

# Control-Oriented Model With Intra-Patient Variations for an Artificial Pancreas

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**Abstract**—In this work, a low-order model designed for glucose regulation in Type 1 Diabetes Mellitus (T1DM) is obtained from the UVA/Padova metabolic simulator. It captures not only the nonlinear behavior of the glucose-insulin system, but also intra-patient variations related to daily insulin sensitivity ( $S_I$ ) changes. To overcome the large inter-subject variability, the model can also be personalized based on a *priori* patient information. The structure is amenable for linear parameter varying (LPV) controller design, and represents the dynamics from the subcutaneous insulin input to the subcutaneous glucose output. The efficacy of this model is evaluated in comparison with a previous control-oriented model which in turn is an improvement of previous models. Both models are compared in terms of their open- and closed-loop differences with respect to the UVA/Padova model. The proposed model outperforms previous T1DM control-oriented models, which could potentially lead to more robust and reliable controllers for glycemia regulation.

**Index Terms**—Intra-patient variations, LPV model, type 1 diabetes, control-oriented model, artificial pancreas.

Manuscript received August 16, 2019; revised December 12, 2019; accepted January 16, 2020. Date of publication January 27, 2020; date of current version September 3, 2020. This work was supported by Nuria (Argentina) and Cellex (Spain) Foundations, by CONICET (PIP-0837), ANPCyT (PICT-3211), and JDRF (2-APF-2019-737-A-N). Funding sources had no active involvement in the development of this work. (Corresponding author: Marcela Moscoso-Vásquez.)

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Digital Object Identifier 10.1109/JBHI.2020.2969389

## I. INTRODUCTION

TYPE 1 Diabetes Mellitus (T1DM) is a chronic disease characterized by an absolute insulin deficit, and therefore, patients rely on exogenous insulin dosage to achieve glucose regulations and avoid complications such as hypo- or hyperglycemia and their long-time adverse effects.

The Artificial Pancreas (AP) is a system conceived to automate the exogenous insulin supply by usually connecting a Continuous Glucose Monitoring (CGM) sensor with a subcutaneous insulin pump through a control algorithm. The core of the AP is the control algorithm, which estimates the amount of insulin to be administered to the patient. The main challenge to achieve good Blood Glucose (BG) control is that each patient can be characterized by nonlinear dynamics with time-varying parameters and responses that change not only from one person to another (inter-subject variability), but also from day to day for the same person (intra-subject variability). Therefore, the control algorithm must be designed with robustness and time-varying properties to make closed-loop control reliable and safe [1]–[3].

Inter-patient variations are mostly related to differences in Insulin Sensitivity ( $S_I$ ), requirements and absorption/action times [1], [4]. These variations are larger than in healthy individuals [5] and preclude the possibility of obtaining a unique control algorithm that works for everyone. In consequence, most recent research efforts are focused on model personalization [1], [2], [6]–[14]. To avoid model identification, these approaches use patient-specific clinical variables like Total Daily Insulin (TDI), Insulin-to-Carbohydrate Ratio (CR) or body weight to individualize the controller's gain. Model Predictive Control (MPC) algorithms are individualized by using patient-specific model parameters or personalizing the MPC cost function weights [15], [16]. Adaptive algorithms (like run-to-run control) that adjust and individualize controller parameters have also been proposed [17]–[25]. It is worth remarking that in the aforementioned control-oriented models no intra-patient variability was embedded into the model structure.

Intra-subject variability is an additional important challenge for the AP. Subject's insulin requirements to control glycemia vary across the daytime [26], attributed to circadian changes in Glucose Tolerance (GT), i.e., the relative amount of glucose taken up by peripheral tissue [27], and  $S_I$  [28], which corresponds to the ability of insulin to stimulate glucose utilization and inhibit its production [29], regulating how sensitive is the body to the effects of insulin. This subject-specific variability is influenced by many factors like meals, stress, sleep architecture,

physical activity, rhythms of counterregulatory hormones, and quality of BG control [3], [8], [30]–[32]. Given that such factors ultimately may be reflected on the patient's  $S_I$ , intra-patient variability can be described by suitable modeling of circadian  $S_I$  variation [26]–[28], [31]. In this regard, intra-patient variations were included in the UVA/Padova metabolic simulator [33]–[35] by associating each *in-silico* subject with one of seven possible variability classes, assigned to a specific time-varying  $S_I$  profile [5], [36]. These profiles were created by modulating  $V_{mx}$ , which governs the insulin-dependent glucose utilization, and  $k_{p3}$ , which regulates the insulin action on the liver, as time-varying parameters. Similar approaches were followed in [22], [37], where sinusoidal deviations of 20% amplitude over the nominal values related to insulin sensitivity and absorption were added for controller testing. In this way, the observed  $S_I$  variation of  $\pm 30\%$  is included [28], but there is no consensus yet on how to model these variations.

Although  $S_I$  variations have been generally considered to test glucose controllers through extensive simulations, better closed-loop performance may be obtained if these variations were included in the controller synthesis stage. Several approaches have been considered in this matter. In [1], [9], the *in-silico* subjects of the UVA/Padova simulator are sorted in four groups according to the average value of their daily CR profile (related to each subject's  $S_I$ ), with a personalized Linear Time Invariant (LTI) model associated with each group. This model is then used as a one-step ahead prediction model to synthesize a customized MPC. However, since LTI models are used, there is a significant loss of information regarding the patient's dynamics, considering its time-varying characteristics.

On a different approach, adaptive control systems consider intra-patient variations by embedding the model in the controller and adjusting controller parameters as experimental data reflects a time-variation in the model dynamics. Other adaptive control systems update the parameters of the model recursively as new data are collected from the system, and use the latest model in the controller [21], [24], or run-to-run control strategies to adapt basal insulin patterns [20], [23], [25], insulin boluses [7], [18], [19], [22], [38], or MPC cost functions [2]. Of these, the works of [18], [19] considered subject's  $S_I$  for assessing the controller's gain, but this  $S_I$  was determined using only some outputs, and therefore, does not characterize the insulin sensitivity of the virtual patient in the traditional sense [19]. On [23], [25] the algorithm is able to adjust intra- and inter-day  $S_I$  variations, by updating CR and basal insulin patterns according to performance indexes computed at the end of each day.

