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RESULTADO  
DE LAS  
OBSERVACIONES CON LA ECUATORIAL  
DE 433 MILÍMETROS DE ABERTURA  
DE 1912 A 1917

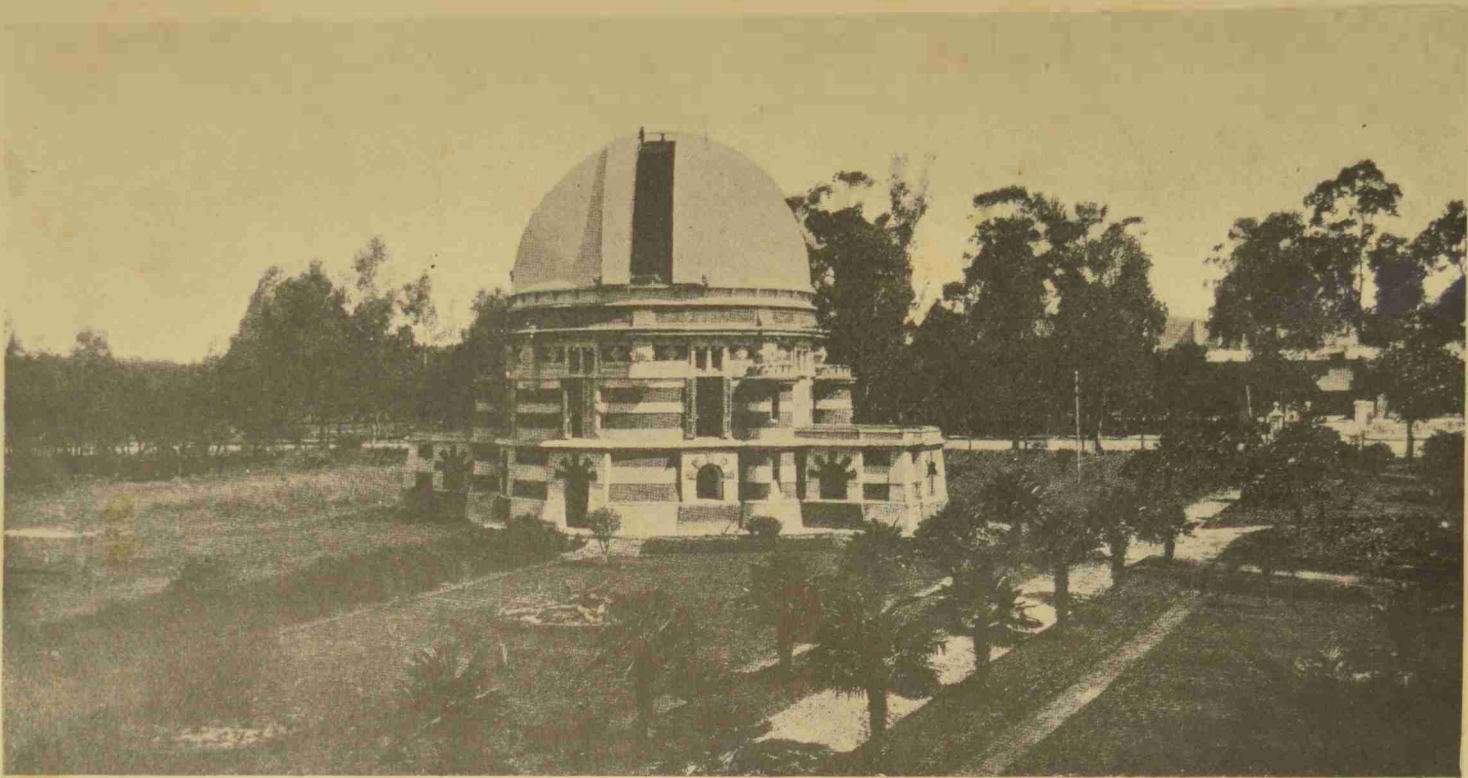


Imprenta y Casa editora CONI, Perú 684, Buenos Aires

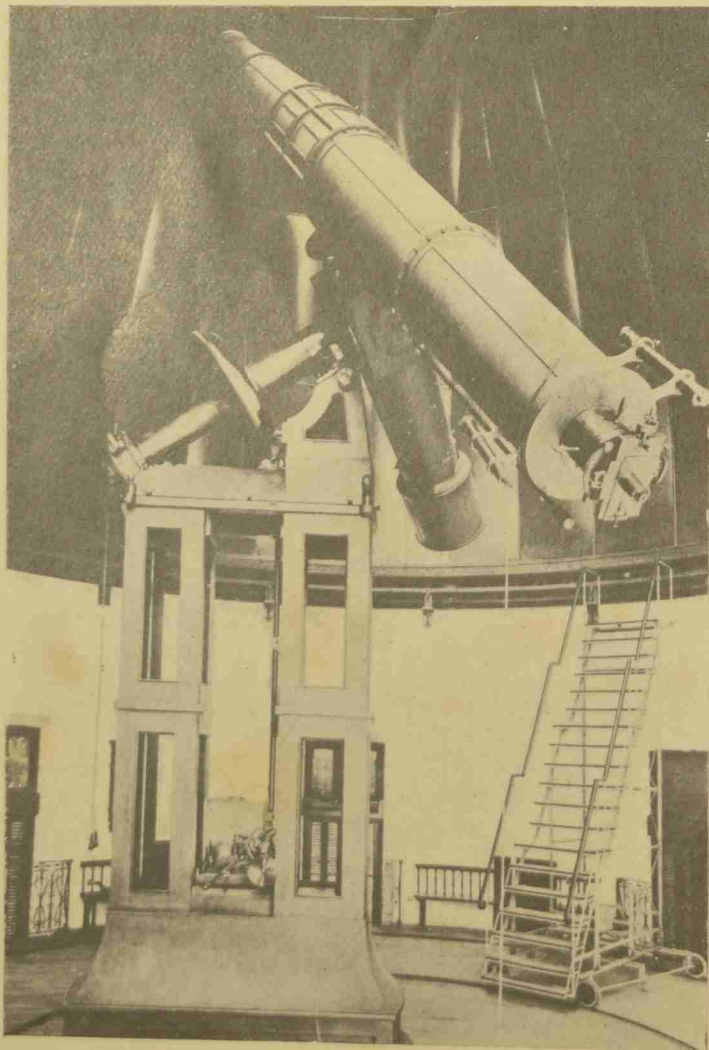




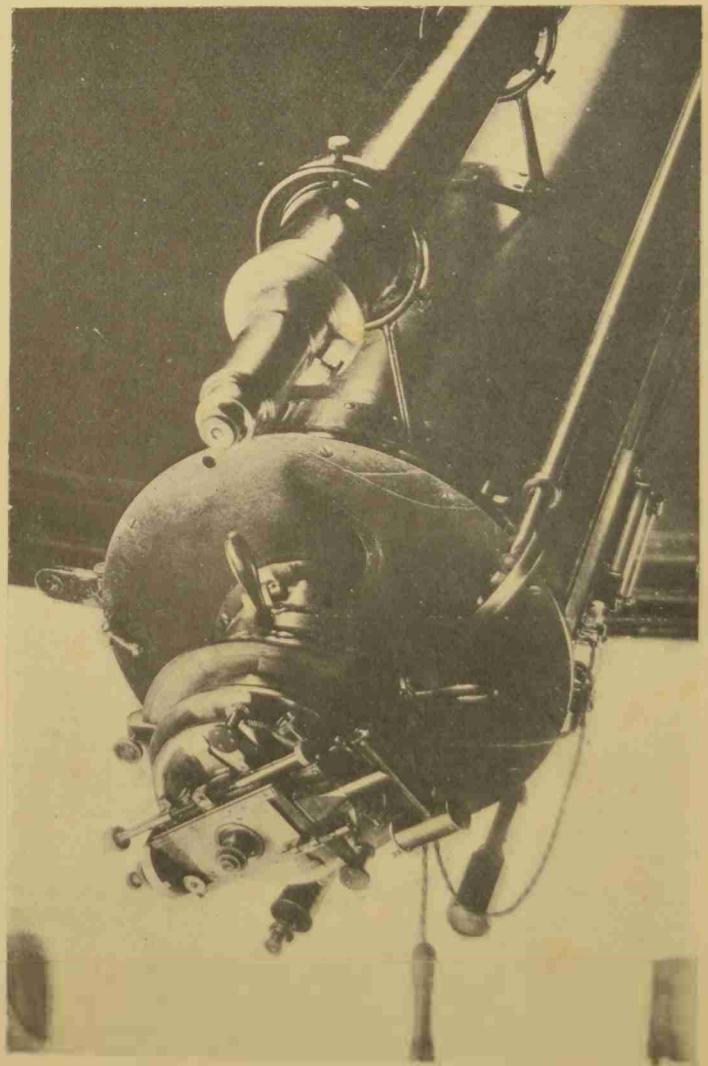




EDIFICIO DE LA ECUATORIAL



EL ANTEOJO



EL MICRÓMETRO NUEVO



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UNIVERSIDAD NACIONAL DE LA PLATA  
OBSERVATORIO ASTRONÓMICO

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RESULTADO  
DE LAS  
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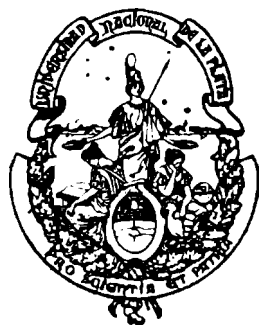
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BERNHARD H. DAWSON



TOMO IV (PARTE I<sup>a</sup>)

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LA PLATA  
OBSERVATORIO ASTRONÓMICO

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THIS WORK IS INSCRIBED TO  
SILVIA KAUDY DAWSON  
WHO HAS CONTINUOUSLY AIDED  
BY INSPIRATION AND BY MATERIAL ASSISTANCE  
TOWARDS ITS PROSECUTION



# MICROMETRIC MEASURES OF DOUBLE STARS

## MEDIDAS MICROMÉTRICAS DE ESTRELLAS DOBLES

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### INTRODUCTION

*Plan and Scope of the Work.* — The principal program has always been the observation of known double stars, especially those discovered by Sir John Herschel at the Cape and published in his *Results of Astronomical Observations at the Cape of Good Hope*. This volume contains a list of over 2100 pairs noted in the course of that work, many of which are still unidentified and unmeasured, and since Prof. Hussey's program of discovery was expected to occupy the nights of best definition, it seemed to be the best source of a working list. As my stay at this Observatory was at first considered temporary (and was in fact interrupted, 1914-16) the entire list seemed out of the question. A tentative selection was accordingly made, rejecting the widest and faintest pairs, and work on this list was begun October 27, 1912.

Conversations with Prof. Hussey, especially while working together in the dome, led to the inclusion of more and more other pairs among those observed, both wide and faint ones of the Herschel list and many of other observers, until the plan of work was changed early in 1913. After that time the work was on the basis of a limited area rather than a selected list and in working over an area *all* stars of Herschel's catalog were

### INTRODUCCIÓN

*Plan del trabajo.* — El programa principal ha sido siempre la observación de estrellas dobles conocidas, especialmente las descubiertas por Herschel durante su estadía en el Cabo de Buena Esperanza y que forman una lista de más de 2100 en su publicación: *Results of Astronomical Observations at the Cape of Good Hope*. Muchas estrellas de esta lista quedan todavía sin identificación ni medidas, y en vista de que el programa del profesor Hussey exigiría las mejores noches, creí conveniente ocuparme principalmente de esa lista. Como mi permanencia en este Observatorio fué considerada al principio como temporánea (fué en realidad interrumpida, 1914-16), la lista entera pareció demasiado e hice una selección rechazando las estrellas más débiles y de gran separación. Empecé las observaciones el 27 de octubre de 1912.

Nuestras conversaciones con el profesor Hussey, especialmente mientras trabajábamos en la cúpula, nos llevaron a incluir nuevas parejas de la lista de Herschel y de otros observadores hasta que terminamos por cambiar el programa de observación a principios de 1913. Desde entonces el trabajo se ha extendido a un área limitada y no a una lista seleccionada de gran área, y al observar una de éstas se ha medido todas las estrellas del catá-

measured and as many other pairs besides as was found convenient.

Two consistent measures have usually been considered sufficient for the wider pairs, while three have been given to those with less separation. For pairs of the Herschel list the division has been made at about ten seconds and for others, five seconds. The greatest variation with which the measures were considered consistent depends on the separation and magnitudes, being on the order of a quarter of a second of arc for the average pair of ten to fifteen seconds separation. With stars known or suspected to be binary greater care has usually been taken and additional measures made. I also publish single measures of a few faint stars which differ so much from Herschel's description that the identity seems doubtful, and of several wider companions not measured by the original observers. This work has been continued since my return to La Plata in 1916, the only variation being that the proportion of stars other than Herschel's has been somewhat less.

This will doubtless seem an uninteresting and perhaps even useless program to those so favorably situated as to have a large proportion of nights with good definition. But it is a fact that our atmospheric conditions rarely allow us to use the full power of the instrument (which is really excellent) and a program made up solely of «interesting» stars would be unobservable the greater part of the time. On the other hand there is the precedent of no less an authority than Prof. Burnham (*General Catalogue of Double Stars*, Intro., p. VI) for the measurement of the wide and faint pairs of the old observers.

The work was started at declination  $-42^\circ$  and has now been pushed to a southern limit ranging

logo de Herschel, más todas aquellas que se juzgó conveniente.

Generalmente he considerado dos medidas concordantes como suficientes para las parejas de mucha separación, mientras he hecho un mínimo de tres de las más juntas. Para las estrellas de la lista de Herschel esta división se ha hecho a los  $10''$ , más o menos, y a los  $5''$  para las de otros observadores. La mayor variación con que las medidas se han considerado concordantes depende de la separación y de las magnitudes de los componentes, siendo cerca de un cuarto de segundo para una pareja típica de  $10''$  ó  $15''$  de separación. Muchas veces he dedicado más cuidado y medidas adicionales a las estrellas binarias, conocidas o sospechadas. De vez en cuando aparece una sola medida de alguna estrella muy débil que difiere tanto de la descripción de Herschel que parece no tratarse de la misma o de algún componente que no fué medido por el observador original. El trabajo ha sido continuado desde mi vuelta a La Plata en 1916 y la única variación ha consistido en la disminución en la proporción de estrellas no pertenecientes a la lista de Herschel.

Probablemente algunos observadores situados ventajosamente y que cuentan con una mayoría de noches con excelentes imágenes, considerarán este programa como de poco interés, y aun posiblemente como inútil. Pero es un hecho que nuestras condiciones atmosféricas raras veces nos permiten usar todo el poder del aparato, que es sumamente bueno, y que durante la mayor parte del tiempo sería imposible trabajar con un programa de observación compuesto sólo de las estrellas «interesantes». Por otra parte hay el precedente del renombrado observador Burnham (*General Catalogue of Double Stars*, introducción página VI) y de otros, relativo a la observación de parejas débiles y muy separadas de los observadores antiguos.

El trabajo se empezó en declinación  $-42^\circ$  y se ha llevado hasta un límite austral que varía de



from  $-58^\circ$  in a few parts of the milky way to  $-78^\circ$  in the last three hours of right ascension, including something over an eighth of the area of the celestial sphere and about half the area expected to be covered eventually. 3860 measures are here published. They are of 1305 stars, or 1448 pairs counting triples twice, and in connection with the few negative results given they account for 985 numbers of the 2107 in the Herschel Cape list. It is intended to carry this survey southward to the pole and northward at least to  $-30^\circ$  and perhaps to  $-22^\circ$ . In either case I hope also to make a review of those stars of Herschel's Cape list north of the bounding parallel that have not been identified and measured by some former observer. Tho this program is now only half completed, yet it seems advisable to publish the available results at this time rather than to delay their publication until the completion of the whole.

Among those stars not of the Herschel list will be found several with the names Aguilar and Delavan. These observers have communicated lists of stars seen double or suspected to be double in their work with Gautier meridian circle. Some of these lists have not yet been revised, but all stars from them that have been measured are here included. Personally I have made no search for new pairs except an occasional examination of intermediate stars when passing from one pair to another. A few of the stars so examined and several looked at for other reasons have been found double and the name Dawson given to them. Other pairs and many additional companions to old pairs have been measured, but have not been considered worthy of separate designation.

A list of neglected stars between declinations  $-10^\circ$  and  $-31^\circ$  was communicated in 1916 by Prof. Eric Doolittle of the Flower Observatory, Philadelphia, and several of the best nights since

$-58^\circ$  en algunas partes de la vía láctea a  $-78^\circ$  en las últimas tres horas de ascensión recta, incluyendo un poco más de un octavo de la superficie de la esfera celeste y alrededor de la mitad del área que espero observar. 3860 medidas están incluidas en la presente publicación. Corresponden a 1305 estrellas, o 1448 pares, contando las triples como dos, y teniendo en cuenta los pocos resultados negativos indicados, explican 985 números de los 2107 en la lista de Herschel. Me propongo extender este estudio hacia el sur hasta llegar al polo y hacia el norte hasta declinación  $-30^\circ$  cuando menos, y tal vez hasta  $-22^\circ$ . En cualquiera de los casos espero hacer una revista adicional de las estrellas de esta lista, situadas al norte del límite, que todavía carecen completamente de medidas e identificación. Aunque este programa no está sino medio concluído, me parece más conveniente publicar ahora los resultados ya obtenidos que esperar hasta la conclusión del trabajo entero.

Entre las estrellas que no son de la lista de Herschel están varias con los nombres Aguilar y Delavan. Estos observadores me han comunicado listas de estrellas notadas como dobles o probablemente dobles en su trabajo con el Círculo meridiano Gautier. Todavía no he revisado todas las estrellas de estas listas, pero las que he observado están incluídas aquí. Yo mismo no he buscado parejas nuevas, fuera de una ocasional mirada a las estrellas intermedias pasando de una del programa a otra. Unas pocas de las estrellas así examinadas y varias de las que he observado con otros fines he encontrado que son dobles y les he dado el nombre Dawson. También he medido muchos pares o componentes adicionales de pares viejos sin considerarlos dignos de designación especial.

El profesor Eric Doolittle, del Flower Observatory, Philadelphia, me comunicó en 1916, una lista de estrellas entre declinaciones  $-10^\circ$  y  $-31^\circ$  que necesitan observaciones. Algunas de

its receipt have been devoted to the measurement of stars from this list. These measures and those of other stars north of declination  $-31^\circ$  have been put into a separate list to facilitate reference on the part of northern observers.

*Telescope and Micrometers.* — The 17 inch Gautier refractor described on pages 39 to 45 of vol. I. of these Publications was used thruout the work, in connection with the two micrometers there described. In addition to these descriptions it may be noted that until March 1913 the only eyepiece available with the (small) micrometer was one of power 300 but with very limited field. During that month eyepieces of powers 280, 420, 666 and 1300  $\pm$  were adapted. Even after this the old 300 continued to be used by preference when its magnification was sufficient, and the 1300 was never used except for the determination of coincidence.

The eyepieces of the Warner and Swasey micrometer are by Alvan Clark and Sons, and give powers of 150 (not used for double star work), 370, 475, 650 and 1125. The 370 has been used for the greater part of the work, changing usually to the 650 when more magnification was needed.

Thru a misinterpretation of the data sent to Ann Arbor for vol. I. of these Publications a slightly erroneous result was derived for the value of the screw. The first two probable errors given on page 44 of vol. I. are the probable errors of the connections only, and do not include the uncertainty of the places of the stars employed. The weights assigned to these determinations in forming the mean were consequently much too large. The paragraph should be changed to read as follows :

las mejores noches, después de recibir la comunicación, las dediqué a medir estrellas de esa lista. Estas medidas y las de otras estrellas al norte de declinación  $-31^\circ$  las he puesto en una lista separada para facilitar la referencia a los observadores del norte.

*Anteojo y Micrómetros.* — La ecuatorial Gautier de 433 milímetros de abertura, descrita en páginas 39 a 45 del primer tomo de estas publicaciones, ha sido usada para todo este trabajo en conexión con los dos micrómetros ahí mencionados. Además de las descripciones citadas conviene notar que hasta marzo de 1913 el único ocular disponible con el (pequeño) micrómetro era uno de aumento de 300 veces, pero con campo muy limitado. Durante ese mes se adaptaron oculares con aumentos de 280, 420, 666, y 1300  $\pm$ . Se continuó usando de preferencia el ocular viejo cuando su aumento era suficiente. El de 1300 ha sido usado únicamente para determinaciones de coincidencia.

Los oculares del micromero por Warner and Swasey fueron hechos por Alvan Clark and Sons, y dan aumentos de 150 (no usado para estrellas dobles), 370, 475, 650 y 1125. El de 370 se usa para la mayoría de las medidas, siendo reemplazado generalmente por el de 650 cuando mayor aumento es necesario.

Por una mala interpretación de los datos mandados a Ann Arbor para el tomo I, el valor del paso del tonillo allí publicado merece una pequeña corrección. Los primeros dos errores probables que figuran en la página 44 del tomo I son de la conexión únicamente, y no incluyen la incertidumbre de las posiciones de las estrellas empleadas. Los pesos dados a estas observaciones al tomar el promedio eran pues demasiado grandes. El párrafo debe cambiarse de la manera siguiente :



... From his measures of the difference of the declinations of 176 B. and 181 B. Geminorum he obtained

$$R = 11''.575 \pm 0''.015,$$

and from  $\varepsilon$  and 102 B. Cancri,

$$R = 11''.584 \pm 0''.009,$$

using in both cases the places derived from Hedrick, *Catalogue of Zodiacal Stars* (*Astr. Papers of the Amer. Ephemeris*, vol. VIII, part 3). From the transits of 7 G. Octantis he obtained

$$R = 11''.5812 \pm 0''.0016$$

and from three series of transits of  $\zeta$  Octantis,

$$R = 11''.5798 \pm 0''.0020,$$

$$R = 11.5719 \pm 0.0020,$$

$$R = 11.5794 \pm 0.0014.$$

Combining these results according to their weights, we have

$$R = 11''.5786 \pm 0''.0009$$

as the value of one revolution...

... De sus medidas de la diferencia de las declinaciones de 176 B. y 181 B. Geminorum obtuvo

$$R = 11''.575 \pm 0''.015,$$

y de  $\varepsilon$  y 102 B. Cancri,

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usando en ambos casos posiciones basadas en el *Catálogo de Zodiacal Stars* por Hedrick (*Astr. Papers of the Amer. Ephemeris*, vol. VIII, parte 3<sup>a</sup>). De los pasajes de 7 G. Octantis obtuvo

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$$R = 11''.5798 \pm 0''.0020,$$

$$R = 11.5719 \pm 0.0020,$$

$$R = 11.5794 \pm 0.0014.$$

Combinando estos resultados según sus pesos correspondientes, tenemos

$$R = 11''.5786 \pm 0''.0009$$

como valor medio de una vuelta del tornillo...

*Methods of Observing.* — The method of observing is believed to be substantially that of Burnham and other North American double star observers. Each measure given is the mean of at least four settings of the micrometer in position angle and of at least three double distances, with the exception of a few very wide stars for which single distance was observed, but a correspondingly greater number of settings made. In case of discordance among the individual settings their number was increased, so that the average number of settings is probably nearly five in each coördinate.

Except in a few sporadic cases of very faint companions, all the settings in position angle are made with a single wire, the other being placed so far away as not to have any influence on the judgment of parallelism. In making the setting the wire is brought parallel to the line joining the two stars by successive approximations from alternate sides, like a strongly damped vibration. After removing the hand from the pinion which rotates the micrometer the setting is checked by

*Método de Observación.* — Creo que el método de observación seguido por mi es, en substancia, igual al de Burnham y otros observadores norteamericanos. Cada medida publicada es el promedio de cuatro o más lecturas del círculo de posición y de tres o más distancias dobles, con la excepción de algunas parejas muy separadas en que la distancia simple se ha observado pero con mayor número de lecturas. En caso de mucha variación entre las lecturas, su número ha sido aumentado, de tal manera que en promedio son casi cinco en cada coordenada.

Exceptuando unos pocos casos aislados de compañeras muy débiles, toda observación de ángulo de posición se hace con un solo hilo, poniendo el otro a tal distancia que no influya sobre la observación. El hilo se lleva a coincidir con la línea entre las imágenes mediante aproximaciones sucesivas de lados alternados, como una vibración fuertemente amortiguada. Después de levantar la mano del tornillo que mueve el micrómetro, la observación se comprueba mirando las estrellas a

observing the stars on each side of the wire before reading the circle. After reading the circle and before returning the eye to the telescope the micrometer is rotated thru at least  $45^\circ$  to make the new setting independent of the preceding. In measuring the distances the wires are placed as accurately as possible on the centres of the images of the two stars. In the measurement of close pairs care is taken to make the last movement of the micrometer screw always in the direction of increasing readings, altho determinations of coincidence made for the purpose indicate that the lost motion is less than  $0^{\text{m}}001$ . In all these measurements the line joining the eyes is kept either parallel or perpendicular to the micrometer wires, using the latter position whenever possible. Since the first few months, only the right eye has been used, it being almost entirely free from astigmatism.

Parallel is checked at least once each night in that part of the sky in which the work is being done, and if the instrument is used in widely different positions on the same night, it is determined for each. This has been found more convenient than the observation of an equatorial star near the meridian, and for work in the higher declinations it is more accurate as well.

No special effort has been made to divide the observations of a pair between east and west of the meridian, tho that has been considered an advantage and has been done whenever convenient. Neither has any definite limiting distance from the meridian ever been set, tho work at great zenith distances has been avoided as far as possible. At zenith distances of from ten to thirty degrees the position of the eye end of the telescope with respect to the observing chair is quite inconvenient and consequently very few measures have been made with the telescope in this position. Many successive nights of cloudiness

cada lado del hilo antes de leer el círculo. Después de la lectura y antes de volver el ojo al ocular giro el micrómetro de un ángulo de  $45^\circ$  o más para que la nueva observación sea independiente de la anterior. Para medir la distancia pongo los hilos tan exactamente como es posible en los centros de las imágenes de las dos estrellas. Midiendo pares de poca separación tengo cuidado de hacer el último movimiento del tornillo siempre en el sentido en que crecen las lecturas, aunque determinaciones de coincidencia hechas con el propósito de conocer el valor del paso muerto indican que es menos de  $0^{\text{m}}001$ . En todas estas observaciones la línea entre los ojos se mantiene o paralela o perpendicularmente a los hilos del micrómetro, siendo preferida la posición perpendicular cuando es posible. Después de los primeros meses he usado sólo el ojo derecho que está casi libre de astigmatismo.

La lectura del paralelo se comprueba una vez en cada noche de observación en la misma parte del cielo en que están las estrellas observadas, y si el instrumento se usa para observar en posiciones muy distintas, se la determina en todas las posiciones usadas. Esto resulta más cómodo que la observación de una estrella ecuatorial cerca del meridiano, y para las estrellas cerca del polo es además más exacto.

No he hecho esfuerzos especiales para repartir las observaciones de una estrella entre este y oeste del meridiano aunque esto se considera una ventaja y se ha hecho cuando era conveniente. Tampoco he puesto límite al ángulo horario de observación, pero he evitado en cuanto fué posible la observación en grandes distancias cenitales. Con distancia cenital de diez a treinta grados la posición del ocular con respecto de la silla de observación es muy incómoda y pocas medidas han sido hechas con el aparato en esta posición. Varias veces una sucesión de muchas noches nubladas o de malas imágenes ha llevado estrellas parcial-

and poor seeing have often carried partially observed stars considerably to the west and into undesirable positions, making it necessary either to observe them there or to leave them till the following year. These have frequently been observed at considerable hour angles in preference to leaving them and the area containing them incomplete. Tho this is not good practice, yet it is that that with pairs of such minor importance as the majority of these, the loss in accuracy will not appreciably affect the value of the results.

The work at the telescope is facilitated by charts on a scale of  $2\frac{1}{4}$  inches to the degree, or nearly 1 mm. = 1', containing stars to magnitude 9.1 or 9.2 inclusive, plotted from the *Córdoba Durchmusterung* within the region covered by that work and from the *Cape Photographic Durchmusterung* further south. While their preparation required considerable time and energy, the saving of time at the instrument, especially on the really good nights, is ample recompense, as they do away with almost all reading of the circles and aid immensely in the rapid identification of the fainter pairs.

*Errors of Observation.* — The absolute magnitude of the errors of double star measures is probably considerably less than in most other lines of astronomical research, but on account of the smallness of the quantities measured the errors often become of considerable importance. As in almost all observations, they are both systematic and accidental, but in the case of double star measures the separation of the systematic errors from those which may be considered accidental is a matter of extreme difficulty. Could they be disentangled, it would be a simple matter to remove the systematic error by the application of proper corrections. Otto Struve and several other observers have attempted this separation

mente observadas muy al oeste. Así resultaba necesario observarlas en posiciones poco deseables o dejarlas hasta el año próximo. Frecuentemente se ha preferido observarlas en ángulos horarios muy grandes a dejar a ellas y al área que las contiene incompletamente medidas. Sé que ésta no es una buena práctica, pero con pares de importancia limitada, como son la mayoría de éstos, la pequeña pérdida de exactitud no ha de tener influencia apreciable en el valor de los resultados.

La observación se facilita con cartas en una escala de 58 milímetros por grado, o sea casi 1 mm. = 1', que contienen las estrellas hasta magnitud 9.1 ó 9.2. Estas fueron hechas con las *Zonas de Exploración* de Córdoba dentro de la región contenida en esta obra y con la *Cape Photographic Durchmusterung* más al sur. Su preparación es algo larga y cansadora, pero el ahorro de tiempo en la observación compensa ampliamente, porque evitan casi toda lectura de los círculos y ayudan muchísimo en la identificación rápida de los pares débiles.

*Errores de Observación.* — La magnitud absoluta de los errores de medidas de estrellas dobles es probablemente mucho menor que en la mayoría de las observaciones astronómicas, pero la pequeñez de las distancias observadas los hace de mayor importancia. Como en casi toda observación, hay errores sistemáticos y accidentales, pero en las medidas de estrellas dobles la separación de los errores sistemáticos de los que pueden considerarse accidentales es un problema difícilísimo. Si pudiesen separarse, sería cosa simple librar las observaciones de errores sistemáticos mediante la aplicación de correcciones apropiadas. Otto Struve y varios otros observadores han intentado esta separación y han calculado y aplicado correc-



and have computed and applied corrections to their measures, but later observers have found that these corrections increase the discrepancies almost as often as they diminish them, and the general opinion seems to be that they are not of sufficient value to repay the labor involved in their derivation. In view of this, no attempt has been made to investigate the measures of the present series for systematic error, either in position angle or in distance. In addition to the data here published a record has usually been kept of whether the eyes were parallel or perpendicular to the wires. I have also some manuscript tables of zenith distance and position angle of the vertical, prepared as a basis for the computation of tables of differential refraction. Should anyone care to undertake an investigation of systematic errors these additional data will gladly be furnished him. In the absence of any discussion it may be stated that it is my *belief* that the effects of systematic error are always considerably smaller than the mean accidental error, and that they are practically limited to the following cases :

1. Stars which present themselves at such an angle that the head must be strongly inclined are recorded too near the vertical with eyes perpendicular, and too near the horizontal with eyes parallel to the wires.

2. Close pairs, especially if bright, are measured too wide with poor definition. This effect is believed to be much smaller in the observations with the new micrometer.

The mean accidental errors can be more easily determined, as they are but little affected by the assumption that no systematic error is involved. With such a heterogeneous list as the present, whose distances range from  $0''.2$  to over  $200''$  and whose combined magnitudes range from 0.2 to 12, no single set of values could be expected to ex-

ciones a sus medidas, pero observadores posteriores han encontrado que estas correcciones aumentan las divergencias casi tan frecuentemente como las disminuyen, y la opinión general parece ser que la ventaja obtenida no justifica el trabajo de calcularlas. Teniendo esto en cuenta, no he pretendido investigar los errores sistemáticos, ni en ángulo de posición ni en distancia, en las medidas de la presente publicación. Además de los datos aquí publicados se ha notado generalmente si la línea entre los ojos estaba paralela o perpendicular a los hilos. También tengo tablas en manuscrito de la distancia cenital y del ángulo de posición de la vertical, calculadas para servir de base a una tabla de refracción diferencial. En el caso que alguien se muestre interesado por hacer una investigación de errores sistemáticos, estos datos se pondrán a su disposición. Faltando tal investigación, indico que es mi opinión que los efectos de error sistemático son siempre mucho menor que el error medio accidental, y que se limitan a los siguientes casos :

1° Aquellas estrellas cuya posición exige una fuerte inclinación de la cabeza, aparecen demasiado cerca de la vertical cuando se observan con la línea de los ojos perpendicularmente, y demasiado cerca de la horizontal cuando con los ojos paralelamente a los hilos ;

2° Parejas muy juntas, especialmente las brillantes, se observan demasiado separadas con malas imágenes. Creo que este efecto es mucho menos notable en las medidas con el micrómetro nuevo.

Es mucho más fácil determinar los errores medios accidentales porque la asunción que no envuelven error sistemático tiene poco efecto en su determinación. Con una lista tan heterogénea como la presente, cuyas distancias varían de  $0''.2$  hasta más de  $200''$  y las magnitudes desde 0.2 hasta 12, no debemos esperar que un solo par de

press the probable errors of the measures. Accordingly four characteristic groups were defined on the basis of separation and difference of magnitude, and the probable errors of observation determined by taking at random fifty stars of each group and comparing the individual observations with their respective means. A fifth set of values was obtained from a comparison of my measures with the mean of all observers in the case of a few of the best determined stars showing no motion and with what seemed the best ephemerides in the case of a few well determined binaries and relative proper motion pairs. This last of course includes the systematic errors with the accidental and leads us to larger values. The results are given in the following table.

valores pueda expresar el error probable de una observación. He definido, pues, cuatro grupos característicos a base de distancia y diferencia de magnitud, y tomando al acaso cincuenta estrellas de cada grupo he determinado sus errores probables comparando las observaciones individuales con sus promedios correspondientes. Un quinto par de valores fué obtenido con una comparación de mis observaciones con los promedios de todos los observadores en algunas estrellas bien determinadas pero fijas, y con las mejores efemérides de otras en movimiento. Los resultados figuran en el siguiente cuadro :

**ERRORES DE OBSERVACIÓN**

Pares	Magnitudes medias		Distancia media	Error probable de una medida		
				$\Delta P$	$s\Delta P$	$\Delta s$
Iguales, juntos . . . . .	8.1	8.5	2".7	$\pm 1.06$	$\pm 0.04$	$\pm 0.06$
Desiguales, juntos . . . . .	7.2	10.4	4.6	0.99	0.07	0.08
Iguales, separados . . . . .	8.8	9.1	20.3	0.19	0.07	0.08
Desiguales, separados . . . . .	7.3	11.3	27.9	0.27	0.13	0.11
Bien determinados . . . . .	3.3	5.2	3.9	0.89	0.06	0.10

As an indication of the relative accuracy which could be expected of the different measures, the seeing has been recorded at the time of making each measure. This is on a scale of five, later subdivided to ten by the use of the half unit and even further by the use of + and —, which last have not been retained in the publication. The five units of the scale have approximately the following significance :

- 5. Ideal conditions.
- 4. Diffraction pattern well defined; equal pairs easily measurable down to about 0".3.

Como una indicación de la exactitud que podía esperarse de las distintas medidas, he notado la condición de las imágenes en el momento de cada medida. He usado una escala de cinco, que pronto fué subdividida en diez, y aun más con los signos + y —, los cuales se han omitido en la publicación. Las cinco unidades de la escala corresponden aproximadamente a las condiciones siguientes :

- 5. Condiciones ideales.
- 4. Dibujo de difracción bien definido; pares iguales de 0".3 y más pueden observarse fácilmente.

3. Diffraction pattern just showing; equal pairs of 1" and over well measurable.
2. No diffraction pattern visible. Stars appear as fuzzy balls about 1" in diameter or as vibrating points with about 1" amplitude.
1. Star images mere blurs of 3" to 5" and more diameter. Work of any value impossible.

It will be noted that these relate entirely to definition and take no account of clouds, haze or moonlight. So long as these elements leave the stars distinctly visible it has been considered that they do not appreciably affect the accuracy of the measures.

*Nomenclature and Places.* — It has been the general aim not only to name each star after its discoverer but also to give the designation applied to it by any subsequent observer who has recorded it as new. The chief exception to this has been that no attempt has been made to find the ultimate discoverers of the Dunlop and Rümker pairs. A star noted at Paramatta as double is given the corresponding designation and that applied by any subsequent observer who considered it new. Furthermore, reference to the Brisbane catalog itself has been omitted when the star appears in either of the other Paramatta lists.

Gilliss did not claim to have discovered the stars in his list, and his number is given in the body of the work only in case he first observed the star, but in the index I have tried to give reference to all stars of his list which have been observed.

The identifications have been made principally in the *Cape Photographic Durchmusterung*, and this is to be understood with any *durchmusterung* number not accompanied by letters indicat-

3. Dibujo de difracción apenas visible; pares iguales de 1" y más bien observables.
2. Dibujo invisible. Las estrellas aparecen como capullos de algodón de cerca de 1" de diámetro o como puntos vibrantes con amplitud de 1".
1. Las estrellas parecen masas difusas de 3" a 5" y más de diámetro. Imposible obtener observaciones de valor.

Se notará que estas definiciones se refieren enteramente a la nitidez de las imágenes y no tienen en cuenta las nubes, la neblina o la luz de la luna. Mientras estos elementos no oculten las estrellas he considerado que no tienen influencia en la exactitud de las medidas.

*Nomenclatura y posiciones.* — En conexión con cada estrella ha sido mi intención dar no sólo el nombre del que la descubrió, sino también la designación aplicada por todo subsiguiente observador quien la consideró como nueva. La excepción principal consiste en que no he pretendido citar observadores anteriores a los de Paramatta. A las estrellas que aparecen en las listas de Dunlop y Rümker o que están como dobles en el catálogo de Brisbane he dado la designación correspondiente y las de observadores subsiguientes. Tampoco he dado referencia del catálogo de Brisbane cuando aparece la estrella en una de las dos listas.

Gilliss no pretendió haber descubierto las estrellas de su lista, y he hecho referencia a ella en las medidas únicamente en los casos en que él era el primero en observar la estrella. Sin embargo, en el índice he hecho referencia a toda estrella observada que aparece en su lista.

Las identificaciones han sido hechas principalmente en la *Cape Photographic Durchmusterung* y ésta debe entenderse con cualquier número cuando no hayan letras que indiquen otra obra.



ing a different work. When the star was not found in the C. P. D. the *Córdoba Durchmusterung* was referred to. If not found there the star was considered anonymous. All stars in connection with which a constellation name had been noted and others which from their brightness were thought likely to have a constellation letter were looked up in the *Uranometría Argentina* and in case a letter was there found it has been substituted for the C. P. D. number. Some lettered stars may however have been overlooked. The Greek letters in the constellation Argo have been used with that name and not with those of the subdivisions.

The C. P. D. and Córdoba epoch of 1875.0 has been used for the places. It is believed that but little inconvenience will be caused by the use of this epoch, as the C. P. D. precession tables afford an easy reduction to 1900.0 and anyone wishing accurate places is almost certain to go to catalogs for 1875.0 or other epoch near that. For identification in other lists of double stars a mental estimate of the precession is almost always sufficient. Concerning stars not in other lists, it may be noted that after the completion of the present program I hope to publish a comprehensive index list of stars south of declination  $-30^\circ$  (or perhaps some other limit) which have been noted as double, reducing the places to 1950.0.

In the list of stars north of  $-31^\circ$  on pages 109 to 114 the places are for 1880.0, in conformity with Burnham's *General Catalogue*.

*Magnitudes.* — As this is not a catalog, but a series of micrometric measures, the question of magnitudes has been considered entirely secondary. The magnitudes given with the means are in general the means of the estimates on the various nights of observation. Since some consider that only the difference of magnitude should be

Cuando la estrella no se encuentra en la C. P. D. la he buscado en las *Zonas de Exploración* de Córdoba. Si tampoco se encuentra ahí, la he considerado anónima. Toda estrella en que había notado un nombre de constelación y otras que por su brillo lo pudieron tener, las he buscado en la *Uranometría Argentina* y en caso de encontrar una letra en ésta, la he usado en vez del número de la C. P. D. Pero puede ser que algunas estrellas con letra me hayan escapado. Las letras griegas, dentro de la constelación Argo, han sido usadas con este nombre y no con los de las subdivisiones.

He usado el equinoccio de 1875.0 que es común a la C. P. D. y a las publicaciones de Córdoba. Creo que ninguna incomodidad resultará del uso de esta época, porque las tablas de precesión que acompañan la C. P. D. dan una reducción fácil a 1900.0 y el que quiera posiciones más exactas casi siempre las buscará en un catálogo con equinoccio de 1875 u otro cercano. Para la identificación en las otras listas de estrellas dobles basta una estimación mental. En cuanto a las estrellas no contenidas en otras listas conviene notar que después de la conclusión del programa actual, espero publicar una lista en forma de índice que comprenderá toda estrella al sur de  $-30^\circ$  (u otro límite) que ha sido notada como doble, con posiciones para 1950.0.

Para las estrellas al norte de  $-31^\circ$  contenidas en páginas 109 a 114 he usado posiciones para 1880.0 conforme con el *General Catalogue* de Burnham.

*Magnitudes.* — Siendo ésta una serie de medidas micrométricas, y no un catálogo, las magnitudes se han considerado como asunto completamente secundario. Las magnitudes que se dan con los promedios son en general los promedios de las magnitudes apreciadas en las noches de observación. Como algunos consideran que debe obser-

observed, leaving the combined magnitude to other authority, the *durchmusterung* magnitude has been given immediately after the *durchmusterung* number and may be combined with the difference of the observed magnitudes by the usual formulas.

In case both components have been noted in the C. P. D. their numbers and magnitudes are both given, tho a few companions separately recorded there may have escaped my notice. When the colon (:) is there given to indicate that the image appears double on the plates, the same sign is here appended to the magnitude. In case the star was observed as one in the C. P. D. but was recorded as two in the *Córdoba Zone Catalogue*, the fact is indicated by placing the magnitude in *italics*, as was done in the C. P. D. reference to that work.

The observed magnitudes are on a subjective and probably variable scale which is believed to be between those of Struve and the Harvard Photometry, but nearer the latter. Theoretically a star of photometric magnitude 15.2 should be visible with our aperture of seventeen inches, but only in a single case has the magnitude of a companion been recorded as 15, and 14 or more occurs but rarely. In general the faintest star visible with direct vision against a dark sky has been considered as of magnitude 13.5 to 14.0 according to the definition. Yet stars recorded at the Lick Observatory as 13.0 to 13.5 are seen only with considerable difficulty, and on the other hand a star indicated as of photometric magnitude 15.1 in a series of comparison stars for a variable was easily seen.

*Notes and Indexes.* — It has not seemed advisable to quote the previous measures of a star or even to give comprehensive references to them, reserving that rather for the index list above

vase únicamente la diferencia de magnitud, basando la magnitud misma en otra autoridad, he dado la magnitud de la *durchmusterung* inmediatamente después del número. Esta puede combinarse con la diferencia observada mediante las relaciones conocidas.

Cuando he notado las dos componentes en la C. P. D. he dado los números y magnitudes de ambas, pero varias compañeras separadamente catalogadas pueden haberme escapado. Si allí dos puntos (:) indican que la imagen en la placa pareció doble, la misma indicación sigue aquí a la magnitud. Si la estrella se observó como una sola en la C. P. D., pero fué observada como dos en el *Catálogo de Zonas Estelares* de Córdoba, el hecho se indica poniendo la magnitud en *tipo inclinado* como hicieron allí en las referencias a esta obra.

Las magnitudes observadas están en una escala subjetiva y tal vez variable, que creo que está entre las de Struve y de Harvard, acercándose más a la de éste. Teóricamente debía ser visible una estrella de magnitud fotométrica 15.2 con nuestra abertura de 433 milímetros pero he anotado una magnitud de 15 una sola vez, y pocas veces 14 o más. Generalmente he considerado la estrella más débil que alcanzaba a ver con mirada directa en cielo obscuro como de magnitud 13.5 a 14.0, según la nitidez de las imágenes. Sin embargo estrellas notadas en el Lick Observatory como de magnitud 13.0 a 13.5 son muy difíciles de ver, y por otra parte he visto fácilmente una estrella indicada como de magnitud fotométrica 15.1 en una serie de estrellas de comparación para una variable.

*Notas e Índices.* — No me ha parecido conveniente citar las medidas anteriores de las estrellas, ni aun dar referencias completas de ellas, dejando esto más bien para la lista-índice arriba

mentioned. Yet some remark or indication of our knowledge of the pair seemed to be called for in the majority of the cases. These notes are generally made by single letters which have the character of abbreviations and are given under that head on page 16. When a numeral replaces these letters it calls attention to a note which could not be expressed in this manner and which is given after the measures, on pages 115 to 122. Many of the abbreviated notes are mere guesses based on the evidence of a single measure by Hargrave and the original observation, and of course may not be borne out by later measures if these stars are ever reobserved. This uncertainty is usually indicated by the addition of an interrogation point (?) to the letter in question.

