J. Phys. B: At. Mol. Opt. Phys. 35 (2002) 3411-3419

PII: S0953-4075(02)34825-9

New energy levels of the 4s²4p5s, 4s²4p4d and 4s²4p5p configurations of the Kr v spectrum

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Received 8 March 2002, in final form 3 July 2002 Published 7 August 2002 Online at stacks.iop.org/JPhysB/35/3411

Abstract

The spectrum of four-times-ionized krypton (Kr v) has been observed in the 240–2500 Å wavelength range. Three of the four possible levels of the $4s^24p5s$ configuration and two of the three remaining energy level values for the $4s^24p4d$ configurations were determined. Nine of the ten possible levels for the $4s^24p5p$ configuration are also reported. The observed configurations were interpreted theoretically by means of Hartree–Fock relativistic calculations and a least-squares fit of the energy parameters to the observed levels. 111 new classified lines are reported among the $4s^24p^2$, $4s^24p5p$, $4s4p^3$, $4s^24p5s$, and $4s^24p4d$ configurations.

1. Introduction

Energy levels of Kr 1 to Kr xxxv1 were reviewed and compiled by Sugar and Musgrove (1991) and tables of the classified lines of Kr v to Kr xxxv1 were compiled by Shirai *et al* (1995).

Four-times-ionized krypton, Kr v, belongs to the Ge I isoelectronic sequence and has the ground configuration $4s^24p^2$. The spectra of the first, second, third and fourth elements of this sequence were presented in the book *Atomic Energy Levels* (Moore 1971). The As II spectrum was reinvestigated by Li and Andrew (1971) and the Br rv spectrum was revised by Joshi and Budhiraja (1971).

The krypton isonuclear sequence has also been studied in different works by members of the Centro de Investigaciones Opticas Group, La Plata, Argentina and the Campinas Group, São Paulo, Brazil. Reyna Almandos *et al* (1996, 1998) published new energy levels for Kr III and Kr IV. Pagan *et al* (1995) reported the study of the 4s4p4d and 4s4p5s configurations of Kr VI and Raineri *et al* (2000) presented the spectroscopic analysis of the 4p4d configuration of Kr VII. All these experiments were carried out using a discharge tube and a theta-pinch discharge.

0953-4075/02/163411+09\$30.00 © 2002 IOP Publishing Ltd Printed in the UK 3411

Trigueiros *et al* (1989, 1993), and references therein, studied the Kr v spectrum using different spectral sources. These authors presented new energy levels of the $4s^24p^2$, $4s4p^3$, $4s^24p4d$ and $4p^4$ configurations.

In this work we report an extended analysis of the four-times-ionized krypton (Kr v). We have established three new energy levels for the $4s^24p5s$, two for the $4s^24p4d$ and nine for the $4s^24p5p$ configurations. 111 new lines were classified as combinations between levels of $4s^24p^2$, $4s^24p5p$, $4s4p^3$, $4s^24p5s$, and $4s^24p4d$ configurations. Analysis of the experimental data used Hartree–Fock calculation and parametric fit.

Configurations of the type $ns^2npn'p$ have been studied by Kramida *et al* (1999) (n = 2, n' = 3) and Gallardo *et al* (1999) (n = 5, n' = 6) for elements of the same homologous sequence.

The interest in spectroscopic data for rare gases is due to applications in collision physics, laser physics, photo-electron spectroscopy and fusion diagnostics.

2. Experiment

The work is based on photographic recordings of the spectra of krypton between 240 and 2500 Å. We have used two different light sources in our experiment, a discharge tube and a thetapinch discharge. In both cases the energy is fed into the plasma using a capacitor bank, charged from a high-voltage power supply. The discharge tube was built at the Centro de Investigaciones Opticas (CIOp), La Plata, Argentina, to study highly ionized gases (Gallardo *et al* 1989). It is made with a Pyrex tube ending in a quartz window. The electrodes, 20 cm apart, were made of tungsten and covered with indium. The gas pressure was measured by a thermocouple vacuum gauge before and after exposures. The pressure range was varied between 20 and 300 mTorr. Gas excitation was produced by discharging through the tube a bank of low-inductance capacitors varying between 2.5 and 100 nF and charged up to 19 kV. A normal-incidence vacuum spectrograph with a concave diffraction grating of 1200 lines mm⁻¹ was used. The plate factor in the first order is 2.77 Å mm⁻¹. Kodak SWR plates were used to record the spectra. C III, N II and N III (Kelly 1987), O III (Pettersson 1982) and known lines of krypton (Kelly 1987, Shirai *et al* 1995, Raineri *et al* 1998) were recorded as internal standard lines.

The other experimental data were obtained several years ago by two of the authors (JRA and AGT) at the Lund Institute of Technology, Sweden, using the theta pinch discharge. This consisted primarily of a cylindrical discharge tube, excited by an induction coil. The spark gap was pressurized with air. It was ignited by lowering the pressure in the spark chamber by means of a magnetic valve and triggered when the capacitor voltage reached a preset value. The theta pinch device had the following specifications: total capacitance 7.7 μ F, total inductance 76 nH, period of damped oscillation 4.8 μ s. Maximum current at 10 kV discharge voltage is about 100 kA. The repetition rate of the discharge was about 15 min⁻¹ at a capacitor bank voltage of 10 kV. A 3 m normal-incidence vacuum spectrograph with a concave diffraction grating of 1200 lines mm⁻¹ was used. The plate factor in the first order was 2.77 Å mm⁻¹. The spectra were exposed on Kodak SWR plates and the lines from C III, N II and N III (Kelly 1987), O III (Pettersson 1982) and known lines of krypton (Kelly 1987) were used as internal standards.

To distinguish between different states of ionization in both spectral sources, a number of experimental parameters, e.g., gas pressure, discharge voltage, capacitance and the number of discharges were varied (Gallardo *et al* 1989, Trigueiros *et al* 1989). The approximate total number of Kr lines for all stages observed over the pertinent wavelength range was 7500. The accuracy of the wavelength values is estimated to be ± 0.01 and ± 0.02 Å in the measurements of Lund and La Plata respectively.

3. Analysis

The line identifications were guided by theoretical predictions of the energy level structure and line strengths obtained from the Cowan (1981) computer code, using Hartree–Fock relativistic (HFR) wavefunctions.

The new Kr v classified lines observed in the present work are given in table 1. The intensities of the lines are based on visual estimates and the wavenumber values in the calculated column are derived from the experimental energy level values, which, in turn, were derived from the observed lines. The predicted wavelength and log gf values, shown in columns 3 and 4 of this table, were obtained considering the fitted values for the energy parameters, in the HF calculation. This kind of calculation was also used to obtain the values of weighted oscillator strengths for Kr III and Kr IV spectra (Raineri *et al* 1998, Bredice *et al* 2000).

The new energy level values derived from the observed lines belonging to the $4s^24p5p$, $4s^24p4d$ and $4s^24p5s$ configurations are given in table 2. The energy level values were determined from the observed wavelengths. In our case the uncertainties of the adjusted experimental energy level values are generally less than 2 cm⁻¹. All level designations in table 2 are in *LS* notation, and in the same table we present the percentage composition of the levels that were taken from the least-squares fit.

The configuration set used in the calculation was $4s^24p^2$, $4s^24p5p$, $4s4p^24d$, $4p^4$ and $4s^24p4f$ for the even parity and $4s4p^3$, $4s^24p4d$ and $4s^24p5s$ for the odd parity.

- (i) $4s^24p4d$. The $4s^24p4d$ configuration was studied by Trigueiros *et al* (1989). In this work we have extended the analysis reporting the new values 190279 and 192949 cm⁻¹ for the ${}^{3}F_{2}$ and ${}^{3}F_{3}$ energy levels respectively. These levels were found by transitions with the new $4s^24p5p$ and ground configurations. The theoretical value for the remaining ${}^{3}F_{4}$ energy level of the $4s^24p4d$ configuration obtained from the least-squares fit is 196425 cm⁻¹.
- (ii) 4s²4p5s. We propose three new energy level values of this configuration. For the ³P₁, ³P₂ and ¹P₁ levels, the experimental values are 240926, 246 798 and 250993 cm⁻¹ respectively. These levels were also found by transitions with the new 4s²4p5p and ground configurations. The calculated value for the ³P₀ energy level, obtained from the least-squares fit, is 238 871 cm⁻¹.
- (iii) $4s^24p5p$. Of the ten possible levels of this configuration, we found nine of them by transitions with the $4s4p^3$ and $4s^24p4d$ configurations. Only the level $4s^24p5p$ 3P_0 was not determined. The theoretical value for this level obtained from the least-squares fit is $284\,942$ cm⁻¹. From the percentage composition of table 1, we can observe that the 3D_1 and 1P_1 levels are very mixed. In this case the *LS* designation has very little physical significance.

4. Theoretical interpretation

The configurations were interpreted by fitting the theoretical energy expression to the observed energy levels using least-squares techniques. The adjusted parameter values for the odd and even configurations are compared with results from HFR calculations in tables 3 and 4 respectively.

