12m	6 34	6 46	0 06	0 18	+2 07
Hu 3808	HR 4185	"	134m	7 33	9 47	1 05	3 19	−1 59
	2-3/3/70	B.						
Hu3809	HR1465	103a-0	15m	7 32	7 47	0 46	1 01	+3 06
Hu3810	HR 4185	"	130m	8 30	10 40	1 44	3 54	−1 04
	21-22/II/70	K.						
Hu 3811	HR 2937	103a-E	6	7 54	− 8 00	1 39	− 1 45	+0 21
3812	HR 2948	"	6	8 20	8 26	2 05	2 11	+0 46
3813	HR 2949	"	6	8 30	8 36	2 15	2 21	+0 56
3814	HR 3398	"	20	9 20	9 40	3 05	3 25	+0 56
	23-24/II/70	K.						
HU3815	HR 3898	103a-E	10	10 20	10 30	3 55	4 05	+0 37
3816	HR 4250	"	16	10 48	11 04	4 23	4 39	+0 05
3817	HR 4327	"	14	11 35	11 49	5 10	5 24	+0 36
3818	HR 4487	"	12	12 07	12 19	5 42	5 54	+0 37
	17-18/III/70	M+HL						
HX3819	HR 2530	103a-0	33m	8 37	9 10	0 48	1 21	+2 04
	HR 3183	"	15m	9 25	9 40	1 36	1 50	+1 26

120 Å/mm	I-1	4	Fe 3^s		t.amb 27,3
"		"	suspendido a los 10^m de exp. a retomó a las 1^{h}20^m TU		
"		"			t.amb 26,5
"		"	Fe 3^s		
40 Å/mm		4	Fe = 7^s		t.amb 27.3
"		3	"		" 25.4
40 Å/mm		4	Fe = 7^s		t.amb: 29°
"		5	"		" 27.7
40 Å/mm	25-7	5	Fe 24^s	F_{cum} = 12.5	t amb. = 22.5
"	"	"	"	Fcal = 25.0	22.2
"	"	"	"		22.0
"	"	"	"		20.9
"	"	4d	"		24.0
"	"	"	"		23.8
"	"	"	"		23.5 ✓
"	"	"	"		23.3
120 Å/mm	I-1	5	Fe 3^s		t.amb 17°
"		"			

		17-18/III/70 H+HL		TS		TU		t h. medio
HX 3819	HR 3551	103a-0	21m	9 50	10 11	2 01	2 22	+1 07
	HR 3588	"	20m	10 23	10 43	2 34	2 54	+1 35
	HR 4025	"	12m	11 37	11 49	3 48	4 00	+1 30
HX 3820	HR 4395	"	14m	12 10	12 24	4 21	4 35	+0 55
	HR 4600	"	16m	12 36	12 52	4 47	5 03	+0 43
	HR 4599	"	6m	13 20	13 26	5 31	5 37	+1 21
	HR 4629	"	19m	13 50	14 09	6 01	6 20	+1 50
	HR 5008	"	21m	14 40	15 01	6 51	7 12	+1 35
	HR 5077	"	20m	15 21	15 41	7 31	7 51	+0 34
HX 3820A	Ver la p. 154. 24-25/III/70	B.-						
Hu 3821	HR 4185	103a-0	156m	8h 18m	10h 54m	0h 04m	2h 50m	-1 03
Hu 3822	HR 4327	"	126m	11 42	13 48	3 27	5 33	+1 39
Hu 3823	HR 6153	"	69m	14 27	15 28	6 13	4 14	-1 33
	30-31/III/70	B.-						
Hu 3824	HR 4185	103a-0	156m	7 52	10 28	23 14	1 50	-1 29
Hu 3825	HR 4327	"	120m	11 32	13 32	2 54	4 54	+1 26
	2-3/IV/70	B.-						
Hu 3826	HR 4185	103a-0	183m	10:24	13 27	1 33	4 36	+1 16
Hu 3827	HR 5049	"	189m	14:42	17:51	5 52	9 01	+2 52
	5-6/IV/70	B.						
Hu 3828	HR 4327	103a-0	155m	9:00	11:35	23:58	2:33	-0 49
Hu 3829	HR 4185	"	185m	12:29	15:34	3:26	6:31	+3 22