For the easier finding of the miscellaneous stars a group of indexes is appended. These contain the right ascensions of, (1) constellation named stars, (2) stars noted as new by observers other than Herschel, and (3) Herschel stars which by considerable error in his places or by supplementary numeration are out of their regular order. Precession has in several cases somewhat disarranged the numerical sequence and several errors of a minute or a wire in Herschel's right ascension have acted similarly, but have not been included in the index. Stars of the second list (those north of  $-31^\circ$ ) are indicated in these indexes by an asterisk (\*) prefixed to the right ascension. Cross references have been avoided by giving directly the right ascension of the star in question whether the name serving as argument be that of the discoverer or not. As the right ascensions are given to seconds there is no danger of ambiguity.

*Arrangement of Results.* — The stars observed have been divided into two groups for publication, those south of declination  $-31^\circ$  and those

mencionada. Sin embargo, era deseable en la mayoría de los casos, alguna anotación o indicación de nuestro conocimiento de la estrella. Estas anotaciones generalmente se hacen con letras que tienen el carácter de abreviaciones y como tales están dadas en la página 16. Cuando una nota no podía expresarse de esta manera, la letra se reemplazó con un número que indica una de las notas que siguen las medidas en páginas 115 a 122. Muchas de las notas abreviadas no tienen otra base que una sola medida por Hargrave y la observación original, y pueden no ser comprobadas por medidas posteriores. Esta incertidumbre generalmente se indica mediante el punto de interrogación (?).

Para facilitar la referencia he agregado un grupo de índices. Estos contienen las ascensiones rectas de, (1) estrellas con letra en su constelación, (2) estrellas notadas como nuevas por otros observadores, y (3) estrellas de Herschel que por numeración suplementaria o por error en la ascensión recta están muy afuera de la sucesión numérica. Errores de un solo minuto en ascensión recta o intercambios debidos a precesión no están incluidos. Las estrellas de la segunda lista (las al norte de  $-31^\circ$ ) están indicadas aquí con un asterisco (\*) que precede la ascensión recta. Referencias de un índice a otro se han evitado dando directamente la ascensión recta de la estrella aunque el nombre usado como argumento no sea el del descubridor. Estando las ascensiones rectas hasta segundos, no hay peligro de equivocación.

*Disposición de los Resultados.* — Las estrellas observadas se han repartido en dos grupos para la publicación, las al sur de declinación  $-31^\circ$  y



north of that limit. This division has been made to aid those whose work is confined to the region of Burnham's *General Catalogue*. Within each group the stars are arranged in the order of right ascension, for 1875 in the southern list and for 1880 in the northern. In the second list every measure at hand is published, whether the corresponding star is considered completely observed or not.

Under each star is given: (1) its name as a double star, its C. P. D. number or other identification, its *durchmusterung* magnitude; (2) its right ascension and declination for 1875.0 (except in the northern list, where 1880.0 is used); (3) the individual measures and the data relating to the observations, and (4) the means of the measures, the means of the estimated magnitudes and a letter or number indicating a note. In the triple and multiple stars the first pair given is to be considered as AB except where otherwise specified.

In the individual measures the separate columns are, in order: (1) the date of observation, (2) the observed position angle, (3) the observed distance, (4) the sidereal time of the observation, (5) the seeing at that time and (6) the magnification used.

The sidereal time of the observation and the seeing seemed of more importance than the individual estimates of magnitude and were consequently substituted for them in the form communicated to me by Prof. Boss as the one approved by the majority of double star observers. Another departure from that form is the giving of the identifications and *durchmusterung* magnitudes, which are of course unnecessary for the stars in Burnham's *General Catalogue*.

To avoid clerical errors the proofs have been compared directly with the observing books.

las al norte de este límite. Esta división se hizo para ayudar a los observadores que trabajan solamente dentro del área correspondiente al *General Catalogue* de Burnham. En cada parte las estrellas están ordenadas según su ascensión recta, las más australes para 1875 y las otras para 1880. En la segunda parte publico toda medida, esté o no concluída la observación de la estrella a que corresponde.

Con cada estrella se dan: (1) su nombre como doble, su número en la C. P. D., u otra identificación, su magnitud en la *durchmusterung*; (2) su ascensión recta y declinación para 1875.0 (para 1880.0 en la segunda parte); (3) las medidas individuales y datos de observación; y (4) los promedios de las medidas y de las magnitudes apreciadas y una letra o un número que indica la nota. En las estrellas triples y múltiples, el par que se da primero debe considerarse AB sino hay otra indicación.

En las medidas individuales, las columnas en orden contienen: (1) la fecha de observación, (2) el ángulo de posición observado, (3) la distancia observada, (4) la hora sidérea de la observación, (5) la condición de las imágenes a esa hora, y (6) el aumento empleado.

Como la hora sidérea de la observación y la condición de las imágenes me parecen de mayor importancia que las apreciaciones individuales de magnitud, las he substituído por éstas en la forma que me comunicó el profesor Boss con la indicación que había recibido la aprobación de la mayoría de los observadores de estrellas dobles. Otra diferencia entre la forma empleada y la indicada por Boss es que doy la identificación y la magnitud de la *durchmusterung*, que no serían necesarias tratándose de estrellas del *General Catalogue* de Burnham.

Para evitar errores de copia, las pruebas se han comparado directamente con los cuadernos de observación.

Finally I wish to acknowledge my indebtedness to Prof. Hussey for assistance in innumerable ways, moral and material, both during his residence in La Plata and afterwards, particularly for advice regarding the choice of program and prosecution of the work and for the loan of his charts of the area observed in 1912, 1913 and 1914, and to Acting Director Aguilar for his aid and interest in the work. Messrs. Castells, Tapia and Garbarino have aided in the preparation of charts used in the work and Mr. Garbarino has also assisted in the preparation of the manuscript and in reading the proof.

Por último quiero expresar mi agradecimiento al profesor Hussey por sus innumerables ayudas, no sólo durante su estadía en La Plata sino también después. Especialmente le estoy reconocido por sus consejos relativos a la confección del programa y a la manera de observar y por haberme prestado sus cartas del área observada en 1912, 1913 y 1914. También estoy muy agradecido al encargado de la dirección, señor Aguilar, por su ayuda e interés en el trabajo. Los señores Castells, Tapia y Garbarino me han ayudado en la preparación de cartas usadas en las observaciones y el señor Garbarino también me ayudó en la preparación del manuscrito y en la lectura de las pruebas.

## ABBREVIATIONS      ABREVIACIONES

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### 1. WORKS      OBRAS

- Results Results of Astronomical Observations \*\*\* at the Cape of Good Hope, *Sir John F. W. Herschel* (London, 1847).
- SD Bonner Sternverzeichniss, Vierte Section, *Dr. Eduard Schönfeld* (Astronomische Beobachtungen auf der Sternwarte \*\*\* zu Bonn, Achter Band, 1886).
- CóD Zonas de Exploración (Córdoba Durchmusterung), *Juan M. Thome* (Resultados del Observatorio Nacional Argentino. Vol. XVI, 1892; XVII, 1894; XVIII, 1900 y XXI, 1914).
- C. P. D. The Cape Photographic Durchmusterung for the Equinox 1875, *David Gill and J. C. Kapteyn* (Annals of the Cape Observatory. Vol. III, 1896; IV, 1897, y V, 1900).
- I. R. C. Reference Catalogue of Southern Double Stars, *R. T. A. Innes* (Annals of the Royal Observatory, Cape of Good Hope. Vol. II, Part II, 1899).

### 2. OBSERVERS      OBSERVADORES

- A Robert Grant Aitken (Lick Observatory).
- § S. W. Burnham (Dearborn, Lick y Yerkes Obs.).
- Có. Los Observadores del Observatorio Nacional Argentino (Córdoba).
- Δ James Dunlop (Paramatta).
- HdA. Los Observadores de la Estación Austral de Harvard (Arequipa).
- h Sir John F. W. Herschel (Cabo de Buena Esperanza).
- Hu W. J. Hussey (Lick, La Plata y Detroit Obs.).
- I R. T. A. Innes (Cape y Transvaal=Union Obs.).
- λ Los Observadores del Lowell Observatory (México y Flagstaff).
- Rü Charles Rümker (Paramatta).
- Rus H. C. Russell (Sydney).

### 3. NOTES      NOTAS

- |  |   |
|--|---|
| <p><b>A</b> Change in angle with constant distance.</p> <p><b>B</b> Binary.</p> <p><b>C</b> Common proper motion.</p> <p><b>D</b> Change in distance with fixed angle.</p> <p><b>F</b> Fixed.</p> <p><b>M</b> Motion shown, but its character uncertain.</p> <p><b>N</b> I have seen no other measures.</p> <p><b>P</b> Probably binary.</p> <p><b>R</b> Relative proper motion.</p> | <p><b>A</b> Cambio en el ángulo, distancia constante.</p> <p><b>B</b> Binaria.</p> <p><b>C</b> Movimiento propio común.</p> <p><b>D</b> Cambio en distancia, ángulo constante.</p> <p><b>F</b> Fija.</p> <p><b>M</b> Movimiento, tipo indeterminado.</p> <p><b>N</b> No conozco otras medidas.</p> <p><b>P</b> Probablemente binaria.</p> <p><b>R</b> Movimiento propio relativo.</p> |
|--|---|



# MICROMETRIC MEASURES OF DOUBLE STARS

## MEDIDAS MICROMÉTRICAS DE ESTRELLAS DOBLES

*h* 3347;  $-50^{\circ} 13$ ; 6.6  
A.R.  $0^h 2^m 50^s$ ; Decl.  $-50^{\circ} 52'$

1914.395	80.6	24.87	19.9	$2\frac{1}{2}$	370
14.479	81.2	25.10	22.1	$1\frac{1}{2}$	370
14.44	80.9	24.98	(7.5 ... 13.0) N		

*h* 3348;  $-60^{\circ} 6$ ; 9.4:  
A.R.  $0^h 3^m 52^s$ ; Decl.  $-60^{\circ} 3'$

16.740	278.7	18.55	23.0	3	370
16.751	279.0	18.61	22.0	2	370
16.75	278.8	18.58	(9.6 ... 10.2) N		

*h* 3349;  $-68^{\circ} 2$ ; 9.2  
A.R.  $0^h 4^m 2^s$ ; Decl.  $-68^{\circ} 1'$

16.886	107.6	15.35	3.0	2	370
16.888	108.0	15.52	0.1	2	370
16.940	108.0	15.16	2.7	2	370
16.90	107.9	15.34	(9.4 ... 10.6) M		

*h* 3350;  $-58^{\circ} 7$ ; 8.2  
A.R.  $0^h 4^m 34^s$ ; Decl.  $-58^{\circ} 11'$

13.885	178.9	3.51	5.4	$1\frac{1}{2}$	420
13.893	179.8	3.40	4.8	3	420
13.918	178.6	3.43	4.8	2	300
13.90	179.1	3.45	(8.7 ... 9.2) F		

*h* 3352;  $-50^{\circ} 18$ ; 8.5  
A.R.  $0^h 5^m 15^s$ ; Decl.  $-50^{\circ} 19'$

13.939	305.5	6.64	3.2	$1\frac{1}{2}$	300
14.395	307.2	6.54	20.1	2	370
14.479	305.5	6.80	22.3	$1\frac{1}{2}$	370
14.27	306.1	6.66	(9.2 ... 10.8) F		

*h* 3357;  $-68^{\circ} 4$ ; 8.1  
A.R.  $0^h 10^m 2^s$ ; Decl.  $-68^{\circ} 36'$

16.886	337.2	9.85	3.2	$1\frac{1}{2}$	370
16.888	336.8	10.07	0.2	2	370
16.943	336.5	9.81	2.3	2	370
16.91	336.8	9.91	(8.6 ... 12.2) N		

*h* 3358;  $-62^{\circ} 20$ ; 9.5:  
A.R.  $0^h 10^m 8^s$ ; Decl.  $-62^{\circ} 9'$

16.740	11.6	15.84	23.1	2	370
16.751	11.9	16.06	22.2	2	370
16.760	12.3	15.87	0.2	2	370
16.798	11.8	15.92	23.0	2	370
16.76	11.9	15.92	(9.6 ... 9.7) N		

*h* 3360;  $-53^{\circ} 72 - 3$ ; 9.8 -- 10.4  
A.R.  $0^h 15^m 28^s$ ; Decl.  $-53^{\circ} 13'$

13.939	31.8	14.06	3.3	$1\frac{1}{2}$	300
14.395	33.1	14.48	20.3	2	370
14.479	32.2	14.47	22.4	$1\frac{1}{2}$	370
14.27	32.4	14.34	(9.6 ... 10.1) N		

*h* 3361; Anon.  
A.R.  $0^h 15^m 35^s$ ; Decl.  $-68^{\circ} 25'$

16.886	113.9	5.01	3.4	2	370
16.888	111.9	5.14	0.4	2	370
16.937	113.2	5.16	2.8	2	370
16.90	113.0	5.10	(10.4 ... 10.5) N		

*h* 3363;  $-72^{\circ} 35$ ; —  
A.R.  $0^h 18^m 32^s$ ; Decl.  $-72^{\circ} 46'$

16.896	250.5	6.33	0.9	2	370
16.926	251.8	6.10	1.9	$1\frac{1}{2}$	370
16.937	250.8	6.21	2.0	2	370
16.92	251.0	6.21	(10.6 ... 11.3) I		

$h\ 3364; -54^\circ 91; 7.2$ A.R.  $0^h\ 18^m\ 39^s$ ; Decl.  $-54^\circ\ 41'$ 

13.535	228.5	33.56	22.2	2	300
13.803	229.3	33.30	3.5	2	300
13.833	228.6	33.14	4.9	3	300
13.72	228.8	33.33	(7.1 ... 9.9)		N

 $h\ 3365; -51^\circ 53 + 4; 8.2 + 9.2$ A.R.  $0^h\ 19^m\ 39^s$ ; Decl.  $-51^\circ\ 32'$ 

13.939	171.5	16.47	3.4	$1\frac{1}{2}$	300
14.395	171.4	16.66	20.5	$2\frac{1}{2}$	370
14.17	171.4	16.57	(8.6 ... 9.8)		F

 $h\ 3366; -68^\circ 13; 8.3$ A.R.  $0^h\ 21^m\ 5^s$ ; Decl.  $-68^\circ\ 25'$ 

16.894	21.2	22.61	0.4	2	370
16.943	22.3	22.64	2.4	2	370
16.92	21.7	22.62	(8.5 ... 13.5)		N

 $I\ 44; -55^\circ 94; 8.0$ A.R.  $0^h\ 22^m\ 15^s$ ; Decl.  $-55^\circ\ 19'$ 

13.507	253.8	1.03	21.9	3	666
13.803	248.4	0.88	3.7	2	420
13.833	246.0	1.01	5.0	3	420
13.893	246.4	1.00	5.0	3	420
13.76	248.5	0.98	(8.6 ... 9.2)		

 $h\ 3369; -65^\circ 34; 9.8$ A.R.  $0^h\ 22^m\ 31^s$ ; Decl.  $-65^\circ\ 29'$ 

16.798	342.6	14.99	23.3	2	370
16.806	341.8	14.98	23.0	2	370
16.80	342.2	14.98	(10.4 ... 12.4)		2

 $Rus. 3; -66^\circ 31; 8.2$ A.R.  $0^h\ 22^m\ 33^s$ ; Decl.  $-66^\circ\ 36'$ 

16.888	244.5	1.71	0.6	2	370
16.894	245.3	1.75	0.7	2	370
16.943	242.0	1.78	2.7	2	370
16.91	243.9	1.75	(8.9 ... 10.9)		

 $AC = h\ 3370; C = -66^\circ 32; 9.4$ 

16.894	64.4	41.30	0.5	2	370
16.937	64.4	41.14	3.8	2	370
16.92	64.4	41.22	(8.9 ... 9.8)		R

 $h\ 3371; -57^\circ 100; 9.7$ A.R.  $0^h\ 23^m\ 58^s$ ; Decl.  $-57^\circ\ 23'$ 

13.918	335.3	10.24	5.2	2	300
13.926	335.5	10.44	4.6	3	300
13.92	335.4	10.34	(10.1 ... 10.6)		N

 $h\ 3372; C6D -61^\circ 81; 9.9$ A.R.  $0^h\ 25^m\ 26^s$ ; Decl.  $-61^\circ\ 43'$ 

16.740	97.4	24.53	23.3	$2\frac{1}{2}$	370
16.751	97.1	24.51	22.5	2	370
16.75	97.3	24.52	(9.2 ... 10.2)		N

 $\Delta I; \beta\ Tucanae; 3.8$ A.R.  $0^h\ 25^m\ 49^s$ ; Decl.  $-63^\circ\ 39'$ 

16.798	169.8	27.05	23.5	2	370
16.806	170.0	27.29	23.1	2	370
16.812	169.9	27.08	0.3	3	370
16.81	169.9	27.14	(3.7 ... 4.0)		C

 $BC = I\ 260$ 

16.812	268.0	0.37	0.6	$2\frac{1}{2}$	650
16.823	Véase la nota		See note		3

 $I\ 45; -56^\circ 103; 7.2$ A.R.  $0^h\ 27^m\ 38^s$ ; Decl.  $-56^\circ\ 1'$ 

13.507	268.6	0.59	22.2	$2\frac{1}{2}$	666
13.893	262.9	0.63	5.3	3	666
14.583	264.6	0.56	22.4	$2\frac{1}{2}$	475
13.99	265.4	0.59	(7.8 ... 8.3)		M

 $AB, C = h\ 3376$ 

13.507	247.2	7.25	22.3	$2\frac{1}{2}$	300
13.833	247.8	7.11	5.3	2	420
13.893	247.9	7.06	5.4	2	420
13.74	247.6	7.14	(7.3 ... 8.6)		F

 $h\ 3378; -61^\circ 29; 7.8$ A.R.  $0^h\ 27^m\ 49^s$ ; Decl.  $-61^\circ\ 50'$ 

16.740	353.4	7.68	23.4	2	370
16.751	353.9	7.47	22.8	2	370
16.765	354.6	7.57	23.0	2	370
16.75	354.0	7.57	(8.3 ... 12.8)		N

 $Rus. 4; -54^\circ 136; 7.8$ A.R.  $0^h\ 29^m\ 20^s$ ; Decl.  $-54^\circ\ 14'$ 

13.535	93.1	2.97	22.4	2	300
13.803	91.9	2.89	4.0	2	420
13.833	92.0	2.82	5.2	3	420
13.72	92.3	2.89	(8.2 ... 8.9)		F

 $h\ 3381; -44^\circ 79; 9.8$ A.R.  $0^h\ 33^m\ 25^s$ ; Decl.  $-44^\circ\ 40'$ 

16.672	39.2	[11.61]	20.6	$1\frac{1}{2}$	370
16.675	39.3	10.91	22.9	$1\frac{1}{2}$	370
16.683	39.4	10.91	21.2	3	370
16.68	39.3	10.91	(9.3 ... 10.5)		N

*h* 3382;  $-63^{\circ} 66$ ; 9.8

A.R.  $0^h 33^m 34^s$ ; Decl.  $-63^{\circ} 30'$

16.798	226.01	25.99	23.7	2	370
16.806	225.8	26.04	23.5	2	370
16.80	226.0	26.02	(9.5 ... 12.0)		N

*h* 3383;  $-54^{\circ} 153$ ; 8.8

A.R.  $0^h 34^m 23^s$ ; Decl.  $-54^{\circ} 4'$

13.535	218.0	7.57	22.6	2	300
13.833	219.0	7.32	5.6	2½	420
13.885	217.3	7.43	5.6	2	420
13.75	218.1	7.44	(9.3 ... 9.8)		N

*h* 3385;  $-41^{\circ} 71$ ; 8.6

A.R.  $0^h 34^m 49^s$ ; Decl.  $-41^{\circ} 54'$

16.675	69.5	4.42	22.8	1½	370
16.683	68.7	4.32	21.4	3	370
16.686	69.1	4.38	22.0	2½	370
16.68	69.1	4.37	(9.5 ... 9.6)		4

*h* 3386;  $-52^{\circ} 77$ ; 9.5

A.R.  $0^h 34^m 59^s$ ; Decl.  $-52^{\circ} 47'$

13.939	75.3	9.85	3.6	1½	300
14.395	77.4	9.78	20.6	2½	370
14.479	76.3	9.67	22.6	1	370
14.27	76.3	9.77	(10.2 ... 10.6)		N

AC

13.939	233.4	24.21	3.7	1½	300
14.395	233.6	[24.80]	20.7	2	370
14.542	233.7	24.27	21.7	2	370
14.575	232.9	24.29	21.9	3	370
14.36	233.4	24.26	(10.2 ... 11.3)		N

*h* 3387;  $\xi$  Phoenicis; 6.1

A.R.  $0^h 36^m 4^s$ ; Decl.  $-57^{\circ} 11'$

13.507	254.0	13.26	22.6	2	300
13.535	253.4	13.45	23.0	2	300
13.803	254.1	13.48	4.2	2	420
13.62	253.8	13.40	(6.1 ... 10.1)		F

Melbourne 1;  $-56^{\circ} 132$ ; 7.5

A.R.  $0^h 36^m 19^s$ ; Decl.  $-56^{\circ} 28'$

13.507	162.8	6.52	22.4	3	300
13.535	163.4	6.79	22.8	2	300
13.803	163.4	6.47	4.4	2	420
13.62	163.2	6.59	(7.8 ... 8.4)		F

*h* 3388;  $-54^{\circ} 160 + 59$ ; 8.4 + 8.4

A.R.  $0^h 36^m 51^s$ ; Decl.  $-54^{\circ} 48'$

13.507	239.9	16.78	22.7	2½	300
13.535	239.5	17.22	22.7	2	300
13.803	240.0	16.93	4.5	2	420
13.62	239.8	16.98	(8.3 ... 8.4)		F

*h* 3390;  $45^{\circ} 81$ ; 7.2

A.R.  $0^h 37^m 22^s$ ; Decl.  $-45^{\circ} 52'$

16.675	312.5	14.27	23.2	3	370
16.683	312.0	14.15	21.7	3	370
16.68	312.3	14.21	(7.2 ... 9.8)		N

*h* 3391;  $\gamma$  Phoenicis; 4.3

A.R.  $0^h 37^m 42^s$ ; Decl.  $-58^{\circ} 9'$

16.751	217.2	20.08	23.0	2	370
16.765	217.2	19.91	23.2	2½	370
16.76	217.2	19.99	(4.0 ... 11.8)		F

*h* 3395;  $-42^{\circ} 68$ ; 8.0

A.R.  $0^h 39^m 49^s$ ; Decl.  $-42^{\circ} 35'$

16.675	78.4	6.98	23.4	3½	370
16.683	78.2	6.86	21.6	2½	370
16.686	78.3	6.99	22.2	2½	370
16.68	78.3	6.94	(8.2 ... 8.5)		M

*h* 3397;  $-54^{\circ} 174$ ; 7.3

A.R.  $0^h 41^m 0^s$ ; Decl.  $-54^{\circ} 47'$

16.751	175.7	12.17	23.3	2	370
16.773	173.6	11.93	22.6	3	370
16.76	174.6	12.05	(8.0 ... 13.8)		N

*h* 3398;  $-52^{\circ} 90 + 91$ ; 9.0 + 9.6

A.R.  $0^h 41^m 3^s$ ; Decl.  $-52^{\circ} 41'$

13.939	130.2	28.05	3.9	2	300
14.395	130.8	27.95	20.9	2	370
14.17	130.5	28.00	(9.0 ... 10.3)		M

*h* 3400;  $-65^{\circ} 85$ ; 9.2

A.R.  $0^h 43^m 20^s$ ; Decl.  $-65^{\circ} 47'$

16.806	139.9	5.70	23.7	2½	370
16.812	140.5	5.64	0.8	3	370
16.823	140.0	5.78	2.7	2½	370
16.81	140.1	5.71	(9.4 ... 10.8)		N

*h* 3402;  $-54^{\circ} 186$ ; 7.8

A.R.  $0^h 43^m 59^s$ ; Decl.  $-54^{\circ} 51'$

14.575	58.0	10.65	22.2	3	300
14.583	60.0	10.96	22.5	2½	475
14.586	59.1	10.50	21.9	2	370
14.58	59.0	10.70	(8.0 ... 11.2)		5

*h* 3404;  $-60^{\circ} 57'$ ; 9.4A.R.  $0^h 46^m 29^s$ ; Decl.  $-60^{\circ} 1'$ 

16.751	242.0	10.34	23.5	2½	370
16.773	241.6	10.49	22.8	3	370
16.76	241.8	10.42	(9.6 ... 10.5)		N

*h* 3403;  $-47^{\circ} 99'$ ; 9.0A.R.  $0^h 46^m 31^s$ ; Decl.  $-47^{\circ} 59'$ 

13.718	337.3	12.76	22.2	3	300
13.833	336.3	12.96	2.5	2	300
13.78	336.8	12.86	(9.5 ... 10.5)		N

*h* 3405;  $-66^{\circ} 64'$ ; 9.2A.R.  $0^h 46^m 34^s$ ; Decl.  $-66^{\circ} 1'$ 

16.806	336.6	12.72	23.9	2½	370
16.812	337.1	12.77	1.3	2½	370
16.81	336.9	12.76	(9.8 ... 10.5)		N

*h* 3406;  $-66^{\circ} 65'$ ; 9.4A.R.  $0^h 46^m 54^s$ ; Decl.  $-66^{\circ} 1'$ 

16.806	227.5	32.83	0.2	2½	370
16.812	229.2	32.55	1.5	2	370
16.823	228.8	32.73	2.8	2	370
16.81	228.5	32.70	(9.1 ... 12.1?)		N

## Anonyma

A.R.  $0^h 47^m 13^s$ ; Decl.  $-66^{\circ} 4'$ 

16.812	91.3	5.95	1.0	2½	370
16.913	93.6	5.83	2.9	2	370
16.88	92.4	5.89	(11.2 ... 12.1)		6

 $\Delta 2 = \text{Rii } 1; \lambda \text{ Tucanae}; 7.6 + 8.0$ A.R.  $0^h 47^m 40^s$ ; Decl.  $-70^{\circ} 11'$ 

16.896	79.9	20.82	1.2	2	370
16.937	79.5	20.80	2.3	2	370
16.92	79.7	20.81	(7.1 ... 7.7)		F

*h* 3408;  $-66^{\circ} 69'$ ; 8.0:A.R.  $0^h 49^m 40^s$ ; Decl.  $-66^{\circ} 8'$ 

16.806	213.4	16.13	0.4	2	370
16.812	213.8	16.23	1.7	2	370
16.81	213.6	16.18	(8.9 ... 10.0)		N

Aguilar 1;  $-57^{\circ} 203'$ ; 8.6A.R.  $0^h 51^m 10^s$ ; Decl.  $-57^{\circ} 14'$ 

13.885	170.9	3.58	5.9	2	420
13.893	171.7	3.33	5.7	3	420
13.918	168.6	3.38	5.6	2	300
13.90	170.4	3.43	(8.9 ... 8.9)		7

*h* 3409;  $-59^{\circ} 61'$ ; 10.2A.R.  $0^h 52^m 3^s$ ; Decl.  $-59^{\circ} 24'$ 

16.751	1.1	13.11	23.8	2	370
16.773	0.7	12.89	22.9	3	370
16.76	0.9	12.00	(10.1 ... 12.4)		N

*h* 3412;  $-56^{\circ} 198 + 9$ ;  $8.5 + 9.8$ A.R.  $0^h 55^m 52^s$ ; Decl.  $-56^{\circ} 50'$ 

13.535	140.0	27.98	23.4	2	300
13.918	138.9	28.03	5.9	2	300
13.73	139.5	28.00	(8.5 ... 10.2)		N

## AC

13.535	327.9	26.38	23.3	2	300
13.918	324.5	24.84	6.2	2	300
13.926	324.9	25.58	5.1	2	300
13.79	325.8	25.60	(8.5 ... 13.0)		N

*h* 3413;  $-47^{\circ} 120'$ ; 9.4A.R.  $0^h 56^m 15^s$ ; Decl.  $-47^{\circ} 38'$ 

16.686	51.0	7.01	22.3	2½	370
16.697	52.5	7.04	22.4	2	370
16.702	53.3	6.82	21.4	2	370
16.70	52.3	6.96	(10.4 ... 10.4)		N

*h* 3414;  $-50^{\circ} 147'$ ; 8.9A.R.  $0^h 56^m 17^s$ ; Decl.  $-50^{\circ} 56'$ 

13.940	31.4	19.06	4.5	2	300
14.395	32.5	19.31	21.2	2	370
14.542	32.2	19.23	22.0	2½	370
14.29	32.0	19.20	(9.1 ... 10.9)		N

*h* 3416;  $-60^{\circ} 72'$ ; 7.0A.R.  $0^h 58^m 12^s$ ; Decl.  $-60^{\circ} 46'$ 

16.740	128.9	4.95	23.7	2	370
16.751	128.2	5.04	23.9	2	370
16.773	128.7	5.03	23.0	3	370
16.75	128.6	5.01	(8.0 ... 8.0)		F

## AC; C = 11.8

16.773	41.0	99.5	23.8	3	370	N
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Sellors 1;  $\beta$  Phoenicis; 5.0A.R.  $1^h 0^m 30^s$ ; Decl.  $-47^{\circ} 23'$ 

16.686	9.5	1.54	22.6	2	370
16.702	10.7	1.58	21.9	2	370
16.705	10.3	1.41	21.5	2	370
16.70	10.1	1.51	(3.8 ... 4.1)		B

(Sigue Continued.)



AC = h 3417

16.686	51.95	57.21	22.7	2	370
16.702	51.1	56.61	21.7	2	370
16.705	52.0	56.86	21.3	2	370
16.70	51.5	56.89	(3.8 ... 10.3)		R

h 3418; -58° 73; 9.4

A.R. 1<sup>h</sup> 0<sup>m</sup> 35<sup>s</sup>; Decl. -58° 34'

16.773	251.2	2.69	23.9	3½	370
16.784	251.8	2.73	22.9	2	370
16.795	253.2	2.89	22.8	2½	370
16.78	252.1	2.77	(10.1 ... 10.8)		N

Rii 2; ζ Phoenicis; 3.2

A.R. 1<sup>h</sup> 3<sup>m</sup> 8<sup>s</sup>; Decl. -55° 55'

13.507	242.2	6.59	23.0	2	300
13.535	245.9	6.57	23.7	2	300
13.803	242.4	6.98	4.7	2	420
13.918	243.5	6.83	6.5	2	420
13.69	242.7	6.74	(4.2 ... 7.0)		D

h 3421; -51° 178 + 9; 8.2 + 8.4

A.R. 1<sup>h</sup> 8<sup>m</sup> 24<sup>s</sup>; Decl. -51° 19'

13.940	67.8	50.27	4.6	2	300
14.542	68.4	50.33	22.2	2	370
14.575	68.1	50.32	22.4	3	370
14.35	68.1	50.31	(8.3 ... 8.3)		R

h 3422; -56° 256; 8.0

A.R. 1<sup>h</sup> 9<sup>m</sup> 53<sup>s</sup>; Decl. -56° 18'

13.803	56.1	14.02	4.9	1½	420
13.926	54.7	13.97	5.4	2	300
13.86	55.4	14.00	(7.6 ... 12.2)		N

h 3423; α Tucanae; 5.2

A.R. 1<sup>h</sup> 11<sup>m</sup> 31<sup>s</sup>; Decl. -69° 32'

16.888	347.3	5.27	1.1	2	370
16.943	347.1	5.42	3.8	1½	370
16.948	348.7	5.52	2.9	2	370
16.951	345.8	5.51	3.2	2	370
16.93	347.2	5.43	(5.2 ... 8.5)		P

h 3426; -67° 81; 6.2

A.R. 1<sup>h</sup> 12<sup>m</sup> 43<sup>s</sup>; Decl. -67° 4'

16.888	333.7	2.73	0.9	2	370
16.894	337.8	2.73	1.0	2	370
16.943	337.9	2.80	3.5	2	370
16.91	336.5	2.75	(6.4 ... 8.9)		M

h 3427; -50° 176; 9.0

A.R. 1<sup>h</sup> 14<sup>m</sup> 41<sup>s</sup>; Decl. -50° 46'

13.940	132.0	21.58	4.8	2	300
14.542	132.0	21.84	22.3	2½	370
14.24	132.0	21.71	(9.2 ... 9.8)		F

h 3428; -49° 175 + 6; 8.0 + 9.2

A.R. 1<sup>h</sup> 14<sup>m</sup> 59<sup>s</sup>; Decl. -49° 20'

13.718	156.8	20.67	23.2	3	300
14.575	156.8	20.72	22.5	3	370
14.15	156.8	20.70	(8.0 ... 9.6)		F

h 3430; -57° 292; 6.8

A.R. 1<sup>h</sup> 15<sup>m</sup> 30<sup>s</sup>; Decl. -57° 60'

13.507	233.0	2.64	23.2	2½	300
13.885	233.3	2.67	6.1	2	300
14.183	236.5	2.59	7.5	2	370
13.86	234.3	2.67	(6.8 ... 8.9)		M

h 3434; Anon.

A.R. 1<sup>h</sup> 18<sup>m</sup> 35<sup>s</sup>; Decl. -59° 12'

16.773	105.6	7.69	0.0	3	370
16.784	106.9	7.53	23.2	2	370
16.795	108.3	6.97	23.0	2	370
16.798	105.5	7.27	0.9	2	370
16.70	106.6	7.38	(12.0 ... 12.4)		N

h 3435; -60° 112 + 11; 7.4 + 9.0

A.R. 1<sup>h</sup> 20<sup>m</sup> 36<sup>s</sup>; Decl. -60° 9'

16.773	359.9	25.36	0.1	3	370
16.784	359.9	25.57	23.6	2	370
16.78	359.9	25.46	(8.0 ... 9.5)		N

h 3438; -50° 196; 11.2

A.R. 1<sup>h</sup> 22<sup>m</sup> 14<sup>s</sup>; Decl. -50° 7'

13.940	33.5	12.23	5.0	2½	300
14.542	34.5	12.23	22.5	2½	370
14.24	34.0	12.23	(10.1 ... 10.4)		N

h 3439; -45° 161; 9.8

A.R. 1<sup>h</sup> 22<sup>m</sup> 35<sup>s</sup>; Decl. -45° 15'

16.683	209.4	7.75	22.1	2½	370
16.686	209.5	7.54	23.0	2	370
16.702	209.2	7.59	22.2	2	370
16.69	209.4	7.63	(9.9 ... 10.5)		N

I 264;  $-54^{\circ} 342$ ; 7.8A.R.  $1^{\text{h}} 26^{\text{m}} 36^{\text{s}}$ ; Decl.  $-54^{\circ} 1'$ 

13.508	113.9	0.61	23.5	$2\frac{1}{2}$	666
14.542	110.0	0.78	22.9	$2\frac{1}{2}$	650
14.575	102.0	0.70	22.9	3	650
14.591	99.2	0.81	21.5	2	370
16.675	105.2	0.82	23.8	3	650
16.708	102.5	0.78	23.5	3	650
16.765	99.2	0.70	0.1	$2\frac{1}{2}$	650

14.30	106.3	0.72			
16.72	102.3	0.77	(8.6 ... 9.0)		B

## AB,C = h 3444

13.508	6.7	39.05	23.3	$2\frac{1}{2}$	300
14.183	5.9	38.66	7.8	2	370
14.542	6.8	38.72	22.7	$2\frac{1}{2}$	370
14.575	6.5	38.94	23.1	3	370

14.20	6.5	38.84	(8.0 ... 10.8)		N
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h 3446;  $-59^{\circ} 107$ ; 8.5A.R.  $1^{\text{h}} 29^{\text{m}} 30^{\text{s}}$ ; Decl.  $-59^{\circ} 57'$ 

16.773	309.7	22.40	0.2	$3\frac{1}{2}$	370
16.784	309.6	22.30	23.8	2	370

16.78	309.7	22.35	(8.6 ... 11.0)		N
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h 3449;  $-53^{\circ} 342$ ; 8.2A.R.  $1^{\text{h}} 30^{\text{m}} 47^{\text{s}}$ ; Decl.  $-53^{\circ} 50'$ 

13.940	174.9	24.91	5.2	2	300
14.542	174.3	24.95	23.2	$2\frac{1}{2}$	370

14.24	174.6	24.93	(7.8 ... 12.4)		N
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h 3450;  $-42^{\circ} 151$ ; 9.8A.R.  $1^{\text{h}} 32^{\text{m}} 15^{\text{s}}$ ; Decl.  $-42^{\circ} 49'$ 

16.683	215.2	15.15	22.6	2	370
16.702	215.4	15.08	22.6	2	370

16.69	215.3	15.12	(9.6 ... 10.8)		N
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Pollock;  $-45^{\circ} 186$ ; 7.7A.R.  $1^{\text{h}} 33^{\text{m}} 26^{\text{s}}$ ; Decl.  $-45^{\circ} 14'$ 

16.683	37.1	1.70	22.3	3	370
16.686	39.1	1.70	23.2	2	370
16.702	39.4	1.81	22.3	2	370

16.69	38.5	1.74	(8.3 ... 8.7)		D
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h 3451;  $-45^{\circ} 187$ ; 10.2A.R.  $1^{\text{h}} 33^{\text{m}} 30^{\text{s}}$ ; Decl.  $-45^{\circ} 53'$ 

16.683	163.0	15.47	22.4	3	370
16.702	162.7	15.54	22.4	2	370

16.69	162.9	15.50	(9.8 ... 9.9)		N
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 $\Delta 4$ ;  $-54^{\circ} 358$ ; 6.9A.R.  $1^{\text{h}} 33^{\text{m}} 58^{\text{s}}$ ; Decl.  $-54^{\circ} 4'$ 

13.508	105.2	10.58	23.7	$2\frac{1}{2}$	300
13.803	103.7	10.63	5.1	2	420
13.885	103.7	10.75	6.3	2	420

13.73	104.2	10.65	(7.2 ... 8.2)		F
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 $\Delta 5$ ; p Eridani; 6.5A.R.  $1^{\text{h}} 35^{\text{m}} 4^{\text{s}}$ ; Decl.  $-56^{\circ} 50'$ 

13.508	215.7	8.50	23.8	3	300
13.535	215.6	8.68	23.8	2	300
13.759	215.8	8.50	0.0	3	300
13.803	214.8	8.89	5.3	2	420
13.833	215.3	8.92	5.9	2	420
14.183	214.6	8.80	8.0	2	370
16.675	213.9	8.65	0.0	3	370
16.702	214.6	8.69	21.2	2	370
16.708	213.4	8.73	23.6	3	650
17.833	214.4	8.80	3.3	2	370
17.934	214.9	8.87	2.7	$2\frac{1}{2}$	370

13.77	215.3	8.71			
17.17	214.2	8.75	(6.6 ... 6.7)		B

h 3460;  $-50^{\circ} 238$ ; 8.4A.R.  $1^{\text{h}} 39^{\text{m}} 18^{\text{s}}$ ; Decl.  $-50^{\circ} 44'$ 

16.792	173.5	18.40	23.0	2	370
16.795	173.2	18.59	22.4	$2\frac{1}{2}$	370

16.79	173.3	18.50	(8.6 ... 12.0)		N
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h 3462; C6D  $-47^{\circ} 535$ ; 9.9A.R.  $1^{\text{h}} 40^{\text{m}} 24^{\text{s}}$ ; Decl.  $-47^{\circ} 27'$ 

16.702	208.6	13.55	22.8	2	370
16.705	211.6	13.66	21.7	2	370
16.708	209.0	13.32	23.7	3	370

16.70	209.7	13.51	(10.6 ... 10.7)		N
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h 3463;  $-44^{\circ} 217 + 18$ ;  $9.6 + 9.6$ A.R.  $1^{\text{h}} 40^{\text{m}} 40^{\text{s}}$ ; Decl.  $-44^{\circ} 35'$ 

16.702	200.7	20.59	22.9	2	370
16.705	200.3	20.77	21.8	2	370

16.70	200.5	20.68	(9.9 ... 10.0)		N
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h 3468;  $-65^{\circ} 149$ ; 9.1A.R.  $1^{\text{h}} 43^{\text{m}} 2^{\text{s}}$ ; Decl.  $-65^{\circ} 25'$ 

16.806	$20\pm$	$20\pm$	(9.2 ... 15.0)		8
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h 3471;  $-44^{\circ} 228$ ; 9.2A.R.  $1^{\text{h}} 47^{\text{m}} 3^{\text{s}}$ ; Decl.  $-44^{\circ} 20'$ 

16.702	46.9	[69.03]	23.1	2	370
16.705	46.7	70.19	22.9	2	370
16.708	46.2	70.29	23.9	3	370

16.71	46.6	70.24	(8.8 ... 12.3)		R
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*h* 3473;  $\chi$  Eridani; 5.8

A.R. 1<sup>h</sup> 51<sup>m</sup> 7<sup>s</sup>; Decl. -52° 14'

16.795	198.7	5.62	22.5	2½	370
16.842	199.5	6.07	2.9	2	370
16.844	197.0	5.83	0.9	2	370
16.872	199.6	5.95	4.7	2	370
16.84	198.7	5.87	(4.2 ... 12.4)		C

*h* 3475 = Rus 12; -60° 162; 6.7

A.R. 1<sup>h</sup> 51<sup>m</sup> 18<sup>s</sup>; Decl. -60° 55'

16.740	54.4	2.55	0.1	2	370
16.751	53.1	2.48	0.1	2	370
16.773	52.5	2.48	0.4	4	370
16.75	53.3	2.50	(7.6 ... 7.7)		P

*h* 3477; -45° 206; 8.4

A.R. 1<sup>h</sup> 54<sup>m</sup> 57<sup>s</sup>; Decl. -45° 9'

16.705	156.5	9.16	23.1	2	370
16.708	155.6	9.03	0.1	3	370
16.716	156.9	9.18	23.2	2	370
16.71	156.3	9.12	(9.3 ... 9.4)		F

*h* 3479; -63° 143 + 2; 7.8 + 9.1

A.R. 1<sup>h</sup> 56<sup>m</sup> 48<sup>s</sup>; Decl. -63° 22'

16.798	275.1	35.36	0.3	2	370
16.806	274.8	35.37	1.0	2	370
16.80	275.0	35.36	(7.9 ... 9.7)		N

*h* 3482; -65° 165; 7.4

A.R. 2<sup>h</sup> 1<sup>m</sup> 16<sup>s</sup>; Decl. -65° 44'

16.806	215.7	49.98	0.8	2	370
16.812	216.1	49.91	2.0	2	370
16.81	215.9	49.95	(7.9 ... 12.8)		N

*h* 3481; -59° 186; 8.0

A.R. 2<sup>h</sup> 1<sup>m</sup> 24<sup>s</sup>; Decl. -59° 46'

16.773	9.0	18.16	0.5	4	370
16.779	9.4	18.31	0.3	2	370
16.78	9.2	18.23	(8.6 ... 10.2)		N

*h* 3483; -71° 102; 8.8

A.R. 2<sup>h</sup> 1<sup>m</sup> 55<sup>s</sup>; Decl. -71° 51'

16.896	287.7	7.24	1.6	2	370
16.957	288.0	7.18	3.3	2	370
16.959	286.2	7.19	4.9	1½	370
16.94	287.3	7.20	(9.4 ... 9.5)		A

I 455; -56° 381; 8.0

A.R. 2<sup>h</sup> 3<sup>m</sup> 59<sup>s</sup>; Decl. -56° 7'

13.885	203.0	5.83	6.6	2	300
13.899	201.6	5.61	6.9	2	300
14.591	199.7	5.61	21.6	2	370
14.13	201.4	5.68	(7.6 ... 11.8)		

*h* 3486; -64° 156; 7.8

A.R. 2<sup>h</sup> 6<sup>m</sup> 45<sup>s</sup>; Decl. -64° 57'

16.806	241.9	58.89	1.3	2	370
16.812	242.0	58.87	2.3	2	370
16.81	242.6	58.88	(7.9 ... 12.2)		N

*h* 3485; -49° 281; 7.6

A.R. 2<sup>h</sup> 6<sup>m</sup> 49<sup>s</sup>; Decl. -49° 55'

13.718	139.1	4.53	23.8	3	300
14.575	138.3	4.50	23.3	3	370
14.583	138.8	4.66	22.9	3	370
14.29	138.7	4.56	(8.4 ... 9.1)		F

*h* 3487; -63° 148; 9.1

A.R. 2<sup>h</sup> 7<sup>m</sup> 51<sup>s</sup>; Decl. -63° 37'

16.806	341.2	18.06	1.6	2	370
16.812	341.0	18.25	2.7	2	370
16.81	341.1	18.16	(9.2 ... 11.7)		N

*h* 3488; -62° 184; 7.7

A.R. 2<sup>h</sup> 8<sup>m</sup> 49<sup>s</sup>; Decl. -62° 14'

16.773	140.9	5.21	0.6	3½	370
16.779	141.0	5.25	0.6	2	370
16.784	140.7	5.27	0.0	2½	370
16.78	140.9	5.24	(8.7 ... 9.2)		A

*h* 3490; -66° 133; 8.5

A.R. 2<sup>h</sup> 9<sup>m</sup> 0<sup>s</sup>; Decl. -66° 22'

16.894	202.9	24.06	1.3	2	370
16.951	203.7	24.13	3.9	2	370
16.92	203.3	24.09	(8.7 ... 13.1)		N

*h* 3489; -71° 110; 7.5

A.R. 2<sup>h</sup> 9<sup>m</sup> 56<sup>s</sup>; Decl. -71° 32'

16.896	243.5	22.31	1.9	2	370
16.957	244.5	22.60	3.7	1½	370
16.959	243.7	22.54	5.1	1½	370
16.94	243.9	22.48	(7.5 ... 11.8)		9

AC; C = 14.0

16.896	270.5	8.01	2.2	1½	370
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$h$  3493;  $-50^{\circ} 323$ ; 8.8A.R.  $2^h 12^m 1^s$ ; Decl.  $-50^{\circ} 9'$ 

13.718	241.4	8.74	23.9	3	300
14.575	242.1	8.58	23.5	3	370
14.583	241.5	8.67	23.0	3	370
14.29	241.7	8.66	(9.0 ... 9.6)		N

 $\Delta$  6;  $\zeta$  Eridani;  $4.1 + 9.2$ A.R.  $2^h 12^m 2^s$ ; Decl.  $-52^{\circ} 6'$ 

16.792	218.5	85.94	23.4	2	370
16.795	218.7	86.18	22.7	$2\frac{1}{2}$	370
16.869	218.5	86.79	2.2	2	370
16.82	218.6	86.33	(4.0 ... 9.1)		10

 $h$  3496;  $-68^{\circ} 131$ ; 8.8A.R.  $2^h 14^m 38^s$ ; Decl.  $-68^{\circ} 46'$ 

16.888	315.8	21.73	1.3	2	370
16.951	315.6	21.56	3.4	2	370
16.92	315.7	21.64	(9.2 ... 10.8)		N

 $h$  3497 = Hda;  $-56^{\circ} 413$ ; 7.2A.R.  $2^h 15^m 51^s$ ; Decl.  $-56^{\circ} 31'$ 

13.508	82.2	33.91	0.0	$2\frac{1}{2}$	300
13.885	81.2	34.35	6.8	2	300
13.899	81.9	34.49	7.0	2	300
13.76	81.8	34.25	(5.7 ... 9.4)		N

Rus. 16; Anon.