For the odd parity the matrix included the $4s4p^3 + 4s^24p4d + 4s^24p5s$ configurations. The fitted energy parameters were in accordance with scaled Hartree–Fock values. The effective electrostatic parameter $\alpha(4p, 4p)$ and the configuration interaction integral R¹(4p4p, 4s4d) between $4s4p^3$ and $4s^24p4d$ configurations were optimized and fixed in order to obtain better

Table 1. Classified lines of Kr v. Int: line intensities from visual estimation. Key to symbols: w, this line appeared wider than the others in our experiment; d, the line contour is not clear in our plate, increasing the error in the measurement; us, shaded to shorter wavelengths; ul, shaded to longer wavelengths. (,): these lines appeared blended.

Int.						
and	λobs	λpred		σ_{obs}	σ_{cal}	
shape ^a	(Å)	(Å)	Log gf	(cm ⁻¹)	(cm ⁻¹) ^b	Transition
12	2490.95	2495.11	-1.043	40 145	40 145	4s ² 4p5p ³ P ₂ -4s ² 4p5s ¹ P ₁
9	2426.80	2429.37	-0.267	41 206	41 207	4s ² 4p5p ³ D ₁ =4s ² 4p4d ¹ P ₁
20w	2387.50	2386.44	0.596	41 885	41 885	4s ² 4p5p ³ P ₁ =4s ² 4p5s ³ P ₂
10w	2341.13	2341.95	-0.911	42714	42 712	4s ² 4p5p ³ S ₁ -4s ² 4p5s ¹ P ₁
50w	2339.19	2335.17	0.141	42 750	42 751	4s ² 4p5p ³ D ₂ -4s ² 4p5s ³ P ₁
100w	2314.79	2316.24	0.475	43 200	43 200	4s ² 4p5p ³ D ₃ -4s ² 4p5s ³ P ₂
100w	2255.34	2259.41	0.280	44 339	44 340	4s ² 4p5p ³ P ₂ -4s ² 4p5s ³ P ₂
100w	2192.60	2190.33	0.290	45 608	45 607	4s ² 4p5p ¹ D ₂ -4s ² 4p5s ¹ P ₁
20w	2181.60	2186.99	-0.659	45 838	45 838	4s ² 4p5p ¹ P ₁ -4s ² 4p4d ¹ P ₁
50w [·]	2176.02	2174.76	-0.194	45 955	45 956	4s ² 4p5p ³ D ₂ -4s ² 4p4d ¹ P ₁
20w	2131.83	2133.08	0.054	46 908	46 907	4s ² 4p5p ³ S ₁ -4s ² 4p5s ³ P ₂
10	2007.96	2006.57	-0.869	49 802	49 802	4s ² 4p5p ¹ D ₂ -4s ² 4p5s ³ P ₂
9	1991.63	1993.77	-1.269ª	50 210	50 212	4s ² 4p5p ³ P ₂ -4s ² 4p5s ³ P ₁
11	1894.70	1894.75	-0.700	52 779	52 779	4s ² 4p5p ³ S ₁ -4s ² 4p5s ³ P ₁
8	1796.21	1794.26	-1.629ª	55 673	55 674	4s ² 4p5p ¹ D ₂ -4s ² 4p5s ³ P ₁
7	1789.65	1790.12	-2.806	55 877	55 877	4s ² 4p5p ³ D ₃ -4s ² 4p4d ¹ F ₃
6	1764.47	1765.43	-0.370	56 674	56 674	4s ² 4p5p ¹ S ₀ -4s ² 4p5s ¹ P ₁
3	1698.42	1698.03	-0.778	58 878	58 879	4s ² 4p5p ¹ D ₂ -4s ² 4p4d ¹ P ₁
10	1661.72	1657.07	-2.726 ^b	60 179	60 181	4s ² 4p5p ³ D ₁ -4s ² 4p4d ³ D ₁
10	1611.49	1616.72	-1.050	62 054	62 053	$4s^24p5p \ ^3D_1-4s^24p4d \ ^1D_2$
8	1599.82	1603.29	-2.786 ^b	62 507	62 508	4s ² 4p5p ³ D ₁ -4s ² 4p4d ³ P ₀
10	1568.91	1568.57	-1.279	63 738	63 736	$4s^{2}4p5p^{1}P_{1}=4s^{2}4p4d^{3}D_{2}$
9	1566.03	1562.27	-1.653	63 856	63 854	4s ² 4p5p ³ D ₂ -4s ² 4p4d ³ D ₂
12w	1555.39	1555.69	-0.883	64 293	64 295	4s ² 4p5p ³ D ₂ -4s ² 4p4d ³ D ₃
3d	1542.91	1540.61	-2.862 ^b	64 813	64 812	$4s^{2}4p5p^{1}P_{1}-4s^{2}4p4d^{3}D_{1}$
15w	1540.07	1534.53	-3.522 ^b	64 932	64 930	4s ² 4p5p ³ D ₂ -4s ² 4p4d ³ D ₁
9	1538.55	1539.95	-1.294	64 996	64 995	4s ² 4p5p ³ D ₁ -4s ² 4p4d ³ P ₁
5	1499.64	1505.67	—2.587 ^ь	66 683	66 684	4s ² 4p5p ¹ P ₁ -4s ² 4p4d ¹ D ₂
2d	1498.28	1498.77	-1.876 ^b	66 743	66 741	4s ² 4p5p ¹ S ₀ -4s ² 4p5s ³ P ₁
10ul	1452.26	1449.56	-1.564	68 858	68 860	$4s^24p5p \ {}^{3}P_1 - 4s^24p4d \ {}^{3}D_2$
10	1436.20	1438.86	-2.530 ^b	69 628	69 626	$4s^{2}4p5p^{1}P_{1}-4s^{2}4p4d^{3}P_{1}$
10)	1433.78	1433.56	-1.551	69 746	69 744	$4s^24p5p \ ^3D_2-4s^24p4d \ ^3P_1$
15wul	1429.84	1425.65	-0.811	69 938	69 936	$4s^24p5p \ ^3P_1 - 4s^24p4d \ ^3D_1$
15wul	1429.84	1431.02	-4.565 ^b	69 938	69 946	$4s^24p5p$ $^1S_0-4s^24p4d$ 1P_1
12w	1424.97	1423.36	-1.668	70 177	70 175	$4s^24p5p \ ^3D_3-4s^24p4d \ ^3D_2$
15w	1416.14	1417.90	-0.516	70 614	70616	$4s^24p5p \ ^3D_3-4s^24p4d \ ^3D_3$
15	1402.20	1401.70	-0.360	71 316	71 315	$4s^24p5p \ ^3P_2-4s^24p4d \ ^3D_2$
14)	1393.61	1396.40	-0.197	71 756	71 756	$4s^24p5p \ {}^{3}P_2-4s^24p4d \ {}^{3}D_3$
15	1392.63	1395.68	-0.447	71 807	71 808	$4s^{2}4p5p^{3}P_{1}-4s^{2}4p4d^{1}D_{2}$
20	1384.59	1386.03	-0.379	72 223	72 222	$4s^24p5p {}^1P_1 - 4s^24p4d {}^3P_2$
9	1383.86	1385.66	-1.350	72 262	72 263	$4s^{2}4p5p^{3}P_{1}-4s^{2}4p4d^{3}P_{0}$
11	1382.35	1381.11	-1.170	72 341	72 340	$4s^24p5p \ ^3D_2 - 4s^24p4d \ ^3P_2$
8	1367.56	1371.37	-2.130	73 123	73 123	$4s^24p5p \ ^3D_3-4s^24p4d \ ^1D_2$
10	1337.77	1338.09	-1.932 ^b	74 751	74 750	$4s^24p5p {}^{3}P_{1}-4s^24p4d {}^{3}P_{1}$
9)	1334.08	1331.19	-0.729	74 958	74 958	$4s^{2}4p5p^{3}S_{1}-4s^{2}4p4d^{3}D_{1}$
11	1302.43	1300.06	-1.258	76 780	76777	$4s^{2}4p5p^{1}D_{2}-4s^{2}4p4d^{3}D_{2}$
10	1301.58	1305.03	-1.339	76 830	76 830	$4s^24p5p \ {}^3S_1 - 4s^24p4d \ {}^1D_2$