120 Å/mm 5-1	5	Fe 3^s		t amb. 16°
"	"			
"	"	"		
"	"	"		
"	"			t amb 15°,5
"	"			
"	4			
"	"			t amb. 15°
"	"	Fe 3^s		
$L = 2^R + \frac{20}{40}$	5	Fe = 7^s.		t. amb = 18.4 °C
$A = 20/40$	"	"		" = 17.8
C = 40 Å/mm	"	"		" 17.8
40 Å/mm	5	Fe = 7^s		t. amb = 22.3
$L = 2^R + \frac{20}{40}$. $A = \frac{20}{40}$	"	"		" 20.6
40 Å/mm	5	Fe = 9^s.		t. amb = 18°3
$L = 2^R + \frac{20}{40}$. $A = \frac{20}{40}$	nubes	" "		" 15°C
40 Å/mm	5	Fe = 9^s.		t. amb = 17.7
$L = 2^R + \frac{20}{40}$. $A = \frac{20}{40}$	5	" "		" " 14.9

		9-10/IV/70	4+HL		TS		TU		Th medio
HX 3830	HR 3318	103a-0	6m		9 05	9 11	23 47	23 53	+ 0 49
	HR 3537	"	18m		9 29	9 47	0 12	0 30	+ 0 48
	HR 3684	"	11m		10 10	10 11	0 42	0 53	+ 0 50
	HR 3759	"	11m		10 27	10 38	1 10	1 21	+ 1 04
	HR 4102	"	6m		10 46	10 52	1 29	1 35	+ 0 25
	23/24 - IV - 70		F+L						
HR 3831	HR 3034	103a-0	1.5		8 10	8 11 30	22 50	22 51 30	+ 0 24
	"	"	4		8 15	8 19	22 55	22 59	+ 0 30
	HR 3237	"	6		8 53	8 59	23 33	23 39	+ 0 43
	"	"	2		8 39	9 01	23 39	23 41	+ 0 47
	HR 3642	"	2		9 10	9 12	23 50	23 52	+ 0 06
	"	"	1		9 15	9 16	23 55	23 56	+ 0 10
	24/25 - IV - 70		F+L						
HX 3832	HR 3498	103a-0	2		8 09	8 11	22 44	22 46	- 0 36
	"	"	4		8 13	8 17	22 48	22 52	- 0 31
	HR 3593	"	12		8 33	8 45	23 08	23 20	- 0 20
	10/11 - IV - 70		F+L						
HX 3833	HR 3498	103a-0	2		8 50	8 52	23 35	23 37	+ 0 05
	"	"	5		8 53	8 58	23 38	23 43	+ 0 09
	HR 3593	"	12		9 08	9 20	23 53	0 05	+ 0 15
	HR 3858	"	1		9 48	9 49	0 33	0 34	+ 0 08
	"	"	5		9 52	9 57	0 37	0 42	+ 0 14
	HR 4009	"	9		10 09	10 18	0 54	1 03	+ 0 03

120 Å/mm	5-1	4	Fe 3^{s}		t amb. 20,7	f cam 6,5
"	"	"				
"	"	"			t amb 19,8	
"	"	"				
"	"	"	Fe 3^{s}		t amb 19,5	
				T. U.		
120 Å/mm	5-1	4	Fe 1^{s}	23 58	23 59,5	
		"		0 03	0 07	
		"		0 41	0 47	
		"		0 47	0 49	
		"		0 58	1 00	
		"		1 03	1 04	f = 6.5
		3	Fe 1^{s}	23 53	23 55	
		"		23 57	0 01	
		"		0 17	0 29	t amb. 21° f = 6.5
120 Å/mm	5-1	4	Fe 1^{s}	23 26	23 28	f = 6.5
		"		23 29	23 34	
		"		23 44	23 56	
		"		0 24	0 25	
		"		0 28	0 33	
		"		0 45	0 54	
		"				