A.R.  $2^h 16^m 51^s$ ; Decl.  $-60^{\circ} 37'$ 

16.784	143.4	18.37	0.1	2	370
16.795	144.0	18.20	23.3	$2\frac{1}{2}$	370
16.79	143.7	18.28	(10.3 ... 10.4)		N

 $h$  3499;  $-60^{\circ} 195$ ; 9.0A.R.  $2^h 17^m 6^s$ ; Decl.  $-60^{\circ} 36'$ 

16.773	61.5	8.07	0.7	$3\frac{1}{2}$	370
16.779	60.6	8.14	0.8	2	370
16.784	62.1	8.11	0.3	2	370
16.78	61.4	8.11	(9.4 ... 10.5)		F

 $h$  3501;  $-63^{\circ} 159$ ; 8.6A.R.  $2^h 22^m 39^s$ ; Decl.  $-63^{\circ} 45'$ 

16.806	336.2	22.80	1.8	2	370
16.812	337.1	22.93	3.0	$2\frac{1}{2}$	370
16.823	336.5	22.97	4.7	$1\frac{1}{2}$	370
16.81	336.6	22.90	(9.0 ... 11.4)		N

Dawson 1;  $-58^{\circ} 214$ ; 7.5A.R.  $2^h 24^m 15^s$ ; Decl.  $-58^{\circ} 42'$ 

16.773	224.7	0.88	0.9	3	650
16.785	227.1	0.93	6.0	3	475
16.795	226.2	0.96	23.5	2	475
16.78	226.0	0.92	(8.7 ... 9.2)		

AB,C =  $h$  3503

16.773	300.5	17.67	0.8	3	370
16.779	300.2	17.69	1.0	$1\frac{1}{2}$	370
16.78	300.4	17.68	(8.2 ... 10.8)		N

 $h$  3507;  $-64^{\circ} 175$ ; 9.4A.R.  $2^h 27^m 28^s$ ; Decl.  $-64^{\circ} 24'$ 

16.812	111.3	20.72	3.3	2	370
16.844	112.4	20.23	1.2	2	370
16.872	111.2	20.29	4.7	2	370
16.84	111.6	20.41	(9.5 ... 13.2)		N

 $h$  3510;  $-43^{\circ} 267$ ; 9.0A.R.  $2^h 29^m 36^s$ ; Decl.  $-43^{\circ} 31'$ 

12.869	12.8	9.11	0.1	2	300
12.886	11.3	8.99	0.6	2	300
14.542	12.5	8.76	23.5	$2\frac{1}{2}$	370
14.575	12.4	8.97	23.7	$2\frac{1}{2}$	370
13.72	12.3	8.96	(9.5 ... 10.4)		D?

 $h$  3514;  $-56^{\circ} 444$ ; 9.4A.R.  $2^h 29^m 58^s$ ; Decl.  $-56^{\circ} 41'$ 

13.885	19.8	33.61	7.0	2	300
13.899	20.0	33.71	7.2	2	300
13.89	19.9	33.66	(9.0 ... 9.6)		N

 $h$  3513;  $-43^{\circ} 268$ ; 10.0A.R.  $2^h 30^m 18^s$ ; Decl.  $-43^{\circ} 3'$ 

16.697	4.1	13.28	0.1	2	370
16.705	3.5	13.48	23.3	2	370
16.70	3.8	13.38	(9.8 ... 9.8)		N

 $h$  3517;  $-69^{\circ} 180$ ; 9.0A.R.  $2^h 31^m 41^s$ ; Decl.  $-69^{\circ} 45'$ 

16.888	238.3	16.51	1.6	2	370
16.951	238.5	16.15	4.2	2	370
16.959	239.1	16.21	5.5	$1\frac{1}{2}$	370
16.93	238.6	16.29	(9.1 ... 11.7)		N

 $h$  3516;  $-48^{\circ} 295$ ; 8.4A.R.  $2^h 31^m 32^s$ ; Decl.  $-48^{\circ} 58'$ 

16.697	334.9	24.22	0.2	2	370
16.705	334.5	24.19	23.5	2	370
16.70	334.7	24.21	(8.4 ... 10.8)		N



Có —; —53° 462; 7.5

A.R. 2<sup>h</sup> 34<sup>m</sup> 41<sup>s</sup>; Decl. —53° 30'

17.009	129.0	8.85	6.1	2	370
17.025	127.9	9.12	5.7	2	370
17.028	129.6	8.97	5.7	2	370
17.02	128.8	8.98	(7.6 ... 8.2)		11

h 3520; —55° 445 + 4; 7.5 + 8.3

A.R. 2<sup>h</sup> 35<sup>m</sup> 3<sup>s</sup>; Decl. —55° 22'

13.508	203.7	20.80	0.2	3	300
13.759	203.5	20.78	0.4	3	300
13.63	203.6	20.79	(8.0 ... 8.5)		F

h 3521; —49° 334; 9.2:

A.R. 2<sup>h</sup> 35<sup>m</sup> 22<sup>s</sup>; Decl. —49° 33'

16.697	262.1	15.16	0.4	2	370
16.705	261.9	15.20	23.8	2	370
16.70	262.0	15.18	(9.8 ... 10.0)		N

Δ 7 = h 3525; —60° 205 + 6; 7.2 + 8.0

A.R. 2<sup>h</sup> 36<sup>m</sup> 20<sup>s</sup>; Decl. —60° 6'

16.773	96.3	36.64	1.1	3	370
16.784	96.1	36.76	0.5	2	370
16.78	96.2	36.70	(7.6 ... 7.8)		12

h 3528; —73° 184; 9.4

A.R. 2<sup>h</sup> 37<sup>m</sup> 34<sup>s</sup>; Decl. —73° 60'

16.918	206.3	14.69	1.9	2	370
16.959	206.8	14.91	6.0	1½	370
16.94	206.5	14.80	(10.1 ... 11.0)		N

I 268; —60° 217; 8.4

A.R. 2<sup>h</sup> 43<sup>m</sup> 41<sup>s</sup>; Decl. —60° 40'

16.773	250.1	0.85	1.3	3	650
16.812	250.5	0.82	4.4	2	475
16.79	250.3	0.84	(9.0 ... 9.5)		

AB,C = h 3534

16.773	214.2	20.94	1.2	3	370
19.784	214.5	20.99	0.7	2	370
16.78	214.3	20.96	(8.5 ... 10.6)		13

h 3538; —62° 233; 9.0

A.R. 2<sup>h</sup> 47<sup>m</sup> 10<sup>s</sup>; Decl. —62° 43'

16.812	297.2	15.22	3.9	2	370
16.844	298.1	15.41	1.5	2	370
16.83	297.6	15.32	(9.4 ... 12.0)		N

h 3540; C6D —61° 515; 9.6

A.R. 2<sup>h</sup> 49<sup>m</sup> 6<sup>s</sup>; Decl. —61° 25'

16.773	8.6	7.78	1.7	3	370
16.784	7.0	7.79	1.4	2½	370
16.812	8.8	—	4.8	1½	370
16.872	6.9	7.91	5.6	2	370
16.81	7.8	7.83	(10.5 ... 11.5)		N

h 3541; —60° 226; 8.4

A.R. 2<sup>h</sup> 49<sup>m</sup> 20<sup>s</sup>; Decl. —60° 26'

16.773	157.7	2.61	1.5	3	650
16.784	157.8	2.62	1.2	2	370
16.872	157.2	2.84	5.3	2½	370
16.81	157.6	2.69	(8.7 ... 9.7)		D?

h 3542; —64° 205; 9.0

A.R. 2<sup>h</sup> 51<sup>m</sup> 10<sup>s</sup>; Decl. —64° 51'

16.806	140.5	12.86	2.2	2	370
16.812	140.7	12.89	3.6	2	370
16.81	140.6	12.88	(9.4 ... 10.0)		F

h 3544; —43° 304; 9.8

A.R. 2<sup>h</sup> 52<sup>m</sup> 12<sup>s</sup>; Decl. —43° 16'

16.697	191.1	4.38	0.6	2	370
16.705	189.8	4.40	0.0	2	370
16.716	192.9	[4.75]	23.4	2	370
16.738	190.3	4.39	0.7	3	370
16.71	191.0	4.39	(10.4 ... 10.8)		N

h 3547; —69° 161; 9.6

A.R. 2<sup>h</sup> 54<sup>m</sup> 10<sup>s</sup>; Decl. —69° 39'

16.888	165.6	13.81	1.8	1	370
16.951	164.6	13.55	4.5	2	370
16.92	165.1	13.68	(9.6 ... 12.1)		N

Δ 10 = h 3550; —51° 361 + 3; 7.4 + 8.4

A.R. 3<sup>h</sup> 0<sup>m</sup> 38<sup>s</sup>; Decl. —51° 49'

16.785	69.7	38.24	5.6	3	370
16.792	70.1	38.33	23.9	2	370
16.79	69.9	38.28	(7.8 ... 8.5)		14

h 3552; —70° 204; 8.6

A.R. 3<sup>h</sup> 2<sup>m</sup> 40<sup>s</sup>; Decl. —70° 58'

16.918	359.2	15.53	3.0	2	370
16.970	360.2	15.49	4.1	3	370
16.94	359.7	15.51	(8.8 ... 11.5)		N

$h$  3559;  $-64^\circ 229 + 31$ ;  $6.6 + 9.1$

A.R.  $3^h 7^m 52^s$ ; Decl.  $-64^\circ 23'$

16.921	40.2	43.08	2.5	2	370
16.970	40.0	43.11	4.6	3	370
16.95	40.1	43.10	(6.6 ... 9.8)		15

I 55 = Sellors 25;  $-44^\circ 338$ ;  $6.4$

A.R.  $3^h 8^m 2^s$ ; Decl.  $-44^\circ 53'$

16.686	165.5	0.83	0.2	$2\frac{1}{2}$	650
16.705	165.4	[1.15]	0.4	2	370
16.738	166.8	0.84	0.9	3	650
16.765	165.3	0.95	0.4	2	650
16.72	165.7	0.87	(6.7 ... 7.2)		M

AB,C =  $h$  3556

16.686	205.5	3.16	0.1	2	370
16.716	207.5	[3.53]	0.5	$1\frac{1}{2}$	370
16.738	206.5	3.16	0.8	3	370
16.765	206.2	3.14	0.5	2	370
16.73	206.4	3.15	(6.2 ... 9.6)		M

$h$  3562;  $-64^\circ 234 + 3$ ;  $8.6 + 9.1$

A.R.  $3^h 10^m 2^s$ ; Decl.  $-64^\circ 48'$

16.921	330.6	34.31	2.6	2	370
16.970	330.6	34.46	4.7	3	370
16.95	330.6	34.39	(8.8 ... 9.0)		F?

$h$  3566;  $-66^\circ 180$ ;  $8.3$

A.R.  $3^h 11^m 58^s$ ; Decl.  $-66^\circ 18'$

16.894	36.5	13.32	1.6	2	370
16.951	36.2	13.27	4.9	2	370
16.92	36.4	13.30	(8.8 ... 12.3)		N

$h$  3564;  $-59^\circ 263$ ;  $7.6$

A.R.  $3^h 12^m 2^s$ ; Decl.  $-59^\circ 59'$

16.765	278.8	29.68	0.9	2	370
16.773	279.1	29.70	1.8	3	370
16.77	279.0	29.69	(7.0 ... 12.0)		N

Aguilar 2;  $-58^\circ 274$ ;  $8.5$

A.R.  $3^h 12^m 30^s$ ; Decl.  $-58^\circ 17'$

13.885	155.1	8.30	7.2	2	300
13.893	153.8	—	6.3	3	420
13.899	153.7	8.40	7.4	2	300
14.328	149.9	8.34	10.3	2	370
14.00	153.1	8.35	(8.6 ... 10.8)		7

$\Delta$  12;  $-64^\circ 235$ ;  $6.5$

A.R.  $3^h 13^m 12^s$ ; Decl.  $-64^\circ 54'$

16.921	103.4	19.08	2.8	2	370
16.970	103.6	19.12	4.8	3	370
16.95	103.5	19.10	(6.7 ... 8.5)		F

$h$  3571; C6D  $-53^\circ 674$ ;  $11\frac{1}{2}$

A.R.  $3^h 15^m 37^s$ ; Decl.  $-53^\circ 34'$

16.785	94.6	20.07	5.9	3	370
16.795	94.8	20.23	0.8	2	370
16.79	94.7	20.15	(10.3 ... 11.0)		N

$h$  3573;  $-50^\circ 441$ ;  $8.5$

A.R.  $3^h 19^m 24^s$ ; Decl.  $-50^\circ 27'$

16.795	234.4	14.63	1.1	2	370
16.798	234.6	14.76	1.2	$2\frac{1}{2}$	370
16.80	234.5	14.70	(8.7 ... 9.6)		N

$h$  3576 =  $\lambda$  24;  $-46^\circ 319$ ;  $7.0$

A.R.  $3^h 20^m 24^s$ ; Decl.  $-46^\circ 6'$

16.686	342.5	3.36	0.4	2	370
16.697	341.0	2.91	0.8	2	370
16.716	342.9	3.10	0.8	2	370
16.738	339.8	3.03	1.2	3	370
16.71	341.6	3.10	(7.6 ... 9.1)		D?

$h$  3575;  $-51^\circ 404$ ;  $6.8$

A.R.  $3^h 20^m 54^s$ ; Decl.  $-51^\circ 30'$

16.795	45.4	34.85	0.9	2	370
16.798	45.3	34.87	1.3	$2\frac{1}{2}$	370
16.80	45.3	34.86	(7.0 ... 10.4)		F?

$h$  3579;  $-44^\circ 366$ ;  $8.6$

A.R.  $3^h 23^m 55^s$ ; Decl.  $-44^\circ 5'$

16.686	255.9	17.46	0.6	2	370
16.697	255.9	17.11	1.0	2	370
16.69	255.9	17.28	(8.6 ... 10.0)		N

$h$  3580;  $\alpha$  Reticuli;  $5.4$

A.R.  $3^h 27^m 12^s$ ; Decl.  $-63^\circ 22'$

16.921	125.2	54.25	3.0	2	370
16.970	125.1	54.03	4.9	3	370
16.95	125.1	54.14	(5.0 ... 10.2)		N

$h$  3584;  $-51^\circ 425$ ;  $8.2$

A.R.  $3^h 32^m 35^s$ ; Decl.  $-51^\circ 37'$

16.795	357.9	15.82	1.3	$1\frac{1}{2}$	370
16.798	357.5	15.65	1.5	2	370
16.872	357.6	15.51	5.9	2	370
16.82	357.7	15.66	(8.3 ... 11.9)		N

$h$  3586;  $-46^\circ 339$ ;  $9.6$

A.R.  $3^h 34^m 43^s$ ; Decl.  $-46^\circ 2'$

16.686	166.7	23.96	0.8	2	370
16.697	166.5	23.67	1.2	2	370
16.69	166.6	23.81	(9.8 ... 9.8)		16

$\Delta 14$ ;  $-60^\circ 262 + 1$ ;  $6.4 + 8.0$

A.R.  $3^h 35^m 41^s$ ; Decl.  $-60^\circ 11'$

16.765	271.01	57.51	1.3	2	370
16.773	271.0	57.47	2.0	3	370
16.77	271.0	57.49	(7.1 ... 8.0) D?		

$h 3587$ ;  $-60^\circ 267$ ;  $8.1$

A.R.  $3^h 36^m 4^s$ ; Decl.  $-60^\circ 14'$

16.765	240.5	14.07	1.7	2	370
16.773	240.3	13.76	2.1	2½	370
16.970	240.6	14.14	5.1	3	370
16.84	240.5	13.99	(8.7 ... 12.8) N		

$h 3590$ . Véase la nota. See note 17

$h 3592$ ;  $-54^\circ 589$ ;  $7.1$

A.R.  $3^h 41^m 22^s$ ; Decl.  $-54^\circ 40'$

13.885	12.3	5.48	7.4	2	300
14.145	13.8	4.97	8.1	3	475
14.183	12.6	5.37	8.5	2	370
14.07	12.9	5.27	(7.0 ... 10.0) 18		

$h 3591$ ;  $-51^\circ 446$ ;  $8.7$

A.R.  $3^h 41^m 31^s$ ; Decl.  $-51^\circ 42'$

16.798	325.9	13.70	1.7	2	370
16.970	326.4	13.66	5.3	3	370
16.88	326.2	13.68	(8.9 ... 11.5) N		

$h 3597$ ;  $-52^\circ 452$ ;  $9.9$

A.R.  $3^h 43^m 15^s$ ; Decl.  $-52^\circ 37'$

16.798	257.0	9.56	2.0	2	370
16.970	255.5	9.51	5.4	3	370
16.88	256.2	9.53	(10.7 ... 12.2) N		

$h 3603$ ;  $-71^\circ 217 + 18$ ;  $8.8 + 9.8$

A.R.  $3^h 44^m 18^s$ ; Decl.  $-71^\circ 23'$

16.918	82.3	19.20	3.2	2	370
16.970	82.7	18.95	4.3	3	370
16.94	82.5	19.07	(9.4 ... 9.9) D		

$h 3600$ ;  $-64^\circ 270 + 1$ ;  $8.5 + 9.0$

A.R.  $3^h 44^m 33^s$ ; Decl.  $-64^\circ 28'$

16.921	18.8	22.84	3.2	2½	370
16.973	19.0	22.65	6.0	2½	370
16.95	18.9	22.74	(8.5 ... 9.1) A		

$h 3598$ ;  $-50^\circ 491$ ;  $8.8$ :

A.R.  $3^h 44^m 41^s$ ; Decl.  $-50^\circ 50'$

16.798	232.5	13.62	2.2	2	370
16.970	232.7	13.51	5.5	3	370
16.88	232.6	13.56	(8.9 ... 10.7) M		

$I 389$ ;  $-55^\circ 570$ ;  $8.8$

A.R.  $3^h 46^m 32^s$ ; Decl.  $-55^\circ 44'$

13.885	202.6	2.67	7.6	2	300
14.145	202.3	2.78	8.4	3	475
14.183	203.0	2.63	8.7	2	370
14.07	202.6	2.69	(9.4 ... 9.6)		

$h 3606$ ;  $-71^\circ 224 + 3$ ;  $9.4 + 9.4$

A.R.  $3^h 48^m 20^s$ ; Decl.  $-71^\circ 11'$

16.918	334.7	16.79	3.4	2	370
16.970	334.9	16.92	4.4	3	370
16.94	334.8	16.86	(9.5 ... 9.8) F		

$h 3604$ ; Cód  $-49^\circ 1114$ ;  $10$

A.R.  $3^h 48^m 8^s$ ; Decl.  $-49^\circ 12'$

16.697	301.0	11.08	2.3	2	370
16.716	301.5	11.12	1.1	2	370
16.71	301.2	11.10	(10.8 ... 11.1) N		

$h 3609$ ; Anon.

A.R.  $3^h 50^m 36^s$ ; Decl.  $-63^\circ 2'$

16.921	310.8	9.84	3.5	2	370
16.973	310.0	9.84	3.0	3	370
17.009	310.4	9.89	6.6	2	370
16.97	310.4	9.86	(10.9 ... 11.2) N		

$h 3610$ ;  $-63^\circ 269$ ;  $10.1$

A.R.  $3^h 51^m 11^s$ ; Decl.  $-63^\circ 2'$

16.921	162.9	4.94	3.9	2	370
16.973	162.6	5.00	3.2	3	370
17.028	162.7	4.93	6.0	2	370
16.97	162.7	4.96	(9.5 ... 12.4) N		

$h 3616$ ;  $-45^\circ 394$ ;  $9.2$

A.R.  $3^h 57^m 10^s$ ; Decl.  $-45^\circ 12'$

16.686	136.1	26.66	1.5	2	370
16.697	136.2	26.44	1.8	2	370
16.69	136.2	26.55	(9.0 ... 10.5) N		

$h 3618$ ;  $-49^\circ 490$ ;  $8.8$

A.R.  $3^h 57^m 50^s$ ; Decl.  $-49^\circ 52'$

16.686	319.0	9.07	1.3	2	370
16.697	319.7	9.10	2.1	2	370
16.716	319.1	9.13	1.3	2	370
16.70	319.3	9.10	(9.9 ... 10.0) F		

Lacaille =  $h 3620$ ;  $-44^\circ 428$ ;  $8.1$

A.R.  $3^h 59^m 45^s$ ; Decl.  $-44^\circ 49'$

16.686	354.7	80.12	1.6	2	370
16.697	354.8	79.71	1.6	2	370
16.69	354.8	79.91	(8.8 ... 9.0) F		

$h$  3625;  $-52^\circ 49'8'' + 9$ ;  $9.7 + 9.7$ A.R.  $4^h 5^m 48^s$ ; Decl.  $-52^\circ 13'$ 

16.844	172.7	11.41	1.8	2	370
16.861	172.6	11.24	1.6	$2\frac{1}{2}$	370
16.85	172.6	11.32	(10.0 ... 10.2)		R

Delavan 1;  $-52^\circ 50'$ ; 8.7A.R.  $4^h 6^m 27^s$ ; Decl.  $-52^\circ 44'$ 

14.328	196.6	3.69	10.9	2	370
14.333	194.0	3.36	10.3	$2\frac{1}{2}$	370
14.347	194.7	3.53	10.0	2	370
14.34	195.1	3.53	(9.1 ... 9.2)		7

 $h$  3631;  $-69^\circ 24'$ ; 9.0A.R.  $4^h 7^m 50^s$ ; Decl.  $-69^\circ 23'$ 

16.918	229.9	7.00	3.9	2	370
16.978	230.2	6.88	3.8	2	370
17.028	229.3	6.93	6.2	2	370
16.97	229.8	6.94	(9.4 ... 10.2)		A

 $h$  3630 =  $h$  3639;  $-49^\circ 514'$ ; 8.6A.R.  $4^h 8^m 35^s$ ; Decl.  $-49^\circ 18'$ 

12.894	99.0	20.01	1.7	2	300
12.897	98.6	20.26	1.4	2	300
12.90	98.8	20.14	(8.5 ... 11.5)		19

 $h$  3634;  $-44^\circ 451'$ ; 8.5:A.R.  $4^h 11^m 26^s$ ; Decl.  $-44^\circ 56'$ 

13.211	331.1	11.20	7.1	$2\frac{1}{2}$	300
13.222	331.0	11.15	7.7	$2\frac{1}{2}$	300
13.22	331.0	11.18	(9.6 ... 9.7)		20

 $h$  3635;  $-56^\circ 648'$ ; 9.9A.R.  $4^h 11^m 42^s$ ; Decl.  $-56^\circ 23'$ 

16.697	326.8	11.66	2.6	2	370
16.716	326.6	12.07	1.6	2	370
16.738	328.0	11.78	1.4	3	370
16.72	327.1	11.84	(9.6 ... 11.4)		N

 $h$  3638;  $\alpha$  Reticuli; 4.0A.R.  $4^h 12^m 48^s$ ; Decl.  $-62^\circ 47'$ 

16.973	354.8	48.41	3.3	$2\frac{1}{2}$	370
17.033	354.3	48.93	6.2	2	370
17.074	353.9	48.37	6.3	$3\frac{1}{2}$	370
17.03	354.3	48.57	(3.7 ... 11.9)		N

 $h$  3641 =  $h$  3748;  $-62^\circ 334'$ ; 6.4A.R.  $4^h 13^m 10^s$ ; Decl.  $-62^\circ 30'$ 

16.973	247.0	8.89	6.3	2	370
17.009	247.1	8.81	3.9	2	370
17.033	247.5	8.93	6.3	2	370
17.00	247.2	8.88	(5.8 ... 12.6)		M

Rii 3;  $\theta$  Reticuli; 5.4A.R.  $4^h 16^m 17^s$ ; Decl.  $-63^\circ 34'$ 

16.921	2.6	4.56	4.1	2	370
16.973	5.3	4.37	6.7	2	370
17.033	4.0	4.41	6.5	2	370
16.98	4.0	4.45	(5.8 ... 8.2)		M

 $h$  3643;  $-44^\circ 464 + 6$ ;  $6.8 + 8.3$ A.R.  $4^h 15^m 19^s$ ; Decl.  $-44^\circ 34'$ 

13.211	114.1	70.36	7.3	$2\frac{1}{2}$	300
13.222	114.2	70.66	7.9	2	300
13.22	114.1	70.51	(6.5 ... 9.0)		F

 $h$  3645;  $-44^\circ 470$ ; 10.0A.R.  $4^h 17^m 30^s$ ; Decl.  $-44^\circ 39'$ 

12.869	134.9	8.58	0.8	3	300
12.872	134.8	8.33	1.9	3	300
12.886	134.8	8.57	1.1	$2\frac{1}{2}$	300
12.88	134.8	8.49	(9.7 ... 9.8)		A

 $h$  3648; C6D  $-43^\circ 1397$ ; 10A.R.  $4^h 18 24^s$ ; Decl.  $-43^\circ 54'$ 

13.211	25.3	11.83	7.5	2	300
13.222	23.4	—	8.2	2	300
13.228	—	11.94	7.2	$1\frac{1}{2}$	300
13.228	24.7	11.81	7.7	2	300
13.22	24.5	11.86	(9.9 ... 10.1)		N

Rii 4;  $-57^\circ 659$ ; 7.1A.R.  $4^h 21^m 46^s$ ; Decl.  $-57^\circ 21'$ 

13.885	238.1	6.59	7.8	$2\frac{1}{2}$	300
13.948	239.2	6.30	2.4	2	300
14.145	237.5	6.39	8.7	$2\frac{1}{2}$	475
13.99	238.3	6.43	(7.0 ... 7.3)		A

 $h$  3651;  $-64^\circ 328$ ; 8.8A.R.  $4^h 23^m 6^s$ ; Decl.  $-64^\circ 28'$ 

16.921	61.8	16.79	4.4	$1\frac{1}{2}$	370
17.033	62.4	16.83	6.8	2	370
16.98	62.1	16.81	(9.2 ... 10.3)		F

 $h$  3654;  $-67^\circ 316$ ; 6.8A.R.  $4^h 23^m 28^s$ ; Decl.  $-67^\circ 2'$ 

16.978	112.4	18.67	4.2	2	370
17.028	113.8	18.20	6.5	2	370
17.061	112.4	18.22	6.0	2	370
17.02	112.9	18.36	(6.8 ... 12.7)		N



*h* 3657; Anon.

A.R. 4<sup>h</sup> 23<sup>m</sup> 45<sup>s</sup>; Decl. -66° 33'

16.918	336.01	11.99	4.2	1½	370
17.028	337.5	12.04	6.8	2	370
16.97	336.8	12.02	(9.8 ... 10.2)		21

*h* 3655; -64° 334; 8.4

A.R. 4<sup>h</sup> 24<sup>m</sup> 2<sup>s</sup>; Decl. -64° 22'

17.033	162.4	48.47	7.1	2	370
17.074	161.9	48.87	6.4	3	370
17.077	161.9	48.74	6.7	2	370
17.06	162.1	48.69	(8.7 ... 12.2)		N

*h* 3656; -64° 335 + 3; 9.4 + 9.9

A.R. 4<sup>h</sup> 24<sup>m</sup> 6<sup>s</sup>; Decl. -64° 31'

17.009	260.2	26.69	4.0	2	370
17.033	260.4	26.68	7.0	2	370
17.02	260.3	26.69	(10.2 ... 10.8)		22

*h* 3658; -49° 551; 7.7

A.R. 4<sup>h</sup> 25<sup>m</sup> 32<sup>s</sup>; Decl. -49° 53'

12.894	120.9	5.93	1.9	2	300
12.897	120.2	5.86	1.6	2	300
13.075	120.6	5.90	7.0	2½	300
12.96	120.6	5.90	(8.0 ... 8.7)		F

*h* 3660; -65° 341; 9.4

A.R. 4<sup>h</sup> 26<sup>m</sup> 4<sup>s</sup>; Decl. -65° 47'

17.009	232.0	34.82	4.2	2	370
17.033	231.9	34.96	7.3	2	370
17.02	232.0	34.89	(10.1 ... 11.1)		N

*h* 3661; Anon.

A.R. 4<sup>h</sup> 26<sup>m</sup> 40<sup>s</sup>; Decl. -67° 34'

16.989	356.4	11.81	4.3	3	370
17.028	356.6	12.20	7.1	2	370
17.061	357.6	12.14	6.2	2	370
17.03	356.9	12.05	(10.4 ... 13.0)		N

*I* 154; -36° 545; 8.1

A.R. 4<sup>h</sup> 26<sup>m</sup> 43<sup>s</sup>; Decl. -36° 3'

16.970	130.9	0.58	5.9	3	650
16.989	135.9	0.42	3.8	3	650
17.118	131.8	0.60	7.1	2	650
17.03	132.9	0.53	(9.1 ... 9.2)		23

*β* 746; -36° 546; 7.6

A.R. 4<sup>h</sup> 27<sup>m</sup> 2<sup>s</sup>; Decl. -36° 10'

16.970	9.6	1.36	5.8	3	650
16.978	8.5	1.51	3.0	2	370
16.989	8.6	1.41	3.6	3	475
16.98	8.9	1.43	(8.5 ... 9.3)		M

*h* 3662; -65° 344 + 5; 8.5 + 8.8

A.R. 4<sup>h</sup> 27<sup>m</sup> 40<sup>s</sup>; Decl. -65° 59'

16.989	71.97	16.21	4.4	3	370
17.033	71.7	16.13	7.6	1½	370
17.01	71.7	16.17	(8.8 ... 9.4)		R

AC

16.989	194.8	37.86	4.5	3	370
17.033	193.5	38.35	7.8	1½	370
17.074	194.8	37.83	6.7	3	370
17.03	194.4	38.01	(8.8 ... 12.7)		

AD

16.989	3.4	21.76	4.6	3	370
17.074	3.5	21.65	6.8	2½	370
17.03	3.4	21.71	(8.8 ... 13.6)		N

*h* 3666; -66° 294; 9.2:

A.R. 4<sup>h</sup> 29<sup>m</sup> 32<sup>s</sup>; Decl. -66° 23'

17.009	205.0	12.88	4.4	2	370
17.061	205.0	12.76	6.3	2	370
17.04	205.0	12.82	(9.4 ... 10.9)		N

*h* 3665; -60° 315; 8.8

A.R. 4<sup>h</sup> 30<sup>m</sup> 0<sup>s</sup>; Decl. -60° 8'

16.773	55.5	6.32	2.3	3	370
16.784	56.1	6.32	2.7	3	370
17.061	55.8	6.39	6.6	2	370
16.87	55.8	6.34	(9.5 ... 9.6)		F

*h* 3668; *z* Doradus; 4.1 + 8.6

A.R. 4<sup>h</sup> 31<sup>m</sup> 19<sup>s</sup>; Decl. -55° 18'

13.948	102.5	78.23	2.6	2	300
14.145	102.1	78.05	8.9	2	475
14.05	102.3	78.14	(3.0 ... 9.0)		N

*h* 3670; -63° 342 + 3; 6.9 + 9.1

A.R. 4<sup>h</sup> 32<sup>m</sup> 16<sup>s</sup>; Decl. -63° 5'

17.074	98.7	31.88	7.4	3	370
17.077	99.0	32.05	7.2	2½	370
17.08	98.8	31.96	(6.7 ... 9.2)		F

*h* 3669; -53° 728; 9.6

A.R. 4<sup>h</sup> 32<sup>m</sup> 37<sup>s</sup>; Decl. -53° 7'

16.844	311.3	14.09	2.0	2	370
16.861	311.5	13.95	1.8	2	370
16.85	311.4	14.02	(10.0 ... 10.6)		N

*h* 3671;  $-50^{\circ} 615$ ; 9.1A.R. 4<sup>h</sup> 33<sup>m</sup> 28<sup>s</sup>; Decl.  $-50^{\circ} 24'$ 

16.844	277.5	6.44	2.3	2	370
16.861	278.2	6.61	2.0	2	370
16.971	278.8	6.54	6.3	3½	370
16.89	278.2	6.53	(10.5 ... 10.9)		F

*h* 3676; Anon.A.R. 4<sup>h</sup> 33<sup>m</sup> 30<sup>s</sup>; Decl.  $-67^{\circ} 49'$ 

17.121	183.2	14.41	8.9	2	370
17.156	182.1	14.30	7.5	2	370
17.14	182.6	14.36	(10.1 ... 11.8)		24

*h* 3675;  $-44^{\circ} 505$ ; 7.8A.R. 4<sup>h</sup> 34<sup>m</sup> 20<sup>s</sup>; Decl.  $-44^{\circ} 53'$ 

13.200	52.8	37.48	7.3	2	300
13.208	53.0	37.24	7.2	2	300
13.20	52.9	37.36	(7.8 ... 11.8)		N

*h* 3679;  $-62^{\circ} 372$ ; 6.9A.R. 4<sup>h</sup> 35<sup>m</sup> 19<sup>s</sup>; Decl.  $-62^{\circ} 19'$ 

17.074	7.0	32.33	7.5	2½	370
17.077	7.7	32.11	7.8	2½	370
17.07	7.4	32.22	(6.5 ... 11.9)		N

## AC

17.074	134.2	34.81	7.6	2½	370
17.077	133.8	34.68	8.0	2	370
17.07	134.0	35.75	(6.5 ... 11.0)		N

*h* 3678;  $-45^{\circ} 498$ ; 8.3A.R. 4<sup>h</sup> 35<sup>m</sup> 56<sup>s</sup>; Decl.  $-45^{\circ} 17'$ 

13.200	328.4	41.20	7.5	2	300
13.208	328.5	41.35	7.5	2	300
13.20	328.4	41.27	(8.1 ... 9.5)		F

*h* 3682;  $-66^{\circ} 309$ ; 8.8A.R. 4<sup>h</sup> 37<sup>m</sup> 10<sup>s</sup>; Decl.  $-66^{\circ} 22'$ 

17.121	12.9	28.70	8.6	2	370
17.156	13.3	29.75	7.2	2	370
17.162	13.3	29.11	8.5	2	370
17.15	13.2	29.19	(8.8 ... 14.3)		N

*h* 3680;  $-52^{\circ} 551$ ; 9.4A.R. 4<sup>h</sup> 37<sup>m</sup> 28<sup>s</sup>; Decl.  $-52^{\circ} 8'$ 

16.844	208.8	10.24	2.5	2½	370
16.861	208.9	10.25	2.2	2	370
16.85	208.8	10.24	(10.6 ... 10.7)		D

*h* 3681;  $-47^{\circ} 469$ ; 7.4A.R. 4<sup>h</sup> 38<sup>m</sup> 12<sup>s</sup>; Decl.  $-47^{\circ} 30'$ 

12.894	254.1	40.94	2.3	2	300
12.897	253.8	41.56	2.0	2	300
12.918	254.2	40.42	2.8	2½	300
12.90	254.0	40.97	(6.7 ... 10.3)		A?

*h* 3683;  $-59^{\circ} 370$ ; 7.1A.R. 4<sup>h</sup> 38<sup>m</sup> 14<sup>s</sup>; Decl.  $-59^{\circ} 11'$ 

16.773	77.1	1.02	2.5	2½	650
16.784	80.0	0.96	2.9	3	475
17.074	75.9	0.87	7.2	3	650
17.077	76.9	0.81	7.0	2½	650
16.93	77.5	0.91	(7.9 ... 8.0)		D

*h* 3684; Anon.A.R. 4<sup>h</sup> 38<sup>m</sup> 55<sup>s</sup>; Decl.  $-67^{\circ} 58'$ 

17.107	278.1	16.75	7.2	2	370
17.156	278.7	17.04	7.7	2	370
17.162	278.3	16.71	8.7	2	370
17.14	278.4	16.83	(9.3 ... 12.6)		N

*h* 3686;  $-61^{\circ} 359$ ; 7.6A.R. 4<sup>h</sup> 40<sup>m</sup> 8<sup>s</sup>; Decl.  $-61^{\circ} 27'$ 

16.773	219.4	7.34	2.7	2½	370
16.785	219.5	7.29	3.1	3	475
17.061	220.4	7.32	6.8	2	370
16.87	219.8	7.32	(8.3 ... 8.4)		M

*h* 3689;  $-65^{\circ} 369$ ; 8.7A.R. 4<sup>h</sup> 40<sup>m</sup> 32<sup>s</sup>; Decl.  $-65^{\circ} 33'$ 

17.074	42.2	20.96	7.8	3	370
17.077	42.6	21.11	8.2	2	370
17.08	42.4	21.03	(8.9 ... 12.3)		N

## BC = Dawson 2

17.074	103.8	3.83	7.9	2	370
17.077	104.5	3.44	8.4	2	370
17.107	106.3	4.16	6.8	2	370
17.121	104.2	3.50	8.4	2	370
17.09	104.7	3.63	(12.3 ... 12.8)		

*h* 3688;  $-54^{\circ} 705$ ; 9.1A.R. 4<sup>h</sup> 40<sup>m</sup> 45<sup>s</sup>; Decl.  $-54^{\circ} 10'$ 

16.697	146.2	14.56	2.8	2	370
16.716	145.3	14.19	2.0	1	370
16.738	146.1	14.31	1.6	3	370
16.72	145.9	14.35	(9.2 ... 11.5)		N

*h* 3685;  $-43^{\circ} 494$ ; 9.0:

A.R.  $4^h 40^m 54^s$ ; Decl.  $-43^{\circ} 38'$

13.200	124.7	17.40	7.8	2	300
13.208	124.9	17.29	7.7	2	300
13.20	124.8	17.35	(9.5 ... 9.8)		M

*h* 3696;  $-56^{\circ} 732$ ; 8.4

A.R.  $4^h 45^m 29^s$ ; Decl.  $-56^{\circ} 14'$

12.875	296.5	3.68	2.1	2	300
12.932	296.3	3.82	2.5	3	300
12.935	295.4	3.63	2.3	2½	300
12.938	296.5	3.78	2.6	3	300
12.92	296.2	3.73	(8.6 ... 9.2)		M

I 730;  $-52^{\circ} 581$ ; 8.4

A.R.  $4^h 45^m 34^s$ ; Decl.  $-52^{\circ} 51'$

16.971	82.9	1.57	6.5	3	370
17.074	82.1	1.66	7.0	3	370
17.121	84.5	1.51	8.2	2	370
17.06	83.2	1.58	(8.9 ... 9.4)		

AC = Dawson 3

16.971	34.4	3.89	6.6	3	370
17.074	31.6	3.77	7.1	3	370
17.118	34.5	[3.11]	7.5	2	370
17.121	32.7	3.84	8.1	2½	370
17.07	33.3	3.83	(8.9 ... 14.4)		

*h* 3694;  $-45^{\circ} 522$ ; 8.2

A.R.  $4^h 45^m 39^s$ ; Decl.  $-45^{\circ} 23'$

12.822	62.0	9.22	3.3	2	300
12.825	62.4	8.79	23.2	2½	300
12.872	62.1	9.12	2.1	2½	300
12.918	62.3	9.01	2.3	2	300
12.86	62.2	9.04	(8.2 ... 9.0)		D

*h* 3699;  $-45^{\circ} 528$ ; 8.0

A.R.  $4^h 46^m 59^s$ ; Decl.  $-45^{\circ} 53'$

13.200	144.0	17.79	8.4	2	300
13.208	144.4	17.76	8.0	2	300
13.20	144.2	17.78	(7.8 ... 10.8)		M?

*h* 3703;  $-62^{\circ} 389$ ; 9.2

A.R.  $4^h 47^m 59^s$ ; Decl.  $-62^{\circ} 6'$

16.774	301.4	10.08	3.0	2½	370
16.785	300.8	9.92	3.3	2½	370
16.78	301.1	10.00	(9.9 ... 11.0)		N

$\Delta$  18;  $\iota$  Pictoris; 6.5

A.R.  $4^h 48^m 9^s$ ; Decl.  $-53^{\circ} 40'$

16.844	58.0	12.20	2.7	2	370
16.861	56.7	12.24	2.3	2	370
16.971	57.9	12.26	6.7	3	370
16.89	57.5	12.33	(6.5 ... 7.6)		F

*h* 3706;  $-57^{\circ} 712$ ; 8.8

A.R.  $4^h 50^m 40^s$ ; Decl.  $-57^{\circ} 24'$

16.738	279.5	21.04	1.8	3	370
16.798	279.8	21.03	2.4	2	370
16.77	279.6	21.04	(8.8 ... 11.9)		N

*h* 3707;  $-59^{\circ} 393$ ; 9.2

A.R.  $4^h 51^m 6^s$ ; Decl.  $-59^{\circ} 58'$

16.774	270.5	8.26	3.2	2	370
16.785	269.4	8.16	3.5	2	370
17.061	271.9	7.94	7.1	2	370
16.87	270.6	8.12	(9.9 ... 12.8)		25

*h* 3710;  $-67^{\circ} 358$ ; 9.1

A.R.  $4^h 53^m 24^s$ ; Decl.  $-67^{\circ} 7'$

17.107	82.8	11.85	7.4	2	370
17.156	84.0	11.59	7.9	2	370
17.162	82.4	11.51	9.0	2	370
17.14	83.1	11.65	(9.4 ... 11.6)		N

*h* 3712; Anon.