Int. and λ_{abs} , λ_{pred} , λ_{pred} , σ_{ods} , σ_{od} , σ_{od} , σ_{od} , σ_{od} , σ_{od} , σ_{od} , $(cm^{-1})^c$, $Transition$ 10. (295.08. (295.51), -1.291, 77.215, 77.218, $4s^2 4p5p$, $D_2 - 4s^2 4p4d$, $^3 D_2$, (10. (292.87, 1292.29, -0.992, 77.347, 77.346, $4s^2 4p5p$, $D_2 - 4s^2 4p4d$, $^3 D_2$, (10. (292.87, 1292.29, -0.992, 77.347, 77.853, $4s^2 4p5p$, $D_2 - 4s^2 4p4d$, $^3 D_2$, (10. (292.87, 1292.29, -0.992, 77.853, 77.853, $4s^2 4p5p$, $D_2 - 4s^2 4p4d$, $^3 D_2$, (12. (254.32, 12.56.55, -1.000, 79.724, 79.725, $4s^2 4p5p$, $D_2 - 4s^2 4p4d$, $^3 D_2$, (12. (255.54, 1254.54, -0.881, 79.777, 79.727, $4s^2 4p5p$, $^3 D_2 - 4s^2 4p4d$, $^3 P_2$, (10. (295.34, 1254.54, -0.881, 79.777, 79.772, $4s^2 4p5p$, $^3 P_2 - 4s^2 4p4d$, $^3 P_1$, (10. (205.63, 1200.66, -1.886, 82.670, 82.667, $4s^2 4p5p$, $P_2 - 4s^2 4p4d$, $^3 P_1$, (11.10.09, 61, 120.90, 68, -1.886, 82.670, 82.667, $4s^2 4p5p$, $P_2 - 4s^2 4p4d$, $^3 P_1$, (12. 1072.04, 1073.97, -0.498, 99.280, 99.728, $4s^2 4p5p$, $P_2 - 4s^2 4p4d$, $^3 P_1$, (12. 1072.04, 1073.97, -0.498, 99.280, 99.3280, $4s^2 4p5p$, $P_1 - 4s^2 4p4d$, $^3 P_2$, (12. 1073.04, 1028.71, -0.841, 97.050, 97.049, $4s^2 4p5p$, $P_1 - 4s^2 4p4d$, $^3 P_2$, (13. 100.69, 1071.01, -0.867, 99.397, 99.398, $4s^2 4p5p$, $P_1 - 4s^2 4p4d$, $^3 P_2$, (14. 1017.35, -0.904, 98.189, 98.189, $4s^2 4p5p$, $P_1 - 4s^2 4p4d$, $^3 P_2$, (15. 1003.37, 1002.96, -5.7449, 99.664, 99.664, $4s^2 4p5p$, $P_1 - 4s^2 4p4d$, $^3 P_2$, (20wus, 905.09, 96.61, 8, -1.041, 98.404, 98.404, $4s^2 4p5p$, $P_1 - 4s^2 4p4d$, $^3 P_2$, (20wus, 905.09, 96.61, 8, -1.784, 103.617, 103.619, $4s^2 4p5p$, $P_1 - 4s^2 4p4d$, $^3 P_2$, (20wus, 905.09, 96.61, 8, -1.784, 103.617, 103.619, $4s^2 4p5p$, $P_2 - 4s^2 4p4d$, $^3 P_2$, (20wus, 905.09, 96.61, 8, -1.784, 103.617, 103.619, $4s^2 4p5p$, $P_2 - 4s^2 4p4d$, $^3 P_2$, (20wus, 905.09, 96.61, 8, -1.784, 103.617, 103.619, $4s^2 4p5p$, $P_2 - 4s^2 4p4d$, $^3 P_2$, (20wus, 905.09, 96.61, 8, -1.784, 103.617, 103.619, 4s^2 4p5p, $P_2 - 4s^$		Table 1. (Continued.)							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Int.								
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	and	λ_{obs}	λ_{pred}		σ_{obs}	σ_{cal}			
	shape ^a	(Å)	(Å)	Log gf	(cm ⁻¹)	(cm ¹) ^c	Transition		
	10	1295.08	1295.51	-1.291	77 215	77 218	4s ² 4p5p ¹ D ₂ -4s ² 4p4d ³ D ₃		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(10	1292.87	1292.29	-0.992	77 347	77 346	4s ² 4p5p ³ P ₁ -4s ² 4p4d ³ P ₂		
	7	1284.47	1280.80	-2.370	77 853	77 853	4s ² 4p5p ¹ D ₂ -4s ² 4p4d ³ D ₁		
	6d	1271.28	1271.42	-2.300 ^b	78 661	78 661	4s ² 4p5p ³ D ₃ -4s ² 4p4d ³ P ₂		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12w	1254.32	1256.55	-1.000	79 724	79 725	4s ² 4p5p ¹ D ₂ -4s ² 4p4d ¹ D ₂		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	1253.54	1254.54	-0.881	79 774	79 772	4s ² 4p5p ³ S ₁ -4s ² 4p4d ³ P ₁		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10)	1253.12	1254.10	-1.022	79 801	79 801	4s ² 4p5p ³ P ₂ -4s ² 4p4d ³ P ₂		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10	1214.07	1214.19	-1.119	82 368	82 368	4s ² 4p5p ³ S ₁ -4s ² 4p4d ³ P ₂		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10	1209.63	1209.68	-1.886	82 670	82 667	4s ² 4p5p ¹ D ₂ -4s ² 4p4d ³ P ₁		
3d 1117.09 1117.40 -1.813 89 518 89 518 4 $s^{2}4p5p^{1}P_{1}-4s4p^{3}P_{1}$ 12w 1102.19 1099.36 0.108 90 728 90 728 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{3}$ (12 1072.04 1073.97 -0.498 93 280 93 280 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 15w 1070.69 1071.01 -0.867 93 397 93 398 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{3}$ 11 1018.44 1017.35 -0.904 98 189 98 189 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{3}$ 11 1016.22 1016.81 -1.041 98 404 99 74 99 664 99 664 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 20wus 1002.74 1003.85 -2.444 99 727 99 719 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 20wus 965.09 964.78 -1.774 1003 652 106 521 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 20wus 965.09 964.78 -1.774 1003 652 106 521 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 20wus 965.09 964.78 -1.770 105 652 106 521 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 9 880.08 879.90 -0.807 113 652 113 651 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 9 880.08 879.90 -0.807 113 626 113 0260 4 $s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{2}$ 9 880.08 879.90 -0.807 113 626 113 0260 4 $s^{2}4p5p^{3}D_{2}-4s^{4}4p4d^{3}F_{3}$ 11 705.67 757.5 -1.467 130 319 130 318 4 $s^{2}4p5p^{3}S_{1}-4s4p^{3}S_{1}$ 9 701.9 702.47 -1.216 142 470 142 470 4 $s^{2}4p5p^{3}D_{2}-4s4p^{3}P_{2}$ 9 701.9 702.47 -1.224 145 039 145 037 4 $s^{2}4p5p^{3}D_{2}-4s4p^{3}P_{2}$ 9 687.66 687.71 -1.226 141 330 141 330 4 $s^{2}4p5p^{3}D_{2}-4s4p^{3}P_{2}$ 9 701.9 702.47 -1.216 142 470 142 470 4 $s^{2}4p5p^{3}D_{2}-4s4p^{3}P_{2}$ 9 687.66 687.71 -1.226 142 470 142 470 4 $s^{2}4p5p^{3}P_{2}-4s4p^{3}P_{2}$ 10 689.47 689.77 -1.234 145 039 145 037 4 $s^{2}4p5p^{3}P_{2}-4s4p^{3}P_{2}$ 9 687.66 687.71 -1.226 143 211 445 418 4 $s^{2}4p5p^{3}P_{2}-4s4p^{3}P_{2}$ 9 687.66 687.71 -1.226 149 217 142 470 4 $s^{2}4p5p^{3}P_{2}-4s4p^{3}P_{2}$ 10 689.47 689.77 -1.234 145 039 145 037 4 $s^{2}4p5p^{3}P_{2}-4s4p^{3}P_{2}$ 9 687.66 687.71 -1.26 142 470 142 470 4 $s^{2}4p5p^{3}P_{2}-4s4p^{3}P_{2}$ 9 687.66 687.71 -1.26 142 470 142 470 4 $s^{2}4p5p^{3}P_{2}-4s4p^{3}P_{2}$ 9 687.66 687.71 -1.26 142 470 142 4	7	1128.04	1129.30	-0.268	88 649	88 649	$4s^24p5p \ ^3D_1-4s^24p4d \ ^3F_2$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3d	1117.09	1117.40	-1.813	89 518	89518	4s ² 4p5p ¹ P ₁ -4s4p ³ ¹ P ₁		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12w	1102.19	1099.36	0.108	90 728	90728	$4s^{2}4p5p^{3}D_{2}-4s^{2}4p4d^{3}F_{3}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(12	1072.04	1073.97	-0.498	93 280	93 280	$4s^24p5p$ ¹ P ₁ - $4s^24p4d$ ³ F ₂		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	15w	1070.69	1071.01	-0.867	93 397	93 398	$4s^24p5p \ {}^{3}D_2 - 4s^24p4d \ {}^{3}F_2$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	1030.40	1028.71	-0.841	97 050	97 049	$4s^24p5p \ ^3D_3-4s^24p4d \ ^3F_3$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	1018.44	1017.35	-0.904	98 189	98 1 8 9	$4s^24p5p \ {}^{3}P_2 - 4s^24p4d \ {}^{3}F_3$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	1016.22	1016.81	-1.041	98 404	98 404	$4s^24p5p^3P_1-4s^24p4d^3F_2$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	1003 37	1002.96	-5 744 ^b	99 664	99 664	$4s^24p5p^3S_1-4s4p^{3}P_1$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2011/115	1002.74	1003.85	-2 444	99 727	99719	$4s^24n5n {}^{3}D_2 - 4s^24n4d {}^{3}F_2$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20110	965.09	964 78	-1 784	103 617	103 619	$4s^24p5p^{-3}P_1-4s4p^{-3}S_1$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7	964 77	962 73	-1 770	103 652	103 651	$4s^24n5n$ $1D_2-4s^24n4d$ $3F_2$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$, 2	940.55	940.92	-2 342	106 321	106 321	$4s^24p5p$ $1D_2-4s^24p4d$ 3F_2		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0	880.08	870.00	-0.807	113 626	113 626	$4s^{2}4p5p^{-1}S_{2}-4s4p^{3}^{-1}P_{1}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 2	815.62	815.85	-0.572	122 606	122 603	$4s^{2}4p5p^{-1}S_{2}-4s4p^{3}^{-3}S_{1}$		
44107.05108.051.17.30150.201150.2004.9.p. P1.2.454p128767.35767.75-1.467130.319130.318 $4s^24p5p^3 S_1-4s4p^3 1D_2$ 50w763.03-3.652b131.001131.003 $4s^24p5p^3 D_1-4s4p^3 1D_2$ 3d707.56707.87-2.046141.330141.330 $4s^24p5p^3 D_3-4s4p^3 3P_2$ 9701.9702.47-1.216142.470142.470 $4s^24p5p^3 S_1-4s4p^3 3P_2$ 9687.66687.71-1.226145.421145.037 $4s^24p5p^3 S_1-4s4p^3 3P_2$ 9687.66687.71-1.226145.421145.418 $4s^24p5p^3 S_1-4s4p^3 3P_1$ 4d685.98685.73-1.683145.777145.780 $4s^24p5p^3 S_1-4s4p^3 3P_0$ 3d676.00675.99-2.798b145.929147.932 $4s^24p5p^1 D_2-4s4p^3 3P_1$ 4d685.98685.73-1.683145.777145.780 $4s^24p5p^1 D_2-4s4p^3 3P_1$ 50674.24674.01-3.251b148.315148.313 $4s^24p5p^1 D_2-4s4p^3 3P_1$ 6649.78650.17-2.361b153.898153.900 $4s^24p5p^3 D_2-4s4p^3 3D_2$ 6649.78650.17-2.135153.898153.900 $4s^24p5p^3 D_2-4s4p^3 3D_2$ 6649.78649.17-2.135153.898153.898 $4s^24p5p^3 D_2-4s4p^3 3D_2$ 6649.78649.17-2.135153.898153.900 $4s^24p5p^3 D_2-4s4p^3 3D_3$ 7628.83628.	4	767.60	769.02	-0.572	122 000	122 005	$4s^2 4p5p^{-3}D_{1} - 4s4p^{-3}B_{2}$		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4u o	767.09	708.05	-1.750	130 201	130 200	$4s^{2}4p5p^{3}S_{1}-4s4p^{3}$		