	10/11-IV-70	F+L	TS		TU		Δt medio
HX3834	HR 4140 · 103-a0	0.5	10 32 30	10 33	1 17 30	1 18	+ 0 02
	" · "	1	10 33	10 34	1 18	1 19	+ 0 02,4
	HR 4018 · "	13	10 46	10 59	1 31	1 44	+ 0 40
	HR 4460 · "	2	11 28	11 30	2 13	2 15	− 0 04
	" · "	5	11 31	11 36	2 16	2 21	+ 0 00
	HR 4621 · "	0.7	11 45	11 45 40	2 30	2 30 40	− 0 22
	" · "	0.3	11 46	11 46 20	2 31	2 31 20	− 0 21
	" · "	0.4	11 47	11 47 25	2 32	2 32 25	− 0 20
	14-15/IV/70						
	14/15-IV-70	A					3 13
HX3835	HR 2451 · 103-a0	$3^{s}5$	9 50	9 50.5	0 16		+ 3 13
	" · "	$1^{m}10^{s}$	9 51	9 52.1	0 17	0 18	+ 3 "15
	HD 52918 · "	$3^{m}20^{s}$	10 01.6	10 09	0 29	0 32	+ 3.0
	HD 63462 · "	$2^{m}20^{s}$	10 25	10 27	0 48	0 50	+ 2.5
	HD 74280 · "	$1^{m}50^{s}$	10 37	10 39	1 00	1 02	+ 2.0
	~~HD 75418~~ · "	$8^{m}50^{s}$	11 01	11 10	1 24	1 33	+ 2.5
	HD 80781 · "	$15^{m}30^{s}$	11 24.5	11 40	1 48	2 03	+ 2.1
	HD 98718 · "	$2^{m}10^{s}$	11 48	11 50	2 11	2 13	+ 2.0
HX 3836	HR 1696 · 103a-0	$1^{m}20^{s}$	8 28	8 29	22 51	22 52	+ 3.15
	" · "	$2^{m}20^{s}$	8 30	8 32	22 53	22 55	"
	" · "	$4^{m}00^{s}$	8 33	8 37	22 56	23 00	+ $3^{h}20^{m}$
	HR 1705 · "	$1^{m}0$	8 47	8 48	23 10	23 11	
	" · "	$1^{h}50^{s}$	8 49	8 51	23 12	23 15	+ $3^{h}40^{m}$
	" · "	$3^{m}10^{s}$	8 52	8 55	23 16	23 19	
	HR 1702 · "	20^{s}	9 06		23 30		+ 4^{h}

T. U.

126 Å/mm	5-1	4	108.5	109	Fe 1^5	t amb ~ 20° f cam = 6.5
"	"	"	109	110		
"	"	"	122	135		
"	"	"	204	206		
"	"	"	207	212		
"	"	"	221	221.7		
"	"	"	222	222,3		
"	"	"	223	223.4	Fe 1^5	

	h.m.m.						
110 Å/mm	+3^{h}13^m	5	011	011.5	Fe 1^5	taus : 14°.8	f cam 6.5
"	+3 15	"	012	013			
							2648
"	+3 07	"	027	030			= HR 2648
"	+2 39	"	046	048			= HR 3034
"	+1 56	"	058	100			= HR 3454
"	+2 21	"	122	131	HD 75416		= HR 3502
"	+2 14	"	145.5	201		taus 15°.7	HR 3717
"	+0 29	"	209	211	Fe 1^5		= HR 4390
"	+3 17	"	2249	2250	Fe 1^5		
"	+3 20	"	2251	2253			
"	+3 24	"	2254	2258			
"	+3 35	"	2308	2309			
"	+3 38	"	2310	2312			
"	+3 41	"	2313	2316			
"	+3 54	"	2327	2327.3			