A.R.  $4^h 53^m 40^s$ ; Decl.  $-68^{\circ} 50'$

17.162	153.8	8.26	9.2	2	370
17.203	150.9	8.52	9.3	2	370
17.18	152.4	8.39	(13.0 ... 13.5)		N

*h* 3715;  $-49^{\circ} 611$ ; 7.0

A.R.  $4^h 56^m 14^s$ ; Decl.  $-49^{\circ} 39'$

12.894	112.0	10.02	2.7	2½	300
12.897	112.4	9.85	2.3	1½	300
12.90	112.2	9.93	(7.6 ... 8.9)		F

*h* 3724;  $-55^{\circ} 731$ ; 8.7

A.R.  $5^h 0^m 23^s$ ; Decl.  $-55^{\circ} 58'$

12.875	101.8	2.91	2.6	2	300
12.935	100.0	2.89	2.8	2	300
12.938	101.0	2.91	3.0	3	300
12.92	100.9	2.90	(9.0 ... 9.1)		20

Anon.;  $-45^{\circ} 56'7$ ; 9.9A.R.  $5^h 3^m 59^s$ ; Decl.  $-45^{\circ} 36'$ 

12.853	80.6	8.35	3.0	3	300
12.872	82.0	8.18	2.5	$2\frac{1}{2}$	300
12.886	82.3	8.26	1.9	2	300
12.87	81.6	8.26	(9.7 ... 10.0)		26

 $h 3729$ ;  $-44^{\circ} 60'4$ ; 8.8A.R.  $5^h 4^m 34^s$ ; Decl.  $-44^{\circ} 59'$ 

12.853	231.6	10.05	2.8	3	300
12.886	232.0	10.17	1.5	2	300
12.87	231.8	10.11	(9.5 ... 9.6)		F

 $h 3731$ ;  $-56^{\circ} 78'7$ ; 9.2A.R.  $5^h 5^m 44^s$ ; Decl.  $-56^{\circ} 3'$ 

12.968	303.1	10.05	3.3	2	300
12.973	302.8	10.46	4.2	$2\frac{1}{2}$	300
12.976	304.4	10.36	4.4	$2\frac{1}{2}$	300
12.981	301.9	10.32	3.3	2	300
12.97	303.1	10.30	(9.4 ... 10.6)		22

 $h 3734$ ;  $-43^{\circ} 56'2$ ; 9.4:A.R.  $5^h 8^m 1^s$ ; Decl.  $-43^{\circ} 2'$ 

13.211	197.2	11.61	8.1	$2\frac{1}{2}$	300
13.228	196.8	11.63	7.9	2	300
13.22	197.0	11.62	(9.6 ... 10.1)		F

 $h 3736$ ;  $-57^{\circ} 75'2$ ; 9.3A.R.  $5^h 8^m 5^s$ ; Decl.  $-57^{\circ} 44'$ 

16.844	323.9	17.15	2.9	2	370
16.861	324.2	17.38	2.5	$2\frac{1}{2}$	370
16.85	324.1	17.27	(9.4 ... 12.8)		N

 $h 3738$ ;  $-55^{\circ} 75'9 + 8$ ;  $10.0 + 10.0$ A.R.  $5^h 9^m 0^s$ ; Decl.  $-55^{\circ} 28'$ 

16.845	10.2	14.05	3.1	2	370
16.861	11.0	14.03	2.7	$2\frac{1}{2}$	370
16.85	10.6	14.04	(10.8 ... 10.8)		N

 $h 3739$ ;  $-48^{\circ} 61'8$ ; 7.9A.R.  $5^h 10^m 6^s$ ; Decl.  $-48^{\circ} 1'$ 

12.894	283.0	3.16	3.1	3	300
12.897	282.6	3.46	2.7	2	300
12.902	281.9	3.38	3.1	2	300
12.90	282.5	3.33	(8.4 ... 8.7)		F

 $h 3742$ ;  $-55^{\circ} 76'6$ ; 7.6A.R.  $5^h 11^m 1^s$ ; Decl.  $-55^{\circ} 43'$ 

16.845	279.0	22.58	3.4	2	370
16.861	279.0	22.95	3.2	$2\frac{1}{2}$	370
16.971	279.2	22.91	7.0	2	370
16.89	279.1	22.81	(7.6 ... 12.7)		N

 $h 3743$ ;  $-60^{\circ} 39'5$ ; 8.6A.R.  $5^h 11^m 28^s$ ; Decl.  $-60^{\circ} 8'$ 

16.774	132.4	5.16	3.3	2	370
16.785	132.1	5.09	3.7	$2\frac{1}{2}$	370
17.028	131.9	5.16	7.8	2	370
16.86	132.1	5.14	(8.9 ... 10.2)		A

 $h 5450$ ;  $-56^{\circ} 81'1$ ; 9.4A.R.  $5^h 11^m 40^s$ ; Decl.  $-56^{\circ} 56'$ 

16.845	270.7	6.76	3.6	$1\frac{1}{2}$	370
16.861	270.8	6.99	3.4	2	370
17.028	271.2	7.02	7.6	$2\frac{1}{2}$	370
16.91	270.9	6.92	(10.5 ... 10.7)		N

 $h 3746$ ;  $-72^{\circ} 35'2$ ; 8.9A.R.  $5^h 12^m 16^s$ ; Decl.  $-72^{\circ} 13'$ 

16.918	263.8	4.11	3.6	2	370
17.066	265.0	4.01	5.0	$2\frac{1}{2}$	370
17.077	265.1	3.94	8.6	$2\frac{1}{2}$	370
17.159	265.1	4.05	8.8	2	370
17.06	264.8	4.03	(9.0 ... 9.3)		27

 $h 3747$ ;  $-67^{\circ} 40'2$ ; 9.1A.R.  $5^h 13^m 52^s$ ; Decl.  $-67^{\circ} 43'$ 

17.031	107.6	7.78	5.2	2	370
17.077	106.4	7.90	8.7	2	370
17.107	106.4	7.91	7.8	2	370
17.07	106.8	7.87	(9.2 ... 11.8)		F?

 $h 3754$ ;  $-70^{\circ} 37'5 + 6$ ;  $9.4 + 9.7$ A.R.  $5^h 15^m 33^s$ ; Decl.  $-70^{\circ} 5'$ 

17.031	132.3	17.12	5.4	2	370
17.063	133.2	17.09	5.0	2	370
17.077	132.3	17.02	9.2	2	370
17.06	132.6	17.08	(9.8 ... 10.9)		F

 $h 3755$ ;  $-62^{\circ} 45'6$ ; 8.4A.R.  $5^h 16^m 56^s$ ; Decl.  $-62^{\circ} 5'$ 

16.785	280.0	21.77	3.8	$2\frac{1}{2}$	370
17.074	280.1	21.73	8.1	3	370
16.93	280.1	21.75	(8.3 ... 12.8)		N

 $h 3756$ ;  $-58^{\circ} 48'7$ ; 8.9A.R.  $5^h 17^m 3^s$ ; Decl.  $-58^{\circ} 54'$ 

16.785	171.5	17.99	4.0	2	370
17.028	171.6	17.92	8.0	2	370
16.91	171.6	17.96	(9.4 ... 11.9)		F?

*h* 3758;  $-47^{\circ} 573$ ; 9.9  
 A.R.  $5^{\text{h}} 19^{\text{m}} 10^{\text{s}}$ ; Decl.  $-47^{\circ} 23'$

13.217	66.5	12.37	8.5	$2\frac{1}{2}$	300
13.228	66.3	12.40	8.5	2	300
13.22	66.4	12.38	(9.9 ... 10.0)		N

$\Delta$  20; 0 Pictoris; 6.8 + 7.2  
 A.R.  $5^{\text{h}} 21^{\text{m}} 56^{\text{s}}$ ; Decl.  $-52^{\circ} 26'$

16.869	287.2	38.23	2.6	2	370
16.886	287.1	38.23	3.9	2	370
16.88	287.2	38.23	(7.2 ... 7.6)		28

*h* 3763;  $-43^{\circ} 606$ ; 7.9  
 A.R.  $5^{\text{h}} 22^{\text{m}} 36^{\text{s}}$ ; Decl.  $-43^{\circ} 29'$

13.211	252.8	12.12	8.7	—	300
13.228	253.5	12.17	8.2	2	300
13.22	253.2	12.14	(8.5 ... 9.2)		F?

*h* 3764; C6D  $-60^{\circ} 1161$ ;  $11\frac{1}{4}$   
 A.R.  $5^{\text{h}} 23^{\text{m}} 58^{\text{s}}$ ; Decl.  $-60^{\circ} 12'$

16.785	273.6	11.77	4.3	2	370
17.028	274.2	—	8.4	$1\frac{1}{2}$	370
17.074	275.1	11.85	8.3	$2\frac{1}{2}$	370
16.96	274.3	11.81	(10.2 ... 13.2)		N

*h* 3768;  $-66^{\circ} 414$ ; 9.4  
 A.R.  $5^{\text{h}} 26^{\text{m}} 5^{\text{s}}$ ; Decl.  $-66^{\circ} 42'$

17.066	34	9.0	5.3	2	370
17.203	36	8.2	9.6	2	370
17.13	35	8.6	(Neb. ... 11.2)		29

*h* 3767;  $-47^{\circ} 595$ ; 6.5  
 A.R.  $5^{\text{h}} 26^{\text{m}} 44^{\text{s}}$ ; Decl.  $-47^{\circ} 10'$

16.978	252.1	25.76	3.3	2	370
17.126	251.7	25.87	8.4	2	370
17.05	251.9	25.82	(5.8 ... 11.0)		R

AC =  $\Delta$  21

13.228	267.7	197.70	8.7	2	300
13.233	267.5	199.05	8.7	$1\frac{1}{2}$	300
13.241	267.6	198.36	8.0	3	300
13.244	267.6	198.38	8.1	3	300
13.24	267.6	198.37	(5.8 ... 7.0)		R

$\Delta$  22;  $-42^{\circ} 686$ ; 7.2  
 A.R.  $5^{\text{h}} 27^{\text{m}} 17^{\text{s}}$ ; Decl.  $-42^{\circ} 24'$

12.853	170.0	7.25	3.4	3	300
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*h* 3774; Véase la nota; See note. 30

$-54^{\circ} 854 + 3$ ; 7.3 + 9.3  
 A.R.  $5^{\text{h}} 31^{\text{m}} 15^{\text{s}}$ ; Decl.  $-54^{\circ} 59'$

AB = *h* 3777

16.697	345.94	53.90	3.1	2	370
16.798	345.5	53.97	2.6	2	370
16.75	345.5	53.94	(7.2 ... 10.1)		R?

BC = *h* 3778

16.697	103.8	11.24	3.3	2	370
16.798	103.8	11.20	2.8	2	370
16.75	103.8	11.22	(10.1 ... 12.2)		

*h* 3783;  $-71^{\circ} 346$ ; 8.5  
 A.R.  $5^{\text{h}} 32^{\text{m}} 22^{\text{s}}$ ; Decl.  $-71^{\circ} 0'$

17.159	259.6	15.53	8.9	2	370
17.162	259.6	15.54	9.4	2	370
17.16	259.6	15.54	(8.4 ... 9.9)		F

*h* 3784;  $-46^{\circ} 609$ ; 8.0  
 A.R.  $5^{\text{h}} 34^{\text{m}} 40^{\text{s}}$ ; Decl.  $-46^{\circ} 10'$

12.822	62.4	5.04	3.7	2	300
12.825	63.3	5.37	0.9	2	300
12.897	62.9	5.51	3.3	2	300
12.902	60.9	5.51	3.4	$1\frac{1}{2}$	300
12.86	62.4	5.36	(8.0 ... 9.1)		M

*h* 3786;  $-53^{\circ} 904$ ; 9.0  
 A.R.  $5^{\text{h}} 35^{\text{m}} 2^{\text{s}}$ ; Decl.  $-53^{\circ} 34'$

16.886	97.4	13.23	4.2	2	370
17.118	97.2	13.30	7.7	2	370
17.00	97.3	13.27	(9.4 ... 11.5)		N

*h* 3790;  $-66^{\circ} 434$ ; 9.5  
 A.R.  $5^{\text{h}} 35^{\text{m}} 2^{\text{s}}$ ; Decl.  $-66^{\circ} 58'$

17.066	163.2	11.13	5.5	2	370
17.203	160.4	11.01	9.8	2	370
17.13	161.8	11.07	(9.1 ... 12.5)		N

*h* 3787;  $-54^{\circ} 857 + 6$ ; 8.2 + 9.4  
 A.R.  $5^{\text{h}} 35^{\text{m}} 19^{\text{s}}$ ; Decl.  $-54^{\circ} 38'$

16.697	248.9	24.88	3.5	2	370
16.861	247.9	24.59	3.6	$2\frac{1}{2}$	370
17.118	248.4	24.58	8.0	2	370
16.89	248.4	24.68	(8.2 ... 10.4)		21

*h* 3789;  $-50^{\circ} 816$ ; 8.2:  
 A.R.  $5^{\text{h}} 36^{\text{m}} 0^{\text{s}}$ ; Decl.  $-50^{\circ} 12'$

17.118	1.0	9.05	7.8	$2\frac{1}{2}$	370
17.167	0.9	8.92	8.6	2	370
17.206	1.3	9.01	8.5	$1\frac{1}{2}$	370
17.233	0.6	9.00	9.8	2	370
17.18	1.0	9.00	(8.8 ... 9.4)		F



*h* 3792;  $-59^{\circ} 492$ ; 9.0A.R. 5<sup>h</sup> 36<sup>m</sup> 48<sup>s</sup>; Decl.  $-59^{\circ} 8'$ 

16.785	147.9	19.72	4.5	2½	370
17.074	148.1	19.79	8.5	2½	370
16.93	148.0	19.76	(9.2 ... 12.6)		N

*h* 3793;  $-48^{\circ} 698$ ; 7.3A.R. 5<sup>h</sup> 38 16<sup>s</sup>; Decl.  $-48^{\circ} 19'$ 

13.217	119.2	11.95	8.7	2	300
13.233	120.3	11.86	9.1	1½	300
13.22	119.7	11.91	(7.1 ... 10.2)		R

*h* 3797;  $-46^{\circ} 627$ ; 8.8A.R. 5<sup>h</sup> 41<sup>m</sup> 14<sup>s</sup>; Decl.  $-46^{\circ} 21'$ 

13.217	173.8	52.06	9.0	2	300
13.241	174.6	52.14	8.4	3	300
13.23	174.2	52.10	(8.8 ... 9.5)		F

*h* 3800;  $-56^{\circ} 928$ ; 7.2A.R. 5<sup>h</sup> 42<sup>m</sup> 12<sup>s</sup>; Decl.  $-56^{\circ} 58'$ 

16.861	292.3	9.28	3.8	2½	370
17.118	294.3	9.31	8.7	2	370
17.167	293.8	8.95	9.1	2	370
17.05	293.5	9.18	(10.7 ... 12.4)		31

*h* 3802;  $-55^{\circ} 864$ ; 7.8A.R. 5<sup>h</sup> 42<sup>m</sup> 56<sup>s</sup>; Decl.  $-55^{\circ} 46'$ 

12.875	306.7	7.55	3.1	2	300
12.932	307.1	7.35	3.8	3	300
12.935	308.9	7.55	3.4	2	300
12.938	308.8	7.52	2.8	3	300
12.92	307.9	7.49	(8.0 ... 9.5)		F

*h* 3801;  $-46^{\circ} 631$ ; 7.1A.R. 5<sup>h</sup> 42<sup>m</sup> 59<sup>s</sup>; Decl.  $-46^{\circ} 39'$ 

13.217	193.6	—	9.2	2	300
13.241	195.2	37.34	8.6	3	300
13.244	194.4	37.00	8.4	3	300
13.247	194.7	36.84	8.8	3	300
13.24	194.4	37.06	(6.0 ... 12.0)		N

*h* 3803;  $-44^{\circ} 725$ ; 7.7A.R. 5<sup>h</sup> 43<sup>m</sup> 23<sup>s</sup>; Decl.  $-44^{\circ} 51'$ 

13.200	114.6	20.28	8.7	2	300
13.208	114.2	20.43	8.3	2	300
13.20	114.4	20.36	(7.5 ... 9.5)		21

*h* 3805;  $-43^{\circ} 692$ ; 8.8A.R. 5<sup>h</sup> 46<sup>m</sup> 1<sup>s</sup>; Decl.  $-43^{\circ} 33'$ 

12.822	125.1	5.10	4.6	2½	300
12.825	125.8	5.14	1.6	2	300
12.853	125.5	5.34	3.6	3	300
12.83	125.5	5.19	(9.5 ... 11.0)		21

Anon.;  $-67^{\circ} 509$ ; 7.8A.R. 5<sup>h</sup> 46<sup>m</sup> 29<sup>s</sup>; Decl.  $-67^{\circ} 45'$ 

17.107	159.2	13.48	8.1	2	370
17.156	154.1	13.88	8.1	2	370
17.203	156.6	13.88	10.1	2	370
17.16	156.6	13.75	(7.8 ... 14.0)		32

*h* 3701;  $-67^{\circ} 511$ ; 9.1A.R. 5<sup>h</sup> 46<sup>m</sup> 44<sup>s</sup>; Decl.  $-67^{\circ} 44'$ 

17.066	127.7	17.26	5.8	2	370
17.107	129.0	17.61	8.2	2	370
17.156	128.3	17.55	8.2	2	370
17.11	128.3	17.47	(9.1 ... 11.9)		32

*h* 3808;  $-57^{\circ} 894$ ; 9.9A.R. 5<sup>h</sup> 47<sup>m</sup> 30<sup>s</sup>; Decl.  $-57^{\circ} 40'$ 

16.861	311.0	6.16	4.0	2	370
17.118	309.3	6.32	9.0	2	370
17.167	308.5	6.17	9.4	1½	370
17.05	309.6	6.22	(11.3 ... 11.3)		N

*h* 3810;  $-61^{\circ} 531 + 2$ ; 9.6 + 10.0A.R. 5<sup>h</sup> 47<sup>m</sup> 44<sup>s</sup>; Decl.  $-61^{\circ} 10'$ 

16.785	172.3	23.56	4.9	2½	370
17.075	172.0	23.76	8.9	3	370
16.93	172.1	23.66	(9.3 ... 12.0)		20

*h* 3813;  $-67^{\circ} 515$ ; 9.1A.R. 5<sup>h</sup> 47<sup>m</sup> 46<sup>s</sup>; Decl.  $-67^{\circ} 48'$ 

17.066	304.7	27.04	5.7	2	370
17.107	304.4	26.90	8.4	2	370
17.09	304.6	26.97	(8.2 ... 12.1)		N

*h* 3812;  $-59^{\circ} 522$ ; 8.6A.R. 5<sup>h</sup> 48<sup>m</sup> 4<sup>s</sup>; Decl.  $-59^{\circ} 52'$ 

16.774	189.8	2.56	3.4	3	370
16.785	191.1	2.49	4.7	3	475
17.075	189.8	2.51	8.7	2½	370
16.88	190.2	2.52	(9.1 ... 9.4)		F

*h* 3815;  $-65^{\circ} 505 + 6$ ;  $9.6 + 10.0$

A.R.  $5^h 48^m 34^s$ ; Decl.  $-65^{\circ} 54'$

17.066	147.7	32.77	6.0	$2\frac{1}{2}$	370
17.107	148.0	32.56	8.8	2	370
17.09	147.8	32.67	(10.2 ... 10.3) 20		

*h* 3816;  $-47^{\circ} 672$ ; 7.6

A.R.  $5^h 49^m 50^s$ ; Decl.  $-47^{\circ} 59'$

13.208	179.1	23.01	8.6	2	300
13.241	180.0	22.81	9.0	3	300
13.22	179.6	22.91	(7.5 ... 10.8) N		

*h* 3820;  $-69^{\circ} 534 + 5$ ;  $7.8 + 9.8$

A.R.  $5^h 52^m 14^s$ ; Decl.  $-69^{\circ} 56'$

17.107	90.6	26.56	8.6	2	370
17.156	90.9	26.53	8.4	2	370
17.13	90.8	26.54	(7.8 ... 10.8) A		

*h* 3822;  $-53^{\circ} 978 + 7$ ;  $7.4 + 7.8$

A.R.  $5^h 54^m 36^s$ ; Decl.  $-53^{\circ} 26'$

17.118	304.2	56.09	9.2	2	370
17.233	304.0	56.17	10.5	$1\frac{1}{2}$	370
17.18	304.1	56.13	(7.5 ... 8.4) F?		

BC

17.118	125.4	20.20	9.3	2	370
17.233	125.3	20.12	10.8	$1\frac{1}{2}$	370
17.18	125.4	20.16	(8.4 ... 13.0) N		

*h* 3824;  $-50^{\circ} 875$ ; 9.3

A.R.  $5^h 55^m 40^s$ ; Decl.  $-50^{\circ} 25'$

17.118	273.1	6.41	9.6	2	370
17.233	271.6	6.64	10.2	2	370
17.241	271.5	6.47	8.3	$2\frac{1}{2}$	370
17.20	272.1	6.51	(9.7 ... 12.7) N		

*h* 3829;  $-62^{\circ} 552$ ; 9.0

A.R.  $5^h 57^m 14^s$ ; Decl.  $-62^{\circ} 46'$

17.156	354.2	21.23	8.5	2	370
17.203	354.5	21.23	10.4	2	370
17.18	354.3	21.23	(8.6 ... 13.0) N		

*h* 3828;  $-53^{\circ} 990$ ; 9.0:

A.R.  $5^h 57^m 32^s$ ; Decl.  $-53^{\circ} 55'$

17.118	119.9	13.53	9.4	2	370
17.241	120.4	13.59	8.4	$2\frac{1}{2}$	370
17.18	120.2	13.56	(9.9 ... 10.7) A		

*h* 3831;  $-41^{\circ} 885$ ; 7.9

A.R.  $6^h 0^m 17^s$ ; Decl.  $-41^{\circ} 9'$

12.822	134.5	2.53	5.2	$2\frac{1}{2}$	300
12.825	133.7	3.02	2.1	$1\frac{1}{2}$	300
12.957	131.9	2.65	2.7	3	300
12.962	130.9	2.55	2.9	$2\frac{1}{2}$	300
12.89	132.8	2.69	(8.5 ... 8.5) A		

*h* 3834;  $-45^{\circ} 755$ ; 7.2

A.R.  $6^h 1^m 4^s$ ; Decl.  $-45^{\circ} 5'$

12.822	227.0	4.07	5.5	2	300
12.825	224.1	3.89	2.6	2	300
12.853	222.4	3.80	3.9	3	300
12.858	222.8	3.89	3.0	3	300
12.872	224.2	3.77	2.8	2	300
12.85	224.1	3.88	(6.4 ... 8.7) M		

*h* 3836;  $-49^{\circ} 862$ ; 9.2

A.R.  $6^h 3^m 39^s$ ; Decl.  $-49^{\circ} 54'$

12.957	295.8	9.12	3.8	3	300
12.962	295.3	9.19	3.3	$2\frac{1}{2}$	300
12.987	296.5	9.04	3.4	3	300
12.97	295.9	9.12	(9.3 ... 9.6) F		

*h* 3837;  $-55^{\circ} 940$ ; 8.2

A.R.  $6^h 3^m 46^s$ ; Decl.  $-55^{\circ} 57'$

13.296	290.9	11.98	9.7	3	300
13.302	290.2	12.35	9.8	2	300
13.307	290.7	12.22	10.0	2	300
13.30	290.6	12.18	(8.1 ... 12.0) N		

AC

13.296	26.9	20.24	9.8	$2\frac{1}{2}$	300
13.307	25.7	20.01	10.1	2	300
13.30	26.3	20.13	(8.1 ... 12.3) M		

*h* 3838; Anon.

A.R.  $6^h 4^m 55^s$ ; Decl.  $-64^{\circ} 58'$

17.108	307.6	10.55	9.2	2	370
17.156	306.5	10.46	8.7	2	370
17.13	307.1	10.51	(11.0 ... 11.0) D?		

*h* 3841;  $-58^{\circ} 638$ ; 9.6

A.R.  $6^h 9^m 10^s$ ; Decl.  $-58^{\circ} 28'$

17.241	164.5	9.59	8.5	2	370
17.266	163.7	9.57	10.5	3	370
17.25	163.7	9.58	(10.5 ... 12.1) N		

$h$  3843;  $-60^{\circ} 563$ ; 7.9A.R.  $6^h 9^m 56^s$ ; Decl.  $-60^{\circ} 18'$ 

17.241	326.97	11.34	8.7	$2\frac{1}{2}$	370
17.266	326.7	11.44	10.6	3	370
17.25	326.7	11.39	(8.6 ... 10.2)		F

 $h$  3846 = Cape 23;  $-49^{\circ} 895$ ; 8.6A.R.  $6^h 11^m 10^s$ ; Decl.  $-49^{\circ} 4'$ 

12.902	60.0	4.97	3.7	2	300
12.918	59.5	4.89	3.4	3	300
12.957	60.7	5.00	3.2	3	300
12.93	60.1	4.95	(8.4 ... 9.2)		M

Delavan 2;  $-53^{\circ} 1045$ ; 8.6A.R.  $6^h 11^m 49^s$ ; Decl.  $-53^{\circ} 2'$ 

14.328	48.2	4.93	11.2	2	370
14.333	49.5	4.97	10.5	$2\frac{1}{2}$	370
14.336	47.6	4.67	11.8	$2\frac{1}{2}$	370
14.347	51.3	4.82	10.2	$2\frac{1}{2}$	370
14.34	49.2	4.85	(8.8 ... 9.7)		7

 $\Delta$  26;  $-65^{\circ} 585 + 6$ ; 7.3 + 8.5A.R.  $6^h 11^m 53^s$ ; Decl.  $-65^{\circ} 30'$ 

17.108	117.3	20.69	9.4	$2\frac{1}{2}$	370
17.156	117.5	20.85	8.9	2	370
17.13	117.4	20.77	(7.1 ... 8.6)		A

 $h$  3848;  $-47^{\circ} 753$ ; 8.8A.R.  $6^h 13^m 27^s$ ; Decl.  $-47^{\circ} 0'$ 

12.957	138.1	5.96	4.3	3	300
12.962	137.7	5.93	3.6	$2\frac{1}{2}$	300
12.987	138.1	5.88	3.7	3	300
12.97	138.0	5.92	(9.3 ... 9.4)		A

 $\Delta$  27;  $-59^{\circ} 619 + 18$ ; 7.4 + 8.0A.R.  $6^h 14^m 34^s$ ; Decl.  $-59^{\circ} 9'$ 

17.266	227.6	44.80	10.3	$2\frac{1}{2}$	370
17.271	227.6	44.76	9.4	2	370
17.27	227.6	44.78	(7.2 ... 8.5)		R

 $h$  3851;  $-61^{\circ} 620$ ; 8.8A.R.  $6^h 16^m 2^s$ ; Decl.  $-61^{\circ} 35'$ 

17.241	79.4	15.94	8.8	2	370
17.266	78.8	15.89	10.7	$2\frac{1}{2}$	370
17.25	79.1	15.91	(9.3 ... 11.7)		22

 $h$  3852 = I 281;  $-44^{\circ} 858$ ; 8.2A.R.  $6^h 17^m 6^s$ ; Decl.  $-44^{\circ} 44'$ 

12.858	8.1	6.49	3.2	4	300
12.872	8.1	6.45	3.9	3	300
12.899	7.8	6.62	3.6	3	300
12.88	8.0	6.52	(8.5 ... 10.0)		C

 $h$  3854;  $-54^{\circ} 1020$ ; 9.3A.R.  $6^h 17^m 54^s$ ; Decl.  $-54^{\circ} 27'$ 

13.296	127.1	11.17	10.1	$2\frac{1}{2}$	300
13.302	128.1	11.27	10.0	2	300
13.30	127.6	11.22	(9.0 ... 10.8)		N

 $h$  3853;  $-42^{\circ} 906$ ; 9.0A.R.  $6^h 18^m 20^s$ ; Decl.  $-42^{\circ} 38'$ 

13.208	67.6	14.62	9.1	2	300
13.214	68.2	14.14	9.0	2	300
13.217	67.3	14.57	9.5	2	300
13.244	69.2	14.40	10.3	3	300
13.22	68.1	14.43	(9.6 ... 10.3)		N

 $h$  3856;  $-45^{\circ} 842$ ; 7.8A.R.  $6^h 19^m 21^s$ ; Decl.  $-45^{\circ} 34'$ 

13.200	4.0	34.40	9.1	2	300
13.208	3.5	34.55	8.8	2	300
13.20	3.8	34.47	(6.8 ... 9.6)		

 $h$  3861;  $-58^{\circ} 690$ ; 8.6A.R.  $6^h 21^m 38^s$ ; Decl.  $-58^{\circ} 7'$ 

12.973	72.2	2.13	4.6	3	300
12.976	70.0	2.25	4.7	2	300
12.981	68.5	2.21	4.2	$2\frac{1}{2}$	300
12.98	70.2	2.20	(9.1 ... 9.5)		M

 $h$  3867;  $-48^{\circ} 863$ ; 9.6A.R.  $6^h 25^m 32^s$ ; Decl.  $-48^{\circ} 27'$ 

13.247	276.8	22.51	9.1	3	300
13.310	277.6	22.64	10.5	2	300
13.28	277.2	22.57	(9.3 ... 10.6)		N

 $h$  3873;  $-57^{\circ} 1011$ ; 8.4A.R.  $6^h 29^m 19^s$ ; Decl.  $-57^{\circ} 31'$ 

12.973	294.6	18.94	4.8	$2\frac{1}{2}$	300
12.976	294.4	18.47	4.9	2	300
12.981	294.4	18.87	4.7	$2\frac{1}{2}$	300
12.98	294.5	18.76	(8.5 ... 10.2)		N

 $h$  3874;  $\mu$  Pictoris; 5.4A.R.  $6^h 30^m 6^s$ ; Decl.  $-58^{\circ} 40'$ 

12.987	231.8	2.67	4.2	3	300
12.992	224.4	2.69	4.4	2	300
12.995	224.9	2.73	4.1	$2\frac{1}{2}$	300
13.020	230.7	2.77	4.5	2	300
13.00	228.0	2.72	(6.4 ... 11.1)		20

*h* 3879;  $-70^{\circ} 529$ ; 9.6:

A.R. 6<sup>h</sup> 31<sup>m</sup> 25<sup>s</sup>; Decl.  $-70^{\circ} 32'$

16.989	257.6	12.95	4.9	3	370
17.077	256.9	12.83	9.5	2	370
17.03	257.3	12.89	(10.2 ... 10.4)		A

*h* 3880;  $-66^{\circ} 567$ ; 9.4

A.R. 6<sup>h</sup> 32<sup>m</sup> 33<sup>s</sup>; Decl.  $-66^{\circ} 10'$

17.108	81.8	5.07	9.6	2½	370
17.156	81.7	5.06	9.0	2½	370
17.203	81.5	4.90	10.6	2	370
17.16	81.7	5.01	(10.3 ... 10.4)		M

*h* 3882;  $-44^{\circ} 1018$ ; 7.6:

A.R. 6<sup>h</sup> 35<sup>m</sup> 5<sup>s</sup>; Decl.  $-44^{\circ} 57'$

12.855	329.9	18.20	4.5	—	300
12.872	330.2	18.13	4.4	2½	300
12.86	330.0	18.16	(8.0 ... 9.7)		33

*h* 3884;  $-55^{\circ} 1028$ ; 7.2

A.R. 6<sup>h</sup> 35<sup>m</sup> 10<sup>s</sup>; Decl.  $-55^{\circ} 14'$

13.296	282.0	26.33	10.4	2	300
13.302	281.5	25.40	10.2	2	300
13.307	282.2	25.60	10.4	2	300
13.310	281.7	25.78	11.2	2	300
13.30	281.8	25.78	(7.4 ... 10.6)		N

*h* 3883;  $-44^{\circ} 1021$ ; 9.0

A.R. 6<sup>h</sup> 35<sup>m</sup> 17<sup>s</sup>; Decl.  $-44^{\circ} 56'$

13.214	75.6	7.10	9.4	2	300
13.217	75.1	7.15	9.7	2	300
13.244	75.3	7.33	10.7	3	300
13.22	75.3	7.19	(9.8 ... 10.7)		A

*h* 3886;  $-62^{\circ} 692 + 90$ ; 9.2 + 9.8

A.R. 6<sup>h</sup> 38<sup>m</sup> 11<sup>s</sup>; Decl.  $-62^{\circ} 41'$

17.108	347.3	13.37	9.8	2	370
17.156	347.4	13.63	9.4	3	370
17.13	347.4	13.50	(9.3 ... 11.7)		

AC

17.108	224.0	32.37	9.9	2	370
17.156	223.9	32.41	9.3	3	370
17.13	223.9	32.39	(9.3 ... 10.6)		34

*h* 3890;  $-72^{\circ} 513$ ; 9.1

A.R. 6<sup>h</sup> 38<sup>m</sup> 35<sup>s</sup>; Decl.  $-72^{\circ} 40'$

16.989	33.2	12.88	5.0	3	370
17.077	32.3	12.76	9.7	2	370
17.03	32.8	12.82	(9.0 ... 12.0)		N

*h* 3887; Véase la nota. See note 35

*h* 3889;  $-50^{\circ} 1042 + 1$ ; 7.0 + 8.6

A.R. 6<sup>h</sup> 39<sup>m</sup> 43<sup>s</sup>; Decl.  $-50^{\circ} 20'$

16.886	266.8	42.20	4.7	2	370
17.075	266.1	42.49	9.2	2½	370
17.094	266.3	42.20	8.6	2½	370
17.02	266.4	42.30	(7.4 ... 9.0)		F

$\Delta$  34;  $-54^{\circ} 1097 + 6$ ; 6.7 + 7.1

A.R. 6<sup>h</sup> 41<sup>m</sup> 40<sup>s</sup>; Decl.  $-54^{\circ} 34'$

13.302	190.9	130.11	10.4	2	300
13.307	191.0	130.09	10.7	2	300
13.30	190.9	130.10	(6.6 ... 6.7)		36

*h* 3894;  $-65^{\circ} 648$ ; 8.2

A.R. 6<sup>h</sup> 42<sup>m</sup> 3<sup>s</sup>; Decl.  $-65^{\circ} 37'$

17.156	217.3	27.24	9.5	2½	370
17.241	217.2	27.34	9.0	2	370
17.20	217.3	27.29	(8.5 ... 10.5)		21

I 181;  $-44^{\circ} 1113$ ; 8.2

A.R. 6<sup>h</sup> 46<sup>m</sup> 11<sup>s</sup>; Decl.  $-44^{\circ} 54'$

13.310	246.7	0.86	10.0	2½	666
13.312	244.1	1.05	10.3	2	666
13.315	251.2	0.88	9.8	2	666
13.323	250.5	0.90	9.7	2½	666
13.31	244.1	0.92	(8.8 ... 9.5)		F

I 159;  $-45^{\circ} 1069$ ; 7.8

A.R. 6<sup>h</sup> 46<sup>m</sup> 19<sup>s</sup>; Decl.  $-45^{\circ} 18'$

13.217	327.2	6.71	10.0	2	300
13.252	322.4	6.69	11.0	2½	300
13.310	323.2	6.66	9.8	3	300
13.26	324.3	6.69	(6.9 ... 11.1)		M

*h* 3897;  $-43^{\circ} 1057$ ; 8.5

A.R. 6<sup>h</sup> 46<sup>m</sup> 53<sup>s</sup>; Decl.  $-43^{\circ} 32'$

13.310	68.3	18.96	9.6	3	300
13.312	69.5	19.09	10.0	2½	300
13.31	68.9	19.02	(9.1 ... 13.2)		N

*h* 3898;  $-56^{\circ} 1180 + 1$ ; 8.6 + 9.0

A.R. 6<sup>h</sup> 48<sup>m</sup> 39<sup>s</sup>; Decl.  $-56^{\circ} 5'$

12.951	129.7	17.00	3.3	2	300
12.973	129.9	16.73	5.7	3	300
12.976	130.0	17.12	5.2	2½	300
12.97	129.9	16.95	(8.3 ... 8.3)		F

$h$  3904;  $-74^\circ 412$ ; 9.4A.R. 6<sup>h</sup> 49<sup>m</sup> 9<sup>s</sup>; Decl.  $-74^\circ 6'$ 

16.989	105.1	8.70	5.3	3	370
16.992	106.1	8.72	5.2	2½	370
17.077	104.3	8.57	9.9	2	370
17.02	105.2	8.66	(9.8 ... 12.1)		N

Gilliss 50;  $-56^\circ 1186 + 5$ ; 8.5 + 8.6A.R. 6<sup>h</sup> 49<sup>m</sup> 54<sup>s</sup>; Decl.  $-56^\circ 21'$ 

12.951	212.1	32.19	3.2	2½	300
12.973	212.5	32.05	5.2	3	300
12.96	212.3	32.12	(8.4 ... 8.8)		37

 $h$  3910;  $-65^\circ 670$ ; 9.0A.R. 6<sup>h</sup> 53<sup>m</sup> 22<sup>s</sup>; Decl.  $-65^\circ 45'$ 

17.156	266.4	29.48	9.7	2	370
17.241	266.2	29.51	9.2	2	370
17.20	266.3	29.50	(9.0 ... 11.8)		N

 $h$  3906;  $-55^\circ 1102 + 1$ ; 9.1 + 9.4A.R. 6<sup>h</sup> 53<sup>m</sup> 31<sup>s</sup>; Decl.  $-55^\circ 26'$ 

13.217	223.6	19.85	10.7	2½	300
13.296	223.9	19.43	10.7	2	300
13.307	223.5	19.48	11.3	2	300
13.310	223.1	19.58	11.4	2	300
13.28	223.5	19.58	(9.2 ... 9.6)		F

 $h$  3909;  $-47^\circ 1040$ ; 8.6A.R. 6<sup>h</sup> 54<sup>m</sup> 34<sup>s</sup>; Decl.  $-47^\circ 15'$ 

12.897	272.1	11.37	4.1	2	300
12.902	271.8	[11.81]	4.7	1	300
12.918	272.7	11.19	4.2	3	300
12.91	272.2	11.28	(9.1 ... 10.1)		20

 $h$  3915;  $-65^\circ 673$ ; 8.2A.R. 6<sup>h</sup> 55<sup>m</sup> 12<sup>s</sup>; Decl.  $-65^\circ 47'$ 

17.156	265.4	19.78	9.8	2	370
17.241	266.3	19.72	9.3	2	370
17.20	265.9	19.75	(8.7 ... 12.8)		N

 $h$  3912;  $-50^\circ 1107$ ; 10.0A.R. 6<sup>h</sup> 55<sup>m</sup> 38<sup>s</sup>; Decl.  $-50^\circ 31'$ 

16.886	46.0	8.29	5.0	2½	370
17.075	45.6	8.05	9.4	2½	370
17.094	46.2	8.30	8.9	2	370
17.02	45.9	8.21	(10.7 ... 11.5)		N

 $h$  3927;  $-74^\circ 422 + 3$ ; 9.5 + 9.6A.R. 6<sup>h</sup> 57<sup>m</sup> 58<sup>s</sup>; Decl.  $-74^\circ 7'$ 

16.989	16.7	14.94	5.4	3	370
17.077	17.0	14.95	10.1	2	370
17.03	16.8	14.94	(9.5 ... 9.6)		M?

 $h$  3921;  $-58^\circ 816$ ; 7.9A.R. 6<sup>h</sup> 58<sup>m</sup> 32<sup>s</sup>; Decl.  $-58^\circ 13'$ 

12.973	272.5	6.02	6.0	3	300
12.984	271.3	6.35	4.1	2½	300
12.987	272.0	6.15	4.5	3	300
12.98	271.9	6.17	(8.3 ... 11.5)		N

 $h$  3922;  $-60^\circ 742$ ; 7.6A.R. 6<sup>h</sup> 58<sup>m</sup> 40<sup>s</sup>; Decl.  $-60^\circ 41'$ 

17.241	237.6	17.08	10.3	2	370
17.266	237.1	17.01	11.1	3	370
17.25	237.3	17.04	(8.2 ... 12.1)		N

 $h$  3920;  $-45^\circ 1031$ ; 8.0A.R. 6<sup>h</sup> 58<sup>m</sup> 51<sup>s</sup>; Decl.  $-48^\circ 49'$ 

12.897	108.9	5.14	4.3	2	300
12.902	110.6	5.19	4.4	1½	300
12.918	110.8	5.22	4.4	3	300
12.91	110.1	5.18	(8.7 ... 8.8)		M

 $h$  3924;  $-60^\circ 744 + 2$ ; 8.9 + 9.4A.R. 6<sup>h</sup> 58<sup>m</sup> 54<sup>s</sup>; Decl.  $-60^\circ 41'$ 

17.241	356.7	16.23	10.4	2	370
17.266	357.2	15.91	11.2	3	370
17.271	357.1	15.99	9.5	2½	370
17.26	357.0	16.04	(9.7 ... 11.4)		F

 $h$  3929;  $-71^\circ 506$ ; 7.8A.R. 6<sup>h</sup> 58<sup>m</sup> 56<sup>s</sup>; Decl.  $-71^\circ 52'$ 

16.989	237.5	9.30	5.5	3	370
16.992	237.7	9.25	5.3	2½	370
17.077	237.2	9.36	10.2	2	370
17.02	237.5	9.30	(8.4 ... 10.9)		F?

 $h$  3925;  $-46^\circ 1188$ ; 9.4A.R. 6<sup>h</sup> 59<sup>m</sup> 42<sup>s</sup>; Decl.  $-46^\circ 43'$ 

13.244	110.4	4.48	11.9	3	300
13.310	106.1	4.22	10.7	2	300
13.885	107.6	4.09	4.2	3	300
14.328	107.5	4.39	11.5	2½	370
13.69	107.9	4.30	(10.6 ... 12.2)		N



$\Delta 38; -43^\circ 1186; 7.2:$

A.R.  $7^h 0^m 8^s$ ; Decl.  $-43^\circ 26^s$

13.209	121.9	20.63	10.3	2	300
13.217	122.8	20.65	10.2	2	300
13.21	122.3	20.64	(6.0 ... 7.2)		F

$h 3936; -73^\circ 426; 9.6$

A.R.  $7^h 4^m 29^s$ ; Decl.  $-73^\circ 33'$

16.990	266.6	7.45	5.6	3	370
16.992	267.4	7.57	5.5	$2\frac{1}{2}$	370
17.118	266.3	7.55	10.2	2	370
17.03	266.8	7.52	(11.2 ... 11.6)		N

$h 3935; -49^\circ 1144; 8.4$

A.R.  $7^h 6^m 3^s$ ; Decl.  $-49^\circ 46'$

12.897	99.9	29.57	4.6	$1\frac{1}{2}$	300
12.918	99.4	29.49	4.6	3	300
12.91	99.6	29.53	(8.5 ... 9.6)		?