30w763.53763.63 -2.632 131001131003 $4s 4pp p D_1 - 4sp^2 D_1$ 11750.67750.72 -0.583 133 214133 213 $4s^24p5p D_2 - 4s4p^3 D_2$ 3d707.56707.87 -2.046 141 330141 330 $4s^24p5p 3D_3 - 4s4p^3 P_2$ 9701.9702.47 -1.216 142 470142 470 $4s^24p5p 3P_2 - 4s4p^3 P_2$ 10689.47689.77 -1.234 145 039145 037 $4s^24p5p 3S_1 - 4s4p^3 P_2$ 9687.66687.71 -1.226 145 421145 418 $4s^24p5p 3S_1 - 4s4p^3 P_2$ 4d685.98685.73 -1.683 145 777145 780 $4s^24p5p 3S_1 - 4s4p^3 P_2$ 3d676.00675.99 -2.798^b 145 929147 932 $4s^24p5p ^3D_2 - 4s4p^3 ^3P_1$ 3d676.00675.99 -2.798^b 145 929147 932 $4s^24p5p ^3D_2 - 4s4p^3 ^3P_1$ 60674.24674.01 -3.251^b 148 315148 313 $4s^24p5p ^3D_2 - 4s4p^3 ^3D_3$ 70655.05655.24 -1.177 152 660152 661 $4s^24p5p ^3D_2 - 4s4p^3 ^3D_3$ 10650.27650.26 -1.046 153 782153 780 $4s^24p5p ^3D_2 - 4s4p^3 ^3D_2$ 6649.78650.17 -2.361^b 153 898153 898 $4s^24p5p ^3D_2 - 4s4p^3 ^3D_3$ 9628.03628.46 -1.018 159 025 $159 025$ $4s^24p5p ^3D_2 - 4s4p^3 ^3D_3$ 9628.83628.86 -1.018 159 025 $159 025$ $4s^24p5p ^3$	0 50m	767.35	762.02	-1.407	121 001	131 003	$4s^{2}4p5p^{3}D_{1}$ $4s^{4}p^{3}^{3}P_{2}$		
11750.67750.72 -0.383 153.214153.21343.35.15 $22.43p$ D_2 3d707.56707.87 -2.046 141.330141.330 $4s^24p5p$ $3D_2-4s4p^3$ $3P_2$ 9701.9702.47 -1.216 142.470142.470 $4s^24p5p$ $3D_2-4s4p^3$ $3P_2$ 10689.47689.77 -1.234 145.039145.037 $4s^24p5p$ $3L4s4p^3$ $3P_2$ 9687.66687.71 -1.226 145.421145.418 $4s^24p5p$ $3L4s4p^3$ $3P_1$ 4d685.98685.73 -1.683 145.777145.780 $4s^24p5p$ $3L4s4p^3$ $3P_1$ 3d676.00675.99 $=2.798^{b}$ 145.929147.932 $4s^24p5p$ $1D_2-4s4p^3$ $3P_1$ 6)674.24674.01 $=3.251^{b}$ 148.315148.313 $4s^24p5p$ $1D_2-4s4p^3$ $3P_1$ 7655.05655.24 -1.177 152.660152.661 $4s^24p5p$ $3D_2-4s4p^3$ $3D_3$ 10650.27650.26 -1.046 153.782153.780 $4s^24p5p$ $1P_1-4s4p^3$ $3D_2$ 6649.78650.17 -2.361^{b} 153.898153.900 $4s^24p5p$ $3D_2-4s4p^3$ $3D_3$ 9628.83628.86 -1.018 159.025159.025 $4s^24p5p$ $3D_3-4s4p^3$ $3D_3$ 9628.83628.86 -1.018 159.025 159.025 $4s^24p5p$ $3D_3-4s4p^3$ $3D_3$ 8627.40 </td <td>50w</td> <td>703.33</td> <td>703.03</td> <td>-5.052</td> <td>122 214</td> <td>132 005</td> <td>$4s^{2}4p5p^{1}D_{1} - 4s4p^{3}^{1}D_{2}$</td>	50w	703.33	703.03	-5.052	122 214	132 005	$4s^{2}4p5p^{1}D_{1} - 4s4p^{3}^{1}D_{2}$		
3d 707.36 707.87 -2.046 141330 141330 $44pp$ D_3exs4p T_2 9 701.9 702.47 -1.216 142470 142470 $4s^24p5n^3P_2-4s4p^3 ^3P_2$ 10 689.47 689.77 -1.234 145039 145037 $4s^24p5p^3S_1-4s4p^3 ^3P_2$ 9 687.66 687.71 -1.226 145421 145418 $4s^24p5p^3S_1-4s4p^3 ^3P_1$ 4d 685.98 685.73 -1.683 145777 145780 $4s^24p5p^3S_1-4s4p^3 ^3P_0$ 3d 676.00 675.99 $=2.798^b$ 145929 147932 $4s^24p5p^3D_2-4s4p^3 ^3P_1$ 6) 674.24 674.01 $=3.251^b$ 148315 148313 $4s^24p5p^1D_2-4s4p^3 ^3P_1$ 7 655.05 655.24 -1.177 152660 152661 $4s^24p5p^3D_2-4s4p^3 ^3D_3$ 10 650.27 650.26 -1.046 153782 153780 $4s^24p5p^1P_1-4s4p^3 ^3D_2$ 6 649.78 650.17 -2.361^b 153898 153900 $4s^24p5p^3D_2-4s4p^3 ^3D_3$ 9 629.00 629.47 -1.414 158982 158982 $4s^24p5p^3D_2-4s4p^3 ^3D_3$ 9 628.83 628.86 -1.018 159025 159025 $4s^24p5p^3P_2-4s4p^3 ^3D_3$ 8 627.40 627.53 -2.219 159388 159380 $4s^24p5p^3P_2-4s4p^3 ^3D_3$ 3 624.13 623.88 -2.660^b 160223 160219 $4s^24p5p^3P_2-4s4p^3 ^3D_3$ 3 624.13 623	11	750.07	750.72	-0.585	133214	133 213	$4s^{2}4p5p^{3}D_{2} - 4s4p^{3}^{3}D_{2}$		
9701.9702.47-1.216142.470142.47043 4pp r_2 -4s4p r_2 10689.47689.77-1.234145.039145.037 $4s^24p5p^3S_1-4s4p^3 ^3P_2$ 9687.66687.71-1.226145.421145.418 $4s^24p5p^3S_1-4s4p^3 ^3P_1$ 4d685.98685.73-1.683145.777145.780 $4s^24p5p^3S_1-4s4p^3 ^3P_0$ 3d676.00675.99=2.798 ^b 145.929147.932 $4s^24p5p^1D_2-4s4p^3 ^3P_1$ 6)674.24674.01=3.251 ^b 148.315148.313 $4s^24p5p^1D_2-4s4p^3 ^3P_1$ 7655.05655.24-1.177152.660152.661 $4s^24p5p^1D_2-4s4p^3 ^3D_2$ 6649.78650.17-2.361 ^b 153.898153.900 $4s^24p5p^1P_1-4s4p^3 ^3D_1$ 6649.78649.17-2.135153.898153.898 $4s^24p5p^3D_2-4s4p^3 ^3D_3$ 9629.00629.47-1.414158.982158.982 $4s^24p5p^3D_3-4s4p^3 ^3D_3$ 9628.83628.86-1.018159.025159.025 $4s^24p5p^3P_2-4s4p^3 ^3D_1$ 8627.40627.53-2.219159.388159.380 $4s^24p5p^3P_2-4s4p^3 ^3D_3$ 3624.13623.88-2.660 ^b 160.120160.122 $4s^24p5p^3P_2-4s4p^3 ^3D_3$ 8619.73619.68-1.339161.361161.359 $4s^24p5p^3P_2-4s4p^3 ^3D_2$ 8619.73619.68-1.339161.361161.359 $4s^24p5p^3P_2-4s4p^3 ^3D_2$ 5 <t< td=""><td>50</td><td>707.30</td><td>707.87</td><td>-2.040</td><td>141 330</td><td>141 330</td><td>$45 4p5p D_3 = 454p F_2$ $4s^2 4p5p ^3 D_2 4s 4p F_2$</td></t<>	50	707.30	707.87	-2.040	141 330	141 330	$45 4p5p D_3 = 454p F_2$ $4s^2 4p5p ^3 D_2 4s 4p F_2$		
10 689.47 689.77 -1.234 143.039 143.037 $48.4p5p$ $51-484p^{3} P_{1}$ 9 687.66 687.71 -1.226 145.421 145.418 $4s^{2}4p5p^{3}S_{1}-4s4p^{3} P_{1}$ 4d 685.98 685.73 -1.683 145.777 145.780 $4s^{2}4p5p^{3}S_{1}-4s4p^{3} P_{0}$ 3d 676.00 675.99 $=2.798^{b}$ 145.929 147.932 $4s^{2}4p5p^{1}D_{2}-4s4p^{3} P_{2}$ 6) 674.24 674.01 $=3.251^{b}$ 148.315 148.313 $4s^{2}4p5p^{1}D_{2}-4s4p^{3} P_{1}$ 7 655.05 655.24 -1.177 152.660 152.661 $4s^{2}4p5p^{1}D_{2}-4s4p^{3} P_{3}$ 10 650.27 650.26 -1.046 153.782 153.780 $4s^{2}4p5p^{1}P_{1}-4s4p^{3} P_{3}$ 6 649.78 650.17 -2.361^{b} 153.898 153.900 $4s^{2}4p5p^{1}P_{1}-4s4p^{3} P_{3}$ 6 649.78 649.17 -2.135 153.898 153.898 $4s^{2}4p5p^{3}D_{2}-4s4p^{3} P_{3}$ 9 629.00 629.47 -1.414 158.982 158.982 $4s^{2}4p5p^{3}P_{3}-4s4p^{3} P_{3}$ 9 628.83 628.86 -1.018 159.025 159.025 $4s^{2}4p5p^{1}S_{0}-4s4p^{3} P_{1}$ 8 627.40 627.53 -2.219 159.388 159.380 $4s^{2}4p5p^{3}P_{2}-4s4p^{3} P_{3}$ 8 619.73 619.68 -1.339 161.361 161.359 $4s^{2}4p5p^{3}P_{2}-4s4p^{3} P_{3}$ 8 619.73 619.66 $-1.$	9	/01.9	/02.47	-1.210	142470	142470	$45^{2}4p5p^{2}r_{2}-4s4p^{2}r_{2}$		
9687.06687.71 -1.226 143421 143418 $48^{2}4p5p^{3}S_{1-4}s4p^{3}P_{1}$ 4d685.98685.73 -1.683 145777 145780 $48^{2}4p5p^{3}S_{1-4}s4p^{3}P_{1}$ 3d676.00 675.99 $=2.798^{b}$ 145929 147932 $48^{2}4p5p^{1}D_{2-4}s4p^{3}P_{2}$ 6) 674.24 674.01 $=3.251^{b}$ 148315 148313 $48^{2}4p5p^{1}D_{2-4}s4p^{3}P_{1}$ 7 655.05 655.24 -1.177 152660 152661 $4s^{2}4p5p^{1}D_{2-4}s4p^{3}D_{2}$ 6 649.78 650.17 -2.361^{b} 153898 153900 $4s^{2}4p5p^{1}P_{1-4}s4p^{3}D_{1}$ 6 649.78 650.17 -2.135 153898 153900 $4s^{2}4p5p^{1}P_{1-4}s4p^{3}^{3}D_{1}$ 6 649.78 69.17 -2.135 153898 153900 $4s^{2}4p5p^{3}D_{2-4}s4p^{3}^{3}D_{2}$ 9 629.00 629.47 -1.414 158982 158982 $4s^{2}4p5p^{3}D_{3}-4s4p^{3}^{3}D_{1}$ 8 627.40 627.53 -2.219 159388 159380 $4s^{2}4p5p^{3}P_{1-4}s4p^{3}^{3}D_{1}$ 8 627.40 627.53 -2.219 159388 159380 $4s^{2}4p5p^{3}D_{3}-4s4p^{3}^{3}D_{3}$ 3 624.13 623.88 -2.660^{b} 160223 160219 $4s^{2}4p5p^{3}D_{2-4}s4p^{3}^{3}D_{2}$ 8 619.73 619.68 -1.339 161361 161359 $4s^{2}4p5p^{3}P_{2-4}s4p^{3}^{3}D_{2}$ 5 619.31 619.60 -2.426 161470	10	689.47	089.77	-1.234	145 039	143 037	$45^{-}4p_{-}5p_{-}3p_{-}4s_{+}p_{-}r_{2}$		
4d 685.98 685.73 -1.683 145777 145780 $48^{2}4p5p^{3}5_{1-4}4s4p^{-7}P_{0}$ 3d 676.00 675.99 $=2.798^{b}$ 145929 147932 $48^{2}4p5p^{1}D_{2-4}s4p^{3}^{3}P_{2}$ 6) 674.24 674.01 $=3.251^{b}$ 148315 148313 $4s^{2}4p5p^{1}D_{2-4}s4p^{3}^{3}P_{1}$ 7 655.05 655.24 -1.177 152660 152661 $4s^{2}4p5p^{1}D_{2-4}s4p^{3}^{3}D_{2}$ 6 649.78 650.17 -2.361^{b} 153898 153900 $4s^{2}4p5p^{1}P_{1-4}s4p^{3}^{3}D_{2}$ 6 649.78 650.17 -2.135 153898 153900 $4s^{2}4p5p^{1}P_{1-4}s4p^{3}^{3}D_{2}$ 6 649.78 69.17 -2.135 153898 153900 $4s^{2}4p5p^{3}D_{2-4}s4p^{3}^{3}D_{2}$ 9 629.00 629.47 -1.414 158982 158982 $4s^{2}4p5p^{3}D_{3}-4s4p^{3}^{3}D_{1}$ 8 627.40 627.53 -2.219 159388 159380 $4s^{2}4p5p^{1}S_{0-4}s4p^{3}^{3}D_{1}$ 8 627.40 627.53 -2.219 159388 159380 $4s^{2}4p5p^{3}P_{2-4}s4p^{3}^{3}D_{3}$ 3 624.13 623.88 -2.660^{b} 160223 160219 $4s^{2}4p5p^{3}P_{2-4}s4p^{3}^{3}D_{2}$ 8 619.73 619.68 -1.339 161361 161359 $4s^{2}4p5p^{3}P_{2-4}s4p^{3}^{3}D_{2}$ 5 619.31 619.60 -2.426 161470 161480 $4s^{2}4p5p^{1}D_{2-4}s4p^{3}^{3}D_{3}$ (4 603.91 604.14 <	9	687.66	687.71	-1.220	145 421	145 418	$4s^{-}4p_{-}5p^{-}S_{1}-4s4p^{-}P_{1}$		