	14/15-IV-70		A	T.S		T.U		A.h.m.
HX 3836	HR 1702	103a-O	40s	9 07.3	9 08	23 30.	23 30.7	+ 4,0
	"	"	1m	9 09.0	9 10	23 33	23 34	
	HR 1956	"	20s	9 18.0	9 18.3	23 42	23 42.3	+4.0
	"	"	40s	9 18.5	9 19	23 42.5	23 43.	
	"	"	1m	9 19	9 20	23 44	23 45	
	2/3-V-70		M+HL	T.S		T.U		A.H.m.
Hu 3837	HR 4802	IIa-O	29m	13h10m	13h39m	2h18m	2h47m	+0h 48m
Hu 3838	HR 5107	IIa-O	12m	14h33m	14h45m	3h42m	3h54m	+1h 06m
	3-4/V/70	B.-						
Hu 3839	HR 4185	IIa-O	150m	10 34	13 04	23 38	2 08	+ 1 10
Hu 3840	HR 4327	"	141m	13 39	16 00	2 44	5 05	+ 3 43
Hu 3841	HR 6153	"	30m	16 29	16 59	5 33	6 03	+ 0 13
	5-6/V/70		M+HL					
Hu 3842	HR 3975	IIa-O	12m	10h53m	11h05	23 53	0 05	+ 0h 54m
Hu 3843	HR 4359	"	7m	11h46m	11 53	0 46	0 53	+ 0 37m
Hu 3844	HR 4405	"	50m	12 24	13 14	1 24	2 14	+ 1 26
HX 3845	HR 4989	"	20m	1435	1455	3 35	3 55	+ 1 33
	HR 5168	"	10m	1504	1514	4 05	4 15	+ 1 25
	HR 5396	"	11m	1526	1537	4 28	4 39	+ 1 07
	HR 5530	"	23m	1512	1615	4 52	5 15	+ 1 15
	10-11/5/70	B.						
Hu 3846	HR 4827	IIa-O	139	12 15	14 34	0 49	3 14	+ 2 18
Hu 3847	HR 5303	"	126	15 18	17 24	0 57	3 03	+ 2 07

	A.h.m.		T. U.			
110 A/mm	+3 56	5 mm	23 28.3	23 29		taub 15.9	taú: 6.5
"	+3 58	"	23 30	23 31			
"	+3 40	"	23 39	23 39.3			
"	+3 40	"	23 39.3	23 40			
"	+3 41	"	23 40	23 41	Fe 1s		
40 A/mm	5		Fe = 7 sec			t. amb = 18.9	
$L = 2R + \frac{20}{40}$ $A = \frac{20}{40}$			Fe = 7 sec			t. amb = 18.3	
40 A/mm	5		Fe = 8s			t. amb = 19.2	
"	4		"			" 18.8	
"	se nubló		"			" 18.5	
40 A/min	4		Fe = 7s			t. amb = 10.7	
"	4		Fe = 7s			t. amb = 9.9	
"	4		Fe = 7s			t. amb 9.6	
110 A/mm 5-1	4					t amb 8.2	
"	"					t amb 7.7	
"	"						
"	"						
40 A/mm	5		Fe = 7s			t amb.: 13.3	
"	"		"			" " : 9.3	

	9-10/IV/70	F+L		TS		TU		± h medio
HX3848	HR 3523	IIa-O	11m	9 36	9 47	23 18	23 29	+ 0 51
	"	"	17	9 50	10 07	23 32	23 49	+ 1 08
	HR 4629	"	22	10 35	10 57	0 17	0 39	− 1 23
	HR 4847	"	10	11 15	11 25	0 57	1 07	− 1 24
	"	"	15	11 26	11 41	1 08	1 23	− 1 11
	HR 5008	"	22	12 01	12 23	1 43	2 05	− 1 04
HX 3849	HR 5349	"	15	13 20	13 35	3 02	3 17	− 0 50
	"	"	9	13 36	13 45	3 18	3 27	− 0 38
	HD 133518	"	33	13 59	14 32	3 41	4 14	− 0 50
	17-18/VI/70	F+L				Δt = − 3m		
HX 3850	HR 6118	IIa-O	1m	16h49	16 50	3h00	3h01	+ 0 24
	"	"	2	16 51	16 53	3 02	3 04	+ 0 26
	"	"	4	16 54	16 58	3 05	3 09	+ 0 30
	HR 6262	"	5	17 08	17 13	3 19	3 24	+ 0 18
	"	"	9	17 15	17 24	3 26	3 35	+ 0 27
	HR 6334	"	5	17 34	17 39	3 45	3 50	+ 0 33
	"	"	9	17 40	17 49	3 51	4 00	+ 0 41
	HR 6451	"	5	17 58	18 03	4 09	4 14	+ 0 39
	"	"	9m	18 05	18 14	4 16	4 25	+ 0 48
	18-19/6/70	B						
Hu 3851	HR 5671	IIa-O	8m	16 29	16 37	2 34	2 42	+ 1 16
Hu 3852	HR 6153	"	95m	17 35	19 10	3 40	5 15	+ 1 52
Hu 3853	HR 7194	"	7m	19 37	19 44	2 42	2 49	+ 0 40