Another approach to cope with intra-patient variability is to compute tight-solution bounds on prediction models. In [32], [39], parametric variations over a glucose-insulin model are used to compute a solution envelope that is used as a prediction model in control structures like MPC. Instead, in [40], a Linear Parameter Varying (LPV) model *set* was obtained to cover both,  $S_I$  variations and dynamic uncertainties, for each patient. From a control design viewpoint, to “cover” intra-patient variations with bounded uncertainty is more conservative than to explicitly include them in the model. The latter embeds these time-varying dynamics in the controller, which could in theory [41], [42], lead to better performance.

$S_I$  parametric variations embedded in the patient's model are considered in [43], where the Medtronic Virtual Patient (MVP) model is identified for ten different subjects based on closed-loop glucose-insulin data and the oral minimal model [44]. Intra-day variations in  $S_I$  related parameters were structured to change during three time-windows inside a 24-hour time period, assuming one value during the first and last time-windows and a different value during the second one.  $S_I$  variations were identified in six of the ten subjects of the study, presenting different starting times and segment duration among them.

Note that these approaches consider a specific  $S_I$  variation profile [43] or average daily  $S_I$  value [1], [4]. Considering that for some subjects parameters can present substantial differences over time, these models would not be able to follow or include such changes. Real-time parametric identification can help improve closed-loop performance. However, the ability of real-time identification algorithms to track time-varying parameters needs to be carefully assessed before their implementation for controller design.

A good control-oriented model should have a structure that allows a well-known, reliable, and numerically robust control synthesis technique to produce a controller that can be implemented in real-time. Considering the time-varying characteristics of the glucose regulation problem, LPV models are good candidates, and can result in LPV or switched LPV (or LTI) control strategies, that can yield better performance for the AP, as presented in [14], [45], [46]. In this regard, in [14], we presented a third-order LPV model that reflects the time-varying and non-linear nature of the glucose regulation problem by an average (over all subjects) structure, including a parameter dependent on the glucose level, which is measured in real-time.

Therefore, this work focuses on developing a model that reflects time-varying  $S_I$  variations within the model, while maintaining a simple structure that allows reliable and robust control synthesis techniques to be used. For this, an extension of [14] that includes  $S_I$  variations is developed, by introducing a second time-varying parameter to its low-order LPV structure. The model now includes intra- and inter-patient variations, and still preserves the possibility of personalizing it based on the 1800-rule, through a procedure that can be carried out in real patients in a non-invasive way.

The paper is organized as follows. In Section II the baseline LPV model [14] is described. Section III presents the procedure to obtain the LPV model with intra-patient variations. Section IV presents the open- and closed- loop evaluation of the model efficiency. Finally, conclusions are discussed in Section V.

## II. MATERIALS AND METHODS

The baseline control-oriented LPV model used in this work is the one developed in [14], [46] that is based on the UVA/Padova metabolic simulator [33]. It has a low-order structure akin to the one presented in [6], where the input corresponds to the subcutaneous insulin infusion (in pmol/min) and the output is the glucose concentration deviation (in mg/dl):

$$G(s) = k \frac{s + z}{(s + p_1)(s + p_2)(s + p_3)} e^{-15s}. \quad (1)$$

An average model was first identified at a glucose concentration  $g = 235$  mg/dl, where the 1800-rule is rendered correct for the nonlinear model [14], [46]. Then, its domain of validity was extended by allowing parameter  $p_1$  to vary with  $g$  in order to fit the average Bandwidth (BW) of the linearized models at different glucose values, keeping all other parameters fixed ( $z = 0.1501$ ,  $p_2 = 0.0138$  and  $p_3 = 0.0143$ ). Pole  $p_1(g)$  was approximated by the following piecewise-polynomial function:

$$p_1(g) = q_i g^3 + r_i g^2 + s_i g + t_i$$

$$\text{with } i = \begin{cases} 1 & \text{if } g \geq 300 \\ 2 & \text{if } 110 \geq g < 300 \\ 3 & \text{if } 65 \geq g < 110 \\ 4 & \text{if } 59 \geq g < 65 \\ 5 & \text{if } g < 59 \end{cases} \quad (2)$$

and with coefficient values given in Table I.

In this way, a simple manner of replicating changes in the model's gain according to the glucose value was obtained, since the BW and Low-Frequency Gain (DC Gain) of the model are related by the time-varying parameter  $p_1$ .

The median glucose-dependent model (1) can then be tuned to a specific subject by adjusting parameter  $k$  with his/her TDI as follows. For each subject  $\#j$ , the LPV model at 235 mg/dl is excited with a 1 U insulin bolus and the value of  $k_j$  is determined so that the glucose drop matches the one predicted by the 1800-rule ( $1800/TDI_j$ ). Here, it is worth remarking that parameter  $k_j$  is time-invariant, but specific to each subject.

A state-space representation of the personalized LPV model (defined as LPV $_g$  model) is given by:

$$\begin{aligned} \dot{x}(t) &= A(p_1)x(t) + Bu(t - \tau) \\ y(t) &= Cx(t) \end{aligned} \quad (3)$$

with  $\tau = 15$  min,  $u$  and  $y$  the insulin delivery and glucose signals, and

$$\begin{aligned} A(p_1) &= \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -p_2 p_3 & -(p_2 + p_3) \end{bmatrix} \\ &+ p_1 \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ -p_2 p_3 & -(p_2 + p_3) & -1 \end{bmatrix}, \\ B &= [0 \ 0 \ 1]^T, \quad C = k_j [z \ 1 \ 0]. \end{aligned} \quad (4)$$

Note that the LPV $_g$  model is affine in parameter  $p_1$ , which is an advantageous characteristic for the design of LPV controllers [47]. Moreover, LPV $_g$  was compared to the UVA/Padova simulator in terms of the Root Mean Square Error (RMSE) and the  $\nu$ -gap metric [48], [49], achieving better performance than control-oriented models presented previously in this field [3], [6], [45]. It is worth noting that this model was used for

TABLE I  
PARAMETER VALUES OF  $p_1(g)$  FROM (2)

$i$	$q_i$	$r_i$	$s_i$	$t_i$
1	0	0	$-3.4321 \times 10^{-6}$	$4.4706 \times 10^{-3}$
2	0	$9.0580 \times 10^{-8}$	$-5.3562 \times 10^{-5}$	$1.1357 \times 10^{-2}$
3	$-4.2382 \times 10^{-8}$	$1.1402 \times 10^{-5}$	$-9.1676 \times 10^{-4}$	$2.5849 \times 10^{-2}$
4	0	$1.7321 \times 10^{-4}$	$-2.3080 \times 10^{-2}$	$7.7121 \times 10^{-1}$
5	0	0	$-2.8336 \times 10^{-5}$	$1.4083 \times 10^{-2}$

controller-design in a recent clinical trial, achieving promising results [50], [51].