$\Delta 40; -56^\circ 1261 + 2; 8.2 + 8.3$

A.R.  $7^h 6^m 50^s$ ; Decl.  $-56^\circ 9'$

12.951	140.5	37.65	3.8	$2\frac{1}{2}$	300
12.973	140.7	37.41	6.2	3	300
12.96	140.6	37.53	(8.2 ... 8.5)		F

$h 3937; -60^\circ 776; 8.6$

A.R.  $7^h 6^m 56^s$ ; Decl.  $-60^\circ 29'$

17.241	31.1	5.71	10.6	2	370
17.266	31.1	5.64	11.3	3	370
17.271	31.8	5.67	9.6	$2\frac{1}{2}$	370
17.26	31.3	5.67	(9.5 ... 9.6)		20

$h 3941; -60^\circ 782; 7.7$

A.R.  $7^h 7^m 41^s$ ; Decl.  $-60^\circ 11'$

17.241	298.0	0.86	10.7	2	650
17.266	298.7	0.85	11.4	3	650
17.271	298.6	0.90	9.8	3	650
17.26	298.4	0.87	(7.9 ... 8.4)		F

$h 3944; -62^\circ 782; 8.9$

A.R.  $7^h 8^m 58^s$ ; Decl.  $-62^\circ 49'$

17.241	279.1	15.49	10.0	2	370
17.266	277.7	15.35	11.0	3	370
17.271	277.9	15.40	10.1	3	370
17.26	278.2	15.41	(9.2 ... 11.6)		M

AC; C = 11.0

17.241	276.0	56.11	10.0	2	370
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$h 3943; L^3 Puppis; 6.9 + 10.2$

A.R.  $7^h 9^m 44^s$ ; Decl.  $-44^\circ 26'$

12.992	213.5	62.00	4.8	$2\frac{1}{2}$	300
13.020	213.9	62.08	4.8	2	300
13.01	213.7	62.04	(var. ... 9.5)		N

$\Delta 42; \gamma Volantis; 5.2$

A.R.  $7^h 9^m 46^s$ ; Decl.  $-70^\circ 18'$

16.990	299.9	13.48	5.7	3	370
17.077	299.4	13.50	10.5	2	370
17.03	299.7	13.49	(4.5 ... 6.4)		F

HdA.;  $-62^\circ 789; 6.7$

A.R.  $7^h 10^m 51^s$ ; Decl.  $-62^\circ 59'$

17.271	149.3	0.45	10.0	$2\frac{1}{2}$	650
17.274	149.5	0.48	9.6	2	650
17.27	149.4	0.46	(6.7 ... 7.6)		

$h 3947; -46^\circ 1340; 8.1$

A.R.  $7^h 12^m 57^s$ ; Decl.  $-46^\circ 1'$

13.025	270.2	7.96	5.0	3	300
13.044	270.2	8.03	5.0	3	300
13.050	271.0	7.89	4.7	3	300
13.04	270.5	7.96	(8.7 ... 9.5)		F

$h 3952; -53^\circ 1302; 7.8$

A.R.  $7^h 13^m 23^s$ ; Decl.  $-53^\circ 49'$

16.886	277.2	16.03	5.5	2	370
17.094	277.1	16.40	9.3	2	370
17.118	277.1	16.56	9.8	2	370
17.03	277.1	16.33	(7.5 ... 11.9)		M

$h 3951; -50^\circ 1203; 10.2$

A.R.  $7^h 13^m 30^s$ ; Decl.  $-50^\circ 46'$

16.886	76.3	8.88	5.3	$2\frac{1}{2}$	370
17.075	76.3	8.82	9.5	$2\frac{1}{2}$	370
17.094	75.9	8.70	9.1	2	370
17.02	76.2	8.80	(9.9 ... 11.0)		R

$h 3953; -73^\circ 434; 9.4$

A.R.  $7^h 13^m 46^s$ ; Decl.  $-73^\circ 43'$

16.990	326.1	16.27	5.9	3	370
17.118	325.4	16.52	10.3	2	370
17.121	324.8	16.05	9.9	2	370
17.08	325.4	16.28	(9.7 ... 12.2)		N

I 1103;  $-65^{\circ} 726$ ; 8.9A.R.  $7^{\text{h}} 15^{\text{m}} 18^{\text{s}}$ ; Decl.  $-65^{\circ} 58'$ 

17.108	111.08	1.11	10.8	2	370
17.280	113.8	1.22	10.5	3	650
17.19	112.8	1.17	(9.1 ... 10.5)		

AC =  $h 3955$ 

17.108	32.7	28.25	10.6	2	370
17.280	32.7	28.31	10.4	$2\frac{1}{2}$	370
17.19	32.7	28.28	(9.1 ... 9.4)		F

Sellors 23;  $-43^{\circ} 1376$ ; 8.3A.R.  $7^{\text{h}} 16^{\text{m}} 59^{\text{s}}$ ; Decl.  $-43^{\circ} 35'$ 

12.899	159.1	2.57	5.1	3	300
12.916	158.7	2.53	5.1	3	300
12.91	158.9	2.55	(9.0 ... 9.8)		F

Rii 6;  $-52^{\circ} 1153$ ; 6.7A.R.  $7^{\text{h}} 17^{\text{m}} 20^{\text{s}}$ ; Decl.  $-52^{\circ} 5'$ 

16.886	20.5	9.81	5.7	2	370
17.075	21.3	9.58	9.6	3	370
17.094	20.8	9.70	9.6	2	370
17.02	20.9	9.70	(6.9 ... 7.6)		M

 $h 3956 = h 3960$ ;  $-48^{\circ} 1137$ ; 7.6A.R.  $7^{\text{h}} 17^{\text{m}} 25^{\text{s}}$ ; Decl.  $-48^{\circ} 17'$ 

12.918	165.4	7.38	4.8	$2\frac{1}{2}$	300
12.921	166.5	7.39	4.6	3	300
12.957	165.0	7.23	4.6	3	300
12.93	165.6	7.33	(8.6 ... 9.3)		38

 $h 3958 = \text{Rus } 74$ ;  $-51^{\circ} 1158 + 6$ ;  $7.2 + 8.8$ A.R.  $7^{\text{h}} 17^{\text{m}} 37^{\text{s}}$ ; Decl.  $-51^{\circ} 58'$ 

16.886	281.1	30.39	5.8	2	370
17.075	280.6	30.31	9.8	3	370
16.98	280.8	30.35	(7.8 ... 9.0)		M

 $\Delta 45$ ;  $-48^{\circ} 1140 + 1$ ;  $7.2 + 7.8$ A.R.  $7^{\text{h}} 17^{\text{m}} 55^{\text{s}}$ ; Decl.  $-48^{\circ} 17'$ 

12.918	157.2	22.88	5.0	$2\frac{1}{2}$	300
12.921	157.0	22.79	4.8	3	300
12.92	157.1	22.83	(7.6 ... 8.8)		38

 $h 3961$ ;  $-57^{\circ} 1195$ ; 8.8A.R.  $7^{\text{h}} 18^{\text{m}} 1^{\text{s}}$ ; Decl.  $-57^{\circ} 27'$ 

13.296	255.9	14.02	10.9	2	300
13.302	255.4	14.08	10.8	$2\frac{1}{2}$	300
13.30	255.6	14.05	(9.4 ... 10.5)		N

 $h 3962$ ;  $-56^{\circ} 1315$ ; 7.5A.R.  $7^{\text{h}} 18^{\text{m}} 30^{\text{s}}$ ; Decl.  $-56^{\circ} 33'$ 

12.973	104.6	8.87	6.6	3	300
12.984	106.0	8.70	4.4	3	300
12.987	105.6	8.55	4.8	3	300
12.98	105.4	8.71	(8.3 ... 9.1)		F

Rus 75;  $-55^{\circ} 1222 + 1$ ;  $9.2 + 9.7$ A.R.  $7^{\text{h}} 18^{\text{m}} 56^{\text{s}}$ ; Decl.  $-55^{\circ} 6'$ 

13.217	269.3	5.32	11.3	$1\frac{1}{2}$	300
13.302	271.8	4.73	11.7	2	300
13.307	272.0	5.14	11.8	2	300
13.312	272.9	4.98	11.0	3	666
13.28	271.5	5.04	(9.6 ... 10.2)		F

AC

13.217	262.0	30.83	11.0	$1\frac{1}{2}$	300
13.302	261.4	30.92	11.5	2	300
13.307	262.1	30.87	11.6	2	300
13.310	261.7	30.96	11.6	2	300
13.28	261.8	30.90	(9.6 ... 10.0)		39

 $h 3963$ ;  $-43^{\circ} 1414$ ; 9.0A.R.  $7^{\text{h}} 19^{\text{m}} 6^{\text{s}}$ ; Decl.  $-43^{\circ} 32'$ 

12.957	259.3	4.80	5.3	3	300
12.962	259.8	4.73	4.3	3	300
12.992	263.0	4.70	5.1	2	300
12.97	260.7	4.74	(9.2 ... 10.0)		F

 $h 3967$ ;  $-55^{\circ} 1227$ ; 7.8A.R.  $7^{\text{h}} 20^{\text{m}} 21^{\text{s}}$ ; Decl.  $-55^{\circ} 20'$ 

13.296	139.1	—	11.4	2	300
13.307	138.5	46.61	12.0	2	300
13.310	138.7	46.32	11.7	2	300
13.30	138.8	46.46	(7.6 ... 13.0)		N

 $h 3971$ ;  $-57^{\circ} 1220$ ; 9.2A.R.  $7^{\text{h}} 22^{\text{m}} 16^{\text{s}}$ ; Decl.  $-57^{\circ} 41'$ 

13.296	188.4	16.39	11.2	$2\frac{1}{2}$	300
13.302	188.5	16.31	11.2	2	300
13.30	188.4	16.35	(9.0 ... 10.5)		N

 $h 3970$ ;  $-45^{\circ} 1471$ ; 9.8A.R.  $7^{\text{h}} 22^{\text{m}} 22^{\text{s}}$ ; Decl.  $-45^{\circ} 22'$ 

12.962	277.7	6.28	4.7	3	300
12.995	278.0	6.02	4.6	3	300
13.020	276.6	6.13	5.2	$2\frac{1}{2}$	300
12.99	277.4	6.14	(9.2 ... 10.0)		N

*h* 3972;  $-62^{\circ} 828 + 9$ ;  $9.0 + 9.4$

A.R.  $7^{\text{h}} 23^{\text{m}} 4^{\text{s}}$ ; Decl.  $-62^{\circ} 17'$

17.280	47.0	20.66	10.7	$2\frac{1}{2}$	370
17.296	46.9	20.55	9.6	3	370
17.29	46.9	20.60	(9.6 ... 10.0)		F

AC

17.280	90.3	—	10.8	$2\frac{1}{2}$	370
17.296	89.6	—	9.8	3	370
17.29	89.9	18.28	(9.6 ... 13.2)		40

Dawson 4;  $-45^{\circ} 1484$ ;  $9.4$

A.R.  $7^{\text{h}} 23^{\text{m}} 33^{\text{s}}$ ; Decl.  $-45^{\circ} 28'$

12.995	130.4	3.13	5.1	3	300
13.020	135.3	2.94	5.4	3	300
13.022	132.4	3.18	4.3	3	300
13.01	132.7	3.08	(9.5 ... 9.5)		

$\Delta$  51;  $\tau$  Argûs;  $6.5$

A.R.  $7^{\text{h}} 25^{\text{m}} 16^{\text{s}}$ ; Decl.  $-43^{\circ} 3'$

13.022	73.1	22.86	4.6	3	300
13.039	73.7	22.61	4.7	3	300
13.066	73.5	22.74	4.6	3	300
13.04	73.4	22.74	(3.5 ... 8.7)		F

*h* 3974;  $-55^{\circ} 1247$ ;  $8.0$

A.R.  $7^{\text{h}} 26^{\text{m}} 50^{\text{s}}$ ; Decl.  $-55^{\circ} 3'$

12.875	239.9	4.83	4.7	2	300
12.932	240.8	5.09	5.0	3	300
12.935	238.7	5.12	4.7	2	300
12.938	239.9	5.05	5.1	$2\frac{1}{2}$	300
12.92	239.8	5.02	(8.4 ... 9.4)		F?

*h* 3977;  $-61^{\circ} 827$ ;  $9.1$

A.R.  $7^{\text{h}} 27^{\text{m}} 9^{\text{s}}$ ; Decl.  $-61^{\circ} 20'$

17.241	70.3	19.41	11.3	2	370
17.274	70.6	19.48	9.7	2	370
17.26	70.5	19.45	(8.9 ... 13.3)		N

*h* 3981;  $48^{\circ} 1206$ ;  $7.4$ :

A.R.  $7^{\text{h}} 29^{\text{m}} 19^{\text{s}}$ ; Decl.  $-48^{\circ} 57'$

12.918	327.8	15.60	5.6	$2\frac{1}{2}$	300
12.921	328.4	15.39	5.0	3	300
13.050	328.9	15.43	5.0	3	300
12.96	328.4	15.47	(8.7 ... 9.3)		F

AC

13.050	87.8	26.33	4.9	3	300
13.063	88.8	[26.82]	4.6	$2\frac{1}{2}$	300
13.066	88.1	26.39	4.8	3	300
13.06	88.2	26.36	(8.7 ... 10.7)		N

*h* 3984;  $-54^{\circ} 1305 + 3$ ;  $8.0 + 8.4$

A.R.  $7^{\text{h}} 30^{\text{m}} 15^{\text{s}}$ ; Decl.  $-54^{\circ} 54'$

13.296	298.04	14.38	11.9	2	300
13.310	296.6	14.26	12.2	$1\frac{1}{2}$	300
13.300	297.5	14.32	(7.8 ... 12.5)		R

AC

13.296	251.8	65.04	11.7	2	300
13.310	252.0	65.24	12.0	2	300
13.30	251.9	65.14	(7.8 ... 8.4)		R

Aguilar 3;  $-57^{\circ} 1261$ ;  $8.8$

A.R.  $7^{\text{h}} 30^{\text{m}} 49^{\text{s}}$ ; Decl.  $-57^{\circ} 40'$

17.381	158.8	4.47	10.6	$2\frac{1}{2}$	370
17.406	157.5	4.52	12.0	2	370
17.409	158.4	4.31	12.5	$2\frac{1}{2}$	370
17.40	158.2	4.43	(9.0 ... 12.1)		7

*h* 3986;  $-50^{\circ} 1298 + 7$ ;  $8.6 + 9.0$

A.R.  $7^{\text{h}} 30^{\text{m}} 52^{\text{s}}$ ; Decl.  $-50^{\circ} 34'$

17.072	219.7	43.81	6.6	$2\frac{1}{2}$	370
17.075	219.5	43.92	10.0	3	370
17.07	219.6	43.87	(8.0 ... 9.2)		F

Anon.;  $-57^{\circ} 1263$ ;  $8.9$

A.R.  $7^{\text{h}} 31^{\text{m}} 20^{\text{s}}$ ; Decl.  $-57^{\circ} 29'$

17.381	193.1	13.25	10.7	2	370
17.406	192.1	13.44	12.2	2	370
17.39	192.6	13.34	(9.4 ... 11.0)		7

*h* 3989;  $-61^{\circ} 843$ ;  $9.7$ :

A.R.  $7^{\text{h}} 32^{\text{m}} 6^{\text{s}}$ ; Decl.  $-61^{\circ} 1'$

17.241	228.2	17.91	11.6	2	370
17.274	228.6	17.96	9.9	2	370
17.25	228.4	17.94	(9.8 ... 10.7)		A?

*h* 3988;  $-48^{\circ} 1225$ ;  $8.8$

A.R.  $7^{\text{h}} 32^{\text{m}} 42^{\text{s}}$ ; Decl.  $-48^{\circ} 34'$

13.025	299.0	16.78	5.6	3	300
13.042	299.1	16.64	4.6	3	300
13.03	299.0	16.71	(8.8 ... 9.8)		F

*h* 3990;  $-47^{\circ} 1470 + 69$ ;  $8.2 + 8.5$

A.R.  $7^{\text{h}} 34^{\text{m}} 50^{\text{s}}$ ; Decl.  $-47^{\circ} 26'$

13.042	342.5	37.31	4.8	3	300
13.044	342.4	37.17	5.2	3	300
13.04	342.4	37.24	(8.5 ... 9.1)		F

$h$  3992;  $-43^{\circ} 1676$ ; 8.1:A.R.  $7^h 35^m 26^s$ ; Decl.  $-43^{\circ} 41'$ 

13.066	121.2	15.68	5.0	3	300
13.072	120.6	15.82	5.6	3	300
13.07	120.9	15.75	(9.0 ... 9.4)		N

 $h$  3994;  $-48^{\circ} 1243$ ; 6.9A.R.  $7^h 35^m 47^s$ ; Decl.  $-48^{\circ} 46'$ 

13.025	17.7	14.73	5.9	3	300
13.042	18.1	14.80	5.0	3	300
13.03	17.9	14.76	(8.1 ... 9.5)		D?

AC

13.025	215.7	22.73	6.1	$2\frac{1}{2}$	300
13.042	215.3	22.88	5.2	3	300
13.03	215.5	22.80	(8.1 ... 9.9)		D

 $h$  3993; C6D.  $-60^{\circ} 1821$ ;  $10\frac{3}{4}$ A.R.  $7^h 35^m 55^s$ ; Decl.  $-60^{\circ} 9'$ 

17.241	199.7	17.90	11.8	2	370
17.274	198.9	17.96	10.0	2	370
17.277	200.1	18.17	10.3	$3\frac{1}{2}$	370
17.26	199.6	18.01	(10.9 ... 11.2)		4I

 $h$  3997;  $-73^{\circ} 457$ ; 6.2A.R.  $7^h 37^m 54^s$ ; Decl.  $-73^{\circ} 60'$ 

16.990	296.7	1.90	6.1	3	475
16.992	296.3	2.14	5.7	$2\frac{1}{2}$	370
17.077	295.4	2.08	10.7	2	370
17.118	295.5	2.23	10.5	2	475
17.04	296.0	2.09	(7.5 ... 7.6)		P

 $h$  4000;  $-58^{\circ} 969$ ; 7.5A.R.  $7^h 40^m 4^s$ ; Decl.  $-58^{\circ} 22'$ 

17.266	242.9	1.57	11.7	2	370
17.274	240.0	1.60	10.2	2	370
17.277	243.0	1.63	10.4	$3\frac{1}{2}$	650
17.27	242.0	1.60	(7.3 ... 10.5)		M

 $h$  3998;  $-52^{\circ} 1259$ ; 9.0:A.R.  $7^h 40^m 15^s$ ; Decl.  $-52^{\circ} 13'$ 

17.072	181.2	9.19	6.8	3	370
17.075	180.9	9.15	10.3	3	370
17.094	181.2	9.21	9.8	2	370
17.08	181.1	9.18	(10.3 ... 11.1)		N

 $h$  3999;  $-54^{\circ} 1363$ ; 9.2A.R.  $7^h 40^m 24^s$ ; Decl.  $-54^{\circ} 7'$ 

12.973	270.5	4.51	7.0	3	300
12.984	272.8	4.73	4.8	$2\frac{1}{2}$	300
12.987	273.3	4.78	5.2	3	300
12.98	272.2	4.66	(9.7 ... 10.2)		N

 $\Delta$  55;  $-50^{\circ} 1356 + 7$ ;  $7.3 + 8.0$ A.R.  $7^h 40^m 51^s$ ; Decl.  $-50^{\circ} 10'$ 

17.072	132.7	51.86	6.7	$2\frac{1}{2}$	370
17.075	132.5	51.70	10.2	3	370
17.07	132.6	51.78	(7.3 ... 8.1)		F

 $h$  4002;  $-49^{\circ} 1346$ ; 7.6A.R.  $7^h 41^m 43^s$ ; Decl.  $-49^{\circ} 59'$ 

13.044	90.0	19.16	5.5	3	300
13.050	90.4	19.87	5.4	3	300
13.063	90.3	19.96	4.8	2	300
13.066	90.7	19.50	5.5	3	300
13.06	90.4	19.57	(8.1 ... 11.2)		N

 $h$  4004;  $-63^{\circ} 788$ ; 8.1A.R.  $7^h 42^m 11^s$ ; Decl.  $-63^{\circ} 6'$ 

17.280	333.2	13.22	11.0	$2\frac{1}{2}$	370
17.299	333.4	13.16	11.3	$2\frac{1}{2}$	370
17.29	333.3	13.19	(8.2 ... 12.5)		N

 $h$  4005;  $-56^{\circ} 1420$ ; 7.0A.R.  $7^h 43^m 0^s$ ; Decl.  $-56^{\circ} 25'$ 

13.315	217.3	35.86	10.1	2	300
13.323	217.9	35.60	10.1	3	300
13.32	217.6	35.73	(7.0 ... 9.6)		M

 $\Delta$  57;  $\zeta$  Volantis; 6.0A.R.  $7^h 43^m 20^s$ ; Decl.  $-72^{\circ} 18'$ 

16.990	116.8	16.74	6.3	3	370
17.118	114.7	16.76	10.7	2	370
17.121	115.7	16.63	10.7	2	370
17.08	115.7	16.71	(5.1 ... 9.7)		F

Cape 20;  $-44^{\circ} 1891$ ; 8.4A.R.  $7^h 44^m 3^s$ ; Decl.  $-44^{\circ} 14'$ 

13.030	86.8	3.04	5.0	$2\frac{1}{2}$	300
13.066	85.8	3.21	5.2	3	300
13.069	87.4	3.19	5.5	3	300
13.06	86.7	3.15	(8.8 ... 9.6)		F

C6.;  $-59^{\circ} 897 + 8$ ;  $8.4 + 8.5$ A.R.  $7^h 44^m 9^s$ ; Decl.  $-59^{\circ} 30'$ 

17.381	43.1	22.82	10.8	3	370
17.406	43.2	22.94	12.4	2	370
17.39	43.1	22.88	(8.6 ... 8.6)		

 $h$  4008;  $-53^{\circ} 1432$ ; 7.1A.R.  $7^h 44^m 20^s$ ; Decl.  $-53^{\circ} 1'$ 

17.072	230.0	20.81	7.0	3	370
17.094	229.7	20.73	10.0	2	370
17.08	229.9	20.77	(8.0 ... 12.7)		N

*h* 4006;  $-44^{\circ}$  1899; 9.0

A.R. 7<sup>h</sup> 44<sup>m</sup> 30<sup>s</sup>; Decl.  $-44^{\circ}$  57'

13.039	302.7	11.34	5.3	3	300
13.066	301.6	11.27	5.4	3	300
13.05	302.2	11.30	(8.6 ... 10.0)		42

Anon.;  $-58^{\circ}$  998; 8.3

A.R. 7<sup>h</sup> 45<sup>m</sup> 25<sup>s</sup>; Decl.  $-58^{\circ}$  13'

17.381	77.0	13.64	10.9	3	370
17.406	77.6	13.71	12.5	2	370
17.39	77.3	13.67	(8.6 ... 10.2)		7

Jacob 93; *P* Puppis; 4.3

A.R. 7<sup>h</sup> 45<sup>m</sup> 26<sup>s</sup>; Decl.  $-46^{\circ}$  4'

13.069	103.6	59.33	5.4	3	300
13.072	103.9	59.12	5.7	3	300
13.07	103.8	59.22	(4.2 ... 9.4)		F

*h* 4012;  $-59^{\circ}$  908; 6.4

A.R. 7<sup>h</sup> 47<sup>m</sup> 9<sup>s</sup>; Decl.  $-59^{\circ}$  58'

17.274	133.4	21.69	10.9	2	370
17.277	132.8	21.29	10.5	3	370
17.280	133.9	21.44	11.3	2½	370
17.28	133.4	21.47	(6.3 ... 12.7)		N

*h* 4014;  $-63^{\circ}$  815; 7.9

A.R. 7<sup>h</sup> 47<sup>m</sup> 14<sup>s</sup>; Decl.  $-63^{\circ}$  22'

17.277	154.7	11.17	11.7	3	370
17.280	154.2	11.12	11.2	2½	370
17.28	154.4	11.15	(7.6 ... 8.9)		F

*h* 4016;  $-51^{\circ}$  1312 + 13; 9.9 + 9.9

A.R. 7<sup>h</sup> 48<sup>m</sup> 28<sup>s</sup>; Decl.  $-51^{\circ}$  5'

17.072	169.6	16.84	7.1	3½	370
17.075	169.3	16.78	10.4	3	370
17.07	169.5	16.81	(10.4 ... 10.4)		F

*h* 4018;  $-59^{\circ}$  921; 7.3

A.R. 7<sup>h</sup> 50<sup>m</sup> 0<sup>s</sup>; Decl.  $-59^{\circ}$  17'

17.241	327.2	5.20	12.6	2	370
17.266	326.9	5.16	12.3	2½	370
17.274	326.8	5.17	11.1	2	370
17.26	327.0	5.18	(7.8 ... 10.2)		20

*h* 4017;  $-50^{\circ}$  1410 + 09; 8.5 + 9.0

A.R. 7<sup>h</sup> 50<sup>m</sup> 19<sup>s</sup>; Decl.  $-50^{\circ}$  35'

17.072	212.6	16.81	7.2	3½	370
17.075	212.8	16.79	10.5	3	370
17.07	212.7	16.80	(8.6 ... 9.2)		N

(*Segue Continued.*)

AC; C = 10.8

17.072	42.8	27.82	7.3	3½	370
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*h* 4023;  $-70^{\circ}$  694; 8.3

A.R. 7<sup>h</sup> 51<sup>m</sup> 23<sup>s</sup>; Decl.  $-70^{\circ}$  27'

14.350	220.4	2.19	10.6	2½	370
14.395	219.4	2.04	12.1	3	370
14.399	220.2	1.94	12.2	3	370
16.990	218.3	2.07	6.4	3	370
17.118	219.6	2.10	10.8	2	475
14.38	220.0	2.06			
17.05	218.9	2.08	(8.7 ... 9.1)		N

*h* 4021;  $-58^{\circ}$  1018; 7.8

A.R. 7<sup>h</sup> 51<sup>m</sup> 48<sup>s</sup>; Decl.  $-58^{\circ}$  14'

17.266	295.2	7.75	11.4	2½	370
17.315	296.9	7.29	12.2	2	370
17.321	295.1	7.51	11.7	2	370
17.30	295.7	7.52	(7.6 ... 13.5)		R

Hargrave;  $-48^{\circ}$  1373; 4.3

A.R. 7<sup>h</sup> 54 39<sup>s</sup>; Decl.  $-48^{\circ}$  54'

13.047	66.7	7.06	4.8	3	300
13.072	67.4	7.05	5.9	3	300
13.077	69.3	6.96	6.2	2½	300
13.07	67.8	7.02	(5.2 ... 10.2)		

AC = *h* 4025 AB

13.047	48.5	19.06	5.0	3	300
13.072	47.2	18.91	6.0	3	300
13.077	48.8	19.18	6.0	2½	300
13.07	48.2	19.05	(5.2 ... 12.2)		

AD = *h* 4025 AC

17.126	37.9	39.24	8.7	2	370
17.471	37.5	39.18	12.3	2	370
17.30	37.7	39.21	(5.2 ... 9.8)		

DE = λ 93

17.126	64.3	10.42	8.8	1½	370
17.471	61.1	10.09	12.4	2	370
17.30	62.7	10.25	(9.8 ... 13.0)		

*h* 4027;  $-60^{\circ}$  944; 7.6

A.R. 7<sup>h</sup> 54<sup>m</sup> 42<sup>s</sup>; Decl.  $-60^{\circ}$  29'

17.170	115.3	9.47	7.5	2	370
17.241	113.4	9.40	12.4	2	370
17.274	114.0	9.38	11.3	2	370
17.23	114.7	9.42	(8.6 ... 9.0)		F

*h* 4026;  $-44^{\circ} 2069$ ; 10.4A.R. 7<sup>h</sup> 55<sup>m</sup> 5<sup>s</sup>; Decl.  $-44^{\circ} 35'$ 

12.995	108.3	7.54	5.4	3	300
13.023	109.2	7.11	6.0	2	300
13.039	109.8	7.28	5.6	3	300
13.02	109.1	7.31	(10.3 ... 10.4)		N

*h* 4029;  $-63^{\circ} 849$ ; 9.1:A.R. 7<sup>h</sup> 55<sup>m</sup> 18<sup>s</sup>; Decl.  $-63^{\circ} 44'$ 

17.280	152.3	16.77	11.5	2	370
17.299	152.9	16.63	11.5	3	370
17.29	152.6	16.70	(9.4 ... 11.3)		N

*h* 4028;  $-49^{\circ} 1447$ ; 5.8A.R. 7<sup>h</sup> 55<sup>m</sup> 41<sup>s</sup>; Decl.  $-49^{\circ} 38'$ 

13.025	46.3	16.51	6.4	3	300
13.042	46.6	16.58	5.3	3	300
13.044	46.6	16.69	5.7	3	300
13.04	46.5	16.59	(7.1 ... 7.1)		F

*h* 4032;  $-46^{\circ} 1984$ ; 7.7A.R. 7<sup>h</sup> 55<sup>m</sup> 59<sup>s</sup>; Decl.  $-46^{\circ} 58'$ 

13.047	351.3	29.18	5.3	3	300
13.050	351.0	29.28	5.6	3	300
13.063	351.4	29.08	5.0	2	300
13.05	351.2	29.18	(7.8 ... 9.1)		43

*h* 4031;  $-60^{\circ} 988$ ; 6.7A.R. 7<sup>h</sup> 56<sup>m</sup> 18<sup>s</sup>; Decl.  $-60^{\circ} 31'$ 

17.170	357.3	5.66	7.7	2	370
17.241	356.8	5.40	12.5	2	370
17.274	357.0	5.56	11.4	2	370
17.23	357.0	5.54	(7.3 ... 8.7)		M

I 1104;  $-60^{\circ} 1005$ ; 7.8A.R. 7<sup>h</sup> 56<sup>m</sup> 44<sup>s</sup>; Decl.  $-60^{\circ} 18'$ 

17.315	243.2	8.67	11.3	2	370
17.321	242.7	8.61	12.2	2	370
17.32	242.9	8.64	(8.5 ... 8.6)		

*h* 4033;  $-47^{\circ} 1765$ ; 8.1A.R. 7<sup>h</sup> 57<sup>m</sup> 5<sup>s</sup>; Decl.  $-47^{\circ} 28'$ 

13.044	67.8	12.22	6.4	2	300
13.047	67.4	12.35	5.6	2½	300
13.050	67.0	12.34	5.7	3	300
13.05	67.4	12.30	(8.9 ... 9.5)		F

*h* 4036;  $-57^{\circ} 1368$ ; 9.0A.R. 7<sup>h</sup> 57<sup>m</sup> 27<sup>s</sup>; Decl.  $-57^{\circ} 26'$ 

13.315	83.9	9.90	10.4	2½	300
13.323	84.1	9.99	10.4	3	300
13.32	84.0	9.95	(10.0 ... 10.2)		44

*h* 4034;  $-42^{\circ} 1957$ ; 7.8A.R. 7<sup>h</sup> 57<sup>m</sup> 52<sup>s</sup>; Decl.  $-42^{\circ} 25'$ 

12.962	296.1	6.47	5.2	3	300
13.023	296.8	6.40	5.0	3	300
13.039	296.7	6.40	5.9	3	300
13.01	296.5	6.42	(8.8 ... 9.5)		F?

C6.;  $-60^{\circ} 1023$ ; 7.9A.R. 7<sup>h</sup> 57<sup>m</sup> 57<sup>s</sup>; Decl.  $-60^{\circ} 26'$ 

17.315	0.5	12.53	11.5	2	370
17.321	0.4	12.35	12.3	2	370
17.32	0.5	12.44	(8.5 ... 9.2)		7

 $\Delta$  60;  $-54^{\circ} 1470 + 1$ ; 6.4 + 7.8A.R. 7<sup>h</sup> 58<sup>m</sup> 21<sup>s</sup>; Decl.  $-54^{\circ} 10'$ 

12.973	161.2	40.66	7.3	2	300
12.987	161.2	40.52	5.4	3	300
17.280	161.7	40.30	10.0	3	370
14.41	161.4	40.49	(6.3 ... 8.2)		45

I 8;  $-44^{\circ} 2138$ ; 7.3A.R. 7<sup>h</sup> 58<sup>m</sup> 25<sup>s</sup>; Decl.  $-44^{\circ} 19'$ 

13.252	304.7	2.69	11.6	2	300
13.310	307.4	2.50	10.3	2½	300
13.312	306.8	2.50	10.7	3	666
13.29	306.3	2.56	(6.9 ... 9.3)		M

*h* 4044;  $-54^{\circ} 1482$ ; 8.9A.R. 7<sup>h</sup> 59<sup>m</sup> 30<sup>s</sup>; Decl.  $-54^{\circ} 41'$ 

12.987	218.6	28.81	5.7	3	300
13.148	219.0	28.83	6.4	2½	300
13.07	218.8	28.82	(8.9 ... 9.4)		N

AC

12.987	202.6	31.04	5.8	3	300
13.148	203.1	30.87	6.5	2½	300
13.07	202.8	30.96	(8.9 ... 9.8)		N

*h* 4043;  $-46^{\circ} 2059$ ; 8.7A.R. 7<sup>h</sup> 59<sup>m</sup> 48<sup>s</sup>; Decl.  $-46^{\circ} 13'$ 

13.047	216.7	19.09	6.1	2	300
13.050	216.3	19.06	6.0	3	300
13.05	216.5	19.07	(8.9 ... 9.1)		A



*h* 4045; —50° 1466; 8.3

A.R. 8<sup>h</sup> 0<sup>m</sup> 0<sup>s</sup>; Decl. —50° 60'

13.025	225.3	4.68	6.8	3	300
13.042	225.0	4.78	5.5	3	300
13.044	225.4	4.68	6.0	2½	300
13.04	225.2	4.71	(8.9 ... 9.8)		F

Jacob 94; —45° 2077 + 8; 8.3 + 8.5

A.R. 8<sup>h</sup> 1<sup>m</sup> 11<sup>s</sup>; Decl. —45° 4'

13.200	17.0	26.97	10.1	2	300
13.203	16.6	27.37	11.6	1½	300
13.209	16.0	27.20	10.6	2	300
13.20	16.5	27.18	(8.3 ... 8.4)		F

Δ 62; —62° 953 + 2; 6.8 + 8.5

A.R. 8<sup>h</sup> 2<sup>m</sup> 55<sup>s</sup>; Decl. —62° 29'

17.277	261.5	87.04	10.8	3	370
17.280	261.4	87.13	12.3	2	370
17.28	261.5	87.08	(5.9 ... 7.1)		M?

Δ 63; —42° 2140; 7.0

A.R. 8<sup>h</sup> 5<sup>m</sup> 34<sup>s</sup>; Decl. —42° 16'

12.962	81.0	5.83	5.6	3	300
13.023	79.8	5.85	6.7	2½	300
12.99	80.4	5.84	(7.1 ... 8.2)		F

Δ 65; γ Argús; 3.5

A.R. 8<sup>h</sup> 5<sup>m</sup> 40<sup>s</sup>; Decl. —46° 58'

13.050	219.7	41.25	6.1	3	300
13.063	220.1	41.36	5.2	2½	300
13.072	220.1	41.26	6.2	3	300
13.06	220.0	41.29	(3.0 ... 6.3)		46

*h* 4054; —61° 971; 9.1

A.R. 8<sup>h</sup> 6<sup>m</sup> 4<sup>s</sup>; Decl. —61° 59'

17.266	289.3	16.87	12.7	2	370
17.277	290.2	16.79	10.9	3	370
17.299	289.8	16.94	11.8	2½	370
17.28	289.8	16.87	(9.0 ... 11.1)		

BC

17.266	351.2	16.60	12.8	2	370
17.277	352.3	16.81	11.1	3	370
17.299	352.6	16.77	11.9	2	370
17.28	352.0	16.73	(11.1 ... 11.9)		N

*h* 4053; —60° 1068; 7.6

A.R. 8<sup>h</sup> 6<sup>m</sup> 4<sup>s</sup>; Decl. —60° 43'

17.266	97.4	11.63	12.5	2½	370
17.277	98.0	11.61	10.6	3	370
17.27	97.7	11.62	(7.2 ... 9.7)		N

(Sigue Continued.)

AC

17.266	318.2	19.36	12.5	2½	370
17.277	317.2	19.43	10.7	3	370
17.27	317.7	19.40	(7.2 ... 10.8)		N

*h* 4057; —42° 2186; 5.7

A.R. 8<sup>h</sup> 7<sup>m</sup> 14<sup>s</sup>; Decl. —42° 37'

13.200	298.4	25.33	10.4	2	300
13.203	297.7	25.18	11.8	1½	300
13.20	298.1	25.26	(5.5 ... 9.2)		D?

*h* 4071; —64° 832; 8.7

A.R. 8<sup>h</sup> 9<sup>m</sup> 40<sup>s</sup>; Decl. —64° 8'

17.280	205.5	7.57	12.5	2	370
17.430	206.0	7.68	12.4	2½	370
17.468	206.0	7.66	12.5	2	370
17.43	205.8	7.64	(9.2 ... 10.1)		F

*h* 4065; —53° 1567 + 9; 9.4 + 9.6

A.R. 8<sup>h</sup> 9<sup>m</sup> 50<sup>s</sup>; Decl. —53° 40'

17.066	44.6	10.80	6.4	3	370
17.075	44.5	10.86	10.7	3	370
17.07	44.5	10.83	(10.3 ... 10.5)		F

*h* 4066; —43° 2345; 8.6

A.R. 8<sup>h</sup> 10<sup>m</sup> 7<sup>s</sup>; Decl. —43° 19'

12.962	189.2	4.46	6.1	3	300
13.023	187.6	4.49	6.9	3	300
13.069	189.3	4.43	5.7	3	300
13.02	188.7	4.46	(9.0 ... 9.7)		47

*h* 4069; —45° 2285; 6.8

A.R. 8<sup>h</sup> 10<sup>m</sup> 23<sup>s</sup>; Decl. —45° 27'

13.069	252.0	32.87	5.8	3	300
13.077	251.4	33.08	6.7	3	300
13.200	251.4	33.00	10.7	2	300
13.12	251.6	32.98	(6.8 ... 8.6)		48

Aguilar 4; —58° 1080; 8.4

A.R. 8<sup>h</sup> 11<sup>m</sup> 11<sup>s</sup>; Decl. —58° 14'

17.381	171.9	6.81	11.1	3	370
17.406	170.8	6.87	12.7	2	370
17.409	171.9	6.79	12.7	2½	370
17.40	171.5	6.82	(8.5 ... 12.1)		7

Aguilar 5; —58° 1082; 8.4

A.R. 8<sup>h</sup> 11<sup>m</sup> 30<sup>s</sup>; Decl. —58° 10'

17.381	349.1	5.03	11.3	3	370
17.406	350.4	5.12	12.8	2	370
17.409	349.6	5.06	12.9	2½	370
17.40	349.7	5.07	(8.6 ... 11.6)		7

Rü 8 = Rus 82; *C* Carinae; 6.0A.R. 8<sup>h</sup> 13<sup>m</sup> 22<sup>s</sup>; Decl. -62° 32'

17.277	63.1	3.94	12.0	3	370
17.299	64.8	3.71	12.0	2½	370
17.430	65.3	3.97	12.0	2½	370
17.34	64.4	3.87	(5.7 ... 8.0)		

*h* 4075; -65° 897; 9.1A.R. 8<sup>h</sup> 13<sup>m</sup> 31<sup>s</sup>; Decl. -65° 53'

17.280	262.8	4.26	12.6	2	370
17.430	264.3	4.07	12.5	2	370
17.468	263.4	3.88	12.6	2	370
17.43	263.5	4.07	(9.7 ... 10.2)		F

*h* 4074; -49° 1589; 9.2A.R. 8<sup>h</sup> 13<sup>m</sup> 45<sup>s</sup>; Decl. -49° 52'

13.042	269.7	13.06	6.5	2	300
13.050	269.7	12.44	6.3	3	300
13.063	270.8	12.56	5.6	2	300
13.05	270.1	12.69	(9.5 ... 10.1)		N

*h* 4077; -62° 988 + 7; 9.2 + 9.4A.R. 8<sup>h</sup> 14<sup>m</sup> 0<sup>s</sup>; Decl. -62° 28'

17.299	303.5	17.30	12.1	2½	370
17.430	303.6	17.04	12.3	2½	370
17.468	303.2	17.12	12.7	2½	370
17.40	303.4	17.15	(9.2 ... 10.0)		F

*h* 4080; -46° 2392; 8.0A.R. 8<sup>h</sup> 14<sup>m</sup> 24<sup>s</sup>; Decl. -46° 45'

12.957	219.4	5.98	6.1	3½	300
12.962	218.2	5.95	6.7	3	300
13.042	217.8	5.91	6.2	3	300
13.050	217.3	5.85	6.7	3	300
13.00	218.2	5.92	(8.5 ... 8.7)		F

*h* 4079; -55° 1499; 7.8A.R. 8<sup>h</sup> 14<sup>m</sup> 43<sup>s</sup>; Decl. -55° 30'

13.028	171.2	30.38	5.0	3	300
13.031	170.2	30.41	6.0	3	300
13.03	170.7	30.40	(8.5 ... 11.0)		49

Brisbane; -44° 2475; 8.0

A.R. 8<sup>h</sup> 14<sup>m</sup> 48<sup>s</sup>; Decl. -44° 39'

12.957	326.6	5.29	5.8	3½	300
12.962	328.1	5.47	6.3	3	300
13.023	327.4	5.44	7.1	3	300
12.98	327.4	5.40	(8.2 ... 8.2)		50

*h* 4084 = Rus 83; -58° 1095 + 6; 7.2 + 8.8A.R. 8<sup>h</sup> 15<sup>m</sup> 21<sup>s</sup>; Decl. -58° 46'

17.277	154.9	43.77	11.2	3	370
17.321	154.8	43.95	12.5	2	370
17.332	154.9	43.64	10.8	2	370
17.31	154.9	43.79	(7.0 ... 9.7)		

BC

17.277	87.7	3.07	11.3	3	370
17.321	86.1	3.02	12.6	2	370
17.332	86.9	3.02	10.9	2	370
17.31	86.9	3.04	(9.7 ... 9.9)		F

*h* 4082; -49° 1596; 8.8A.R. 8<sup>h</sup> 15<sup>m</sup> 28<sup>s</sup>; Decl. -49° 53'

13.050	267.0	6.32	6.5	2½	300
13.063	267.2	6.34	5.7	2½	300
13.077	263.6	6.17	6.8	3	300
13.154	265.3	6.18	6.5	2	300
13.09	265.8	6.25	(9.4 ... 9.6)		21

Anon.; -57° 1484 + 3; 8.6 + 8.7

A.R. 8<sup>h</sup> 17<sup>m</sup> 12<sup>s</sup>; Decl. -57° 16'

17.381	337.2	15.86	11.4	2½	370
17.406	337.2	15.89	12.9	2	370
17.39	337.2	15.87	(8.3 ... 8.9)		7

*h* 4089; -44° 2552; 8.8A.R. 8<sup>h</sup> 18<sup>m</sup> 31<sup>s</sup>; Decl. -44° 27'

13.034	271.1	14.62	5.1	3	300
13.039	271.2	14.75	6.4	2½	300
13.04	271.1	14.68	(9.4 ... 9.9)		F

*h* 4090; -42° 2426; 8.4A.R. 8<sup>h</sup> 19<sup>m</sup> 7<sup>s</sup>; Decl. -42° 24'

13.034	12.5	20.29	5.2	3	300
13.039	12.7	20.24	6.5	2½	300
13.04	12.6	20.27	(8.9 ... 9.8)		F

Brisbane; -71° 677 + 8 + 9; 5.8 + 6.7 + 9.0

A.R. 8<sup>h</sup> 20<sup>m</sup> 10<sup>s</sup>; Decl. -71° 7'

16.990	57.0	65.01	6.6	3	370
17.118	56.7	65.07	11.0	2	370
17.05	56.9	65.03	(5.8 ... 6.0)		A

AC

16.990	30.0	37.71	6.8	3	370
17.118	29.8	37.82	11.0	2	370
17.05	29.9	37.76	(5.8 ... 8.5)		D†

*h* 4095;  $-73^{\circ} 493$ ; 9.8

A.R.  $8^{\text{h}} 20^{\text{m}} 16^{\text{s}}$ ; Decl.  $-73^{\circ} 6'$

16.992	251.7	12.33	6.0	2	370
17.129	253.3	12.15	11.7	2	370
17.06	252.5	12.24	(10.6 ... 12.2)		N

AC

16.992	335.9	20.61	6.2	2	370
17.129	335.3	20.80	11.8	2	370
17.06	335.6	20.70	(10.6 ... 11.2)		N

*h* 4091;  $-43^{\circ} 2550$ ; 8.3

A.R.  $8^{\text{h}} 20^{\text{m}} 44^{\text{s}}$ ; Decl.  $-43^{\circ} 54'$

13.017	300.4	18.57	6.2	2	300
13.023	300.8	18.65	7.2	3	300
13.02	300.6	18.61	(8.6 ... 10.4)		N

AC

13.017	45.0	11.95	6.3	2	300
13.023	46.7	11.62	7.4	3	300
13.028	45.3	11.78	5.6	2	300
13.02	45.7	11.78	(8.6 ... 11.2)		N

*h* 4096;  $-60^{\circ} 1109$ ; 9.6

A.R.  $8^{\text{h}} 21^{\text{m}} 4^{\text{s}}$ ; Decl.  $-60^{\circ} 36'$

17.321	89.1	14.95	12.9	2	370
17.332	89.6	14.94	11.0	2	370
17.33	89.4	14.94	(9.3 ... 11.8)		51

*h* 4097;  $-60^{\circ} 1110$ ; 9.6

A.R.  $8^{\text{h}} 21^{\text{m}} 5^{\text{s}}$ ; Decl.  $-60^{\circ} 35'$

17.321	5.9	11.87	13.0	2	370
17.332	5.6	12.02	11.1	2	370
17.33	5.7	11.91	(9.4 ... 10.8)		51

*h* 4103;  $\eta$  Volantis; 5.1

A.R.  $8^{\text{h}} 23^{\text{m}} 9^{\text{s}}$ ; Decl.  $-72^{\circ} 60'$

16.992	288.0	30.82	6.4	2	370
17.127	287.1	31.00	11.5	2	370
17.162	287.3	30.54	10.9	2½	370
17.09	287.5	30.79	(5.2 ... 11.9)		N

AC

16.992	161.9	42.38	6.7	2	370
17.127	161.4	42.49	11.4	2	370
17.06	161.6	42.44	(5.2 ... 11.7)		N

*h* 4101;  $-49^{\circ} 1650$ ; 8.7

A.R.  $8^{\text{h}} 23^{\text{m}} 50^{\text{s}}$ ; Decl.  $-49^{\circ} 55'$

12.921	52.2	7.57	5.7	3	300
13.025	53.1	7.55	7.2	3	300
13.063	50.5	7.61	5.8	2	300
13.066	51.9	7.32	6.3	3	300
13.02	51.9	7.51	(9.3 ... 9.3)		N

*h* 4102;  $-42^{\circ} 2551 + 46$ ; 6.9 + 9.2

A.R.  $8^{\text{h}} 24^{\text{m}} 30^{\text{s}}$ ; Decl.  $-42^{\circ} 10'$

13.200	280.9	68.40	11.4	2	300
13.203	280.4	68.55	12.0	1½	300
13.20	280.7	68.47	(7.1 ... 9.4)		N

*h* 4104; *A* Velorum; 6.4

A.R.  $8^{\text{h}} 25^{\text{m}} 8^{\text{s}}$ ; Decl.  $-47^{\circ} 31'$

12.921	245.6	3.45	5.4	3	300
12.957	245.5	3.58	6.6	3	300
12.962	243.3	3.41	6.8	3	300
12.95	244.8	3.48	(6.0 ... 8.2)		F

AC

13.050	38.6	18.94	7.0	3	300
13.063	39.2	18.67	6.0	2	300
13.066	39.6	18.92	6.4	3	300
13.06	39.1	18.84	(6.0 ... 8.8)		F

*h* 4108;  $-60^{\circ} 1133$ ; 9.2

A.R.  $8^{\text{h}} 27^{\text{m}} 6^{\text{s}}$ ; Decl.  $-60^{\circ} 41'$

17.332	229.2	19.99	11.3	2	370
17.334	229.5	19.83	12.5	2	370
17.33	229.4	19.91	(9.5 ... 10.6)		N

*Có.* 77;  $-50^{\circ} 1647$ ; 8.6

A.R.  $8^{\text{h}} 28^{\text{m}} 34^{\text{s}}$ ; Decl.  $-50^{\circ} 33'$

17.072	99.8	3.77	7.5	3	370
17.075	98.4	3.70	11.6	3	370
17.091	97.6	3.77	10.5	2	370
17.08	98.6	3.75	(8.5 ... 10.4)		

*Sellers* 8;  $-52^{\circ} 1517$ ; 7.0

A.R.  $8^{\text{h}} 28^{\text{m}} 37^{\text{s}}$ ; Decl.  $-52^{\circ} 47'$

17.072	303.0	0.90	7.7	3	650
17.075	298.5	1.03	11.1	3	650
17.091	299.3	1.04	10.7	2	475
17.08	300.3	0.99	(7.5 ... 8.3)		D

$h$  4111;  $-49^\circ 17'01''$ ; 8.6A.R.  $8^h 30^m 0^s$ ; Decl.  $-49^\circ 31'$ 

13.063	107.7	9.68	6.2	3	300
13.066	106.1	9.63	6.5	$2\frac{1}{2}$	300
13.077	106.6	9.53	7.0	3	300
13.07	106.8	9.61	(8.8 ... 9.8)		F

 $h$  4112;  $-48^\circ 17'83''$ ; 8.2A.R.  $8^h 30^m 50^s$ ; Decl.  $-48^\circ 23'$ 

13.063	201.3	9.26	6.3	3	300
13.066	202.5	9.46	6.6	2	300
13.077	202.6	9.41	7.1	3	300
13.07	202.1	9.38	(9.2 ... 9.3)		A

 $h$  4118;  $-73^\circ 51'11''$ ; 9.2A.R.  $8^h 31^m 26^s$ ; Decl.  $-73^\circ 3'$ 

16.992	27.0	24.59	7.0	2	370
17.129	27.1	24.85	12.2	2	370
17.06	27.0	24.72	(9.3 ... 10.9)		N

 $h$  4117;  $-61^\circ 10'45''$ ; 8.0A.R.  $8^h 32^m 3^s$ ; Decl.  $-61^\circ 4'$ 