110 Å/mm en	5	Fe 3ss	t amb - 16°	P/cám. 6.5
"	"			
"	"			
"	"			
"	"	Fe 3s		
"	"	Fe 3s	t amb = 13°5	
"	"			
"	"	Fe 3s		f/cám 6.5
110 Å/mm	5	Fe 3s	t amb = 11°5	
"	"			
"	"			
"	"			
"	"			
"	"		t amb. = 10°	
"	"			
"	"			
"	"	Fe 3s	t amb = 9°	
40 Å/mm	5	Fe= 9s	t. amb = 8.9	
A = 23/40	"	"	" =	
L = 2R + 20/40	"	Fe=7s	t amb = 8°7	

	25-26/6/70	M+H₂		T.S.		T.U		t h medio
Hx 3854	HR 5698	IIa-0	14m	16 06	16 20	1 44	1 58	+0 53
	HR 5825	"	10m	16 32	16 42	2 10	2 20	+0 58
	HR 6109	"	14m	16 50	17 04	2 28	2 42	+0 32
	HR 6243	"	8m	17 19	17 27	2 56	3 04	+0 35
	28-29/6/70	B.						
Hu 3857	HR 5049	IIa-0	201m	14 09	17 30	23 33	2 54	+2 26
Hu 3858	HR 6153	"	88m	17 46	19 14	3 11	4 39	+1 59
Hu 3859	HR 7552	"	135m	19 36	21 51	5 01	7 16	+0 53
	11-12/7/70	A						
Hx 3860	HD 93163	IIa-0	12m	13 34.5	13 46.5	23 09	23 21	+2 50
	"	"	19m.5	13 46.5	14 06	23 21	23 41	+3 10
	HD 98718	"	1m.8	14 22	14 24	23 57	23 59	+3 00
	"	"	3m.5	14 24	14 27.5	23 59	00 03	+3 05
	HD 99556	"	7m.3	14 37.5	14 45	00 14	00 21	+3 10
	"	"	12m.3	14 45.5	14 58	00 21.5	00 34	+3 30
	HD 103192	"	2m.3	15 11.5	15 14	00 47.5	00 50	
	"	"	3m.8	15 14.5	15 18	00 50.5	00 54	+3 30
	HD 120324	"	1m.2	15 39.0	15 40.2	01 13.5	01 15	
	"	"	3m.5	15 40.5	15 44	01 15.5	01 19	
	"	"	5m.5	15 44.5	15 50	01 19.5	01 25	

110 Å/mm	5	Fe 3°	t amb. 9°	fcam 6.5
"	"		t amb 8°,8	
"	"			
"	"	Fe 3°	t amb 8°,5	

40 Å/mm	5	Fe = 7°	t. amb. 7°,9	
A = 23/40	"	Fe = 7°	" 5°.2	
L = 2R + 20/40	"	Fe = 7°	" 5°.2	

		A.h.m.	T.V.			
						= HR 4204
110 Å/mm	5	+ 2 58 = 4°	22 09	22 21	t amb 8°.5	fcam 6.5
"	"	+ 3 13	22 21	22 41		
"	"	+ 3 03	22 57	22 59		= HR 4390
"	4	+ 3 06	22 59	23 03	t amb 8°.2	
"	"	+ 3 15	23 13	23 20		= HR 4415
"	"	+ 3 26	23 21	23 33	" 7°.7	
"	velo	+ 3 21	23 47	23 49		= HR 4552
"	velo	+ 3 25	23 50	23 54	" 7°.7	
"	velo en arrière	+ 1 52	0 15	0 16		= HR 5193
"		+ 1 54	0 16	0 20		
"		+ 1 59	0 20	0 25	" 7°.2	