### III. PROPOSED LPV MODEL

#### A. Inclusion of Intra-Patient Variations

In this section, an extension of model (4) that includes intra-patient variability is developed — the LPV $_i$  model. The proposed structure is identified from linearizations of the UVA/Padova metabolic model around several operating points defined by steady-state glucose concentrations achieved by only accommodating the insulin infusion rate.

Glucose concentrations in the range [40, 400] mg/dl were considered to span the usual measurement range of CGM sensors, within a non-uniform grid. Since an average structure was pursued instead of specific  $S_I$  values, an Insulin Sensitivity Variation Factor ( $S_{I,VF}$ ) was defined as  $S_{I,VF} = S_I/S_{I,nom}$ , where  $S_{I,nom}$  could be considered as its average daily or basal [52] value.  $S_{I,VF}$  was selected in the range [0.4, 1.7] over a uniform grid with a step of 0.1, to cover the previously observed variations of [40, 60]% around the nominal subject-specific  $S_I$  [5], [22], [53].

For each subject, the operating points ( $g_{op}, S_{I,VF,op}$ ) were defined over each pair ( $g, S_{I,VF}$ ) on the grid. The insulin infusion rate was adjusted accordingly to achieve steady-state conditions at the glucose level  $g_{op}$  when parameters  $V_{mx}$  and  $k_{p3}$  were modulated by  $S_{I,VF,op}$ . Then, as in [14], linearizations of the UVA/Padova model were obtained for each *in-silico* adult of the distribution version of the simulator.

Fig. 1 shows the average variation of the BW and DC Gain for LPV $_g$  and all *in-silico* adults linearized at different  $g$  and  $S_{I,VF}$  values. Note that both BW and DC Gain coincide exactly at  $S_{I,VF} = 1$ .

Given that the DC Gain of model (1) is  $\frac{kz}{p_1 p_2 p_3}$ , and that the BW is independent of  $k$ , the LPV $_g$  model is expanded by making parameter  $k$  dependent on  $g$  and  $S_{I,VF}$  as depicted in Fig. 2. Following this approach, variations of the model's gain due to  $S_I$  changes (see Fig. 1) can be reproduced, without affecting the previous BW fitting.

In this way,  $k$  is used to compensate both inter-patient variations through the 1800-rule and intra-patient variations by making  $k$  change according to a suitable  $S_I$  profile. The latter could be a general profile (such as those in [22], [36], [37]) or a profile obtained from clinical data using the pump/CGM index in [54], or through an estimation based on real-time measurements. This grants flexibility to the selected model structure, so it can be used together with the  $S_I$  profile that best suits subject-specific circadian variations in  $S_I$ , or even considering other factors that



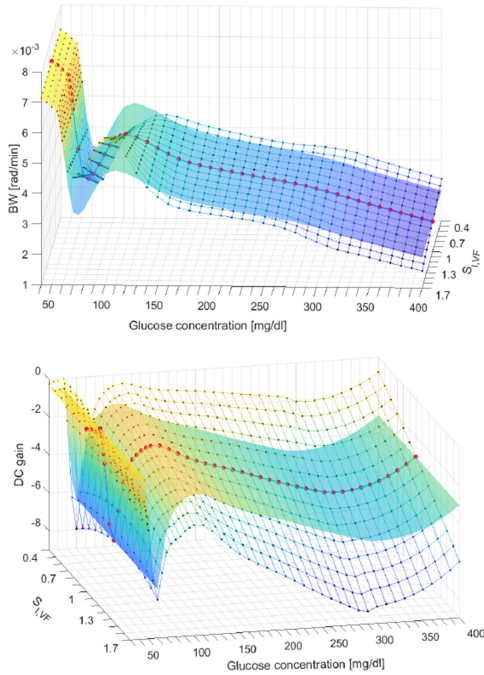


Fig. 1. BW (top) and DC Gain (bottom) of  $LPV_g$  (smooth surface) for all *in-silico* adults from the UVA/Padova simulator linearized at different  $g$  and  $S_{I,VF}$  values (gridded surface). The red dotted line indicates the BW at nominal  $S_{I,VF}$ .

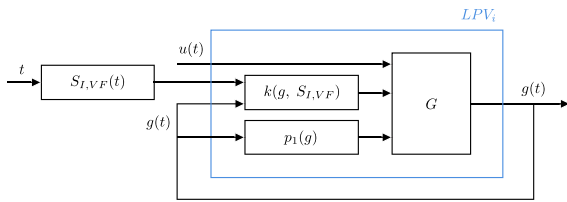


Fig. 2. Average  $LPV_i$  model structure.

influence  $S_{I,VF}$  such as physical exercise or stress [28], [30], [31], [55]–[57].

In order to characterize the dependence of parameter  $k$  on  $g$  and  $S_{I,VF}$ , the definition of the DC Gain of model (1) is used. Here, the observed values for the DC Gain of the linearized models at each  $(g, S_{I,VF})$  pairs (defined as  $DCG_{NL}(g, S_{I,VF})$ ), together with the constant parameters  $p_2$ ,  $p_3$  and  $p_1(g)$  from (2), are used to compute an average value for parameter  $k$ , defined as  $k_{avg}$ :

$$k_{avg}(g, S_{I,VF}) = \frac{p_2 p_3}{z} p_1(g) DCG_{NL}(g, S_{I,VF}) \quad (5)$$

Then, the result was fitted using a piecewise polynomial function as indicated in the Appendix, and presented in Fig. 3.