17.332	194.7	16.74	11.5	2	370
17.334	195.0	16.69	12.7	2	370
17.33	194.8	16.72	(8.2 ... 12.8)		52

 $h$  4116;  $-47^\circ 24'43''$ ; 7.8A.R.  $8^h 32^m 39^s$ ; Decl.  $-47^\circ 4'$ 

12.957	1.5	7.72	6.9	3	300
12.962	2.3	7.72	7.0	3	300
13.044	1.1	7.59	7.0	2	300
12.99	1.6	7.68	(8.2 ... 9.2)		F

 $h$  4119;  $-48^\circ 18'06''$ ; 7.3A.R.  $8^h 33^m 17^s$ ; Decl.  $-48^\circ 59'$ 

13.063	226.3	10.32	6.4	$2\frac{1}{2}$	300
13.066	226.3	9.99	6.8	$2\frac{1}{2}$	300
13.077	225.4	10.10	7.1	3	300
13.07	226.0	10.14	(7.8 ... 9.2)		F

 $-53^\circ 17'80'' + 2''$ ; 8.4 + 9.6A.R.  $8^h 34^m 1^s$ ; Decl.  $-53^\circ 10'$ 

17.066	102.0	30.14	6.8	$2\frac{1}{2}$	370
17.091	101.6	30.09	10.9	2	370
17.08	101.8	30.12	(8.5 ... 10.7)		53

 $h$  4122;  $-45^\circ 27'78''$ ; 8.3:A.R.  $8^h 34^m 54^s$ ; Decl.  $-45^\circ 47'$ 

13.069	156.3	10.48	6.4	$2\frac{1}{2}$	300
13.077	155.9	10.34	7.3	3	300
13.07	156.1	10.41	(8.8 ... 9.0)		54

 $h$  4126;  $-52^\circ 15'79''$ ; 5.6A.R.  $8^h 36^m 24^s$ ; Decl.  $-52^\circ 37'$ 

17.066	29.5	16.74	7.0	$2\frac{1}{2}$	370
17.075	30.3	16.62	11.3	3	370
17.091	30.8	16.76	11.0	2	370
17.08	30.2	16.71	(5.3 ... 9.6)		F

 $h$  4127;  $b$  Velorum; 5.5A.R.  $8^h 36^m 29^s$ ; Decl.  $-46^\circ 12'$ 

13.063	57.2	37.31	6.6	3	300
13.066	57.3	37.60	6.9	$2\frac{1}{2}$	300
13.077	57.7	37.51	7.4	3	300
13.07	57.4	37.47	(4.3 ... 9.4)		N

 $h$  4128;  $-59^\circ 10'75''$ ; 6.8A.R.  $8^h 36^m 33^s$ ; Decl.  $-59^\circ 53'$ 

17.274	215.5	1.70	11.5	2	370
17.277	215.8	1.74	11.4	3	650
17.332	215.4	1.81	11.6	2	370
17.29	215.6	1.75	(7.1 ... 8.0)		M

 $h$  4130 =  $h$  4142;  $-57^\circ 16'44''$ ; 7.2A.R.  $8^h 37^m 41^s$ ; Decl.  $-57^\circ 6'$ 

13.031	231.6	3.75	6.9	3	300
13.080	232.1	3.82	6.0	3	300
13.091	231.9	3.89	6.6	3	300
13.07	231.9	3.82	(7.4 ... 8.9)		55

 $h$  4134;  $\theta$  Volantis; 5.5A.R.  $8^h 38^m 35^s$ ; Decl.  $-69^\circ 56'$ 

16.990	108.1	45.02	7.0	2	370
17.154	107.6	45.14	11.2	$1\frac{1}{2}$	370
17.162	107.8	44.82	11.2	2	370
17.10	107.8	44.92	(5.7 ... 9.8)		N

Brisbane;  $-52^\circ 16'07'' + 5''$ ; 5.2 + 6.8A.R.  $8^h 38^m 50^s$ ; Decl.  $-52^\circ 40'$ 

17.066	310.6	76.67	7.2	$2\frac{1}{2}$	370
17.094	310.4	76.81	10.3	2	370
17.08	310.5	76.74	(5.3 ... 6.1)		F

 $h$  4133;  $d$  Velorum; 6.6A.R.  $8^h 39^m 57^s$ ; Decl.  $-42^\circ 12'$ 

13.017	61.7	45.76	7.2	2	300
13.023	61.5	45.81	7.6	3	300
13.034	62.3	45.49	6.6	2	300
13.02	61.8	45.69	(4.6 ... 9.7)		F†

I 10;  $\delta$  Argûs; 3.5

A.R. 8<sup>h</sup> 41<sup>m</sup> 17<sup>s</sup>; Decl.  $-54^{\circ} 15'$

13.080	161.0	3.33	5.8	2	300
13.091	164.6	3.50	7.0	2½	300
13.104	163.2	3.46	6.5	2½	300
16.785	163.9	2.77	5.3	3	475
16.990	160.3	3.06	7.3	2½	370
17.075	164.9	2.87	11.4	2½	475
17.277	165.0	2.87	11.5	3	650
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13.09	162.9	3.43			
17.03	163.5	2.89	(2.7 ... 6.3)		P

AB,C = h 4136

13.031	61.1	69.30	6.5	3	300
13.080	61.1	69.40	5.7	2½	300
<hr/>					
13.06	61.1	69.35	(2.6 ... 9.8)		

h 4139;  $-59^{\circ} 1096 + 7$ ; 9.7 + 9.9

A.R. 8<sup>h</sup> 41<sup>m</sup> 36<sup>s</sup>; Decl.  $-59^{\circ} 30'$

17.332	49.2	12.85	12.0	2	370
17.334	49.7	12.74	13.0	2	370
<hr/>					
17.33	49.4	12.80	(10.4 ... 10.8)		N

Aguilar 6;  $-57^{\circ} 1688$ ; 8.7

A.R. 8<sup>h</sup> 41<sup>m</sup> 58<sup>s</sup>; Decl.  $-57^{\circ} 53'$

17.381	349.6	3.65	11.5	2½	370
17.406	352.1	3.76	13.1	2	370
17.409	350.1	3.55	13.0	3	370
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17.40	350.6	3.65	(9.3 ... 9.7)		7

Rü 9;  $-58^{\circ} 1202$ ; 6.6

A.R. 8<sup>h</sup> 42<sup>m</sup> 7<sup>s</sup>; Decl.  $-58^{\circ} 16'$

13.091	292.1	4.56	7.5	2½	300
13.104	292.7	4.41	6.6	3	300
13.107	292.5	4.34	6.9	2½	300
<hr/>					
13.10	292.4	4.44	(7.6 ... 7.8)		20

AC

13.104	359.4	51.03	6.7	3	300
13.107	359.1	50.78	7.0	2½	300
<hr/>					
13.11	359.3	50.91	(7.6 ... 10.0)		

AD

13.104	222.0	61.39	6.8	2½	300
13.107	222.1	61.34	7.1	2	300
<hr/>					
13.11	222.0	61.37	(7.6 ... 9.8)		

Jacob 110;  $-42^{\circ} 2938$ ; 7.8

A.R. 8<sup>h</sup> 42<sup>m</sup> 48<sup>s</sup>; Decl.  $-42^{\circ} 9'$

13.034	86.1	5.48	6.8	2	300
13.069	86.5	5.53	6.8	2½	300
13.077	85.2	5.62	7.5	3½	300
<hr/>					
13.06	85.9	5.54	(9.0 ... 9.1)		F

h 4145;  $-53^{\circ} 1923$ ; 8.3

A.R. 8<sup>h</sup> 46<sup>m</sup> 11<sup>s</sup>; Decl.  $-53^{\circ} 36'$

17.066	256.2	5.45	7.4	2½	370
17.072	256.0	5.41	8.0	3½	370
17.075	256.2	5.34	11.5	2½	370
<hr/>					
17.07	256.1	5.40	(9.1 ... 10.6)		F

h 4147; C6D  $-61^{\circ} 2042$ ; 10½

A.R. 8<sup>h</sup> 46<sup>m</sup> 51<sup>s</sup>; Decl.  $-61^{\circ} 48'$

17.332	259.1	8.64	12.3	2	370
17.334	258.7	8.45	13.1	2	370
17.337	258.6	8.22	12.4	2	370
<hr/>					
17.33	258.8	8.44	(11.4 ... 12.1)		N

h 4148;  $-53^{\circ} 1943$ ; 8.0

A.R. 8<sup>h</sup> 47<sup>m</sup> 13<sup>s</sup>; Decl.  $-53^{\circ} 39'$

17.066	111.1	5.89	7.5	2½	370
17.072	110.7	5.92	8.1	3	370
17.075	110.9	5.93	11.6	2½	370
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17.07	110.9	5.91	(8.4 ... 11.2)		F

h 4151;  $-53^{\circ} 1967$ ; 9.0

A.R. 8<sup>h</sup> 50<sup>m</sup> 3<sup>s</sup>; Decl.  $-53^{\circ} 2'$

17.066	256.2	5.81	7.6	2½	370
17.384	256.3	5.77	12.5	2½	370
17.468	257.7	5.64	12.8	2	370
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17.31	256.7	5.74	(9.4 ... 12.0)		N

h 4155;  $-60^{\circ} 1233$ ; 9.7

A.R. 8<sup>h</sup> 50<sup>m</sup> 17<sup>s</sup>; Decl.  $-60^{\circ} 58'$

17.332	194.8	10.68	12.6	2	370
17.334	194.4	10.67	13.3	2	370
17.376	193.7	10.47	12.5	2	370
<hr/>					
17.35	194.3	10.61	(10.8 ... 11.3)		N

AC

17.332	246.7	9.16	12.8	2	370
17.334	245.7	8.93	13.2	2	370
17.376	244.1	8.86	12.4	2	370
<hr/>					
17.35	245.5	8.98	(10.8 ... 12.5)		56

h 4153;  $-44^{\circ} 3226$ ; 7.0

A.R. 8<sup>h</sup> 50<sup>m</sup> 56<sup>s</sup>; Decl.  $-44^{\circ} 34'$

13.020	130.7	35.15	5.9	3	300
13.036	130.6	34.94	7.1	3	300
<hr/>					
13.03	130.6	35.04	(6.8 ... 12.8)		N

h 4156; e Carinae; 4.3

A.R. 8<sup>h</sup> 52<sup>m</sup> 12<sup>s</sup>; Decl.  $-60^{\circ} 10'$

17.376	318.1	21.23	12.8	2	370
17.381	318.0	21.48	12.7	2	370
<hr/>					
17.38	318.0	21.36	(4.0 ... 13.0)		57

$\Delta 73; -55^\circ 1852 + 3; 8.6 + 8.6$ A.R.  $8^h 52^m 41^s$ ; Decl.  $-55^\circ 2'$ 

13.031	357.9	65.98	7.2	3	300
13.080	358.1	65.78	6.1	2	300
13.06	358.0	65.88	(8.4 ... 8.6)		F

AC =  $h 4156\frac{1}{3}$ 

13.031	239.8	27.61	7.4	3	300
13.080	239.8	27.47	6.3	2	300
13.06	239.8	27.54	(8.4 ... 10.0)		N

 $h 4159; -53^\circ 2007; 8.8$ A.R.  $8^h 53^m 32^s$ ; Decl.  $-53^\circ 7'$ 

17.384	195.1	15.22	12.7	$2\frac{1}{2}$	370
17.468	194.6	15.15	12.9	2	370
17.43	194.9	15.19	(8.9 ... 12.5)		N

 $\Delta 74; b' \text{ Carinae}; 4.8$ A.R.  $8^h 53^m 55^s$ ; Decl.  $-58^\circ 45'$ 

17.332	75.2	40.47	13.1	2	370
17.337	75.2	40.24	12.7	2	370
17.33	75.2	40.36	(5.3 ... 6.8)		F

 $h 4161; -46^\circ 3297; 6.2$ A.R.  $8^h 54^m 38^s$ ; Decl.  $-46^\circ 45'$ 

13.063	337.3	25.08	6.8	3	300
13.066	336.9	25.26	7.0	2	300
13.077	336.7	24.67	7.7	3	300
13.154	337.1	25.36	7.2	2	300
13.203	337.1	25.19	12.4	$1\frac{1}{2}$	300
13.11	337.0	25.11	(6.3 ... 11.1)		N

 $h 4165; -51^\circ 1821; 5.5$ A.R.  $8^h 57^m 52^s$ ; Decl.  $-51^\circ 42'$ 

17.066	104.1	1.37	7.8	$2\frac{1}{2}$	475
17.241	104.4	1.25	12.8	2	650
17.384	103.3	1.12	13.0	3	650
17.468	105.5	1.11	13.0	2	650
17.29	104.3	1.21	(6.0 ... 7.6)		M

 $h 4170; -59^\circ 1237; 9.9$ A.R.  $8^h 59^m 38^s$ ; Decl.  $-59^\circ 26'$ 

17.332	246.3	8.49	13.3	2	370
17.376	247.1	8.41	13.0	2	370
17.381	248.5	8.09	12.9	2	370
17.36	247.3	8.33	(10.9 ... 11.4)		58

 $h 4175; -61^\circ 1167; 8.1:$ A.R.  $9^h 0^m 30^s$ ; Decl.  $-61^\circ 51'$ 

17.154	131.6	20.07	11.5	$1\frac{1}{2}$	370
17.376	131.7	19.82	13.2	$2\frac{1}{2}$	370
17.26	131.7	19.94	(8.0 ... 10.1)		N

 $h 4177; -55^\circ 1924; 7.1$ A.R.  $9^h 1^m 1^s$ ; Decl.  $-55^\circ 51'$ 

13.031	259.5	13.11	7.8	$2\frac{1}{2}$	300
13.080	258.9	13.30	6.5	3	300
13.06	259.2	13.21	(7.5 ... 9.1)		A

AC

13.031	296.0	35.42	7.7	$2\frac{1}{2}$	300
13.080	296.2	35.50	6.6	3	300
13.06	296.1	35.46	(7.5 ... 9.5)		59

 $h 4178; -57^\circ 1859; 7.4$ A.R.  $9^h 1^m 28^s$ ; Decl.  $-57^\circ 21'$ 

13.148	157.7	3.60	7.6	3	300
13.157	161.6	3.43	6.8	3	300
13.184	161.9	3.38	6.9	2	280
13.16	160.4	3.47	(7.8 ... 11.2)		N

 $h 4181; -54^\circ 2020; 9.1$ A.R.  $9^h 2^m 29^s$ ; Decl.  $-54^\circ 14'$ 

17.384	311.2	2.92	13.3	3	650
17.468	311.5	2.94	13.1	$2\frac{1}{2}$	370
17.471	311.2	2.75	12.9	2	370
17.44	311.3	2.87	(9.7 ... 9.9)		60

 $h 4180; -43^\circ 3354; 8.7$ A.R.  $9^h 2^m 50^s$ ; Decl.  $-43^\circ 27'$ 

13.020	127.4	22.85	6.5	3	300
13.023	127.5	22.47	7.8	3	300
13.039	127.8	22.47	6.9	3	300
13.03	127.6	22.60	(9.0 ... 9.8)		N

Delavan 3;  $-52^\circ 1957; 9.0$ A.R.  $9^h 3^m 47^s$ ; Decl.  $-52^\circ 40'$ 

14.328	354.3	8.70	12.0	2	370
14.334	355.2	8.44	12.0	2	370
14.336	355.4	8.85	12.0	3	370
14.350	355.2	8.93	11.5	2	370
14.34	355.0	8.73	(9.2 ... 10.4)		7

AC

14.328	105.3	14.83	12.1	2	370
14.336	106.7	14.42	12.2	3	370
14.33	106.0	14.62	(9.2 ... 12.5)		

 $h 4186; -44^\circ 3489; 9.2$ A.R.  $9^h 6^m 22^s$ ; Decl.  $-44^\circ 48'$ 

13.020	281.3	9.18	7.0	3	300
13.023	280.5	8.90	8.0	3	300
13.039	280.7	9.07	7.2	3	300
13.03	280.8	9.05	(9.3 ... 9.6)		N



Aguilar 7;  $-59^{\circ} 1294$ ; 8.7

A.R.  $9^h 6^m 28^s$ ; Decl.  $-59^{\circ} 30'$

17.430	337.9	5.49	13.9	2	370
17.479	337.0	5.63	12.6	2	370
17.496	335.3	5.34	13.6	2	370
17.47	336.7	5.49	(9.2 ... 11.0)		7

*h* 4188;  $-43^{\circ} 3450$ ; 6.1

A.R.  $9^h 7^m 53^s$ ; Decl.  $-43^{\circ} 6'$

12.916	284.7	2.82	6.6	2	300
13.017	286.0	2.72	7.5	$2\frac{1}{2}$	300
13.020	285.0	2.84	7.4	3	300
12.98	285.2	2.79	(7.0 ... 7.6)		F

*h* 4190;  $-57^{\circ} 1914$ ; 6.8

A.R.  $9^h 8^m 8^s$ ; Decl.  $-57^{\circ} 27'$

13.091	22.6	8.25	8.3	2	300
13.104	24.1	8.26	7.3	$2\frac{1}{2}$	300
13.123	23.1	8.08	6.5	2	300
13.11	23.3	8.20	(6.9 ... 9.7)		F

*h* 4189;  $-53^{\circ} 2209$ ; 7.6

A.R.  $9^h 8^m 13^s$ ; Decl.  $-53^{\circ} 27'$

17.384	106.5	20.12	13.4	3	370
17.468	107.1	20.14	13.3	2	370
17.43	106.8	20.13	(8.0 ... 10.2)		61

*h* 4191;  $\alpha$  Velorum; 5.7

A.R.  $9^h 9^m 45^s$ ; Decl.  $-42^{\circ} 43'$

12.916	13.6	5.91	6.4	$2\frac{1}{2}$	300
13.017	12.1	6.05	7.7	$2\frac{1}{2}$	300
13.020	16.9	5.69	7.5	3	300
13.069	14.0	5.73	7.0	$2\frac{1}{2}$	300
13.01	14.1	5.85	(5.6 ... 10.1)		F?

*h* 4192;  $-49^{\circ} 2288 + 9$ ; 8.6 + 8.6

A.R.  $9^h 10^m 0^s$ ; Decl.  $-49^{\circ} 50'$

13.042	11.0	25.80	7.0	3	300
13.063	10.8	25.87	7.0	3	300
13.05	10.9	25.84	(9.1 ... 9.2)		D?

*h* 4196;  $-51^{\circ} 2073$ ; 9.2

A.R.  $9^h 12^m 34^s$ ; Decl.  $-51^{\circ} 24'$

17.384	122.6	3.20	13.5	$2\frac{1}{2}$	370
17.468	123.0	3.33	13.4	$2\frac{1}{2}$	370
17.471	123.2	3.36	13.2	2	370
17.44	122.9	3.30	(9.5 ... 10.8)		20

Rus 107;  $-57^{\circ} 1966$ ; 9.0

A.R.  $9^h 13^m 9^s$ ; Decl.  $-57^{\circ} 53'$

17.411	281.96	9.27	13.6	2	370
17.496	280.0	9.63	13.8	2	370
17.501	284.0	9.73	13.8	2	370
17.47	281.9	9.54	(9.3 ... 11.0)		7

*h* 4197;  $-52^{\circ} 2185$ ; 8.7

A.R.  $9^h 13^m 31^s$ ; Decl.  $-52^{\circ} 19'$

17.384	203.5	21.24	13.6	$2\frac{1}{2}$	370
17.468	202.9	21.41	13.5	2	370
17.43	203.2	21.32	(9.0 ... 11.8)		N

*h* 4202;  $-45^{\circ} 3677$ ; 8.2

A.R.  $9^h 16^m 35^s$ ; Decl.  $-45^{\circ} 29'$

13.069	152.0	18.00	7.1	3	300
13.077	152.0	17.98	7.9	3	300
13.07	152.0	17.99	(8.4 ... 11.2)		N

*h* 5452;  $-44^{\circ} 3713$ ; 9.2

A.R.  $9^h 16^m 53^s$ ; Decl.  $-44^{\circ} 57'$

13.209	105.8	10.70	11.7	2	300
13.241	106.1	10.46	11.5	3	300
13.22	106.0	10.58	(9.6 ... 11.5)		N

*h* 4207;  $-54^{\circ} 2238 + 9$ ; 8.8 + 9.0

A.R.  $9^h 19^m 41^s$ ; Decl.  $-54^{\circ} 21'$

13.123	127.6	16.36	6.8	2	300
13.126	128.0	16.26	7.0	2	300
13.12	127.8	16.31	(9.0 ... 9.1)		N

*h* 4209;  $-47^{\circ} 3307 + 6$ ; 8.6 + 9.3

A.R.  $9^h 20^m 54^s$ ; Decl.  $-47^{\circ} 44'$

13.025	336.9	25.63	7.8	3	300
13.042	337.1	25.46	7.7	3	300
13.03	337.0	25.54	(8.8 ... 9.4)		F

AC

13.025	16.0	13.26	7.9	3	300
13.042	15.7	13.11	7.8	3	300
13.03	15.9	13.19	(8.8 ... 10.8)		N

*h* 4213;  $-61^{\circ} 1271$ ; 6.7

A.R.  $9^h 22^m 20^s$ ; Decl.  $-61^{\circ} 25'$

17.154	326.7	8.95	11.7	$1\frac{1}{2}$	370
17.376	326.6	8.81	13.4	3	370
17.381	327.3	8.75	13.2	2	370
17.30	326.9	8.84	(6.5 ... 10.8)		F

$h 4212; -42^\circ 3716; 7.7$ A.R.  $9^h 22^m 58^s$ ; Decl.  $-42^\circ 2'$ 

13.195	61.7	20.97	7.9	2	300
13.208	62.7	21.00	12.0	2	300
13.20	62.2	20.98	(7.5 ... 11.5)		N

C6.;  $-58^\circ 1523; 8.7$ A.R.  $9^h 23^m 29^s$ ; Decl.  $-58^\circ 28'$ 

14.334	198.3	4.35	12.2	2	370
14.336	197.5	4.29	12.5	3	370
14.350	198.6	4.34	11.8	3	370
14.34	198.1	4.33	(9.1 ... 9.6)		7

 $\lambda 112; -44^\circ 3798; 7.6$ A.R.  $9^h 23^m 55^s$ ; Decl.  $-44^\circ 57'$ 

13.077	268.2	9.48	8.1	3	300
13.088	271.8	9.65	7.0	2	300
13.195	267.1	[10.12]	7.6	2	300
13.244	269.1	9.50	12.2	3½	300
13.15	269.1	9.54	(7.6 ... 11.2)		F

AC =  $\Delta 76$ 

13.077	98.6	60.46	8.2	3	300
13.088	98.4	60.81	7.1	2	300
13.195	98.3	60.83	7.7	2	300
13.12	98.4	60.70	(7.6 ... 7.8)		F

 $h 4215; -48^\circ 2474; 9.0:$ A.R.  $9^h 24^m 3^s$ ; Decl.  $-48^\circ 57'$ 

13.025	260.7	10.43	7.6	3	300
13.063	260.3	10.21	7.2	3	300
13.04	260.5	10.32	(9.4 ... 9.6)		F

 $\Delta 77; -43^\circ 3729 + 34; 7.7 + 7.7$ A.R.  $9^h 24^m 37^s$ ; Decl.  $-43^\circ 60'$ 

13.077	76.8	108.38	8.3	3	300
13.088	76.8	108.46	7.2	2	300
13.195	76.5	108.43	8.0	2	300
13.12	76.7	108.42	(7.3 ... 7.4)		F

Copeland;  $\psi$  Argús; 3.8A.R.  $9^h 25^m 47^s$ ; Decl.  $-39^\circ 55'$ 

14.350	[126.5]	1.45	11.0	2½	370
14.396	119.7	1.54	12.5	3	475
14.399	119.8	1.20	12.7	3	650
14.405	119.9	1.42	13.3	3	370
17.340	133.2	1.01	11.0	3	650
17.444	128.8	1.02	13.7	2	650
17.471	131.1	1.12	12.7	2½	475
14.39	119.8	1.40			
17.42	131.0	1.05	(3.8 ... 5.2)		B

 $h 4219; -42^\circ 3802; 9.3$ A.R.  $9^h 28^m 8^s$ ; Decl.  $-42^\circ 14'$ 

13.069	324.1	25.33	7.3	2½	300
13.077	324.0	25.25	8.5	3	300
13.07	324.0	25.29	(9.2 ... 10.5)		N

 $h 4222; \text{Anon.}$ A.R.  $9^h 28^m 35^s$ ; Decl.  $-70^\circ 33'$ 

16.992	333.5	7.45	7.5	2	370
17.162	333.3	7.46	11.4	2	370
17.239	333.0	7.57	12.9	2½	370
17.13	333.3	7.49	(10.7 ... 12.3)		N

 $h 4221; -52^\circ 2515; 9.2$ A.R.  $9^h 29^m 11^s$ ; Decl.  $-52^\circ 53'$ 

17.384	129.1	5.23	13.7	2½	370
17.471	127.0	[5.62]	13.3	2	370
17.474	131.8	5.25	12.8	3	370
17.476	129.3	5.44	12.9	2½	370
17.45	129.3	5.31	(9.1 ... 12.9)		N

 $\Delta 79; -49^\circ 2570 + 3; 8.2 + 8.4$ A.R.  $9^h 29^m 12^s$ ; Decl.  $-49^\circ 12'$ 

13.438	31.5	135.50	13.4	1½	300
13.466	31.7	135.29	14.1	3	300
13.45	31.6	135.39	(7.5 ... 7.6)		62

 $h 4220; -48^\circ 2532; 5.8$ A.R.  $9^h 29^m 16^s$ ; Decl.  $-48^\circ 27'$ 

12.921	207.4	2.35	7.4	3	300
13.017	207.6	2.57	8.1	2	300
13.050	207.4	2.42	7.3	3	300
13.00	207.5	2.45	(6.0 ... 6.8)		M

 $h 4225; \text{Anon.}$ A.R.  $9^h 29^m 20^s$ ; Decl.  $-70^\circ 36'$ 

17.162	230.7	17.08	11.8	2	370
17.239	231.8	17.42	13.2	2½	370
17.20	231.3	17.25	(10.1 ... 12.6)		N

Rus 123;  $-57^\circ 2122; 6.9$ A.R.  $9^h 29^m 33^s$ ; Decl.  $-57^\circ 24'$ 

13.104	34.5	2.31	7.6	2	300
13.121	34.4	[2.08]	7.1	2	300
13.126	34.4	2.42	7.3	2	300
13.143	33.6	2.43	7.4	2½	300
13.12	34.2	2.39	(7.5 ... 7.6)		20

Aguilar 8;  $-59^{\circ} 1420$ ; 8.9

A.R.  $9^h 31^m 2^s$ ; Decl.  $-59^{\circ} 50'$

17.496	275.2	2.46	14.1	2	370
17.512	272.8	2.70	13.7	2	370
17.50	274.0	2.58	(9.0 ... 11.8)		7

Rus 125;  $-48^{\circ} 2558$ ; 7.4

A.R.  $9^h 31^m 54^s$ ; Decl.  $-48^{\circ} 11'$

13.025	171.1	3.48	8.1	3	300
13.050	173.1	3.48	7.5	$2\frac{1}{2}$	300
13.063	171.5	3.65	7.4	$2\frac{1}{2}$	300
13.05	171.9	3.54	(7.0 ... 9.1)		63

$h 4232$ ;  $-56^{\circ} 2393$ ; 7.6

A.R.  $9^h 34^m 34^s$ ; Decl.  $-56^{\circ} 58'$

13.104	301.7	10.97	7.9	2	300
13.121	302.7	11.07	7.2	2	300
13.123	301.6	11.03	7.1	2	300
13.12	302.0	11.02	(8.1 ... 8.5)		F

$h 4234$ ;  $-51^{\circ} 2496 + 5$ ; 8.9 + 10.0

A.R.  $9^h 36^m 26^s$ ; Decl.  $-51^{\circ} 44'$

17.384	215.4	21.92	13.9	$2\frac{1}{2}$	370
17.471	216.1	22.02	13.4	2	370
17.43	215.7	21.97	(9.2 ... 10.6)		D?

$h 4235$ ;  $-50^{\circ} 2603$ ; 8.6

A.R.  $9^h 36^m 50^s$ ; Decl.  $-50^{\circ} 35'$

17.384	88.7	5.22	14.0	$2\frac{1}{2}$	370
17.474	88.1	5.19	12.9	3	370
17.476	88.0	5.14	13.1	3	370
17.44	88.3	5.18	(9.0 ... 9.1)		F

$-71^{\circ} 860$ ; 9.4

A.R.  $9^h 37^m 35^s$ ; Decl.  $-71^{\circ} 11'$

17.162	227.8	7.64	12.1	2	370 64
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Rus 129;  $-55^{\circ} 2452$ ; 7.9

A.R.  $9^h 38^m 38^s$ ; Decl.  $-55^{\circ} 16'$

13.031	294.5	3.65	8.1	3	300
13.088	292.2	3.82	7.7	2	300
13.104	292.4	3.62	8.1	2	300
13.07	293.0	3.70	(8.2 ... 8.3)		D

$h 4238$ ;  $-51^{\circ} 2543$ ; 9.2

A.R.  $9^h 39^m 14^s$ ; Decl.  $-51^{\circ} 22'$

17.474	54.1	19.39	13.0	$2\frac{1}{2}$	370
17.477	54.0	19.24	13.2	2	370
17.48	54.1	19.32	(9.4 ... 11.8)		N

(Sigue Continued.)

AC

17.474	241.5	18.49	13.1	$2\frac{1}{2}$	370
17.477	240.0	18.11	13.4	2	370
17.48	240.8	18.30	(9.4 ... 13.2)		N

$h 4240$ ;  $-59^{\circ} 1464$ ; 7.4

A.R.  $9^h 39^m 36^s$ ; Decl.  $-59^{\circ} 27'$

17.376	56.5	12.44	13.7	2	370
17.496	56.6	12.48	14.3	2	370
17.44	56.5	12.46	(8.0 ... 10.0)		F

$\Delta 80$ ;  $-48^{\circ} 2671 + 70$ ; 8.5 + 8.6

A.R.  $9^h 40^m 29^s$ ; Decl.  $-48^{\circ} 55'$

13.154	250.1	18.76	7.4	2	300
13.209	249.7	18.76	12.7	2	300
13.18	249.9	18.76	(8.0 ... 8.0)		65

$h 4245$ ;  $-45^{\circ} 4014$ ; 7.7

A.R.  $9^h 41^m 20^s$ ; Decl.  $-45^{\circ} 20'$

13.069	215.8	9.39	7.5	$2\frac{1}{2}$	300
13.077	215.1	9.39	8.7	3	300
13.195	215.7	9.45	8.1	2	300
13.11	215.5	9.41	(7.6 ... 9.2)		F

$h 4247$ ;  $-51^{\circ} 2616$ ; 8.9

A.R.  $9^h 42^m 37^s$ ; Decl.  $-51^{\circ} 28'$

17.384	83.1	6.54	14.2	$2\frac{1}{2}$	370
17.474	83.8	6.37	13.3	3	370
17.477	82.3	6.30	13.6	2	370
17.44	83.1	6.40	(9.0 ... 9.5)		66

$h 4251$ ;  $-60^{\circ} 1500$ ; 8.4

A.R.  $9^h 43^m 58^s$ ; Decl.  $-60^{\circ} 27'$

17.376	311.1	12.78	14.1	3	370
17.496	311.7	12.74	14.4	2	370
17.44	311.4	12.76	(9.2 ... 10.3)		?

BC; C = 11.7

17.376	330.7	17.19	14.0	$2\frac{1}{2}$	370
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$h 4252$ ; Véase la nota: See note 67

$h 4254$ ;  $u$  Velorum; 5.5 + 9.2

A.R.  $9^h 45^m 6^s$ ; Decl.  $-45^{\circ} 9'$

13.195	46.1	66.25	8.3	2	300
13.208	46.3	66.44	12.4	2	300
13.20	46.2	66.34	(5.8 ... 9.1)		N

$h$  4255;  $-58^\circ 1663$ ; 9.8A.R.  $9^h 45^m 28^s$ ; Decl.  $-58^\circ 7'$ 

13.088	78.2	9.51	8.4	2½	300
13.104	78.0	9.56	8.3	2½	300
13.126	77.7	9.68	7.5	2	300
13.11	78.0	9.58	(9.5 ... 9.7)		N

 $h$  4257;  $-49^\circ 2848 + 50$ ;  $9.0 + 9.3$ A.R.  $9^h 45^m 50^s$ ; Decl.  $-49^\circ 36'$ 

13.050	120.7	19.40	7.9	3	300
13.066	120.5	19.62	7.3	2½	300
13.06	120.6	19.51	(9.4 ... 10.0)		N

C6.;  $-56^\circ 2569$ ; 8.6A.R.  $9^h 46^m 12^s$ ; Decl.  $-56^\circ 58'$ 

17.409	161.8	7.04	13.3	3	370
17.411	161.9	6.98	13.8	2	370
17.41	161.8	7.01	(8.8 ... 9.5)		7

 $h$  4260;  $-57^\circ 2367$ ; 7.8A.R.  $9^h 46^m 12^s$ ; Decl.  $-57^\circ 38'$ 

13.031	119.1	13.23	8.4	2½	300
13.088	118.9	13.03	8.0	2	300
13.06	119.0	13.13	(8.2 ... 9.9)		68

 $h$  4263;  $-59^\circ 1516$ ; 8.4A.R.  $9^h 48^m 8^s$ ; Decl.  $-59^\circ 51'$ 

17.376	71.1	11.72	14.3	3	370
17.512	71.4	11.87	14.0	2	370
17.44	71.2	11.79	(8.6 ... 9.8)		N

 $h$  4264;  $-50^\circ 2839$ ; 8.6A.R.  $9^h 48^m 51^s$ ; Decl.  $-50^\circ 55'$ 

17.384	206.9	9.40	14.3	3	370
17.474	207.6	9.20	13.4	3	370
17.477	207.3	9.18	13.8	2	370
17.44	207.3	9.26	(9.6 ... 9.8)		N

 $h$  4266;  $-51^\circ 2761$ ; 9.0:A.R.  $9^h 50^m 17^s$ ; Decl.  $-51^\circ 30'$ 

17.384	90.8	12.79	14.4	2½	370
17.474	90.4	12.76	13.5	2	370
17.43	90.6	12.78	(9.5 ... 10.0)		N

 $h$  4269;  $-47^\circ 3775$ ; 6.2A.R.  $9^h 52^m 55^s$ ; Decl.  $-47^\circ 49'$ 

13.026	320.3	14.19	8.6	3	300
13.050	321.4	13.91	8.4	3	300
13.066	320.8	13.91	7.5	2½	300
13.05	320.6	14.00	(6.5 ... 9.4)		69

 $h$  4273;  $-44^\circ 4416$ ; 7.2A.R.  $9^h 54^m 27^s$ ; Decl.  $-44^\circ 21'$ 

13.020	135.3	15.49	7.8	3	300
13.023	134.9	15.61	8.6	3	300
13.02	135.1	15.55	(7.1 ... 9.4)		N

 $h$  4274;  $-49^\circ 2987 + 5$ ;  $9.0 + 9.3$ A.R.  $9^h 54^m 44^s$ ; Decl.  $-49^\circ 25'$ 

13.050	349.0	18.64	8.2	3	300
13.066	350.1	18.72	7.4	3	300
13.06	349.6	18.68	(9.5 ... 9.8)		N

 $h$  4278;  $-58^\circ 1766 + 5$ ;  $8.6 + 9.2$ A.R.  $9^h 55^m 42^s$ ; Decl.  $-58^\circ 40'$ 

17.376	308.3	15.67	14.6	2	370
17.512	308.6	15.65	14.3	3	370
17.44	308.5	15.69	(8.6 ... 9.3)		N

AC

17.376	4.6	22.73	14.5	2	370
17.512	4.9	22.88	14.4	3	370
17.44	4.8	22.81	(8.6 ... 11.9)		N

 $\Delta$  83;  $-54^\circ 3043 + 1$ ;  $8.6 + 8.0$ A.R.  $9^h 57^m 35^s$ ; Decl.  $-54^\circ 23'$ 

13.088	224.0	110.46	8.7	2½	300
13.110	224.1	110.71	7.1	3	300
13.10	224.1	110.59	(8.1 ... 8.2)		F

 $h$  4282;  $-51^\circ 2924 + 3$ ;  $8.0 + 8.3$ A.R.  $9^h 58^m 31^s$ ; Decl.  $-51^\circ 27'$ 

17.072	199.4	47.81	12.1	2	370
17.384	199.0	47.56	14.5	2	370
17.477	199.3	47.60	13.9	2	370
17.31	199.2	47.66	(7.9 ... 8.7)		R

 $h$  4283;  $-51^\circ 2938$ ; 7.7A.R.  $9^h 59^m 47^s$ ; Decl.  $-51^\circ 12'$ 

17.066	182.0	8.11	8.0	3	370
17.072	180.7	8.02	12.2	2	370
17.384	180.8	7.92	14.5	2	370
17.17	181.2	8.02	(7.7 ... 9.3)		F

 $h$  4284;  $-45^\circ 4362$ ; 7.8A.R.  $10^h 0^m 6^s$ ; Decl.  $-45^\circ 17'$ 

13.023	67.4	6.88	8.7	3	300
13.034	65.2	6.71	7.4	3	300
13.036	65.1	6.59	7.7	3	300
13.03	65.9	6.73	(7.8 ... 9.1)		20

*h* 4290;  $-45^{\circ} 4430$ ; 7.5

A.R.  $10^h 5^m 6^s$ ; Decl.  $-45^{\circ} 10'$

13.020	311.5	15.12	8.0	2½	300
13.023	311.9	15.26	8.9	3	300
13.034	311.6	15.07	7.5	2½	300
13.03	311.7	15.15	(7.9 ... 9.4)		N

*h* 4291;  $-58^{\circ} 1950$ ; 10.0

A.R.  $10^h 5^m 13^s$ ; Decl.  $-58^{\circ} 13'$

13.148	222.2	8.85	9.1	3	300
13.154	222.8	8.62	7.9	2	300
13.178	223.0	8.90	8.1	2	666
13.16	222.7	8.69	(10.0 ... 10.3)		N

*h* 4294; Anon.

A.R.  $10^h 5^m 30^s$ ; Decl.  $-72^{\circ} 38'$

17.239	270.0	6.30	13.8	2½	370
17.277	269.3	6.09	12.9	3	370
17.332	270.4	5.89	13.6	2	370
17.28	269.9	6.09	(10.8 ... 11.2)		N

*h* 4297;  $-54^{\circ} 3269$ ; 8.8

A.R.  $10^h 7^m 33^s$ ; Decl.  $-54^{\circ} 30'$

13.121	303.3	11.14	7.8	2	300
13.126	303.5	10.97	7.8	2½	300
13.12	303.4	11.05	(9.0 ... 9.5)		F?

*h* 4299;  $-50^{\circ} 3185 + 4$ ; 8.7 + 8.4

A.R.  $10^h 8^m 30^s$ ; Decl.  $-50^{\circ} 17'$

17.066	327.2	31.20	8.2	2½	370
17.072	327.1	31.17	12.4	2	370
17.07	327.2	31.19	(8.4 ... 9.0)		N

*h* 4302;  $-57^{\circ} 2909$ ; 9.9

A.R.  $10^h 12^m 21^s$ ; Decl.  $-57^{\circ} 22'$

13.176	116.2	23.15	8.6	2½	666
13.178	116.0	23.49	8.5	2	666
13.18	116.1	23.32	(9.4 ... 10.2)		70

Rus 140;  $-55^{\circ} 3229$ ; 7.6

A.R.  $10^h 14^m 26^s$ ; Decl.  $-55^{\circ} 24'$

13.126	281.2	3.41	8.1	2	300
13.143	280.0	3.63	8.4	3	300
13.154	277.0	3.46	8.9	2	300
13.178	280.6	3.92	8.8	2	666
13.15	279.7	3.60	(8.1 ... 8.5)		F

*h* 4307;  $-50^{\circ} 3352$ ; 7.8

A.R.  $10^h 14^m 59^s$ ; Decl.  $-50^{\circ} 56'$

17.066	264.2	14.15	8.4	3	370
17.072	263.2	14.13	12.6	2	370
17.07	263.7	14.14	(7.5 ... 11.0)		R

BC = I 852

17.066	127.4	2.04	8.5	2½	370
17.277	126.6	2.16	13.9	3	370
17.17	127.0	2.10	(11.0 ... 12.7)		N

*h* 4308;  $-71^{\circ} 959 + 60$ ; 9.4 + 9.4

A.R.  $10^h 15^m 4^s$ ; Decl.  $-71^{\circ} 26'$

17.067	59.1	16.35	10.2	2½	370
17.239	59.3	16.33	14.3	2½	370
17.15	59.2	16.34	(9.4 ... 9.4)		F

AC

17.067	318.6	13.84	10.3	2½	370
17.239	318.4	14.18	14.1	2½	370
17.15	318.5	14.01	(9.4 ... 13.2)		N

Rü 13; *J* Velorum; 4.8

A.R.  $10^h 16^m 17^s$ ; Decl.  $-55^{\circ} 25'$

13.088	102.6	7.42	8.9	2	300
13.104	102.4	7.30	8.6	2	300
13.107	103.9	7.10	7.3	2	300
13.10	103.0	7.27	(5.0 ... 8.7)		F

AC

13.088	190.0	37.07	9.0	2	300
13.104	190.1	36.97	8.7	2	300
13.107	190.2	36.97	7.4	2	300
13.10	190.1	37.00	(5.0 ... 9.0)		F

*h* 4312;  $-47^{\circ} 4176$ ; 7.4

A.R.  $10^h 17^m 16^s$ ; Decl.  $-47^{\circ} 20'$

13.026	265.0	25.06	8.9	3	300
13.042	265.0	25.45	8.1	2½	300
13.063	265.4	25.18	7.7	3	300
13.04	265.1	25.23	(8.0 ... 9.3)		D

*h* 4315;  $-43^{\circ} 4634 + 3$ ; 9.2 + 9.6

A.R.  $10^h 18^m 17^s$ ; Decl.  $-43^{\circ} 30'$

13.020	210.3	26.28	8.4	3	300
13.023	210.1	26.44	9.2	3	300
13.02	210.2	26.36	(9.0 ... 9.6)		22

*h* 4316;  $-42^{\circ} 4586$ ; 8.0

A.R.  $10^h 18^m 52^s$ ; Decl.  $-42^{\circ} 7'$

13.239	237.3	13.35	8.1	2	300
13.244	237.2	13.13	12.5	3½	300
13.24	237.2	13.24	(8.2 ... 10.2)		N

$h$  4317;  $+45^\circ 4624 + 5$ ;  $9.6 + 10.2$ A.R.  $10^h 19^m 27^s$ ; Decl.  $-45^\circ 33'$ 

13.034	193.8	21.97	7.7	3	300
13.036	193.4	21.86	7.8	3	300
13.04	193.6	21.91	(8.2 ... 9.0)		N

Aguilar 9;  $57^\circ 3143$ ;  $9.0$ A.R.  $10^h 19^m 51^s$ ; Decl.  $-57^\circ 52'$ 

17.409	41.1	2.28	13.5	3	370
17.512	38.2	2.23	14.7	$2\frac{1}{2}$	370
17.46	39.7	2.26	(9.3 ... 11.2)		7

 $h$  4319;  $-53^\circ 3793$ ;  $7.8$ :A.R.  $10^h 21^m 23^s$ ; Decl.  $-53^\circ 15'$ 

17.066	122.8	12.12	8.7	$2\frac{1}{2}$	370
17.075	122.5	12.00	11.9	3	370
17.07	122.6	12.06	(7.2 ... 11.8)		N

Rus 146;  $-54^\circ 3642$ ;  $8.2$ :A.R.  $10^h 21^m 34^s$ ; Decl.  $-54^\circ 51'$ 

13.126	96.8	14.90	8.3	3	300
13.143	97.0	14.75	8.5	$2\frac{1}{2}$	300
13.13	96.9	14.82	(8.4 ... 8.6)		D

 $h$  4320;  $-49^\circ 3467$ ;  $8.4$ A.R.  $10^h 22^m 2^s$ ; Decl.  $-49^\circ 2'$ 

13.050	341.9	18.59	8.7	3	300
13.064	341.9	18.62	7.0	3	300
13.06	341.9	18.60	(8.8 ... 9.8)		N

 $\Delta$  85 =  $h$  4323;  $-61^\circ 1677 + 6$ ;  $8.7 + 8.6$ A.R.  $10^h 24^m 30^s$ ; Decl.  $-61^\circ 57'$ 

17.266	220.2	21.83	13.3	$2\frac{1}{2}$	370
17.493	220.0	21.83	14.5	2	370
17.38	220.1	21.83	(8.8 ... 9.2)		F

 $h$  4324;  $-46^\circ 4573$ ;  $8.2$ A.R.  $10^h 24^m 52^s$ ; Decl.  $-46^\circ 43'$ 

13.047	244.7	8.26	8.0	3	300
13.064	245.2	8.43	8.0	3	300
13.066	245.2	8.57	7.7	3	300
13.06	245.0	8.42	(9.0 ... 9.1)		D

 $h$  4327;  $-53^\circ 3899 + 3900$ ;  $8.8 + 9.0$ A.R.  $10^h 25^m 52^s$ ; Decl.  $-53^\circ 51'$ 

17.066	171.8	114.05	8.9	$2\frac{1}{2}$	370
17.277	171.5	114.08	14.0	3	370
17.17	171.6	114.07	(8.2 ... 8.8)		F

C6.;  $-45^\circ 4714$ ;  $9.5$ A.R.  $10^h 25^m 56^s$ ; Decl.  $-45^\circ 31'$ 

13.036	327.1	7.08	7.9	3	300
13.039	326.6	7.16	7.6	3	300
13.04	326.8	7.12	(9.4 ... 9.5)		23

 $h$  4328;  $-51^\circ 3358 + 60$ ;  $9.5 + 10.0$ A.R.  $10^h 26^m 14^s$ ; Decl.  $-51^\circ 14'$ 

16.990	110.7	17.39	8.0	2	370
17.075	110.0	17.41	12.3	3	370
17.03	110.3	17.40	(9.9 ... 10.6)		M?