3d 676.00 675.99 $=2.798^\circ$ 145929 147932 $48^\circ 4p5p^\circ D_2-484p^\circ P_2$ 6) 674.24 674.01 $=3.251^{b}$ 148315 148313 $4s^24p5p^\circ D_2-4s4p^3 ^3P_1$ 7 655.05 655.24 -1.177 152660 152661 $4s^24p5p^\circ ^3D_2-4s4p^3 ^3D_3$ 10 650.27 650.26 -1.046 153782 153780 $4s^24p5p^\circ ^1P_1-4s4p^3 ^3D_2$ 6 649.78 650.17 -2.361^{b} 153898 153900 $4s^24p5p^\circ ^3D_2-4s4p^3 ^3D_1$ 6 649.78 649.17 -2.135 153898 153900 $4s^24p5p^\circ ^3D_2-4s4p^3 ^3D_2$ 9 629.00 629.47 -1.414 158982 158982 $4s^24p5p^\circ ^3D_3-4s4p^3 ^3D_3$ 9 628.83 628.86 -1.018 159025 159025 $4s^24p5p^\circ ^3P_1-4s4p^3 ^3D_1$ 8 627.40 627.53 -2.219 159388 159380 $4s^24p5p^\circ ^3P_2-4s4p^3 ^3D_3$ 40wul 624.53 625.20 -0.664 160120 160122 $4s^24p5p^\circ ^3P_2-4s4p^3 ^3D_3$ 3 624.13 623.88 -2.660^{b} 160223 160219 $4s^24p5p^\circ ^3P_2-4s4p^3 ^3D_2$ 8 619.73 619.68 -1.339 161361 161359 $4s^24p5p^\circ ^3P_2-4s4p^3 ^3D_2$ 5 619.31 619.60 -2.426 161470 161480 $4s^24p5p^\circ ^3P_2-4s4p^3 ^3D_3$ (4 603.91 604.14 -1.368 165588 165584 $4s^24p5p^\circ ^1D_2-4s4p^3 ^3D_3$ <td>4d</td> <td>685.98</td> <td>685.73</td> <td>-1.083</td> <td>145 ///</td> <td>145 /80</td> <td>$4s^{2}4p^{2}5p^{-}51-4s4p^{-}P_{0}$</td>	4d	685.98	685.73	-1.083	145 ///	145 /80	$4s^{2}4p^{2}5p^{-}51-4s4p^{-}P_{0}$		
6) $6/4.24$ $6/4.01$ $=3.251^{\circ}$ 148315 148313 $4s^{\circ}4pp$ $D_2-4s4p^{\circ} P_1$ 7 655.05 655.24 -1.177 152660 152661 $4s^24p5p$ $^{3}D_2-4s4p^{3}$ $^{3}D_3$ 10 650.27 650.26 -1.046 153782 153780 $4s^24p5p$ $^{1}P_1-4s4p^{3}$ $^{3}D_2$ 6 649.78 650.17 -2.361° 153898 153900 $4s^24p5p$ $^{1}P_1-4s4p^{3}$ $^{3}D_2$ 6 649.78 649.17 -2.135 153898 153890 $4s^24p5p$ $^{3}D_2-4s4p^{3}$ $^{3}D_2$ 9 629.00 629.47 -1.414 158982 158982 $4s^24p5p$ $^{3}D_1-4s4p^{3}$ $^{3}D_2$ 9 628.83 628.86 -1.018 159025 159025 $4s^24p5p$ $^{3}P_1-4s4p^{3}$ $^{3}D_1$ 8 627.40 627.53 -2.219 159388 159380 $4s^24p5p$ $^{3}D_2-4s4p^{3}$ $^{3}D_3$ 40wul 624.53 625.20 -0.664 160120 160122 $4s^24p5p$ $^{3}D_2-4s4p^{3}$ $^{3}D_3$ 3 624.13 623.88 -2.660^{b} 160223 160219 $4s^24p5p$ $^{3}D_2-4s4p^{3}$ $^{3}D_2$ 8 619.73 619.68 -1.339 161361 161359 $4s^24p5p$ $^{3}D_2-4s4p^{3}$ $^{3}D_2$ 5 619.31 619.60 -2.426 161470 161480 $4s^24p5p$ $^{3}D_2-4s4p^{3}$ $^{3}D_1$ <	30	676.00	675.99	=2.798°	145 929	147932	$4s^{-}4p_{-}5p^{-}D_{2}^{-}4s^{+}4p^{-}P_{2}^{-}$		
7655.05655.24 -1.177 152 660152 661 $4s^24p5p^2D_2-4s4p^2 D_3$ 10650.27650.26 -1.046 153 782153 780 $4s^24p5p^2P_1-4s4p^3 D_2$ 6649.78650.17 -2.361^b 153 898153 900 $4s^24p5p^3P_1-4s4p^3 D_1$ 6649.78649.17 -2.135 153 898153 898 $4s^24p5p^3D_2-4s4p^3 D_2$ 9629.00629.47 -1.414 158 982158 982 $4s^24p5p^3D_3-4s4p^3 3D_3$ 9628.83628.86 -1.018 159 025159 025 $4s^24p5p^3P_1-4s4p^3 3D_1$ 8627.40627.53 -2.219 159 388159 380 $4s^24p5p^3P_2-4s4p^3 3D_1$ 40wul624.53625.20 -0.664 160 120160 122 $4s^24p5p^3P_2-4s4p^3 ^3D_3$ 3624.13623.88 -2.660^b 160 223160 219 $4s^24p5p^3D_3-4s4p^3 ^3D_2$ 8619.73619.68 -1.339 161 361161 359 $4s^24p5p^3P_2-4s4p^3 ^3D_2$ 5619.31619.60 -2.426 161 470161 480 $4s^24p5p^3P_2-4s4p^3 ^3D_3$ (4603.91604.14 -1.368 165 588165 584 $4s^24p5p^1D_2-4s4p^3 ^3D_3$	6)	674.24	674.01	=3.251	148 315	148 313	$4s^{-}4p_{-}5p^{-}D_{2}-4s^{-}4p_{-}^{-}P_{1}$		
10 650.27 650.26 -1.046 153782 153780 $4s^24p5p^3P_1-4s4p^3^3D_2$ 6 649.78 650.17 -2.361^b 153898 153900 $4s^24p5p^3P_1-4s4p^3^3D_1$ 6 649.78 649.17 -2.135 153898 153898 $4s^24p5p^3D_2-4s4p^3^3D_2$ 9 629.00 629.47 -1.414 158982 158982 $4s^24p5p^3D_3-4s4p^3^3D_3$ 9 628.83 628.86 -1.018 159025 159025 $4s^24p5p^3P_1-4s4p^3^3D_1$ 8 627.40 627.53 -2.219 159388 159380 $4s^24p5p^3P_2-4s4p^3^3D_1$ 40wul 624.53 625.20 -0.664 160120 160122 $4s^24p5p^3P_2-4s4p^3^3D_3$ 3 624.13 623.88 -2.660^b 160223 160219 $4s^24p5p^3P_2-4s4p^3^3D_2$ 8 619.73 619.68 -1.339 161361 161359 $4s^24p5p^3P_2-4s4p^3^3D_2$ 5 619.31 619.60 -2.426 161470 161480 $4s^24p5p^3P_2-4s4p^3^3D_3$ (4 603.91 604.14 -1.368 165588 165584 $4s^24p5p^3D_2-4s4p^3^3D_3$	7	655.05	655.24	-1.177	152 660	152 661	$4s^{2}4p^{2}D_{2}-4s^{4}p^{3}D_{3}$		
6 649.78 650.17 -2.361° 153898 153900 $4s^{-}4p5p^{-}P_{1}-4s4p^{-} D_{1}$ 6 649.78 649.17 -2.135 153898 153898 $4s^{2}4p5p^{-}3D_{2}-4s4p^{-}3D_{2}$ 9 629.00 629.47 -1.414 158982 158982 $4s^{2}4p5p^{-}3D_{3}-4s4p^{-}3D_{3}$ 9 628.83 628.86 -1.018 159025 $4s^{2}4p5p^{-}3P_{1}-4s4p^{-}3D_{1}$ 8 627.40 627.53 -2.219 159388 159380 $4s^{2}4p5p^{-}3P_{2}-4s4p^{-}3D_{1}$ 40wul 624.53 625.20 -0.664 160120 160122 $4s^{2}4p5p^{-}3P_{2}-4s4p^{-}3D_{3}$ 3 624.13 623.88 -2.660^{b} 160223 160219 $4s^{2}4p5p^{-}3D_{3}-4s4p^{-}3D_{2}$ 8 619.73 619.68 -1.339 161361 161359 $4s^{2}4p5p^{-}3P_{2}-4s4p^{3}^{-}3D_{2}$ 5 619.31 619.60 -2.426 161470 161480 $4s^{2}4p5p^{-}3P_{2}-4s4p^{3}^{-}3D_{1}$ (4 603.91 604.14 -1.368 165588 165584 $4s^{2}4p5p^{-}1D_{2}-4s4p^{3}^{-}3D_{3}$	10	650.27	650.26	-1.046	153 782	153 780	$4s^{2}4p5p^{4}P_{1}-4s4p^{3}D_{2}$		
	6	649.78	650.17	-2.361 ^b	153 898	153 900	$4s^24p5p P_1-4s4p^3 D_1$		
9 629.00 629.47 -1.414 158982 158982 $4s^24p5p^3D_3-4s4p^3^3D_3$ 9 628.83 628.86 -1.018 159025 159025 $4s^24p5p^3P_1-4s4p^3^3D_1$ 8 627.40 627.53 -2.219 159388 159380 $4s^24p5p^3P_2-4s4p^3^3P_1$ 40wul 624.53 625.20 -0.664 160120 160122 $4s^24p5p^3P_2-4s4p^3^3D_3$ 3 624.13 623.88 -2.660^{b} 160223 160219 $4s^24p5p^3D_3-4s4p^3^3D_2$ 8 619.73 619.68 -1.339 161361 161359 $4s^24p5p^3P_2-4s4p^3^3D_2$ 5 619.31 619.60 -2.426 161470 161480 $4s^24p5p^3P_2-4s4p^3^3D_1$ (4 603.91 604.14 -1.368 165588 165584 $4s^24p5p^1D_2-4s4p^3^3D_3$	6	649.78	649.17	-2.135	153 898	153 898	$4s^24p5p\ ^{3}D_2-4s4p^{3}\ ^{3}D_2$		
9 628.83 628.86 -1.018 159025 159025 $4s^24p5p^{-3}P_1-4s4p^{-3}J_1$ 8 627.40 627.53 -2.219 159388 159380 $4s^24p5p^{-1}S_0-4s4p^{-3}J_1$ 40wul 624.53 625.20 -0.664 160120 160122 $4s^24p5p^{-3}P_2-4s4p^{-3}J_3$ 3 624.13 623.88 -2.660^{b} 160223 160219 $4s^24p5p^{-3}D_2-4s4p^{-3}J_2$ 8 619.73 619.68 -1.339 161361 161359 $4s^24p5p^{-3}P_2-4s4p^{-3}J_2$ 5 619.31 619.60 -2.426 161470 161480 $4s^24p5p^{-3}P_2-4s4p^{-3}J_1$ (4 603.91 604.14 -1.368 165588 165584 $4s^24p5p^{-1}D_2-4s4p^{-3}J_3$	9	629.00	629.47	-1.414	158 982	158 982	$4s^{2}4p5p^{3}D_{3}-4s4p^{3}^{3}D_{3}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9	628.83	628.86	-1.018	159 025	159 025	$4s^{2}4p5p^{3}P_{1}-4s4p^{3}^{3}D_{1}$		
40wul624.53625.20 -0.664 160 120160 122 $4s^24p5p$ $^3P_2-4s4p^3$ 3D_3 3624.13623.88 -2.660^b 160 223160 219 $4s^24p5p$ $^3D_3-4s4p^3$ 3D_2 8619.73619.68 -1.339 161 361161 359 $4s^24p5p$ $^3P_2-4s4p^3$ 3D_2 5619.31619.60 -2.426 161 470161 480 $4s^24p5p$ $^3P_2-4s4p^3$ 3D_1 (4603.91604.14 -1.368 165 588165 584 $4s^24p5p$ $^1D_2-4s4p^3$ 3D_3	8	627.40	627.53	-2.219	159 388	159 380	$4s^{2}4p5p^{1}S_{0}-4s4p^{3}^{3}P_{1}$		
3 624.13 623.88 -2.660^{b} 160223 160219 $4s^{2}4p5p^{3}D_{3}-4s4p^{3}{}^{3}D_{2}$ 8 619.73 619.68 -1.339 161361 161359 $4s^{2}4p5p^{3}P_{2}-4s4p^{3}{}^{3}D_{2}$ 5 619.31 619.60 -2.426 161470 161480 $4s^{2}4p5p^{3}P_{2}-4s4p^{3}{}^{3}D_{1}$ (4 603.91 604.14 -1.368 165588 165584 $4s^{2}4p5p^{1}D_{2}-4s4p^{3}{}^{3}D_{3}$	40wul	624.53	625.20	-0.664	160 120	160 122	$4s^{2}4p5p^{3}P_{2}-4s4p^{3}^{3}D_{3}$		
	3	624.13	623.88	-2.660 ^b	160 223	160 219	$4s^{2}4p5p^{3}D_{3}-4s4p^{3}^{3}D_{2}$		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	8	619.73	619.68	-1.339	161 361	161 359	$4s^{2}4p5p^{3}P_{2}-4s4p^{3}^{3}D_{2}$		
$(4 603.91 604.14 -1.368 165588 165584 4s^2 4p5p {}^1D_2 - 4s4p^3 {}^3D_3$	5	619.31	619.60	-2.426	161 470	161 480	$4s^{2}4p5p^{3}P_{2}-4s4p^{3}^{3}D_{1}$		
	(4	603.91	604.14	-1.368	165 588	165 584	4s ² 4p5p ¹ D ₂ -4s4p ³ ³ D ₃		