Note that as shown in Fig. 1, there is an abrupt change at 60 mg/dl. The reason for this discontinuity is that the insulin-dependent glucose utilization in the UVA/Padova simulator is associated with a risk function that increases when glucose decreases below the subject's basal glucose concentration and saturates when glucose reaches 60 mg/dl. To avoid translating

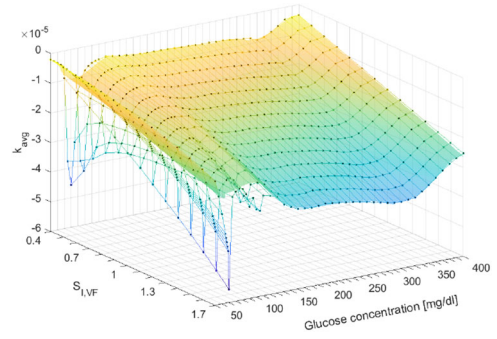


Fig. 3. Parameter  $k_{avg}$  for different values of  $g$  and  $S_{I,VF}$  (gridded surface) and piecewise polynomial function  $k_{avg}(g, S_{I,VF})$  (smooth surface).

this artifact discontinuity to the glucose output, a smooth surface was fitted instead.

In this way, the state-space representation of the average  $LPV_i$  model is similar to (4), but now with the output matrix:

$$C = k_{avg}(g, S_{I,VF}) \begin{bmatrix} z & 1 & 0 \end{bmatrix}. \quad (6)$$

## B. Model Personalization

In Section III, it was shown how  $k$  can be used to tackle intra-patient variability. In this Section,  $k$  is further tuned to reduce inter-patient uncertainty. This model personalization is carried out in a similar way as the one described in [14], i.e., by adjusting model's  $k$  using the 1800-rule.

In this case, a suitable gain  $k^*$  is computed as the gain that makes the  $LPV_i$  model achieve the same glucose drop as the one predicted by the 1800-rule when excited with a 1 U insulin bolus at  $g = 235$  mg/dl and  $S_{I,VF} = 1$ . This point was selected since it was the one at which the 1800-rule was satisfied on average for all the *in-silico* adults [14]. A simple Proportional-Integral (PI) control loop, which modified  $k$  of the  $LPV_i$  model until the model's glucose drop matched the one predicted by the 1800-rule, was used to obtain  $k^*$  for each adult.

Considering that for each subject the DC gain of the model at  $g = 235$  mg/dl and  $S_{I,VF} = 1$  should be  $k^*$ , a subject-specific scaling factor  $k_j$  is computed as  $k_j = k^*/k_{avg}(235, 1)$ , where  $k_{avg}(235, 1) = -1.822 \times 10^{-5}$ . Then, a parameter  $k_s(g, S_{I,VF})$  is defined as  $k_s = k_j k_{avg}$ , with  $k_j$  given in Table II and  $k_{avg}$  the same fitted-surface of 3. Model personalization is thus achieved by replacing  $k_{avg}$  in (6) with parameter  $k_s(g, S_{I,VF})$ . Note that this corresponds to a vertical shifting of the fitted  $k_{avg}$  surface.

Variations of  $k_s(g, S_{I,VF})$  for the average *in-silico* subject, and the most and least sensitive subjects are presented in Fig. 4. Note that the most sensitive subject (Adult #009), whose TDI is the lowest, is associated with the highest scaling factor  $k_j$ , and therefore, higher values of  $k_s$  (in module).

## IV. RESULTS AND DISCUSSION

A good simulation model, i.e., one that fits properly the experimental data, is not necessarily a good candidate to design

TABLE II  
SCALING FACTOR  $k_j$  FOR EACH *IN-SILICO* ADULT

Adult	TDI [U/day]	$k^* \times 10^{-5}$	$k_j$
1	42	-1.7888	0.9818
2	43	-1.7451	0.9578
3	52	-1.4343	0.7872
4	35	-2.1396	1.1743
5	40	-1.8650	1.0236
6	72	-1.0343	0.5677
8	52	-1.4379	0.7892
9	34	-2.2024	1.2088
10	47	-1.5919	0.8737
11	39.9	-1.8864	1.0354

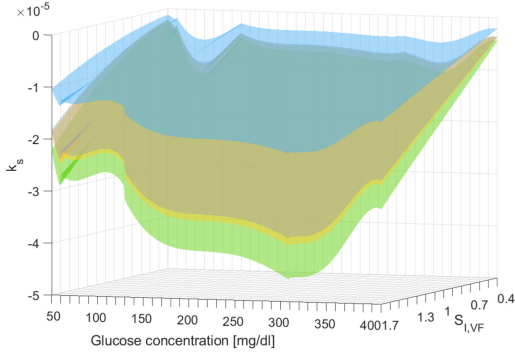


Fig. 4.  $k_{avg}$  (gray surface) and personalized  $k_s$  for the average subject (yellow surface), Adult #006 (blue surface) and Adult #009 (green surface).

controllers [58]. Therefore, in this section, a comparison of both LPV<sub>g</sub> and LPV<sub>i</sub> with respect to the UVA/Padova model is carried out not only for simulation (open-loop) purposes, but also for controller synthesis (closed-loop). No other models are considered here, since in [14] LPV<sub>g</sub> already showed lower closed- and open-loop errors than previous control-oriented models [3], [6], [45].

### A. Open-Loop Comparison

Considering that  $S_I$  varies mostly during the day, the simulations are performed incorporating the time-varying profiles determined in [36]. First, the class 1 profile is analyzed, by maintaining the same  $S_I$  value during the day, but changing its nominal value in the simulator. For each of the 10 *in-silico* subjects of the distribution version of the UVA/Padova simulator, an insulin bolus of 1 U was applied at different operating points to test the personalized LPV<sub>i</sub> and LPV<sub>g</sub> models in comparison with the UVA/Padova nonlinear simulator. Next, the other six profiles were considered.