 $h$  4329; Y Velorum;  $6.4$ A.R.  $10^h 26^m 30^s$ ; Decl.  $-53^\circ 5'$ 

16.990	89.8	37.93	8.2	2	370
17.075	89.3	37.86	12.1	3	370
17.03	89.5	37.89	(6.0 ... 9.1)		R

 $h$  4330; t Velorum;  $7.3 + 8.5$ A.R.  $10^h 27^m 41^s$ ; Decl.  $-46^\circ 22'$ 

13.026	162.4	40.52	9.4	3	300
13.047	162.4	40.28	8.2	3	300
13.063	162.4	40.37	8.1	3	300
13.05	162.4	40.39	(6.0 ... 9.1)		71

 $h$  4333;  $-72^\circ 981$ ;  $7.7$ A.R.  $10^h 28^m 6^s$ ; Decl.  $-72^\circ 35'$ 

17.067	100.5	32.25	10.5	2	370
17.239	99.9	31.98	14.6	$2\frac{1}{2}$	370
17.15	100.2	32.11	(6.5 ... 12.5)		A

 $h$  4332;  $-46^\circ 4618 + 19$ ;  $7.8 + 9.2$ A.R.  $10^h 28^m 16^s$ ; Decl.  $-46^\circ 20'$ 

13.026	161.6	28.76	9.1	3	300
13.047	162.0	28.35	8.4	3	300
13.066	162.1	28.56	7.8	2	300
13.05	161.9	28.56	(8.0 ... 9.6)		F

Gilliss 147;  $-54^\circ 3795 + 7$ ;  $8.0 + 7.9$ A.R.  $10^h 28^m 23^s$ ; Decl.  $-54^\circ 44'$ 

13.154	29.8	26.14	9.1	2	300
13.178	30.3	26.33	9.0	2	666
13.184	30.1	26.34	7.7	2	666
13.17	30.1	26.27	(7.4 ... 8.0)		F

BC = Holden 106

13.154	251.3	1.72	9.2	2	300
13.178	249.4	1.81	9.2	2	666
13.184	254.2	1.98	7.8	2	666
13.187	252.4	1.76	7.2	2	666
13.18	251.8	1.82	(8.0 ... 8.7)		D

*h* 4338;  $-57^{\circ} 35'84''$ ; 7.9

A.R.  $10^{\text{h}} 32^{\text{m}} 36^{\text{s}}$ ; Decl.  $-57^{\circ} 58'$

13.187	91.2	5.36	7.6	2	666
13.211	89.2	5.51	14.3	2	300
13.228	89.9	5.48	12.6	2	300
13.21	90.1	5.45	(8.1 ... 8.8)		N

Dawson 5; Anon.

A.R.  $10^{\text{h}} 32^{\text{m}} 40^{\text{s}}$ ; Decl.  $-58^{\circ} 0'$

13.187	346.0	4.19	7.7	2	666
13.228	342.2	4.16	12.8	2	300
13.244	342.7	4.19	12.8	3	666
13.22	343.6	4.18	(10.8 ... 11.3)		

$\Delta$  94;  $t^2$  Carinae; 7.3

A.R.  $10^{\text{h}} 34^{\text{m}} 0^{\text{s}}$ ; Decl.  $-58^{\circ} 32'$

17.266	20.2	14.58	13.7	2½	370
17.318	19.7	14.50	10.4	3	370
17.29	19.9	14.54	(5.3 ... 9.2)		R

Gilliss 152 = Rus 153;  $-58^{\circ} 24'74''$ , 5; 8.4, 8.6

A.R.  $10^{\text{h}} 34^{\text{m}} 14^{\text{s}}$ ; Decl.  $-58^{\circ} 10'$

13.307	74.7	20.77	12.7	2	300
13.310	75.4	20.73	12.9	2½	300
13.31	75.1	20.75	(6.8 ... 8.6)		R

$\Delta$  95;  $-54^{\circ} 39'15'' + 16''$ ; 5.8 + 6.8

A.R.  $10^{\text{h}} 34^{\text{m}} 24^{\text{s}}$ ; Decl.  $-54^{\circ} 57'$

13.088	105.3	51.99	9.1	2	300
13.121	105.6	52.16	8.3	2	300
13.10	105.5	52.08	(5.5 ... 7.0)		F

BC = *h* 4341

13.121	177.3	20.29	8.5	2	300
13.154	175.3	20.18	9.3	2	300
13.14	176.3	20.23	(7.0 ... 11.2)		N

*h* 4344;  $-72^{\circ} 9'97'' + 8''$ ; 9.1 + 9.2

A.R.  $10^{\text{h}} 34^{\text{m}} 38^{\text{s}}$ ; Decl.  $-72^{\circ} 56'$

17.277	106.3	20.98	13.2	3	370
17.332	106.6	21.09	13.8	2	370
17.384	106.5	20.86	14.7	2	370
17.33	106.5	20.98	(9.2 ... 9.3)		72

Có.;  $-58^{\circ} 25'24'' + 3''$ ; 8.7 + 9.4

A.R.  $10^{\text{h}} 35^{\text{m}} 48^{\text{s}}$ ; Decl.  $-58^{\circ} 53'$

13.468	274.9	17.29	13.0	3½	300
13.471	274.6	17.30	12.5	3	300
13.47	274.8	17.29	(8.3 ... 9.7)		73

*h* 4345 = I 859;  $-53^{\circ} 40'60''$ ; 8.3

A.R.  $10^{\text{h}} 36^{\text{m}} 22^{\text{s}}$ ; Decl.  $-53^{\circ} 27'$

17.066	1.4	5.38	9.2	2½	370
17.075	0.3	5.18	12.5	3	370
17.277	1.1	5.26	14.4	2½	370
17.14	0.9	5.27	(8.4 ... 11.6)		R

*h* 4347;  $-59^{\circ} 24'78''$ ; 8.4

A.R.  $10^{\text{h}} 37^{\text{m}} 22^{\text{s}}$ ; Decl.  $-59^{\circ} 15'$

13.189	304.7	3.40	7.6	2	280
13.228	304.4	3.58	13.2	2	666
13.244	304.3	3.46	14.0	3	666
13.22	304.5	3.48	(8.6 ... 9.8)		73

*h* 4348 =  $\lambda$  122;  $-59^{\circ} 24'79''$ ; 8.9

A.R.  $10^{\text{h}} 37^{\text{m}} 25^{\text{s}}$ ; Decl.  $-59^{\circ} 19'$

13.195	348.8	3.85	14.0	2	300
13.228	350.1	3.94	13.5	2	666
13.244	350.3	3.84	14.1	3	666
13.22	349.7	3.88	(9.3 ... 9.9)		R

AC

13.468	256.2	13.59	13.1	3½	300
13.471	256.8	13.67	12.8	3	300
13.47	256.5	13.63	(9.3 ... 10.9)		73

*h* 4350;  $-59^{\circ} 25'18''$ ; 8.9

A.R.  $10^{\text{h}} 38^{\text{m}} 24^{\text{s}}$ ; Decl.  $-59^{\circ} 5'$

13.195	148.6	10.93	14.2	2	300
13.228	149.1	11.14	13.8	2	666
13.247	149.0	11.10	12.8	3	300
13.22	148.9	11.06	(9.2 ... 10.7)		N

*h* 4353;  $-58^{\circ} 26'08''$ ; 9.7

A.R.  $10^{\text{h}} 38^{\text{m}} 52^{\text{s}}$ ; Decl.  $-58^{\circ} 56'$

13.195	180.1	5.09	14.4	2	300
13.228	180.2	5.00	14.1	1½	666
13.247	180.3	5.20	13.2	2	300
13.310	180.2	5.07	13.3	2½	300
13.25	180.2	5.09	(10.2 ... 10.9)		N

*h* 4354;  $-59^{\circ} 25'40''$ ; 8.8

A.R.  $10^{\text{h}} 39^{\text{m}} 0^{\text{s}}$ ; Decl.  $-59^{\circ} 26'$

13.195	221.0	10.04	14.6	2	300
13.244	219.3	10.13	14.2	3	666
13.247	219.2	10.15	13.4	2½	300
13.23	219.8	10.11	(9.5 ... 10.1)		73

$h$  4355;  $-59^\circ 25'42'' + 7$ ;  $9.3 + 9.7$

A.R.  $10^h 39^m 2^s$ ; Decl.  $-59^\circ 18'$

13.195	78.2	15.29	14.8	2	300
13.209	78.1	14.97	13.7	2	300
13.244	78.5	14.78	14.3	3	666
13.21	78.3	15.01	(9.5 ... 9.8)		N

Có.;  $-58^\circ 26'17$ ; 8.4

A.R.  $10^h 39^m 4^s$ ; Decl.  $-58^\circ 54'$

13.468	241.3	6.71	13.2	3	300
13.471	241.1	6.59	12.8	3	300
13.47	241.2	6.65	(9.1 ... 10.1)		73

$h$  4356;  $-58^\circ 26'18$ ; 8.4:

A.R.  $10^h 39^m 6^s$ ; Decl.  $-58^\circ 54'$

13.195	151.4	2.82	15.0	2	666
13.209	149.4	2.99	14.0	2	300
13.244	149.7	2.86	15.0	3	666
13.22	150.2	2.89	(7.6 ... 9.1)		F

$\lambda$  123;  $-58^\circ 26'20$ ; 9.2

A.R.  $10^h 39^m 10^s$ ; Decl.  $-58^\circ 53'$

13.468	311.2	4.11	13.5	3	300
13.471	308.3	3.90	12.9	2½	300
13.487	309.1	4.22	13.6	2½	300
13.48	309.5	4.08	(9.6 ... 11.9)		73

$h$  4357;  $-59^\circ 25'56$ ; 8.3

A.R.  $10^h 39^m 12^s$ ; Decl.  $-59^\circ 13'$

13.209	156.3	12.17	13.9	2	300
13.244	156.6	12.39	14.5	3	666
13.293	156.3	12.42	8.9	2	300
13.25	156.4	12.33	(8.3 ... 11.5)		N

$h$  4358;  $-59^\circ 25'55$ ; 8.6

A.R.  $10^h 39^m 12^s$ ; Decl.  $-59^\circ 26'$

13.195	236.3	6.20	15.4	2	300
13.209	236.3	6.56	13.3	2	300
13.244	235.5	6.39	14.6	3	666
13.329	235.2	6.24	9.4	3	300
13.24	235.8	6.35	(8.8 ... 10.0)		74

Dawson 6;  $-59^\circ 25'54$ ; 8.7

A.R.  $10^h 39^m 13^s$ ; Decl.  $-59^\circ 27'$

13.244	113.4	3.08	14.8	3	666
13.247	113.8	3.21	14.0	2½	300
13.296	116.5	2.86	12.6	3	300
13.310	111.9	3.26	13.5	2	666
13.27	113.9	3.10	(8.9 ... 12.3)		

(*Sigue* *Continued.*)

AC =  $h$  4359

13.209	194.95	8.03	13.4	2	300
13.244	193.9	8.06	14.7	3	666
13.247	193.6	8.09	13.7	2½	300
13.23	194.0	8.06	(8.9 ... 10.3)		74

$-58^\circ 26'31$ ; 7.8

A.R.  $10^h 39^m 18^s$ ; Decl.  $-58^\circ 55'$

A,BC = Brisbane

13.195	107.6	13.77	15.3	2	300
13.244	108.5	13.64	15.1	3	666
13.293	108.5	13.63	9.1	2	300
13.24	108.2	13.68	(7.6 ... 7.9)		F

BC =  $h$  4360

13.195	113.5	2.06	15.1	2	666
13.244	113.9	1.97	15.2	3	666
13.293	114.5	2.06	9.3	2	300
13.24	114.0	2.03	(8.5 ... 8.5)		20

$h$  4361;  $-59^\circ 25'62$ ; 9.2

A.R.  $10^h 39^m 23^s$ ; Decl.  $-59^\circ 16'$

13.209	124.0	14.45	13.6	2	300
13.244	125.5	14.28	15.4	3	666
13.293	124.5	14.21	9.6	2	300
13.25	124.7	14.31	(9.8 ... 11.5)		N

Dawson 7;  $-59^\circ 25'69$ ; 9.5

A.R.  $10^h 39^m 28^s$ ; Decl.  $-59^\circ 28'$

13.296	11.1	3.35	12.8	3	300
13.310	10.3	[3.80]	13.8	2	666
13.315	9.5	3.36	12.5	3	666
13.329	9.1	3.28	9.6	3	300
13.31	10.0	3.33	(10.1 ... 10.5)		

Dawson 8;  $-59^\circ 25'72$ ; 7.0

A.R.  $10^h 39^m 34^s$ ; Decl.  $-59^\circ 20'$

13.296	276.1	6.94	13.0	3	300
13.315	276.8	6.98	12.7	3	300
13.329	278.2	7.27	10.0	2½	300
13.31	277.0	7.06	(7.1 ... 13.0)		

Brisbane;  $-59^\circ 25'87 + 4$ ; 8.6 + 8.6

A.R.  $10^h 39^m 45^s$ ; Decl.  $-59^\circ 5'$

13.209	213.9	19.11	14.2	2	300
13.244	213.5	18.99	15.7	3	666
13.329	214.3	18.84	10.2	2	300
13.26	213.9	18.96	(8.2 ... 8.5)		F



*h* 4363;  $-59^{\circ} 2594 + 3$ ;  $9.3 + 9.4$

A.R.  $10^h 39^m 49^s$ ; Decl.  $-59^{\circ} 22'$

13.209	195.8	12.81	14.4	2	300
13.244	195.8	12.69	15.5	3	666
13.310	195.7	12.76	14.1	2	300
13.25	195.8	12.75	(9.7 ... 9.9)		N

*h* 4362;  $-43^{\circ} 4922 + 3$ ;  $9.0 + 9.4$

A.R.  $10^h 39^m 51^s$ ; Decl.  $-43^{\circ} 3'$

13.069	123.0	25.36	7.7	3	300
13.077	123.1	25.31	8.9	3	300
13.07	123.0	25.34	(9.5 ... 9.6)		F

*h* 4364;  $-58^{\circ} 2659$ ;  $8.2$ :

A.R.  $10^h 39^m 52^s$ ; Decl.  $-58^{\circ} 42'$

13.209	351.7	7.92	14.5	2	300
13.247	352.7	8.09	15.2	2	300
13.310	351.4	7.94	14.3	2	300
13.26	351.9	7.98	(8.8 ... 9.4)		20

AC; C = 10.0

13.209	149.4	8.79	14.6	2	300
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$\eta$  Argûs;  $8.4 (+ 8.6 + 9.2)$

A.R.  $10^h 40^m 13^s$ ; Decl.  $-59^{\circ} 2'$

AB = *h* 4366

13.209	60.2	13.77	14.8	2	300
13.293	60.2	13.50	10.1	2	300
13.315	61.0	13.50	13.0	3	300
13.27	60.5	13.59	(- ... 10.3)		

AC = *h* 4366

13.209	41.2	14.18	15.0	2	300
13.293	41.1	13.65	10.2	2	300
13.315	41.1	13.82	12.9	3	300
13.27	41.1	13.88	(- ... 10.1)		

AD = Powell

13.460	67.7	38.48	15.0	2	300
13.466	67.6	38.49	14.6	3	300
13.46	67.6	38.48	(- ... 9.8)		

AE =  $\Delta$  98

13.460	17.1	61.15	14.8	2	300
13.466	17.0	61.10	14.4	3	300
13.46	17.0	61.12	(- ... 8.6)		75

*h* 4367;  $-55^{\circ} 3807?$ ;  $9.1$

A.R.  $10^h 40^m 17^s$ ; Decl.  $-55^{\circ} 46'$

13.154	164.5	4.97	9.5	2	300
13.184	165.7	5.12	8.1	2	666
13.211	165.2	4.92	14.7	2	300
13.18	165.1	5.00	(9.5 ... 9.6)		22

Có.;  $-59^{\circ} 2635 + 3$ ;  $9.1 + 9.1$

A.R.  $10^h 40^m 22^s$ ; Decl.  $-59^{\circ} 5'$

13.468	194.6	14.53	13.7	3	300
13.471	194.2	14.73	13.1	3	300
13.474	194.6	14.60	15.1	3½	300
13.47	194.5	14.62	(9.2 ... 9.3)		73

$\Delta$  99;  $-70^{\circ} 1183 + 5 + 4$ ;  $7.2, 7.3, 9.4$

A.R.  $10^h 40^m 34^s$ ; Decl.  $-70^{\circ} 12'$

17.067	74.6	63.05	10.8	2½	370
17.332	74.5	63.09	14.2	2	370
17.23	74.7	63.04	(7.0 ... 6.9)		

AC

17.067	41.9	39.88	10.7	2½	370
17.277	41.9	39.88	13.3	3	370
17.23	41.8	39.92	(7.0 ... 10.5)		

BC

17.277	291.4	36.59	13.5	3	370
17.332	290.7	36.63	14.3	2	370
17.23	290.9	36.58	(6.9 ... 10.5)		76

*h* 4368;  $-42^{\circ} 4859$ ;  $9.8$

A.R.  $10^h 40^m 49^s$ ; Decl.  $-42^{\circ} 49'$

13.077	108.5	5.02	9.1	3	300
13.258	109.8	4.98	8.5	3	300
13.433	110.8	5.19	13.8	2	300
13.26	109.7	5.06	(10.1 ... 11.0)		77

*h* 4369;  $-58^{\circ} 2683 + 5$ ;  $9.0 + 9.5$

A.R.  $10^h 40^m 58^s$ ; Decl.  $-58^{\circ} 50'$

13.209	40.7	14.51	15.3	2	300
13.310	41.0	—	14.5	2½	300
13.315	41.4	14.11	13.1	3	300
13.348	43.7	14.04	9.8	2	300
13.29	41.7	14.22	(7.6 ... 10.1)		73

*h* 4370;  $-58^{\circ} 2690 + 89$ ;  $9.3 + 9.4$

A.R.  $10^h 41^m 14^s$ ; Decl.  $-58^{\circ} 54'$

13.209	208.2	26.18	15.5	2	300
13.315	208.2	25.94	13.2	3	300
13.348	208.1	26.17	9.9	2	300
13.29	208.2	26.10	(9.6 ... 9.7)		N

Rus 156;  $-58^{\circ} 2692$ ;  $8.0$

A.R.  $10^h 41^m 20^s$ ; Decl.  $-58^{\circ} 40'$

13.307	30.6	2.06	13.3	2	300
13.315	30.8	1.96	13.4	2½	666
13.329	29.5	1.81	10.5	3	666
13.348	29.3	2.01	10.1	2	300
13.32	30.0	1.96	(8.5 ... 8.6)		F

Rus 155;  $\mu$  Argús; 4.9A.R.  $10^h 41^m 24^s$ ; Decl.  $-48^\circ 46'$ 

14.328	64.05	2.15	12.8	2	370
14.334	67.6	2.23	12.5	2	370
14.336	63.3	2.21	9.9	4	650
14.33	65.1	2.20	(2.6 ... 6.5)		C

 $h$  4371;  $-58^\circ 2698 + 2700$ ; 9.2 + 9.9A.R.  $10^h 41^m 44^s$ ; Decl.  $-58^\circ 53'$ 

13.209	33.8	20.56	15.7	2	300
13.315	33.1	20.38	13.7	3	300
13.348	32.3	20.46	10.3	2 $\frac{1}{2}$	300
13.29	33.1	20.47	(8.7 ... 10.3)		N

C6.;  $-59^\circ 2696 + 2700$ ; 8.8 + 9.6A.R.  $10^h 42^m 21^s$ ; Decl.  $-59^\circ 26'$ 

13.468	127.2	16.74	13.9	3	300
13.471	127.3	16.80	13.3	2 $\frac{1}{2}$	300
13.47	127.2	16.77	(8.9 ... 10.3)		73

Dawson 9;  $-59^\circ 2702$ ; 9.3A.R.  $10^h 42^m 24^s$ ; Decl.  $-59^\circ 26'$ 

13.468	269.5	5.17	14.1	3	300
13.471	267.8	5.24	13.6	2 $\frac{1}{2}$	300
13.487	270.2	5.24	13.9	2	300
13.48	269.2	5.22	(10.0 ... 11.9)		78

## AC = C6.—

13.468	275.8	8.67	14.0	3	300
13.471	275.4	8.57	13.5	2 $\frac{1}{2}$	300
13.487	275.4	8.75	13.8	2 $\frac{1}{2}$	300
13.48	275.5	8.66	(10.0 ... 10.6)		73

Dawson 10;  $-43^\circ 4955$ ; 8.4A.R.  $10^h 43^m 29^s$ ; Decl.  $-43^\circ 8'$ 

13.039	110.6	5.51	7.9	3	300
13.069	109.0	5.51	8.0	2 $\frac{1}{2}$	300
13.077	108.9	5.97	9.3	3	300
13.258	110.1	5.61	8.6	3	300
13.11	109.6	5.65	(9.0 ... 9.2)		

 $h$  4374;  $-58^\circ 2747$ ; 8.0A.R.  $10^h 43^m 59^s$ ; Decl.  $-58^\circ 47'$ 

13.209	119.0	13.79	15.8	2	300
13.315	120.1	13.69	13.8	2 $\frac{1}{2}$	300
13.348	118.7	14.04	10.5	2	300
13.460	119.5	13.66	15.2	2	300
13.33	119.3	13.80	(8.0 ... 9.9)		73

Rus 161;  $-58^\circ 2755$ ; 5.9A.R.  $10^h 44^m 27^s$ ; Decl.  $-58^\circ 40'$ 

13.315	267.4	1.42	14.1	2 $\frac{1}{2}$	666
13.329	273.3	1.22	10.6	2	666
13.466	271.9	1.23	14.8	3	666
13.468	270.9	1.22	14.3	3	666
13.39	271.8	1.27	(7.2 ... 8.1)		P

 $h$  4377;  $-72^\circ 1039$ ; 9.4A.R.  $10^h 45^m 38^s$ ; Decl.  $-72^\circ 57'$ 

17.277	282.8	6.45	13.6	3	370
17.332	283.8	6.24	14.0	2	370
17.384	284.1	6.21	14.8	2	370
17.33	283.6	6.30	(10.0 ... 12.3)		N

 $u$  Carinae; 5.6 + 6.4 + 8.9A.R.  $10^h 48^m 24^s$ ; Decl.  $-58^\circ 11'$  $\Delta$  102 =  $-58^\circ 2834 + 0$ 

17.376	201.7	153.81	15.1	3	370
17.469	201.8	153.95	15.2	2	370
17.42	201.7	153.88	(4.7 ... 6.4)		79

 $\Delta$  103 =  $-58^\circ 2834 + 6$ 

17.376	10.4	61.60	15.0	3	370
17.469	10.8	61.38	15.3	2	370
17.42	10.6	61.49	(4.7 ... 8.2)		R

 $h$  4379;  $-48^\circ 3599 + 3601$ ; 8.8 + 9.8A.R.  $10^h 48^m 32^s$ ; Decl.  $-48^\circ 40'$ 

13.047	51.2	24.32	8.7	3	300
13.066	51.4	24.35	8.0	1 $\frac{1}{2}$	300
13.06	51.3	24.34	(9.0 ... 10.1)		N

 $h$  4383;  $-70^\circ 1246$ ; 6.4A.R.  $10^h 49^m 35^s$ ; Decl.  $-70^\circ 3'$ 

17.067	284.6	1.57	11.0	2 $\frac{1}{2}$	475
17.075	285.4	1.51	12.8	3	650
17.159	284.0	[1.96]	14.8	2	370
17.239	284.1	1.56	14.9	3	370
17.13	284.5	1.55	(6.7 ... 7.4)		F

C6. = Hu 1478;  $-57^\circ 3974$ ; 8.6A.R.  $10^h 49^m 47^s$ ; Decl.  $-57^\circ 54'$ 

17.409	329.5	5.82	13.8	3	370 79a
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 $h$  4387;  $-56^\circ 4016 + 17$ ; 7.8 + 10.0A.R.  $10^h 51^m 14^s$ ; Decl.  $-56^\circ 53'$ 

13.154	152.4	23.54	9.7	2	300
13.187	152.7	23.77	9.0	2	280
13.17	152.5	23.65	(8.0 ... 9.5)		N

*h* 4386;  $-52^{\circ} 4039$ ; 9.4

A.R.  $10^{\text{h}} 51^{\text{m}} 18^{\text{s}}$ ; Decl.  $-52^{\circ} 50'$

17.066	17.25	9.29	9.4	2½	370
17.075	17.2	9.11	12.6	3	370
17.277	17.2	9.29	14.5	3	370
17.14	17.3	9.23	(10.2 ... 11.4)		80

BC

17.334	243.6	8.91	14.6	2½	370
17.376	243.0	—	15.7	2	370
17.463	243.7	8.86	15.6	2	370
17.589	245.8	8.79	16.0	2	370
17.44	244.0	8.85	(11.0 ... 11.5)		N

*h* 4388;  $-45^{\circ} 5062$ ; 7.5

A.R.  $10^{\text{h}} 52^{\text{m}} 2^{\text{s}}$ ; Decl.  $-45^{\circ} 12'$

13.034	208.1	35.38	8.7	3	300
13.036	206.7	34.93	8.6	3	300
13.039	207.5	35.57	8.6	3	300
13.069	208.1	35.43	8.1	2½	300
13.04	207.6	35.39	(7.5 ... 10.6)		N

*h* 4398;  $-56^{\circ} 4117$ ; 8.4

A.R.  $10^{\text{h}} 56^{\text{m}} 26^{\text{s}}$ ; Decl.  $-56^{\circ} 36'$

13.107	249.7	7.77	8.4	2	300
13.110	249.6	7.86	8.5	2	300
13.121	250.3	7.76	8.8	2	300
13.11	249.9	7.80	(8.6 ... 9.4)		F

*h* 4392;  $-70^{\circ} 1260 + 1$ ; 8.3 + 8.3

A.R.  $10^{\text{h}} 52^{\text{m}} 54^{\text{s}}$ ; Decl.  $-70^{\circ} 41'$

17.159	157.6	24.87	14.9	2	370
17.239	157.7	24.99	15.2	2½	370
17.20	157.7	24.93	(8.3 ... 8.4)		A?

*h* 4399;  $-59^{\circ} 2964$ ; 8.6

A.R.  $10^{\text{h}} 57^{\text{m}} 14^{\text{s}}$ ; Decl.  $-59^{\circ} 51'$

17.334	309.3	8.81	14.8	2½	370
17.463	309.9	8.90	15.3	2	370
17.589	309.8	8.90	16.1	2	370
17.46	309.7	8.87	(9.1 ... 9.4)		F

*h* 4394;  $-42^{\circ} 4991 + 0$ ; 8.6 + 9.4

A.R.  $10^{\text{h}} 53^{\text{m}} 41^{\text{s}}$ ; Decl.  $-42^{\circ} 28'$

13.034	260.2	28.66	8.9	3	300
13.036	260.9	28.56	8.9	3	300
13.039	260.7	28.44	8.2	3	300
13.04	260.6	28.55	(8.5 ... 9.3)		N

Aguilar 10;  $-57^{\circ} 4141$ ; 8.6

A.R.  $10^{\text{h}} 57^{\text{m}} 56^{\text{s}}$ ; Decl.  $-57^{\circ} 43'$

17.409	200.9	9.02	13.9	3	370
17.428	199.9	9.26	15.6	1½	370
17.463	200.2	9.00	15.0	2	370
17.43	200.3	9.09	(8.7 ... 11.3)		7

*h* 4395; Anon.

A.R.  $10^{\text{h}} 54^{\text{m}} 50^{\text{s}}$ ; Decl.  $-59^{\circ} 40'$

17.334	0.5	9.36	14.2	2½	370
17.589	1.3	9.30	15.7	2	370
17.46	0.9	9.33	(12.2 ... 12.5)		81

*h* 4401;  $-54^{\circ} 4294$ ; 9.8

A.R.  $10^{\text{h}} 59^{\text{m}} 21^{\text{s}}$ ; Decl.  $-54^{\circ} 34'$

13.154	229.8	14.70	10.0	2	300
13.187	229.6	14.63	9.2	2	280
13.17	229.7	14.67	(9.6 ... 9.9)		N

*h* 4397 a;  $-59^{\circ} 2944$ ; 9.4

A.R.  $10^{\text{h}} 56^{\text{m}} 10^{\text{s}}$ ; Decl.  $-59^{\circ} 10'$

17.334	116.3	7.71	14.4	2	370
17.376	116.9	7.68	15.4	3	370
17.35	116.6	7.69	(10.5 ... 13.2)		N

$\Delta$  105;  $-60^{\circ} 2505$ ; 7.6:

A.R.  $10^{\text{h}} 59^{\text{m}} 45^{\text{s}}$ ; Decl.  $-60^{\circ} 23'$

17.334	221.4	23.88	15.0	2	370
17.463	221.5	24.14	15.8	2	370
17.469	221.4	23.95	15.5	2	370
17.42	221.4	23.99	(7.8 ... 9.8)		N

*h* 4397 b;  $-59^{\circ} 2945$ ; 9.6:

A.R.  $10^{\text{h}} 56^{\text{m}} 10^{\text{s}}$ ; Decl.  $-59^{\circ} 11'$

17.334	260.7	7.68	14.5	2	370
17.376	259.7	—	15.6	2	370
17.463	259.1	7.08	15.4	2	370
17.589	261.6	7.65	15.9	2	370
17.44	260.3	7.47	(10.8 ... 11.0)		N

(Sigue Continued.)

Dawson 11;  $-58^{\circ} 3055$ ; 8.7

A.R.  $10^{\text{h}} 59^{\text{m}} 59^{\text{s}}$ ; Decl.  $-58^{\circ} 24'$

17.409	23.3	4.03	14.2	3	370
17.463	24.3	3.97	15.1	2	370
17.592	25.4	[4.35]	15.9	1	370
17.594	24.0	3.93	16.1	2	370
17.51	24.2	3.98	(8.9 ... 12.5)		

C6.; —57° 4235; 8.5

A.R. 11<sup>h</sup> 0<sup>m</sup> 14<sup>s</sup>; Decl. —57° 57'

17.409	356.9	8.26	14.1	3	370
17.430	356.4	8.52	14.2	1½	370
17.42	356.7	8.39	(8.6 ... 9.5)		7

*h* 4404; —58° 3099; 8.4A.R. 11<sup>h</sup> 0<sup>m</sup> 53<sup>s</sup>; Decl. —58° 1'

13.212	296.4	8.53	15.4	2	300
13.296	297.5	8.43	15.1	2½	300
13.316	297.0	8.47	15.3	3	300
13.27	297.0	8.48	(9.7 ... 10.1)		N

*h* 4405; —52° 4217; 7.9A.R. 11<sup>h</sup> 1<sup>m</sup> 0<sup>s</sup>; Decl. —52° 36'

17.064	48.2	19.23	11.0	2	370
17.277	48.2	19.26	14.7	2	370
17.17	48.2	19.25	(8.3 ... 10.4)		N

*h* 4403; —43° 5152; 8.2A.R. 11<sup>h</sup> 1<sup>m</sup> 1<sup>s</sup>; Decl. —43° 23'

13.034	256.7	15.46	9.2	3	300
13.036	257.2	15.21	9.2	3	300
13.039	256.6	15.49	8.9	3	300
13.04	256.8	15.39	(8.6 ... 10.5)		N

*h* 4407; —43° 5153; 8.9A.R. 11<sup>h</sup> 1<sup>m</sup> 12<sup>s</sup>; Decl. —43° 22'

13.034	293.9	27.41	9.4	3	300
13.036	294.0	27.24	9.4	3	300
13.039	294.8	27.44	9.1	3	300
13.04	294.2	27.36	(9.2 ... 10.1)		N

*h* 4411; —52° 4251; 10.0A.R. 11<sup>h</sup> 3<sup>m</sup> 4<sup>s</sup>; Decl. —52° 19'

17.066	260.9	7.34	9.7	2½	370
17.277	262.9	7.38	14.8	2	370
17.332	262.5	6.96	14.7	2	370
17.22	262.1	7.23	(11.2 ... 11.7)		N

*h* 4414; *γ* Carinae; 5.1A.R. 11<sup>h</sup> 7<sup>m</sup> 12<sup>s</sup>; Decl. —59° 38'

17.463	276.7	21.72	16.0	2	370
17.594	277.5	21.98	16.3	2	370
17.605	278.2	21.97	16.0	3	370
17.55	277.5	21.89	(5.0 ... 11.2)		F

Rus 165; —46° 5201; 7.5

A.R. 11<sup>h</sup> 7<sup>m</sup> 19<sup>s</sup>; Decl. —46° 22'

13.047	63.5	3.33	8.9	3	300
13.075	65.2	3.53	7.8	2	300
13.077	63.7	3.36	9.5	3	300
13.07	64.1	3.41	(8.3 ... 8.3)		20

*h* 4416; —70° 1339; 9.6:A.R. 11<sup>h</sup> 7<sup>m</sup> 31<sup>s</sup>; Decl. —70° 45'

17.159	169.5	14.72	15.1	2	370
17.239	169.9	14.61	15.5	3	370
17.20	169.7	14.66	(10.5 ... 11.9)		82

*h* 4417; —54° 4397; 9.0A.R. 11<sup>h</sup> 7<sup>m</sup> 56<sup>s</sup>; Decl. —54° 45'

13.102	146.4	19.82	9.1	3	300
13.107	147.4	19.79	8.6	3	300
13.10	146.9	19.81	(9.0 ... 9.9)		D?

*h* 4420; —56° 4340; 9.3A.R. 11<sup>h</sup> 9<sup>m</sup> 22<sup>s</sup>; Decl. —56° 50'

13.102	286.2	7.15	9.2	3	300
13.107	287.3	7.33	9.0	3	300
13.121	286.0	7.15	9.3	2	300
13.11	286.5	7.21	(9.1 ... 10.2)		142

*h* 4421; —47° 4886; 7.4A.R. 11<sup>h</sup> 10<sup>m</sup> 7<sup>s</sup>; Decl. —47° 14'

13.047	67.0	23.51	9.1	3	300
13.075	66.9	23.17	8.0	2	300
13.077	67.0	23.30	9.6	3	300
13.07	67.0	23.33	(7.1 ... 10.1)		D?

*h* 4423; —45° 5338; 7.7A.R. 11<sup>h</sup> 10<sup>m</sup> 40<sup>s</sup>; Decl. —45° 12'

13.017	277.7	2.37	9.4	2	300
13.020	276.7	2.45	8.7	3	300
13.023	278.1	2.59	9.5	3	300
13.02	277.5	2.47	(7.2 ... 7.6)		D

*h* 4426; —42° 5246; 7.6A.R. 11<sup>h</sup> 15<sup>m</sup> 42<sup>s</sup>; Decl. —42° 52'

13.020	173.7	13.25	9.1	3	300
13.023	174.1	13.30	9.7	3	300
13.02	173.9	13.28	(7.6 ... 10.2)		N

*h* 4429;  $-59^{\circ} 3389$ ; 8.4

A.R.  $11^{\text{h}} 16^{\text{m}} 18^{\text{s}}$ ; Decl.  $-59^{\circ} 18'$

17.463	150.7	9.10	16.1	2½	370
17.597	151.0	9.29	16.3	2	370
17.605	150.2	8.99	16.2	3	370
17.56	150.6	9.13	(8.9 ... 11.1)		N

*h* 4431;  $-54^{\circ} 4499$ ; 9.4

A.R.  $11^{\text{h}} 16^{\text{m}} 50^{\text{s}}$ ; Decl.  $-54^{\circ} 20'$

13.176	222.9	12.93	9.0	2	666
13.184	222.8	12.89	8.6	2	280
13.18	222.9	12.91	(9.6 ... 10.4)		21

AC

13.176	16.3	7.30	9.4	2	666
13.316	15.9	7.16	15.5	3	300
13.433	12.5	7.15	14.8	1½	300
13.28	15.4	7.21	(9.6 ... 12.7)		N

Brisbane;  $-60^{\circ} 2911$ ; 8.7

A.R.  $11^{\text{h}} 19^{\text{m}} 15^{\text{s}}$ ; Decl.  $-60^{\circ} 58'$

17.384	82.0	1.90	15.2	3	370
17.597	84.5	2.06	16.4	2	370
17.605	84.9	1.73	16.3	3	370
17.608	83.9	2.02	16.4	3	370
17.55	83.8	1.93	(8.0 ... 9.3)		B

Rus 171;  $46^{\circ} 5361$ ; 8.2

A.R.  $11^{\text{h}} 19^{\text{m}} 45^{\text{s}}$ ; Decl.  $-46^{\circ} 48'$

13.274	346.2	2.74	8.3	2½	300
13.288	342.6	2.99	8.5	2	300
13.460	341.8	2.94	15.6	2½	300
13.34	343.5	2.89	(8.6 ... 11.4)		F

*h* 4434;  $-54^{\circ} 4538$ ; 8.8

A.R.  $11^{\text{h}} 20^{\text{m}} 45^{\text{s}}$ ; Decl.  $-54^{\circ} 47'$

13.102	249.9	13.67	9.9	3	300
13.107	250.2	13.67	9.5	2	300
13.10	250.0	13.67	(8.9 ... 10.2)		22

*h* 4435;  $-50^{\circ} 4233 + 2$ ; 8.6 + 9.0

A.R.  $11^{\text{h}} 21^{\text{m}} 0^{\text{s}}$ ; Decl.  $-50^{\circ} 2'$

13.266	190.9	18.05	9.5	2	300
13.271	188.7	17.74	8.9	2½	300
13.274	187.7	17.78	8.4	2½	300
13.27	189.1	17.86	(8.9 ... 11.2)		N

AC

13.266	300.7	28.73	9.3	2	300
13.271	301.2	28.61	8.7	2½	300
13.27	301.0	28.67	(8.9 ... 9.1)		N

*h* 4436;  $-54^{\circ} 4543 + 2$ ; 9.4 + 10.0

A.R.  $11^{\text{h}} 21^{\text{m}} 11^{\text{s}}$ ; Decl.  $-54^{\circ} 10'$

13.178	357.9	14.38	9.7	2	666
13.184	359.0	13.96	8.8	2	280
13.296	358.0	13.75	15.3	2	300
13.313	359.4	13.62	16.9	2½	300
13.24	358.6	13.93	(9.2 ... 10.7)		N

Brisbane;  $-41^{\circ} 5379$ ; 5.7

A.R.  $11^{\text{h}} 22^{\text{m}} 34^{\text{s}}$ ; Decl.  $-41^{\circ} 59'$

13.017	167.2	13.13	9.7	2	300
13.020	167.6	13.21	9.2	3	300
13.02	167.4	13.17	(5.9 ... 8.0)		F

Rus 172;  $-55^{\circ} 4402 + 3$ ; 9.0 + 9.4

A.R.  $11^{\text{h}} 23^{\text{m}} 32^{\text{s}}$ ; Decl.  $-55^{\circ} 15'$

13.178	105.9	26.61	10.2	2	666
13.184	106.9	26.39	8.9	2	280
13.18	106.4	26.50	(9.3 ... 9.4)		F

AC

13.178	34.1	12.61	10.4	2	666
13.184	37.3	11.69	9.0	2	280
13.296	35.6	12.01	15.5	2	300
13.313	32.9	12.12	17.1	2½	300
13.26	34.7	12.09	(9.3 ... 11.6)		N

*h* 4441;  $-55^{\circ} 4408$ ; 9.3:

A.R.  $11^{\text{h}} 23^{\text{m}} 56^{\text{s}}$ ; Decl.  $-55^{\circ} 11'$

13.178	179.1	10.38	10.0	2	666
13.184	178.5	10.51	9.1	2	280
13.18	178.8	10.45	(9.2 ... 10.5)		D?

*h* 4442;  $-53^{\circ} 4587$ ; 8.8

A.R.  $11^{\text{h}} 24^{\text{m}} 18^{\text{s}}$ ; Decl.  $-53^{\circ} 59'$

13.296	229.3	3.78	15.9	2	300
13.313	230.4	3.62	17.3	2½	300
13.316	230.0	3.68	15.9	3	300
14.334	229.4	3.75	12.9	2½	370
14.336	229.1	3.07	10.1	4	370
14.375	229.3	3.51	10.9	3	370
14.396	230.4	3.50	12.9	3	370
13.31	229.9	3.69			N
14.36	229.5	3.46	(9.3 ... 10.2)		7

*h* 4444;  $-47^{\circ} 5055$ ; 9.0

A.R.  $11^{\text{h}} 25^{\text{m}} 28^{\text{s}}$ ; Decl.  $-47^{\circ} 59'$

13.050	137.8	12.18	9.6	3	300
13.271	135.5	12.15	9.3	2½	300
13.16	136.7	12.17	(9.5 ... 10.1)		N

*h* 4445 = I 77;  $\alpha^1$  Centauri; 7.2A.R. 11<sup>h</sup> 26<sup>m</sup> 0<sup>s</sup>; Decl. -58° 45'

17.463	125.2	13.78	16.3	2	370
17.597	125.0	13.78	16.5	2	370
17.603	125.5	13.65	15.8	2	370
17.55	125.2	13.74	(5.1 ... 11.4)		N

*h* 4446; -51° 4266; 8.6A.R. 11<sup>h</sup> 26<sup>m</sup> 2<sup>s</sup>; Decl. -51° 46'

17.064	298.4	10.47	11.2	2	370
17.277	297.5	10.49	15.0	2	370
17.17	298.0	10.48	(9.1 ... 9.2)		F?

*h* 4450 = *h* 4458; -73° 864; 7.2A.R. 11<sup>h</sup> 26<sup>m</sup> 40<sup>s</sup>; Decl. -73° 13'

17.067	40.0	20.89	11.4	2	370
17.159	40.3	21.17	15.3	1½	370
17.239	39.7	20.99	15.8	2½	370
17.15	40.0	21.02	(7.2 ... 10.7)		83

*h* 4448; -43° 5461; 7.7A.R. 11<sup>h</sup> 26<sup>m</sup> 50<sup>s</sup>; Decl. -43° 0'

13.017	89.3	7.79	10.0	2	300
13.020	87.2	7.95	9.3	3	300
13.023	89.4	7.77	10.0	3	300
13.02	88.6	7.84	(8.0 ... 9.6)		N

*h* 4451; -45° 5517; 8.6A.R. 11<sup>h</sup> 27<sup>m</sup> 33<sup>s</sup>; Decl. -45° 37'

13.069	263.7	23.61	8.4	2	300
13.195	263.5	23.34	9.4	2	300
13.13	263.6	23.48	(9.0 ... 11.5)		84

*h* 4453; -48° 4071; 9.2A.R. 11<sup>h</sup> 28<sup>m</sup> 21<sup>s</sup>; Decl. -48° 44'

13.050	123.8	10.90	9.4	3	300
13.271	122.1	10.92	9.5	2	300
13.16	123.0	10.91	(9.6 ... 9.8)		N

Rus 173; -46° 5443; 9.2

A.R. 11<sup>h</sup> 31<sup>m</sup> 25<sup>s</sup>; Decl. -46° 15'

13.271	149.1	4.38	9.9	2	300
13.274	150.6	4.31	8.7	2	300
13.277	153.5	4.11	8.9	2	300
13.288	151.5	4.14	8.7	2	300
13.28	151.2	4.24	(9.5 ... 10.3)		D?