Table 1. (Continued.)						
Int. and shape ^a	λ _{øbs} (Å)	λ _{pred} (Å)	Log gf	σ _{obs} (cm ⁻¹)	σ_{cal} $(cm_{-}^{-1})^{c}$	Transition
12ul	586.31	585.90	-1.519	170 555	170 556	4s ² 4p ² ¹ D ₂ -4s ² 4p4d ³ F ₂
10	577.28	577.75	-2.109	173 226	173 226	$4s^24p^2$ ¹ D ₂ - $4s^24p4d$ ³ F ₃
9	547.38	547.08	-1.822	182 688	182 684	$4s^24p^2$ ³ P ₂ - $4s^24p4d$ ³ F ₂
11w	539.50	539.97	-1.210	185 357	185 354	4s ² 4p ² ³ P ₂ -4s ² 4p4d ³ F ₃
11ul	536.08	535.91	-1.854	186 539	186 536	$4s^24p^2 {}^3P_1 - 4s^24p4d {}^3F_2$
7	495.72	495.82	0.019	201 727	201 722	4s ² 4p ² ¹ S ₀ -4s ² 4p5s ³ P ₁
7	472.19	472.22	0.037	211 779	211789	4s ² 4p ² ¹ S ₀ -4s ² 4p5s ¹ P ₁
5	452.08	452.03	-2.672 ^b	221 200	221 203	4s ² 4p ² ¹ D ₂ -4s ² 4p5s ³ P ₁
6	440.37	440.29	-1.168	227 082	227 075	4s ² 4p ² ¹ D ₂ -4s ² 4p5s ³ P ₂
15	432.41	432.33	0.034	231 262	231 270	4s ² 4p ² ¹ D ₂ -4s ² 4p5s ¹ P ₁
12d	428.56	428.57	-0.679	233 340	233 331	4s ² 4p ² ³ P ₂ -4s ² 4p5s ³ P ₁
10	421.63	421.68	0.855	237 175	237 183	4s ² 4p ² ³ P ₁ -4s ² 4p5s ³ P ₁
15w	418.08	418.01	-0.109	239 234	239 203	4s ² 4p ² ³ P ₂ -4s ² 4p5s ³ P ₂
10	415.08	415.13	-0.692	240 917	240 926	4s ² 4p ² ³ P ₀ -4s ² 4p5s ³ P ₁
10	411.45	411.45	-0.519	243 043	243 055	4s ² 4p ² ³ P ₁ -4s ² 4p5s ³ P ₂
6	410.87	410.83	-1.658 ^b	243 386	243 398	4s ² 4p ² ³ P ₂ -4s ² 4p5s ¹ P ₁
6	404.45	404.49	-1.761	247 249	247 250	4s ² 4p ² ³ P ₁ -4s ² 4p5s ¹ P ₁