1) *Fixed  $S_I$  Values (Class 1)*: Fig. 5 presents the time-responses for Adult #009 (most sensitive subject) to a 1 U insulin bolus for multiple  $S_{I,VF}$  values at basal glucose concentrations of 120, 180, and 240 mg/dl. Parameters  $p_1$  and  $k_s$  variations for the LPV<sub>g</sub> and LPV<sub>i</sub> models are also depicted. Note that a better fit is achieved with LPV<sub>i</sub> than with LPV<sub>g</sub> for most  $S_{I,VF}$  values. The reason is that only LPV<sub>i</sub> adjusts its gain to reflect changes in  $S_I$ . In addition, it is worth clarifying that despite the LPV<sub>i</sub> model is an extension of the LPV<sub>g</sub> model, its

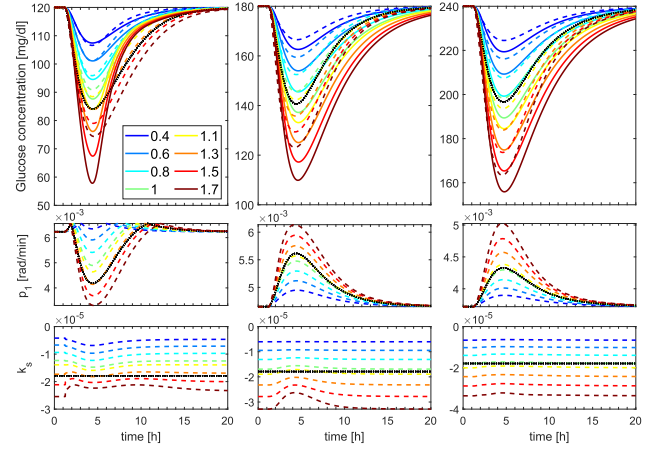


Fig. 5. Responses to a 1U insulin bolus starting from 120 mg/dl, 180 mg/dl and 240 mg/dl for Adult #009 at different  $S_{I,VF}$  values for models LPV<sub>g</sub> (dotted black line), LPV<sub>i</sub> (dashed lines) and the UVA/Padova nonlinear model (solid lines). Top: Glucose drop. Middle: Evolution of parameter  $p_1$ . Bottom: Evolution of parameter  $k_s$ .

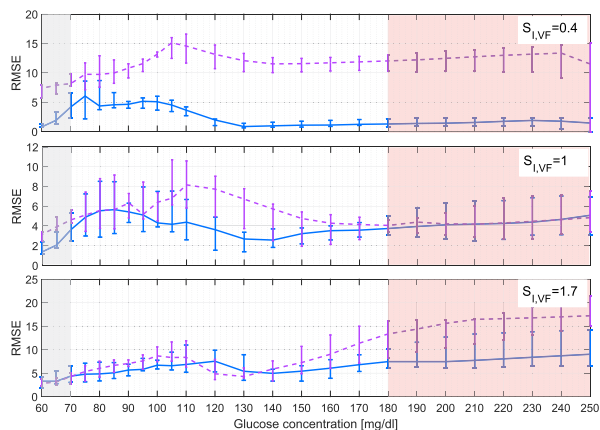
behavior for nominal insulin sensitivity ( $S_{I,nom}$ ) is the same only at 235 mg/dl as an operating point, i.e., the glucose concentration at which they were both identified. For other glucose concentrations, the gain adjustment through variation of parameter  $k_s(g, S_{I,VF})$  generates the differences between both models.

The RMSE between the time-responses of each LPV ( $y_p$ ) and the UVA/Padova model ( $y$ ), for each subject at each operating point on the ( $g, S_{I,VF}$ ) grid, was computed according to the following equation:

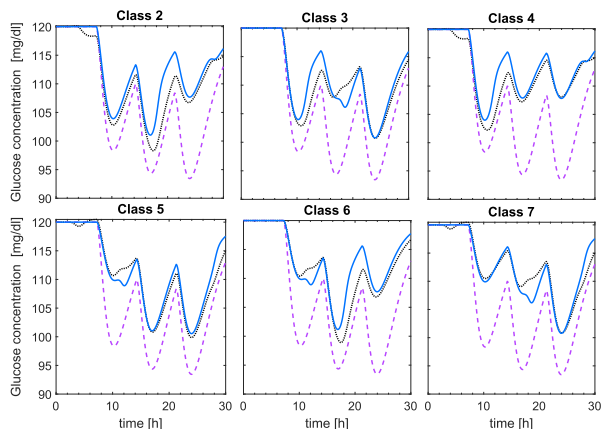
$$\text{RMSE} = \frac{\|y_p - y\|_2}{\sqrt{n_t}} \quad (7)$$

where  $\|\cdot\|_2$  represents the 2-norm, and  $n_t$  the number of points. In order to capture the complete glucose variation at each point,  $n_t = 1200$  points with a sampling time of 1 minute, were selected. In Fig. 6, median values of the RMSE for all 10 *in-silico* adults at different  $g$  and  $S_{I,VF}$  values are shown. Note that a lower RMSE can be obtained with LPV<sub>i</sub> than with LPV<sub>g</sub> for most glucose concentrations. Considering  $S_I$  variations, for the least sensitive case ( $S_{I,VF} = 0.4$ ), LPV<sub>i</sub> outperforms LPV<sub>g</sub> for the whole glucose range. For  $S_{I,nom}$  ( $S_{I,VF} = 1$ ), both LPV models have approximately the same RMSE, except for glucose concentrations around 90–180 mg/dl, where the increased sensitivity of the UVA/Padova model is further adjusted by the variation of the  $k_s$  parameter in LPV<sub>i</sub>. For a glucose concentration of 235 mg/dl, similar errors are observed since, as discussed before, at this point both models are equivalent. For the most sensitive case ( $S_{I,VF} = 1.7$ ), LPV<sub>i</sub> has a similar RMSE as LPV<sub>g</sub> for  $g < 140$  mg/dl, but at higher  $g$  values the difference in the DC Gain between both models becomes larger and LPV<sub>i</sub> provides a better fit.