	11-12/7/70	A		T. S		T. U		Δ h m
HX 3861	HD 125823	IIa-0	1m.8	16 50	16 53	02 26	02 28	
	"	"	3m.2	16 53	16 56	02 29	02 32	+2 40
	HD 129957	"	11m.5	17 08.5	17 20	02 44.5	02 56	+2 30
	"	"	20m.0	17 20.5	17 39.5	02 57	03 15.0	+3.0
	HD 131168	"	51m.5	18 01.5	18 52.0	03 37	04 28.5	+3 30
	HD 136298	"	0m.6	19 03	19 04	04 38	04 39	
	"	"	1m.2	19 04.3	19 05.5	04 39	04 40	+3 40
	HD 142165	"	5m.3	19 35	19 40	05 19.5	05 25	
	"	"	9m.0	19 40.5	19 49.5	05 25.5	05 34.5	+3 40
	12-13/7/70	B						
Hu 3862	HR 5303	IIa-0	120m	15 14	17 14	23 43	1 43	+1 59
Hu 3863	HR 6153	"	73m	17 40	18 53	2 09	3 22	+1 46
Hu 3864	HR 7552	"	154m	19 26	22 00	3 55	6 29	+0 53
	22-23/7/70	M+H$_4$						
HX 3865	HR 6409	IIa-0	16m	18 44	19 00	2 33	2 59	+1 37
	HR 6751	"	43m	19 15	19 58	3 04	3 47	+1 27
	HR 7213	"	20m	20 10	20 30	4 00	4 20	+1 16
HX 3866	HR 7496	"	16m	21 10	21 26	5 00	5 16	+1 36
	HR 7715	"	22m	21 50	22 12	5 39	6 01	+1 50
	24-25/7/70	B						
Hu 3867	HR 6153	IIa-0	88m	17 44	19 12	1 26	2 54	+1 57
Hu 3868	HR 7552	"	143m	19 39	22 02	3 21	5 44	+1 00

	HR	A.h.m.		T.V.				
110 Å/mm =	5378	+229	Fe 4s	124	126	t amb	6°7	f. calm 6,5
"	"	+233		127	130			
" =	5500	+228		142	154	t amb	6°3	
"	"	+244		154	214			
"	—	+336		236	328	"	5°7	
" =	5695	+344		339	340			
"	"	+345		340	341	"	5°7	
" =	5906	+345		409	414			4:09 4:14
"	"	+353		415	424	"	5°6	

velo da avvento

40 Å/mm		Fe: 7s		t. amb:	7°8
"		"		"	7°4
"		"		"	7°6
110 Å/mm	4	Fe 3s.		t amb	12,5 f.calm 6,5
"	"				
"	"			"	12,2
"	3	Fe 3s			"
"	"				"
40 Å/mm	5	Fe: 7s		t. amb.	17°C
"	3	" "		"	15.7

	27-28/7/70	M+HL		T.S.		T.U.		A.H. medio
Hu 3869	HR 588	IIa-0	18m	17h 18m	17h 36m	0h 48m	1h 06m	+1h 39m
	29-30 VII/70	A						
HX 3870	HD 18/869	IIa-0	2m 10s	22 05	22 07	23	25	
	"	"	3m 50s	22 08	22 12	26	30	+2h 40m
	HR 7437	"	4m 30s	22 31	22 35	52	57	
	"	"	8m 00s	22 36	22 44	58	6 05	+3h 00m
	HR 8137	"	6m 00s	23 13	23 19	6 35	6 41	
	"	"	11m 00s	23 19	23 30	6 34	6 23	+1h 40m
	HR 8141	"	9m 00s	23 33	23 42	~~7 07~~ 6 52	7 06	
	"	"	14m 30s	23 42	23 56	7 07	7 16	+2h 10m
	HD 212571	"	2m 15s	0 14	0 16	7 36	7 38	
	"	"	4m 00s	0 17	0 21	7 39	7 43	+2h 00m
	30-31/VIII/70	M+HL						
HX 3871	HR 5396	IIa-0	2m	14 46	14 48	22 06	22 08	+0h 21m
	"	"	5m	14 51	14 56	22 11	22 16	+0h 29m
	"	"	8m	14 57	15 05	22 17	22 25	+0h 37m

10/8/70 Se colocaron capas antireflectantes en los lentes. Se realizaron las pruebas de foco correspondientes obteniendo y para la de 110 Å/mm, 8 . El foco del colim

	1/2/9/70	M+HL						
Hu 3872	HR 6556	IIa-0	15m	19h 09m	19h 24m	0h 16m	0h 31m	+1h 43m

Disp.