^a Lines with cancellation factor (Cowan 1981) <0.05.

^b Calculated wavenumber.

Table 2. New energy levels of the $4s^24p4d$, $4s^24p5s$ and $4s^24p5p$ configurations of Kr v.

Designation		E_{exp} (cm ⁻¹)	E_{exp} (cm ⁻¹) E_{calc} (cm ⁻¹) ^a Percentage composition ^b	
4s ² 4p4d	³ F ₂	190 279	190 362	99
	³ F ₃	192 949	192 770	99
	³ F ₄		196 425	100
4s ² 4p5s	³ P ₀		238 871	99
	³ P1	240 926	240 908	67 + 24 4s ² 4p4d ¹ P + 5 4s4p ³ ¹ P
	${}^{3}P_{2}$	246 798	246 806	100
	¹ P1	250 993	250 987	79 + 12 4s ² 4p5s ³ P + 7 4s ² 4p4d ¹ P
4s ² 4p5p	$^{3}D_{1}$	278 928	278 926	56 + 42 4s ² 4p5p ¹ P
	$^{3}D_{2}$	283 677	283 745	$85 + 8 4s^2 4p5p^3P + 6 4s^2 4p5p^1D$
	$^{3}D_{3}$	289 998	289 992	99
	³ P ₀		284 942	92 + 6 4s ² 4p5p ¹ S
	³ P1	288 683	288 722	64 + 22 4s ² 4p5p ¹ P + 12 4s ² 4p5p ³ D
	³ P ₂	291 138	291 079	78 + 13 4s ² 4p5p ³ D + 8 4s ² 4p5p ¹ D
	³ S ₁	293 705	293 699	86 + 9 4s ² 4p5p ³ P
	$^{1}D_{2}$	296 600	296 656	85 + 13 4s ² 4p5p ³ P
	¹ P ₁	283 559	283 488	32 + 32 4s ² 4p5p ³ D + 26 4s ² 4p5p ³ P + 9 4s ² 4p5p ³ S
	¹ S ₀	307 667	307 640	$68 + 21 4p^{4} {}^{1}S$

^a Calculated energy level values obtained using the fitted energy parameters.