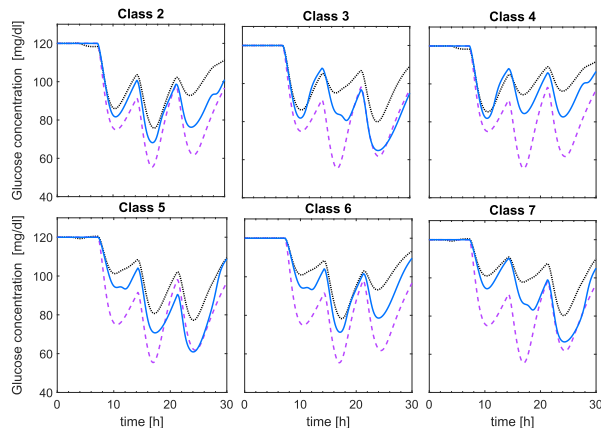
2) *Time-Varying  $S_I$  Profiles (Classes 2–7)*: Fig. 7 and 9 present the time responses for Adult #009 to three insulin boluses in the set  $\{0.5, 1, 1.5\}$  U, applied at 7, 14, and 21 hours, respectively, for different profiles of  $S_I$  variation with a glucose operation point of 120 mg/dl. For these scenarios, the basal



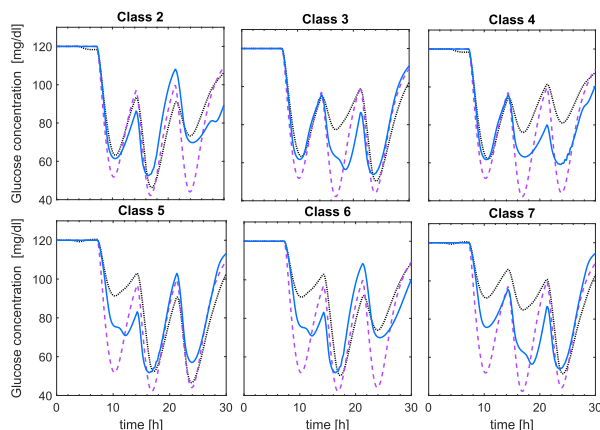
**Fig. 6.** Median RMSE between the time-responses of the personalized  $LPV_g$  (violet dashed lines) and  $LPV_i$  (blue solid lines), as compared with the UVA/Padova nonlinear model to an insulin bolus of 1 U for different  $S_{I,VF}$  values. Top: most resistant case ( $S_{I,VF} = 0.4$ ), middle: nominal case ( $S_{I,VF} = 1$ ), bottom: most sensitive case ( $S_{I,VF} = 1.7$ ). The vertical bars are limited by the 25th and 75th percentiles.



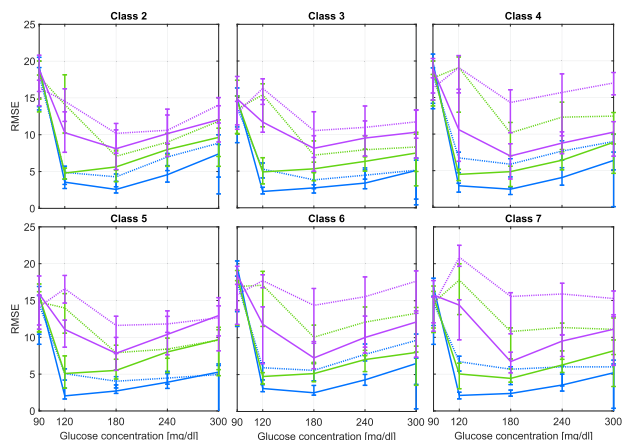
**Fig. 7.** Responses to three 0.5 U insulin boluses starting at 120 mg/dl for Adult #009 with different  $S_I$  profiles for models  $LPV_g$  (dotted violet line),  $LPV_i$  (solid blue lines) and the UVA/Padova nonlinear model (dotted black lines).



**Fig. 8.** Responses to three 1 U insulin boluses starting at 120 mg/dl for Adult #009 with different  $S_I$  profiles for models  $LPV_g$  (dotted violet line),  $LPV_i$  (solid blue lines) and the UVA/Padova nonlinear model (dotted black lines).



**Fig. 9.** Responses to three 1.5 U insulin boluses starting at 120 mg/dl for Adult #009 with different  $S_I$  profiles for models  $LPV_g$  (dotted violet line),  $LPV_i$  (solid blue lines) and the UVA/Padova nonlinear model (dotted black lines).



**Fig. 10.** Median RMSE between the time-responses of the personalized  $LPV_g$  (dashed lines) and  $LPV_i$  (solid lines), as compared with the UVA/Padova nonlinear model to three insulin boluses of 0.5 U (blue), 1.0 U (green) and 1.5 U (violet) for different  $S_I$  profiles. Vertical bars are limited by the 25th and 75th percentiles.

insulin infusion rates were accommodated to maintain steady-state conditions after  $S_I$  changes, as performed in [59]. In these cases, the  $LPV_i$  model is able to reflect the  $S_I$  variation regardless of the  $S_I$  profile or the applied bolus, better than the  $LPV_g$  model. In this way, the  $LPV_i$  model obtains a more accurate representation of the UVA/Padova model, adapted to the subject's individual  $S_I$  profile. Additionally, the same scenario was tested at glucose operating points in the set  $\{90, 180, 240, 300\}$  mg/dl, obtaining the same results as for 120 mg/dl. These values were selected in order to span the complete glycemic range with the simulated glucose traces, bearing in mind that only insulin was considered as input.

The average RMSE between the time-responses of both  $LPV_i$  and  $LPV_g$  models and the UVA/Padova model is shown in Fig. 10. Note that for all  $S_I$  variation classes, a lower RMSE was obtained with the  $LPV_i$  model than with the  $LPV_g$  model.