42 Å/mm	3 insg. p-d		Fe 9^{s}	t ambiante	11°	
		T.U	A.h.m			
110 Å/mm	4	528	5 30 + 2 44	Fe 4^{s}	t amb	8°8 = HR 7348
"	"	531	5 35 + 2 48			
"	"	554	5 58 + 3 00			
"	"	559	6 07 + 3 07		t amb	8°
"	"	636	6 42 + 1 59			
"	"	642	653 + 2 08		t amb	8°0
"	"	656	705 + 2 21			
"	"	705	719 + 2 32		t amb	7°7
"	"	737	739 + 1 51			= HR 8539
"	"	740	744 + 1 55	c 4^{s}	t amb	7°4

110 Å/mm	4	Fe 3^{s}	t amb 11°7	
"	"			
"	"			

de las cámaras de 20 Å/mm y 40 Å/mm y en las del colimador
-s para la de 20 Å/mm 28.3, para la de 40 Å/mm = 35.0
das se encuentra en 25.0.

20 Å/mm	2 (velo)	Fe 6^{s} (suciedad)	t = 14°

Agregar a la página 130 : 9-10/I/70 ; A;

HX 3774A	HR 944	HI 19548.	HX 3774B	HR 2676	HI 53929.
9-10/I/70	HR 1375	HI 27742.	11-12/I/70	HR 2825	HI 58343.
	HR 1378	HI 27778.		HR 2695	HI 54669.
	HR 1659	HI 32990.		HR 2907	HI 60559.
	HR 1810	HI 35708.		HR 2972	HI 61987.
	HR 2787	HI 57150.		HR 3462	HI 74455.
	HR 3454	HI 74280.		HR 3501	HI 75387.

HX 3623 A Agregar a la pag. 80 ; 29-30/III/69; B

HR 2534 HI 49976.
HR 3151 HI 66255.
HR 3466 HI 74535.

HU 3635A Agregar a la pag. 88; 22-23/IV/69; B.

HR 3447 HI 74195.

HU 3750A Agregar a la pag. 124; 1-XII-69; B.

HR 1465 HI 29305.

HX 3741 B Agregar a la pag. 122; 15-X-69; A.

HR 1121 HI 22920.
HR 1100 HI 22470.
HR 1375 HI 27742.
HR 1141 HI 23300.

Agregar a la página 130:

HX 3774C

8-9/I/70 HR 2787 HD 57150 · (em Hp)
HR 3454 HD 74280 ·

HX 3774D

10-I-70 HR 2669 HD 53744 ·
HR 2413 HD 46885 ·
HR 2433 HD 47247 ·

HX 3774G

10-I-70 HR 1660 ·
HR 1961 ·
HR 2207 ·
HR 2309 ·

HX 3774E

11-12/I/70 HR 3032 HD 63401 ·
HR 3661 HD 79416 ·

HX 3774F

13-14/I/70 HR 2521 HD 49643 ·
HR 2669 HD 53744 ·
HR 1906 HD 37150 ·

HX 3741C

14-15-X-69

Agregar a la pag 122

HR 8137 HD 202671 ·
HR 7040 HD 173370 ·
HR 7035 HD 173117 ·
HR 7236 HD 177756 ·
HR 7415 HD 183656 ·

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f.c. 235
f.c. 7.
a r $12 + 5/40$
l r $11^R + \frac{12}{40}$.

Agregar a la pag. 136:

HX 3820 A
20-21/III/70

HR 1660	HD 32991 ·
HR 2461	HD 47964 ·
HR 2521	HD 49643 ·
HR 3501	HD 75387 ·
HR 3539	HD 76161 ·
HR 4204	HD 93163 ·
HR 4390	HD 98718 ·