^b Percentages below 5% have been omitted.

results in the least-squares fit. The standard deviation was 124 cm^{-1} . If we compare this work with the report of Trigueiros *et al* (1989), we find that our electrostatic energy parameters are lower than those reported in that paper, except for the G³(4p4d) parameter of the 4s²4p4d

Configuration	Parameter	HF value	Fitted value	F/HF
4s4p ³	E_{av}	148 381	151 658 ± 63	1.022 ± 0.001
	F ² (4p, 4p)	65 943	48764 ± 493	0.739 ± 0.007
	α(4p, 4p)		659 (FIX)	
	ζ4p	4619	5949 ± 106	1.287 ± 0.023
	G ¹ (4s,4p)	88 242	64666 ± 181	0.733 ± 0.002
4s ² 4p4d	E_{av}	208 466	206922 ± 52	0.993 ± 0.001
	ζ4p	4784	4528 ± 109	0.946 ± 0.023
	ζ4d	273	273 (FIX)	1.000
	F ² (4p,4d)	52 205	41807 ± 426	0.801 ± 0.008
	G ¹ (4p, 4d)	62 999	48954 ± 204	0.777 ± 0.003
	G ³ (4p, 4d)	39 020	29318 ± 485	0.751 ± 0.012
4s ² 4p5s	E_{av}	245 727	245132 ± 97	0.998 ± 0.001
-	ζ4p	4953	5309 ± 182	1.172 ± 0.036
	G ⁱ (4p, 5s)	7504	6283 ± 306	0.837 ± 0.041
Configura				
4s4p ³ -4s ² 4p4d	R ¹ (4p4p, 4s4d)	72 645	57 252 (FIX)	0.788
4s4p ³ -4s ² 4p5s	R ¹ (4p4p, 4s5s)	1472	1252 (FIX)	0.850
4s ² 4p4d-4s ² 4p5s	R ² (4p4d, 4p5s)	-10756	-9143 (FIX)	0.850
- •	R ¹ (4p4d, 5s4p)	-3103	-2638 (FIX)	0.850

Table 3. Energy parameters (cm^{-1}) for the odd-parity configurations of Kr v studied.

configuration. The inclusion of the ${}^{3}F_{2}$ and ${}^{3}F_{3}$ levels of the $4s^{2}4p4d$ configuration and the three new energy levels of the $4s^{2}4p5s$ configuration affect this calculation, although the interaction integrals with the latter are not very significant.

For the even parity the matrix included the $4s^24p^2 + 4s^24p5p + 4s4p^24d + 4p^4 + 4s^24p4f$ configurations. The configuration interaction integrals among these configurations are very strong except for those involving the $4s^24p5p$ because this has little influence on the calculation. The fitted average energy value of the $4s^24p^2$ configuration is affected when we include the $4p^4$ and $4s4p^24d$ configurations in the calculation. The fitted value is increased by 8022.74 cm⁻¹ with respect to the experimental energy value. If we consider in the calculation only the $4s^24p^2 + 4s^24p5p$ configurations, the average energy value maintains its real value but the standard deviation increases substantially.

The levels belonging to the $4s4p^24d$ configuration are intermixed with the levels of the $4p^4$ configuration. For this reason we did not fix E_{av} for both configurations in the least-squares fit calculation. The energy parameters ζ_{nl} , $F^k(nl, nl)$ and $G^k(nl, nl)$ for the $4s4p^24d$ configuration were fixed at 1.00, 0.85 and 0.85 of their Hartree–Fock values respectively.

From the $4s^24p^2$ and $4p^4$ we obtained two adjusted parameters (in addition to E_{av}), by linking together all Coulomb parameters $F_2(4p4p)$ in one group and the spin-orbit parameter ζ_{4p} in a second group. A similar procedure was adopted in the work of Cavalcanti *et al* (1996) for Ar v. These authors also include ns^2nd^2 (n = 3) type configurations in the calculation, but in our case (n = 4) this was not necessary because the E_{av} is so far from the other configurations. However, we included the same ns^2np4f (n = 4) type configurations as Gallardo *et al* (1999) for Xe v (n = 5), as this reduces the standard deviation in our calculation. The energy parameters E_{av} , ζ_{nl} , $F^k(nl, nl)$ and $G^k(nl, nl)$ for the ns^2np4f configuration were fixed at 1.00, 1.00, 0.85 and 0.85 of their Hartree-Fock values respectively.

All the configuration integration integrals were held fixed in the calculation at 0.85 of their Hartree–Fock values, except for the direct radial integrals of the $4s^24p^2-4p^4$, $4s4p^24d-4p^4$ and $4s4p^24d-4s^24p4f$ that were fixed in the calculation to 0.75, 0.70 and 0.75 of their Hartree–Fock

Configuration	Parameter	HF value	Fitted value	F/HF			
4s ² 4p ²	Eav	12468	20491 ± 43	1.643 ± 0.003			
	F ² (4p, 4p)	65 984ª	52183 ± 216	0.791 ± 0.003			
	α(4p, 4p)		90 (FIX)				
	ζ4p	4627ª	5008 ± 64	1.082 ± 0.014			
4s ² 4p5p	Eav	289 834	289398 ± 31	0.998 ± 0.001			
	ζ4p	5014	5379 ± 72	1.073 ± 0.014			
	ζ5p	1255	1420 ± 69	1.131 ± 0.055			
	F ² (4p, 5p)	21614	19865 ± 303	0.919 ± 0.014			
	G ⁰ (4p, 5p)	5302	4036 ± 57	0.761 ± 0.011			
	G ² (4p, 5p)	6671	4961 ± 332	0.744 ± 0.050			
4p ⁴	Eav	309959	291684 ± 997	0.941 ± 0.003			
	F ² (4p, 4p)	65 920ª	443212 ± 184	0.672 ± 0.003			
	α(4p, 4p)		0 (FIX)				
	ζ4p	4616ª	4995 ± 63	1.082 ± 0.013			
4s4p ² 4d	E_{av}	335 994	333337 ± 398	0.992 ± 0.001			
	F ² (4p, 4p)	66 699	56 694 (FIX)	0.85			
	α(4p, 4p)		0 (FIX)				
	ζ4p	4769	4769 (FIX)	1.000			
	ζ4d	282	282	1.000			
	F ² (4p, 4d)	52 804	44 884 (FIX)	0.850			
	G ¹ (4s, 4p)	89 160	75 786 (FIX)	0.850			
	G ² (4s, 4d)	44 464	37 795 (FIX)	0.850			
	G ¹ (4p, 4d)	64 06 1	54 452 (FIX)	0.850			
	G ³ (4p, 4d)	39 678	33 726 (FIX)	0.850			
4s ² 4p4f	E_{av}	341 257	341 257 (FIX)	1.000			
	ζ4p	4986	4986 (FIX)	1.000			
	ζ4f	3	3 (FIX)	1.000			
	F ² (4p, 4f)	27 406	23 295(FIX)	0.850			
	G ² (4p, 4f)	18 274	15 533 (FIX)	0.850			
	G ⁴ (4p, 4f)	12 165	10 339 (FIX)	0.850			
Configuration interaction integrals							
4s ² 4p ² -4s ² 4p5p	R ⁰ (4p4p, 4p5p)	2325	1976 (FIX)	0.850			
	R²(4p4p, 4p5p)	10824	9200 (FIX)	0.850			
$4s^24p^2-4p^4$	R ¹ (4s4s, 4p4p)	88 21 1	66 159 (FIX)	0.750			
4s ² 4p ² -4s4p ² 4d	R ¹ (4s4p, 4p4d)	73 683	62 631 (FIX)	0.850			
	R ² (4s4p, 4d4p)	54 405	46 245 (FIX)	0.850			
4s ² 4p ² -4s ² 4p4f	R ² (4p4p, 4p4f)	32 895	27 961 (FIX)	0.850			
4s ² 4p5p-4s4p ² 4d	R ¹ (4s5p, 4p4d)	-2359	-2005 (FIX)	0.850			
	R ² (4s5p, 4d4p)	7837	6662 (FIX)	0.850			
4s ² 4p5p-4s ² 4p4f	R ² (4p5p, 4p4f)	9187	-7809 (FIX)	0.850			
•	R ² (4p5p, 4p4f)	2381	2025 (FIX)	0.850			
4p ⁴ 4s4p ² 4d	R ¹ (4p4p, 4s4d)	73 265	51 285 (FIX)	0.700			
4s4p ² 4d-4s ² 4p4f	R ¹ (4p4d, 4s4f)	46 595	34 946 (FIX)	0.750			
	$R^{2}(4n4d 4f4s)$	27418	23 306 (FIX)	0.850			

Table 4. Energy parameters (cm⁻¹) for the even-parity configurations of Kr v studied. (Note: the values for the E_{av} listed in the column 'HF value' were obtained by adding the experimental average energy of the ground configuration to the Hartree–Fock values.)

^a Linked parameters. These parameters were linked (i.e. the mutual ratios of their values remained constant during the iteration) during the least-squares calculation (Cowan 1981).

values respectively. In this way we achieved better results in the least-squares fit. The standard deviation was 82 cm^{-1} .

Acknowledgments

We are grateful to Dr W Persson and Dr S-G Pettersson for the use of experimental facilities, and support from the Swedish Natural Science Research Council (NFR), the Conselho Nacional de Desenvolvimiento Científico e Tecnológico, Brazil, the Fundação de Amparo à Pesquisa do Estado de São Paulo (Fapesp), Brazil and the Consejo Nacional de Investigaciones Científicas y Técnicas (CONICET). The Comisión de Investigaciones Científicas (CIC) de la Provincia de Buenos Aires, Argentina, where MR, FB and JRA are researchers, is gratefully acknowledged.

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