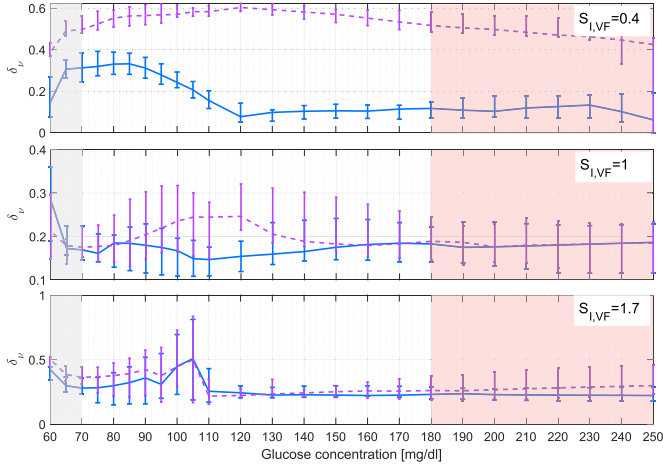


Fig. 11. Median  $\nu$ -gap ( $\delta_\nu$ ) between the linearizations of the UVA/Padova nonlinear model and models  $LPV_g$  (violet dashed lines) and  $LPV_i$  (blue solid lines) for different  $S_{I,VF}$  values. Top: most resistant case ( $S_{I,VF} = 0.4$ ), middle: nominal case ( $S_{I,VF} = 1$ ), bottom: most sensitive case ( $S_{I,VF} = 1.7$ ). The vertical bars are limited by the 25th and 75th percentiles.

### B. Closed-Loop Comparison

In this case, the  $\nu$ -gap distance [48], [49] between each personalized LPV model and the UVA/Padova model linearized at different points of the  $(g, S_{I,VF})$  grid is computed. This metric considers the distance ( $\delta_\nu$ ) between two models regarding their achievable closed-loop performance, without having to design the controllers for each loop.

For LTI models, given a controller  $K$  and a model  $P_1$ , with  $K$  and  $P_1$  transfer matrices, a performance measure/stability margin for the (stable) closed-loop system  $(P_1, K)$  is defined in [48], [49] as:

$$b_{P_1, K} = \left\| \begin{bmatrix} P_1 \\ I \end{bmatrix} (1 - KP_1)^{-1} \begin{bmatrix} -K & I \end{bmatrix} \right\|_\infty^{-1} \quad (8)$$

where  $\|\cdot\|_\infty$  indicates the  $\mathcal{H}_\infty$ -norm. Here, larger values of  $b_{P_1, K}$  correspond to better performance of the feedback system comprising  $P_1$  and  $K$ . The difference between the performances of the nominal model and a perturbed one  $P_2$  for the same controller  $K$  can be quantified through the  $\nu$ -gap, i.e.  $\delta_\nu(P_1, P_2)$ , with  $b_{P_2, K} \geq b_{P_1, K} - \delta_\nu(P_1, P_2)$ . This indicates that the smaller  $\delta_\nu(P_1, P_2)$  the closer their closed loop performances. Considering that if  $P_1$  and  $P_2$  represent alternate models of the same system (the UVA/Padova model and the  $LPV_g$  or  $LPV_i$  for example), a small  $\delta_\nu(P_1, P_2)$  indicates that the differences between both models are negligible from a feedback perspective. Note that for its computation (see [48], [49]), only the plant models are required, and therefore their closed-loop performances can be compared without having to design the controller and compare on a one-by-one basis.

Fig. 11 presents the median  $\nu$ -gap for all 10 adults for three different  $S_{I,VF}$  values, obtaining lower values with  $LPV_i$ , similar to the analysis presented in Section IV-A.

TABLE III

PERCENTAGE OF CASES OF MODEL IMPROVEMENT IN TERMS OF THE RMSE ( $\%RMSE$ ) AND  $\nu$ -GAP ( $\%\nu$ -GAP).  $h_{RMSE}$  OR  $h_{\nu$ -GAP EQUAL TO ONE INDICATE A SIGNIFICANT REDUCTION ON THE AVERAGE RMSE OR  $\nu$ -GAP OBTAINED WITH  $LPV_i$ , CONSIDERING A 5% SIGNIFICANCE. TIME-VARYING  $S_{I,VF}$  VALUES CORRESPOND TO ALL  $S_{I,VF}$  PROFILES THAT WERE CONSIDERED

Adult # j	Constant $S_{I,VF}$		Time-varying $S_{I,VF}$		$\%\nu$ -gap	$h_{\nu$ -gap
	$\%RMSE$	$h_{RMSE}$	$\%RMSE$	$h_{RMSE}$		
1	73.47	1	44.4	0	79.88	1
2	80.92	0	100.0	1	76.32	1
3	74.4	1	55.6	0	74.4	1
4	71.74	1	100	1	63.9	1
5	71.19	1	88.9	1	61.17	1
6	79.5	1	83.3	1	79.81	1
8	80.81	1	100.0	1	71.29	1
9	78.38	1	100.0	1	79.78	1
10	77.94	1	100.0	1	76.63	1
11	84.05	1	100.0	1	79.75	1
All	77.17	1	87.22	1	73.82	1

### C. Overall Comparison

The difference between the RMSE and  $\nu$ -gap obtained with both LPV models was computed for all  $(g, S_{I,VF})$  points considered in Section IV-A1, and all 10 *in-silico* adults, according to:

$$\delta_{\nu, d} = \delta_{\nu, LPV_i} - \delta_{\nu, LPV_g} \quad (9)$$

$$RMSE_d = RMSE_i - RMSE_g \quad (10)$$

In this way, negative values of  $\delta_{\nu, d}$  or  $RMSE_d$  indicate points where  $LPV_i$  outperforms  $LPV_g$ .

A two-sampled t-test was carried out for each *in-silico* adult, to determine if the average RMSE obtained with  $LPV_i$  is lower than the one obtained with  $LPV_g$  at all  $(g, S_{I,VF})$  points and for all the time-varying  $S_I$  profiles considered. The same analysis was performed for the  $\nu$ -gap to determine if including the  $S_I$  variation in the controller design stage could lead to a better closed-loop performance. Test results for each adult and the whole population (row 'All') are presented in Table III, along with the percentage of  $(g, S_{I,VF})$  points in which an improvement over  $LPV_g$  is obtained, both in open- and closed-loop. According to these results, both open-loop and closed-loop metrics show an overall improvement using  $LPV_i$  above 73.8%. It should be taken into account that the comparison measures were computed based on a simulated population and has an average significance. A better and more personalized result could be obtained by using clinical data from the  $S_I$  variations for a particular subject.

To recap, the main result here is the computation of an LPV structure, amenable to controller design. The procedure allows to include both inter- and intra-patient variations maintaining the time-varying characteristics of the system with a control-oriented focus based on real-time measurements and clinical data in a non-invasive way.

The model is able to accommodate variations in  $S_I$ , which are the main cause of this variability. Therefore, the next step would be to couple the model with a  $S_I$  estimator from real-time measurements to include, for instance, exercise or stress influence on  $S_I$ . Alternatively, this variability can be also represented as uncertainty bounds through an invalidation procedure, as the one carried out in [40], using field collected data.

TABLE IV  
PARAMETER VALUES FOR  $k_{avg}(g, S_{I,VF})$  FROM (11)

$n$	1	2	3	4
$\lambda_{1,n}$	$-7.641 \times 10^{-03}$	$5.514 \times 10^{-05}$	$8.356 \times 10^{-05}$	$-2.011 \times 10^{-05}$
$\lambda_{2,n}$	$9.024 \times 10^{-05}$	$-1.186 \times 10^{-06}$	$-2.645 \times 10^{-06}$	$2.942 \times 10^{-06}$
$\lambda_{3,n}$	$4.785 \times 10^{-04}$	$3.262 \times 10^{-05}$	$-5.145 \times 10^{-05}$	$-1.352 \times 10^{-04}$
$\lambda_{4,n}$	$-4.296 \times 10^{-06}$	$-6.907 \times 10^{-07}$	$8.635 \times 10^{-07}$	$7.641 \times 10^{-06}$
$\lambda_{5,n}$	$-3.971 \times 10^{-07}$	$9.342 \times 10^{-09}$	$2.470 \times 10^{-08}$	$-1.323 \times 10^{-07}$
$\lambda_{6,n}$	$-4.243 \times 10^{-05}$	$3.838 \times 10^{-06}$	$5.062 \times 10^{-06}$	$8.139 \times 10^{-05}$
$\lambda_{7,n}$	$1.225 \times 10^{-08}$	$3.270 \times 10^{-09}$	$-4.359 \times 10^{-09}$	$-1.399 \times 10^{-07}$
$\lambda_{8,n}$	$1.885 \times 10^{-07}$	$-3.542 \times 10^{-08}$	$-5.847 \times 10^{-08}$	$-3.266 \times 10^{-06}$
$\lambda_{9,n}$	$-1.966 \times 10^{-10}$	$6.014 \times 10^{-11}$	0	$2.696 \times 10^{-08}$
$\lambda_{10,n}$	$7.718 \times 10^{-10}$	$-3.175 \times 10^{-11}$	$-7.066 \times 10^{-11}$	$2.400 \times 10^{-09}$
$\lambda_{11,n}$	$5.622 \times 10^{-06}$	$-2.428 \times 10^{-06}$	0	$-1.458 \times 10^{-05}$
$\lambda_{12,n}$	$-1.153 \times 10^{-11}$	$-5.211 \times 10^{-12}$	0	$8.254 \times 10^{-10}$
$\lambda_{13,n}$	$-1.546 \times 10^{-08}$	$8.127 \times 10^{-09}$	0	$3.713 \times 10^{-07}$
$\lambda_{14,n}$	$-5.588 \times 10^{-13}$	$3.937 \times 10^{-14}$	0	$-1.575 \times 10^{-11}$

## V. CONCLUSION

In this work, a low-order control-oriented model that includes intra-patient variations and generalizes previous works was proposed. This model depends on two parameters,  $p_1(g)$  and  $k_{avg}(g, S_{I,VF})$ , which in turn are functions of the glucose concentration and insulin sensitivity factors. These parameters can be computed in real-time and allow representing the non-linear dynamics and the intra-patient variations. In addition, the model can also be easily personalized to reduce the inter-patient uncertainty by means of the well-known 1800-rule.

The use of  $S_{I,VF}$  allowed obtaining a general average structure that is not dependent on a particular model that describes changes in  $S_I$ , i.e., it could be used in combination with any real-time  $S_I$  estimator (block  $S_{I,VF}(t)$  on Fig. 2). In this way, other factors influencing the subject's  $S_I$  like stress, exercise, meal size and composition, etc., could be considered in real time to obtain more robust and reliable controllers.

The proposed  $LPV_i$  was compared to the  $LPV_g$  model without the intra-patient variations in terms of its open- and closed-loop characteristics, by means of the RMSE and  $\nu$ -gap, respectively. The proposed  $LPV_i$  showed better performance with smaller errors, highlighting the advantages of including  $S_I$  variations in the model's structure.

## APPENDIX

### AVERAGE PARAMETER-DEPENDENT GAIN

The piecewise polynomial function  $k_{avg}(g, S_{I,VF})$  is fitted as follows:

$$\begin{aligned}
 k_{avg}(g, S_{I,VF}) &= \lambda_{1,n} + \lambda_{2,n} g + \lambda_{3,n} S_{I,VF} + \lambda_{4,n} g S_{I,VF} \\
 &+ \lambda_{5,n} g^2 + \lambda_{6,n} S_{I,VF}^2 + \lambda_{8,n} g S_{I,VF}^2 + \lambda_{7,n} g^2 S_{I,VF} \\
 &+ \lambda_{9,n} g^2 S_{I,VF}^2 + \lambda_{10,n} g^3 + \lambda_{11,n} S_{I,VF}^3 \\
 &+ \lambda_{12,n} g^3 S_{I,VF} + \lambda_{13,n} g S_{I,VF}^3 + \lambda_{14,n} g^4
 \end{aligned}$$

$$\text{with } n = \begin{cases} 1 & \text{if } g \geq 300 \\ 2 & \text{if } 120 \leq g < 300 \\ 3 & \text{if } 45 \leq g < 120 \\ 4 & \text{if } g < 45 \end{cases}$$

with parameters values presented in Table IV.

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