*h* 4459; -48° 4105 + 6; 9.4 + 9.6A.R. 11<sup>h</sup> 31<sup>m</sup> 50<sup>s</sup>; Decl. -48° 14'

13.050	163.0	12.84	9.8	3	300
13.271	162.7	13.18	9.7	2½	300
13.274	162.8	12.86	8.6	2½	300
13.20	162.8	12.96	(9.9 ... 10.1)		N

*h* 4460; -57° 4894; 7.6A.R. 11<sup>h</sup> 33<sup>m</sup> 14<sup>s</sup>; Decl. -57° 3'

13.296	176.8	8.72	16.2	2	300
13.313	176.7	8.63	17.5	2	300
13.316	176.6	8.72	16.6	3	300
13.31	176.7	8.69	(7.8 ... 8.9)		F

*h* 4464; -42° 5449; 8.2A.R. 11<sup>h</sup> 34<sup>m</sup> 23<sup>s</sup>; Decl. -42° 28'

13.020	159.6	10.90	9.6	3	300
13.023	159.3	10.66	10.2	3	300
13.02	159.4	10.78	(9.1 ... 9.9)		N

HdA.; -60° 3248; 8.1

A.R. 11<sup>h</sup> 35<sup>m</sup> 15<sup>s</sup>; Decl. -60° 27'

17.474	328.4	1.24	15.7	3	650
17.605	325.6	0.98	16.5	3	650
17.608	324.5	1.17	17.0	3	650
17.56	326.2	1.13	(7.5 ... 7.8)		

Rus 175; -60° 3252; 9.4

A.R. 11<sup>h</sup> 35<sup>m</sup> 30<sup>s</sup>; Decl. -60° 18'

17.474	11.9	7.00	15.4	3	370
17.597	8.3	6.99	16.7	2	370
17.608	11.5	6.85	17.1	3½	370
17.56	10.6	6.95	(10.2 ... 11.7)		85

Rus 176; -60° 3254; 8.6

A.R. 11<sup>h</sup> 35<sup>m</sup> 36<sup>s</sup>; Decl. -60° 18'

17.474	313.5	2.17	15.5	3	370
17.597	312.5	1.93	16.8	2	370
17.605	312.8	2.35	16.8	3	650
17.56	312.9	2.15	(9.5 ... 10.9)		85

*h* 4467; -46° 5483 + 4; 9.1 + 10.2A.R. 11<sup>h</sup> 37<sup>m</sup> 27<sup>s</sup>; Decl. -46° 25'

13.271	142.9	15.82	10.1	2	300
13.274	142.0	16.02	8.9	2	300
13.27	142.5	15.92	(9.4 ... 9.9)		N

Rus 177 = Hargrave 70;  $-46^{\circ} 54'93''$ ; 8.5

A.R.  $11^{\text{h}} 39^{\text{m}} 26^{\text{s}}$ ; Decl.  $-46^{\circ} 32'$

13.271	153.5	3.90	10.2	2	300
13.274	155.2	4.06	9.0	2	300
13.277	156.2	4.06	9.0	2	300
13.27	155.0	4.01	(8.5 ... 9.3)		20

$-48^{\circ} 42'20''$ ; 9.1

A.R.  $11^{\text{h}} 41^{\text{m}} 52^{\text{s}}$ ; Decl.  $-48^{\circ} 20'$

A,BC = *h* 4473

13.050	108.3	15.53	10.1	3	300
13.274	109.2	15.68	9.2	2	300
13.16	108.7	15.60	(9.4 ... 11.0)		N

BC = Dawson 12

13.460	121.5	2.43	15.9	$2\frac{1}{2}$	300
13.468	120.9	2.74	14.7	3	300
13.471	119.1	3.02	14.0	3	300
13.512	119.9	2.67	15.8	2	666
13.47	120.4	2.72	(11.9 ... 11.9)		86

*h* 4474;  $-53^{\circ} 47'72''$ ; 8.9

A.R.  $11^{\text{h}} 42^{\text{m}} 18^{\text{s}}$ ; Decl.  $-53^{\circ} 28'$

17.064	98.2	17.70	11.4	$2\frac{1}{2}$	370
17.239	98.5	17.50	16.3	3	370
17.15	98.4	17.60	(9.1 ... 11.4)		N

Rus 176a;  $-60^{\circ} 33'65''$ ; 8.9

A.R.  $11^{\text{h}} 42^{\text{m}} 38^{\text{s}}$ ; Decl.  $-60^{\circ} 52'$

17.463	326.0	6.12	16.6	$2\frac{1}{2}$	370
17.603	325.1	6.05	16.0	2	370
17.633	324.6	5.73	17.6	$1\frac{1}{2}$	370
17.57	325.2	5.97	(8.8 ... 10.9)		85

*h* 4475;  $-60^{\circ} 33'73''$ ; 9.2

A.R.  $11^{\text{h}} 42^{\text{m}} 55^{\text{s}}$ ; Decl.  $-60^{\circ} 45'$

17.463	125.4	4.80	16.7	2	370
17.603	127.3	4.32	16.1	2	370
17.53	126.4	4.56	(10.2 ... 11.0)		85

*h* 4476;  $-47^{\circ} 51'81''$ ; 10.1

A.R.  $11^{\text{h}} 43^{\text{m}} 17^{\text{s}}$ ; Decl.  $-47^{\circ} 34'$

13.274	170.1	19.77	9.4	2	300
13.277	170.0	19.62	9.2	2	300
13.28	170.0	19.69	(9.5 ... 10.2)		N

*h* 4480;  $-53^{\circ} 48'32''$ ; 8.6

A.R.  $11^{\text{h}} 48^{\text{m}} 22^{\text{s}}$ ; Decl.  $-53^{\circ} 59'$

13.140	5.1	6.83	9.0	3	300
13.148	5.7	6.94	9.6	3	300
13.157	6.4	6.84	10.3	3	300
13.15	5.7	6.87	(9.0 ... 9.9)		N

Có. = Holden 114;  $-55^{\circ} 47'11''$ ; 7.6

A.R.  $11^{\text{h}} 48^{\text{m}} 43^{\text{s}}$ ; Decl.  $-55^{\circ} 24'$

13.140	194.2	2.55	9.1	3	300
13.148	194.1	2.53	9.4	3	300
13.14	194.1	2.54	(8.0 ... 8.2)		11

*h* 4482;  $-43^{\circ} 56'08''$ ; 7.5

A.R.  $11^{\text{h}} 51^{\text{m}} 30^{\text{s}}$ ; Decl.  $-43^{\circ} 1'$

13.036	289.9	22.95	9.8	3	300
13.039	290.0	22.52	9.9	3	300
13.261	289.9	22.49	9.2	2	300
13.433	290.0	23.22	14.2	2	300
13.19	289.9	22.80	(7.9 ... 11.9)		N

*h* 4483;  $-70^{\circ} 14'47''$ ; 9.1:

A.R.  $11^{\text{h}} 51^{\text{m}} 34^{\text{s}}$ ; Decl.  $-70^{\circ} 40'$

17.064	109.2	11.05	11.8	2	370
17.067	109.2	10.96	11.6	$2\frac{1}{2}$	370
17.07	109.2	11.00	(9.9 ... 10.0)		F?

*h* 4491;  $-43^{\circ} 56'38'' + 9''$ ;  $8.0 + 9.0$

A.R.  $11^{\text{h}} 57^{\text{m}} 21^{\text{s}}$ ; Decl.  $-43^{\circ} 26'$

13.036	40.6	23.57	10.0	3	300
13.039	40.4	23.37	10.1	3	300
13.04	40.5	23.47	(8.2 ... 8.5)		N

*h* 4492;  $-54^{\circ} 49'35''$ ; 8.1

A.R.  $11^{\text{h}} 57^{\text{m}} 23^{\text{s}}$ ; Decl.  $-54^{\circ} 1'$

17.064	273.8	15.93	11.6	$2\frac{1}{2}$	370
17.239	272.8	15.93	16.5	3	370
17.15	273.3	15.93	(8.4 ... 11.9)		N

*h* 4493;  $-55^{\circ} 48'28''$ ; 8.8

A.R.  $11^{\text{h}} 58^{\text{m}} 13^{\text{s}}$ ; Decl.  $-55^{\circ} 55'$

13.140	95.6	10.10	10.0	3	300
13.148	95.7	10.04	9.9	3	300
13.157	95.0	10.14	10.4	3	300
13.15	95.4	10.09	(9.2 ... 9.9)		N

AC

13.157	313.1	15.26	10.5	3	300
13.176	311.6	15.29	9.8	2	666
13.17	312.4	15.28	(9.2 ... 12.3)		N

*h* 4494;  $-49^{\circ} 48'28'' + 7''$ ;  $8.4 + 9.7$

A.R.  $11^{\text{h}} 59^{\text{m}} 30^{\text{s}}$ ; Decl.  $-49^{\circ} 9'$

13.274	71.0	12.86	9.7	2	300
13.288	70.9	13.11	9.2	$1\frac{1}{2}$	300
13.460	71.5	12.86	16.1	$2\frac{1}{2}$	300
13.34	71.1	12.94	(9.3 ... 9.3)		N

(Sigue Continued.)

## AC

13.274	1.3	21.75	9.8	1½	300
13.288	0.8	21.80	9.3	1½	300
13.460	0.6	21.59	16.3	2½	300
13.34	0.9	21.71	(9.3 ... 10.6)		N

 $h$  4497;  $-47^\circ 5338$ ; 10.0A.R.  $11^h 59^m 43^s$ ; Decl.  $-47^\circ 4'$ 

13.271	320.8	11.30	10.5	2	300
13.274	322.1	11.10	10.1	1½	300
13.27	321.4	11.20	(10.0 ... 11.8)		M

Jacob 147;  $\delta$  Centauri; 3.7 + 5.0 + 6.8A.R.  $12^h 1^m 53^s$ ; Decl.  $-50^\circ 2'$ 

13.468	325.1	268.46	15.1	3	300
13.471	324.9	268.80	14.4	3	300
13.47	325.0	268.63	(1.3 ... 3.8)		87

## AC

13.468	227.0	216.37	15.4	3	300
13.471	226.7	216.72	14.6	3	300
13.47	226.9	216.55	(1.3 ... 6.3)		

 $h$  4503;  $-58^\circ 4133$ ; 8.8A.R.  $12^h 4^m 12^s$ ; Decl.  $-58^\circ 7'$ 

13.151	246.2	8.09	10.2	2	300
13.157	245.8	8.11	10.6	3	300
13.184	244.8	8.14	10.4	2	280
13.16	245.6	8.11	(9.3 ... 10.1)		N

Delavan 4;  $-54^\circ 5046$ ; 9.0A.R.  $12^h 6^m 11^s$ ; Decl.  $-54^\circ 39'$ 

14.334	276.4	7.13	13.4	2½	370
14.336	274.4	7.01	10.2	4	370
14.375	275.0	7.14	11.3	3	370
14.35	275.3	7.09	(9.3 ... 9.9)		7

 $h$  4507;  $-44^\circ 5880 + 79$ ; 8.8 + 9.0A.R.  $12^h 6^m 22^s$ ; Decl.  $-44^\circ 12'$ 

13.020	222.1	16.10	9.8	2½	300
13.036	223.1	16.02	10.3	3	300
13.039	222.6	16.27	10.3	3	300
13.03	222.6	16.13	(8.6 ... 9.2)		D

Rü 14;  $D$  Centauri; 7.5A.R.  $12^h 7^m 31^s$ ; Decl.  $-45^\circ 2'$ 

13.020	244.2	3.56	10.0	2½	300
13.023	244.0	3.23	10.6	3	300
13.036	244.8	3.09	10.4	3½	300
13.039	245.2	3.04	10.5	3	300
13.03	244.6	3.18	(6.9 ... 7.9)		F

 $h$  4508;  $-55^\circ 4936$ ; 8.6A.R.  $12^h 8^m 15^s$ ; Decl.  $-55^\circ 6'$ 

13.151	33.5	24.15	10.6	2	300
13.157	33.5	23.88	10.7	3	300
13.15	33.5	24.01	(8.6 ... 9.1)		F

 $h$  4511;  $-54^\circ 5103$ ; 8.6A.R.  $12^h 11^m 24^s$ ; Decl.  $-54^\circ 50'$ 

13.151	297.4	9.01	10.9	2½	300
13.157	296.1	8.96	10.9	3	300
13.184	297.2	9.24	10.5	2	280
13.16	296.9	9.07	(9.2 ... 9.7)		F?

 $h$  4520;  $-52^\circ 5564 + 5$ ; 9.2 + 9.4A.R.  $12^h 17^m 40^s$ ; Decl.  $-52^\circ 9'$ 

17.271	219.3	35.65	11.9	3	370
17.332	219.8	35.78	14.9	2	370
17.30	219.5	35.71	(9.4 ... 9.7)		N

Brisbane;  $-57^\circ 5451$ ; 7.6A.R.  $12^h 18^m 0^s$ ; Decl.  $-57^\circ 26'$ 

13.017	333.8	5.51	10.7	2½	300
13.107	333.3	5.63	10.2	2½	300
13.121	334.6	5.44	10.2	2½	300
13.123	334.7	5.29	9.5	2	300
13.132	333.8	5.44	9.4	3	300
13.10	334.0	5.48	(8.2 ... 8.4)		N

 $\alpha$  Crucis; 2.4A.R.  $12^h 19^m 38^s$ ; Decl.  $-62^\circ 24'$ AB =  $\Delta$  123

13.031	118.1	5.07	10.3	2½	300
13.176	117.7	5.04	10.3	2	666
13.247	116.8	5.00	11.0	3	300
13.316	117.7	5.02	17.3	3	300
13.323	117.3	5.04	11.2	3	666
13.22	117.5	5.03	(1.7 ... 2.1)		F

AC =  $\Delta$  122

13.031	202.1	90.50	10.8	2½	300
13.247	201.7	90.15	11.3	3	300
13.316	202.0	90.01	17.5	2½	300
13.323	201.9	89.93	11.3	3	300
13.23	201.9	90.15	(1.7 ... 6.1)		F

 $h$  4523 = Rus 199;  $-56^\circ 5242$ ; 8.8A.R.  $12^h 20^m 3^s$ ; Decl.  $-56^\circ 55'$ 

13.107	273.0	6.61	10.3	3	300
13.121	273.8	6.79	10.3	2½	300
13.132	273.6	6.62	10.0	2½	300
13.12	273.5	6.67	(9.7 ... 9.9)		A?



*h* 4524;  $-59^{\circ} 4237 + 6$ ;  $8.7 + 9.9$

A.R.  $12^{\text{h}} 21^{\text{m}} 12^{\text{s}}$ ; Decl.  $-59^{\circ} 21'$

17.518	338.5	31.06	16.2	2	370
17.526	338.2	31.03	15.5	2	370
17.584	338.1	31.09	16.6	2	370
17.54	338.3	31.06	(8.6 ... 10.3)		N

*h* 4525;  $-57^{\circ} 5513$ ;  $9.6$

A.R.  $12^{\text{h}} 22^{\text{m}} 48^{\text{s}}$ ; Decl.  $-57^{\circ} 10'$

13.107	102.2	[7.64]	10.5	$2\frac{1}{2}$	300
13.151	102.6	8.20	11.1	2	300
13.184	101.2	8.03	10.9	$1\frac{1}{2}$	280
13.195	103.0	8.21	10.4	$2\frac{1}{2}$	300
13.16	102.3	8.15	(9.4 ... 11.4)		22

*h* 4526;  $-52^{\circ} 5649 + 8$ ;  $9.1 + 9.4$

A.R.  $12^{\text{h}} 24^{\text{m}} 11^{\text{s}}$ ; Decl.  $-52^{\circ} 30'$

17.271	258.2	16.27	12.0	3	370
17.332	258.4	16.35	15.1	2	370
17.30	258.3	16.31	(9.6 ... 9.8)		88

AC; C = 10.0

17.271	7.4	30.78	12.1	3	370
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$\Delta$  124;  $\gamma$  Crucis;  $4.8 + 7.3$

A.R.  $12^{\text{h}} 24^{\text{m}} 14^{\text{s}}$ ; Decl.  $-56^{\circ} 25'$

13.110	31.7	109.16	9.9	3	300
13.121	31.8	109.22	9.8	2	300
13.12	31.8	109.19	(2.0 ... 7.5)		R

*h* 4531;  $-51^{\circ} 5313 + 14$ ;  $9.6 + 9.6$

A.R.  $12^{\text{h}} 29^{\text{m}} 7^{\text{s}}$ ; Decl.  $-51^{\circ} 31'$

17.272	21.1	16.06	12.2	$3\frac{1}{2}$	370
17.332	21.6	16.26	15.4	2	370
17.30	21.3	16.16	(10.0 ... 10.5)		A?

AC

17.272	64.8	6.22	12.3	$3\frac{1}{2}$	370
17.332	63.7	6.26	15.5	2	370
17.30	64.3	6.24	(10.0 ... 12.7)		N

*h* 4534 = Rus 204;  $-57^{\circ} 5606 + 7$ ;  $9.2 + 9.2$

A.R.  $12^{\text{h}} 31^{\text{m}} 12^{\text{s}}$ ; Decl.  $-57^{\circ} 26'$

13.110	100.4	15.73	10.3	3	300
13.121	100.0	15.65	9.9	2	300
13.12	100.2	15.69	(9.2 ... 9.3)		F?

*h* 4536;  $-44^{\circ} 6028$ ;  $9.2$

A.R.  $12^{\text{h}} 32^{\text{m}} 22^{\text{s}}$ ; Decl.  $-44^{\circ} 5'$

13.020	103.4	17.29	10.3	3	300
13.036	103.1	17.27	10.6	$3\frac{1}{2}$	300
13.03	103.2	17.28	(9.4 ... 10.5)		N

*h* 4539;  $\gamma$  Centauri;  $3.6$

A.R.  $12^{\text{h}} 34^{\text{m}} 38^{\text{s}}$ ; Decl.  $-48^{\circ} 16'$

13.245	168.8	1.28	16.4	3	666
13.247	169.5	1.42	15.6	2	666
13.458	171.2	1.65	16.7	2	666
13.460	166.4	1.64	16.7	$2\frac{1}{2}$	666
13.471	167.8	1.67	15.3	$2\frac{1}{2}$	666
13.471	167.9	1.45	15.6	$2\frac{1}{2}$	666
13.512	169.2	1.64	16.3	2	666
13.578	168.8	1.13	16.5	3	666
13.583	—	1.40	16.8	2	666
17.075	165.4	0.98	12.9	3	650
17.266	344.4	0.95	14.0	$2\frac{1}{2}$	650
17.271	346.3	0.97	11.6	3	650
13.45	348.6	1.42			88a
17.20	345.4	0.97	(3.10 ... 3.15)		B

*h* 4543;  $-58^{\circ} 4453$ ;  $8.3$

A.R.  $12^{\text{h}} 36^{\text{m}} 17^{\text{s}}$ ; Decl.  $-58^{\circ} 13'$

13.178	95.5	30.80	10.9	2	666
13.187	97.0	31.36	10.3	$2\frac{1}{2}$	280
13.195	96.3	31.24	10.7	2	300
13.19	96.3	31.13	(7.2 ... 9.3)		N

Rus 206;  $-55^{\circ} 5203 + 2$ ;  $9.2 + 9.3$

A.R.  $12^{\text{h}} 37^{\text{m}} 10^{\text{s}}$ ; Decl.  $-55^{\circ} 12'$

13.187	274.9	16.88	10.5	2	280
13.195	274.0	16.63	11.0	2	300
13.19	274.4	16.75	(9.2 ... 9.6)		

*h* 4546;  $-52^{\circ} 5847$ ;  $7.4$ :

A.R.  $12^{\text{h}} 37^{\text{m}} 49^{\text{s}}$ ; Decl.  $-52^{\circ} 4'$

17.272	221.9	15.03	12.4	$3\frac{1}{2}$	370
17.332	222.8	15.02	15.7	2	370
17.30	222.3	15.03	(8.0 ... 9.9)		F?

*h* 4547;  $-60^{\circ} 4273$ ;  $7.6$

A.R.  $12^{\text{h}} 38^{\text{m}} 18^{\text{s}}$ ; Decl.  $-60^{\circ} 18'$

17.526	29.8	26.70	15.8	$1\frac{1}{2}$	370
17.584	28.6	26.55	16.7	2	370
17.633	28.4	26.65	17.7	$1\frac{1}{2}$	370
17.58	28.9	26.63	(6.8 ... 10.1)		R

Rus 207;  $\beta$  Muscae;  $4.1$

A.R.  $12^{\text{h}} 38^{\text{m}} 38^{\text{s}}$ ; Decl.  $-67^{\circ} 25'$

17.266	352.6	1.31	14.3	$2\frac{1}{2}$	650
17.272	353.7	1.37	16.8	$2\frac{1}{2}$	650
17.277	355.1	1.28	12.4	3	650
17.321	352.0	1.24	11.5	$2\frac{1}{2}$	650
17.28	353.4	1.30	(3.1 ... 3.8)		B

*h* 4548;  $-55^{\circ} 52'15'' + 16$ ;  $5.0 + 8.6$

A.R.  $12^{\text{h}} 39^{\text{m}} 14^{\text{s}}$ ; Decl.  $-55^{\circ} 48'$

13.110	168.06	52.69	10.6	$2\frac{1}{2}$	300
13.121	168.8	52.58	10.6	$2\frac{1}{2}$	300
13.12	168.7	52.64	(5.2 ... 8.5) R		

Rus 208;  $-55^{\circ} 52'23''$ ;  $9.3$

A.R.  $12^{\text{h}} 39^{\text{m}} 54^{\text{s}}$ ; Decl.  $-55^{\circ} 6'$

13.348	8.4	4.63	11.0	2	300
13.359	9.4	4.31	10.7	2	300
13.433	8.5	4.46	16.5	2	300
13.38	8.8	4.47	(9.5 ... 10.0)		

*h* 4552;  $-46^{\circ} 59'9'' + 3$ ;  $8.8 + 9.2$

A.R.  $12^{\text{h}} 44^{\text{m}} 14^{\text{s}}$ ; Decl.  $-46^{\circ} 11'$

13.045	313.3	28.39	10.8	3	300
13.064	313.4	28.71	10.2	3	300
13.067	313.9	28.59	10.3	3	300
13.06	313.5	28.56	(8.8 ... 9.3) F?		

*h* 4555;  $-42^{\circ} 60'21''$ ;  $7.4$

A.R.  $12^{\text{h}} 46^{\text{m}} 37^{\text{s}}$ ; Decl.  $-42^{\circ} 24'$

13.036	304.8	22.61	11.0	3	300
13.039	304.4	23.00	10.7	3	300
13.214	303.3	22.66	16.0	2	300
13.10	304.2	22.76	(7.9 ... 11.3) N		

$\Delta$  126; *p*. Crucis;  $4.1$ :

A.R.  $12^{\text{h}} 47^{\text{m}} 16^{\text{s}}$ ; Decl.  $-56^{\circ} 30'$

13.110	17.4	34.96	10.4	3	300
13.121	16.9	34.84	10.8	$2\frac{1}{2}$	300
13.140	17.6	34.99	10.4	3	300
13.12	17.3	34.93	(4.5 ... 5.7) F		

*h* 4557;  $-47^{\circ} 57'25'' + 4$ ;  $9.6 + 10.2$

A.R.  $12^{\text{h}} 48^{\text{m}} 15^{\text{s}}$ ; Decl.  $-47^{\circ} 43'$

13.050	338.8	16.54	11.2	3	300
13.064	338.0	16.39	10.5	$2\frac{1}{2}$	300
13.06	338.4	16.47	(9.5 ... 10.8) N		

HdA;  $-56^{\circ} 54'9''$ ;  $6.0$

A.R.  $12^{\text{h}} 48^{\text{m}} 36^{\text{s}}$ ; Decl.  $-56^{\circ} 10'$

13.140	315.2	28.61	10.9	3	300
13.148	315.1	29.13	10.8	3	300
13.151	314.8	29.10	11.3	2	300
13.15	315.0	28.95	(6.2 ... 9.8)		

Dawson 13;  $-47^{\circ} 57'44''$ ;  $8.0$

A.R.  $12^{\text{h}} 50^{\text{m}} 14^{\text{s}}$ ; Decl.  $-47^{\circ} 58'$

13.050	134.05	5.12	10.6	3	300
13.064	133.9	4.95	10.3	$2\frac{1}{2}$	300
13.067	132.2	4.98	10.4	3	300
13.06	133.5	5.02	(8.4 ... 9.8)		

*h* 4562;  $-47^{\circ} 57'64''$ ;  $8.0$

A.R.  $12^{\text{h}} 52^{\text{m}} 24^{\text{s}}$ ; Decl.  $-47^{\circ} 51'$

13.045	72.3	11.34	11.0	3	300
13.064	72.4	11.37	10.8	$2\frac{1}{2}$	300
13.05	72.3	11.35	(8.9 ... 9.0) F?		

$\Delta$  127;  $-55^{\circ} 53'16'' + 17$ ;  $8.1 + 8.2$

A.R.  $12^{\text{h}} 52^{\text{m}} 26^{\text{s}}$ ; Decl.  $-55^{\circ} 14'$

13.110	125.7	16.76	11.0	3	300
13.148	126.3	16.81	10.9	3	300
13.13	126.0	16.79	(8.2 ... 8.4) F		

Cape 13;  $-47^{\circ} 57'74''$ ;  $7.7$

A.R.  $12^{\text{h}} 53^{\text{m}} 8^{\text{s}}$ ; Decl.  $-47^{\circ} 56'$

13.045	67.5	5.27	11.3	3	300
13.064	65.8	5.39	10.7	2	300
13.067	67.2	5.26	10.5	3	300
13.06	66.8	5.31	(7.5 ... 9.3) F		

Có.;  $-57^{\circ} 28'52'' + 1$ ;  $8.8 + 8.8$

A.R.  $12^{\text{h}} 53^{\text{m}} 58^{\text{s}}$ ; Decl.  $-57^{\circ} 28'$

17.406	351.3	14.51	16.6	2	370
17.409	350.8	14.46	16.7	2	370
17.41	351.0	14.48	(8.8 ... 8.9) 7		

*h* 4564;  $-55^{\circ} 53'43''$ ;  $8.9$

A.R.  $12^{\text{h}} 55^{\text{m}} 21^{\text{s}}$ ; Decl.  $-55^{\circ} 0'$

13.110	218.6	21.93	11.1	3	300
13.148	218.1	21.83	11.0	3	300
13.13	218.3	21.88	(8.9 ... 9.5) N		

Có. 29 = Hargrave 81;  $-45^{\circ} 6'20''$ ;  $8.2$

A.R.  $12^{\text{h}} 57^{\text{m}} 52^{\text{s}}$ ; Decl.  $-45^{\circ} 54'$

13.020	100.4	4.88	10.6	$2\frac{1}{2}$	300
13.036	99.6	4.88	11.2	3	300
13.039	100.1	5.07	11.0	3	300
13.03	100.0	4.94	(8.3 ... 9.1) D?		

*h* 4567; *f* Centauri;  $5.2$

A.R.  $12^{\text{h}} 59^{\text{m}} 3^{\text{s}}$ ; Decl.  $-47^{\circ} 48'$

13.067	79.1	11.55	10.6	$2\frac{1}{2}$	300
13.077	78.8	11.71	10.6	$2\frac{1}{2}$	300
13.212	77.6	11.49	16.2	2	300
13.12	78.5	11.58	(5.2 ... 10.2) F		

*h* 4568;  $-61^{\circ} 3461 + 0$ ;  $9.8 + 10.1$

A.R.  $12^h 59^m 37^s$ ; Decl.  $-61^{\circ} 27'$

17.526	277.5	16.44	16.2	$1\frac{1}{2}$	370
17.584	277.1	16.46	17.0	2	370
17.56	277.3	16.45	(9.4 ... 11.6)		N

$\Delta$  128;  $\xi^2$  Centauri; 4.6

A.R.  $12^h 59^m 38^s$ ; Decl.  $-49^{\circ} 14'$

13.067	99.3	25.40	10.7	3	300
13.077	99.9	25.85	10.5	3	300
13.212	99.3	25.24	16.0	2	300
13.214	99.2	25.06	16.3	2	300
13.14	99.4	25.39	(4.1 ... 9.3)		C

*h* 4569;  $-56^{\circ} 5593$ ; 7.6

A.R.  $13^h 0^m 29^s$ ; Decl.  $-56^{\circ} 1'$

13.105	243.2	4.97	10.1	3	300
13.110	242.4	5.02	11.3	3	300
13.149	243.1	5.00	11.2	3	300
13.12	242.9	5.00	(8.0 ... 9.2)		F

Có. 72;  $-46^{\circ} 6207$ ; 7.8

A.R.  $13^h 3^m 56^s$ ; Decl.  $-46^{\circ} 37'$

13.045	279.2	3.78	11.5	3	300
13.064	280.4	4.16	10.9	2	300
13.067	277.2	3.73	10.8	3	300
13.077	280.2	3.80	10.8	$2\frac{1}{2}$	300
13.06	279.2	3.87	(8.8 ... 9.4)		D?

*h* 4573;  $-55^{\circ} 5439$ ; 9.2

A.R.  $13^h 6^m 4^s$ ; Decl.  $-55^{\circ} 36'$

13.105	56.6	7.70	10.2	3	300
13.149	57.0	7.77	11.4	3	300
13.157	55.2	7.98	11.1	3	300
13.14	56.3	7.81	(9.5 ... 10.2)		N

Ward 35;  $-56^{\circ} 5669$ ; 8.8

A.R.  $13^h 7^m 44^s$ ; Decl.  $-56^{\circ} 22'$

13.105	208.7	1.44	10.4	3	300
13.149	210.4	1.35	11.7	3	300
13.157	208.2	1.35	11.3	3	300
13.14	209.1	1.38	(9.0 ... 9.0)		

*h* 4576 = Rus 216;  $-56^{\circ} 5673$ ; 7.8

A.R.  $13^h 8^m 24^s$ ; Decl.  $-56^{\circ} 24'$

13.105	127.7	5.75	10.3	3	300
13.110	127.7	5.78	11.4	3	300
13.149	127.5	5.63	11.9	3	300
13.12	127.6	5.72	(7.7 ... 9.2)		F

Delavan 5;  $-54^{\circ} 5516$ ; 8.7

A.R.  $13^h 9^m 32^s$ ; Decl.  $-54^{\circ} 9'$

14.334	342.2	7.81	13.8	3	370
14.336	343.3	7.75	10.4	$3\frac{1}{2}$	370
14.375	341.9	7.68	11.6	$2\frac{1}{2}$	370
14.35	342.5	7.75	(9.1 ... 9.9)		7

Sellers 18;  $-47^{\circ} 5982$ ; 7.1

A.R.  $13^h 15^m 27^s$ ; Decl.  $-47^{\circ} 17'$

14.347	226.3	0.61	12.5	3	650
14.377	228.8	0.57	12.6	3	650
14.394	230.6	0.59	10.9	3	650
14.37	228.6	0.59	(7.1 ... 7.2)		89

*h* 4580;  $-47^{\circ} 5983$ ; 6.6

A.R.  $13^h 15^m 35^s$ ; Decl.  $-47^{\circ} 54'$

Véase la nota. See note. 89

Có. 30; Véase la nota. See note 146

Cape 32;  $-52^{\circ} 6487$ ; 8.4

A.R.  $13^h 18^m 30^s$ ; Decl.  $-52^{\circ} 38'$

14.334	261.2	4.33	14.0	$2\frac{1}{2}$	370
14.336	262.6	4.22	10.5	$3\frac{1}{2}$	370
14.347	262.4	4.27	12.3	$2\frac{1}{2}$	370
14.34	262.1	4.27	(8.8 ... 9.3)		7

*h* 4587;  $-42^{\circ} 6258$ ; 8.4

A.R.  $13^h 19^m 7^s$ ; Decl.  $-42^{\circ} 24'$

13.030	87.1	5.29	10.9	3	300
13.039	86.7	5.22	11.3	3	300
13.077	86.1	5.24	11.0	$2\frac{1}{2}$	300
13.04	86.6	5.25	(9.1 ... 9.1)		F

Rus 218;  $-43^{\circ} 6149$ ; 7.9

A.R.  $13^h 20^m 45^s$ ; Decl.  $-43^{\circ} 7'$

13.036	170.1	2.65	11.5	3	300
13.039	169.6	2.48	11.5	3	300
14.533	168.4	2.32	15.3	$2\frac{1}{2}$	370
14.536	169.8	2.47	14.2	$2\frac{1}{2}$	370
13.79	169.5	2.48	(7.6 ... 9.2)		F

*h* 4589;  $-54^{\circ} 5606$ ; 8.4

A.R.  $13^h 21^m 24^s$ ; Decl.  $-54^{\circ} 16'$

13.105	99.0	14.84	10.7	3	300
13.110	98.9	14.60	11.6	$2\frac{1}{2}$	300
13.11	99.0	14.72	(8.5 ... 9.9)		N

I 518;  $-55^{\circ} 5647$ ; 8.4A.R.  $13^{\text{h}} 28^{\text{m}} 55^{\text{s}}$ ; Decl.  $-55^{\circ} 31'$ 

13.105	179.5	2.87	10.9	3	300
13.157	178.1	2.87	11.4	3	300
13.181	178.5	[2.26]	11.9	3	666
13.189	179.1	2.84	10.9	2	280
13.17	178.8	2.86	(8.5 ... 11.4)		142

Rus 223;  $-57^{\circ} 6169$ ; 7.3A.R.  $13^{\text{h}} 29^{\text{m}} 57^{\text{s}}$ ; Decl.  $-57^{\circ} 47'$ 

13.157	19.8	2.48	11.8	3	300
13.181	23.4	2.79	11.5	3	666
13.187	20.1	2.84	11.7	2	280
13.189	26.3	2.82	11.4	2	280
13.18	22.4	2.74	(7.3 ... 11.6)		

I 1072;  $-55^{\circ} 5658$ ; 8.0A.R.  $13^{\text{h}} 30^{\text{m}} 6^{\text{s}}$ ; Decl.  $-55^{\circ} 35'$ 

13.157	107.2	5.42	11.5	3	300
13.181	109.0	5.37	11.7	2 $\frac{1}{2}$	666
13.187	107.6	5.24	11.4	2	280
13.18	107.9	5.34	(8.1 ... 11.8)		23

h 4600;  $-48^{\circ} 5720 + 1$ ; 8.2 + 8.8A.R.  $13^{\text{h}} 31^{\text{m}} 35^{\text{s}}$ ; Decl.  $-48^{\circ} 22'$ 

13.045	118.5	16.78	11.8	3	300
13.064	119.3	17.13	11.2	2	300
13.067	119.1	16.76	11.0	3	300
13.077	118.7	17.17	11.3	2	300
13.06	118.9	16.96	(8.2 ... 9.2)		F

h 4602;  $-45^{\circ} 6488 + 9$ ; 8.7 + 9.0A.R.  $13^{\text{h}} 32^{\text{m}} 42^{\text{s}}$ ; Decl.  $-45^{\circ} 4'$ 

13.077	187.8	23.45	11.1	2 $\frac{1}{2}$	300
13.209	187.4	23.55	16.4	2	300
13.14	187.6	23.50	(9.0 ... 9.2)		M?

 $\Delta$  141; Q Centauri; 6.1A.R.  $13^{\text{h}} 33^{\text{m}} 45^{\text{s}}$ ; Decl.  $-53^{\circ} 56'$ 

13.105	163.2	5.24	11.1	3	300
13.110	163.7	5.41	11.7	2	300
13.154	163.8	5.41	10.3	2	300
13.12	163.6	5.35	(6.0 ... 7.2)		F

h 4603;  $-50^{\circ} 6254$ ; 9.1A.R.  $13^{\text{h}} 33^{\text{m}} 54^{\text{s}}$ ; Decl.  $-50^{\circ} 0'$ 

13.064	148.3	8.94	11.4	3	300
13.067	147.9	8.90	11.1	3	300
13.077	147.5	8.85	11.5	3	300
13.07	147.9	8.90	(9.4 ... 9.9)		21

Aguilar 11;  $-57^{\circ} 6237$ ; 8.8A.R.  $13^{\text{h}} 35^{\text{m}} 39^{\text{s}}$ ; Decl.  $-57^{\circ} 13'$ 

17.406	184.9	4.40	17.0	2	370
17.430	182.1	4.27	16.5	2	370
17.512	184.1	4.67	17.3	2	370
17.45	183.7	4.45	(8.9 ... 11.9)		7

h 4614;  $-42^{\circ} 6402$ ; 8.8A.R.  $13^{\text{h}} 40^{\text{m}} 59^{\text{s}}$ ; Decl.  $-42^{\circ} 32'$ 

13.209	280.5	13.87	16.7	2	300
13.247	280.9	13.74	16.1	2 $\frac{1}{2}$	300
13.23	280.7	13.80	(9.4 ... 10.1)		F

 $\Delta$  144;  $-46^{\circ} 6506$ ; 8.0A.R.  $13^{\text{h}} 41^{\text{m}} 50^{\text{s}}$ ; Decl.  $-46^{\circ} 45'$ 

13.050	256.3	9.29	11.6	3	300
13.064	256.7	9.36	11.5	2 $\frac{1}{2}$	300
13.06	256.5	9.32	(8.1 ... 8.9)		F

h 4619;  $-47^{\circ} 6234 + 3$ ; 8.0 + 8.7A.R.  $13^{\text{h}} 44^{\text{m}} 16^{\text{s}}$ ; Decl.  $-47^{\circ} 15'$ 

13.045	199.2	23.64	12.0	3	300
13.064	198.7	23.69	11.6	2	300
13.05	199.0	23.66	(7.6 ... 8.9)		F

h 4620;  $-57^{\circ} 6366$ ; 9.1A.R.  $13^{\text{h}} 45^{\text{m}} 6^{\text{s}}$ ; Decl.  $-57^{\circ} 11'$ 

13.105	83.3	5.75	11.4	3	300
13.157	81.7	5.93	12.1	2 $\frac{1}{2}$	300
13.181	83.5	5.76	12.1	2 $\frac{1}{2}$	666
13.15	82.8	5.81	(9.9 ... 10.2)		N

h 4624 = I 37;  $-46^{\circ} 6546$ ; 6.8A.R.  $13^{\text{h}} 46^{\text{m}} 11^{\text{s}}$ ; Decl.  $-46^{\circ} 30'$ 

13.064	349.9	21.24	11.8	2 $\frac{1}{2}$	300
13.067	350.0	21.36	11.3	2 $\frac{1}{2}$	300
13.077	349.3	21.51	11.6	2	300
13.07	349.7	21.37	(6.9 ... 10.3)		R?

h 4628; Véase la nota. See note 145

 $\Delta$  150;  $-57^{\circ} 6410 + 09$ ; 8.6 + 8.4A.R.  $13^{\text{h}} 48^{\text{m}} 53^{\text{s}}$ ; Decl.  $-57^{\circ} 6'$ 

13.105	266.2	59.33	11.6	3	300
13.157	266.1	59.07	12.3	3	300
13.181	266.5	59.14	12.4	3	666
13.15	266.3	59.18	(7.4 ... 8.7)		N

## BC = h 4633

13.105	305.5	9.87	11.7	3	300
13.157	305.1	10.04	12.5	3	300
13.181	303.6	10.12	12.5	3	666
13.15	304.7	10.01	(8.7 ... 10.5)		N

$\Delta 151 = h 4634; -55^\circ 5794 + 3; 8.2 + 8.8$

A.R.  $13^h 49^m 0^s$ ; Decl.  $-55^\circ 26'$

13.105	33.5	16.61	11.9	2½	300
13.157	33.2	16.66	12.7	3	300
13.181	33.3	16.73	12.3	3	666
13.15	33.3	16.67	(8.0 ... 8.8)		R

Dawson 14;  $-52^\circ 6882; 8.4$

A.R.  $13^h 50^m 36^s$ ; Decl.  $-52^\circ 13'$

14.334	9.0	1.11	14.2	3	370
14.336	10.0	1.13	10.9	3	650
14.377	7.7	1.13	12.8	3	650
14.35	8.9	1.12	(8.8 ... 9.4)		

AC = Delavan 6

14.334	80.7	8.23	14.3	2½	370
14.336	79.5	8.59	10.7	3	370
14.377	79.8	8.41	12.9	3	370
14.35	80.0	8.41	(8.8 ... 9.6)		7

$h 4638; -46^\circ 6590; 8.8$

A.R.  $13^h 52^m 9^s$ ; Decl.  $-46^\circ 37'$

13.064	313.3	8.11	11.9	2½	300
13.067	313.2	7.82	11.4	3	300
13.214	314.3	8.09	16.8	2	300
13.12	313.6	8.01	(9.5 ... 10.2)		N

AC

13.064	110.4	9.33	12.0	2	300
13.067	111.2	9.31	11.7	2½	300
13.214	110.7	[9.73]	16.9	1½	300
13.272	110.2	9.38	11.5	2	300
13.430	108.6	9.26	16.7	2	300
13.21	110.3	9.32	(9.5 ... Var.)		N

AD

13.064	260.1	9.65	12.0	2½	300
13.067	259.1	9.24	11.6	2½	300
13.272	256.7	9.58	11.3	2	300
13.460	260.9	9.28	17.0	2½	300
13.22	259.2	9.44	(9.5 ... Var.)		90

Có. 32;  $-49^\circ 6634; 8.1$

A.R.  $13^h 57^m 23^s$ ; Decl.  $-49^\circ 48'$

13.045	66.1	2.60	12.3	3	300
13.050	68.3	2.65	11.9	3	300
13.067	68.5	2.67	11.8	3	300
13.05	67.6	2.64	(8.5 ... 8.6)		91

$h 4645 = \text{Rus } 239; -57^\circ 6502 + 1; 9.4 + 9.6$

A.R.  $13^h 58^m 53^s$ ; Decl.  $-57^\circ 6'$

13.187	307.6	14.72	12.2	2	280
13.195	306.8	14.67	12.4	2	300
13.19	307.2	14.69	(9.6 ... 10.1)		92

Rus 238;  $-57^\circ 6505 + 4; 9.4 + 10.0$

A.R.  $13^h 59^m 5^s$ ; Decl.  $-57^\circ 2'$

13.187	285.8	22.46	12.4	2	280
13.195	286.0	22.37	12.2	2	300
13.19	285.9	22.41	(9.6 ... 10.8)		

$\Delta 155; -53^\circ 5880 + 79; 8.4 + 9.0$

A.R.  $13^h 59^m 26^s$ ; Decl.  $-53^\circ 5'$

17.272	17.7	20.63	12.7	3	370
17.304	17.5	20.79	13.0	2	370
17.29	17.6	20.71	(8.0 ... 8.5)		R

$h 4646 = h 4647; -47^\circ 6377; 8.5$

A.R.  $13^h 59^m 30^s$ ; Decl.  $-47^\circ 43'$

13.064	295.0	11.10	12.3	3	300
13.272	294.4	11.00	11.9	2	300
13.17	294.7	11.05	(9.2 ... 9.3)		93

Dawson 15;  $-47^\circ 6380; 9.4$

A.R.  $13^h 59^m 36^s$ ; Decl.  $-47^\circ 47'$

13.064	157.5	6.03	12.4	3	300
13.272	160.8	6.08	12.1	2½	300
13.274	159.8	6.13	12.0	2	300
13.20	159.4	6.08	(10.1 ... 10.1)		93

Sellers 19;  $-49^\circ 6679; 7.3$

A.R.  $13^h 59^m 37^s$ ; Decl.  $-49^\circ 16'$

13.272	259.5	1.33	12.3	2½	666
13.458	258.5	1.18	17.4	2	666
13.460	258.8	1.42	17.4	2	666
13.485	263.0	1.17	17.6	2½	666
13.42	259.9	1.27	(7.5 ... 7.8)		P

$h 4649; -59^\circ 5427; 8.2$

A.R.  $14^h 0^m 16^s$ ; Decl.  $-59^\circ 8'$

17.463	243.8	8.41	17.3	3	370
17.469	245.2	8.46	16.7	2	370
17.471	244.9	8.52	17.9	2	370
17.47	244.6	8.46	(8.8 ... 8.9)		F

$h 4653; -42^\circ 6557; 6.7$

A.R.  $14^h 1^m 8^s$ ; Decl.  $-42^\circ 52'$

13.209	34.5	28.42	16.9	2	300
13.247	34.9	28.70	16.4	3	300
13.23	34.7	28.56	(6.6 ... 12.0)		N

$h$  4651;  $-50^\circ 6654 + 7$ ;  $6.7 + 9.0$

A.R.  $14^h 1^m 22^s$ ; Decl.  $-50^\circ 55'$

17.272	132.3	63.95	12.9	3	370
17.304	132.4	63.78	13.4	2	370
17.29	132.3	63.87	(6.4 ... 8.6)		93

Pollock;  $-46^\circ 6669$ ; 8.1

A.R.  $14^h 3^m 1^s$ ; Decl.  $-46^\circ 19'$

13.064	53.3	4.00	12.5	3	300
13.245	54.7	4.02	17.4	3	300
13.247	53.9	4.14	17.4	3	300
13.19	54.0	4.05	(8.2 ... 9.0)		F

$h$  4656;  $-51^\circ 6650 + 49$ ;  $9.1 + 9.6$

A.R.  $14^h 3^m 55^s$ ; Decl.  $-51^\circ 29'$

17.272	107.3	16.17	13.2	3	370
17.304	107.5	16.32	13.7	2	370
17.29	107.4	16.24	(9.4 ... 9.7)		9

$h$  4659;  $-54^\circ 5921$ ; 8.6

A.R.  $14^h 4^m 4^s$ ; Decl.  $-54^\circ 53'$

13.178	105.8	18.49	12.4	2	666
13.189	105.7	18.64	11.9	2	280
13.18	105.8	18.56	(8.5 ... 10.5)		N

HdA.;  $-56^\circ 6206$ ; 5.4

A.R.  $14^h 6^m 15^s$ ; Decl.  $-56^\circ 30'$

13.359	169.9	33.96	11.1	2	300
13.408	169.7	33.89	12.2	2	300
13.38	169.8	33.92	(5.2 ... 10.6)		

Brisbane;  $-56^\circ 6215$ ; 7.6

A.R.  $14^h 7^m 48^s$ ; Decl.  $-56^\circ 43'$

13.359	115.6	30.23	11.3	2	300
13.408	115.6	30.25	12.5	2	300
13.38	115.6	30.24	(8.2 ... 9.4)		

$h$  4665;  $-42^\circ 6604$ ; 8.4

A.R.  $14^h 8^m 43^s$ ; Decl.  $-42^\circ 41'$

13.209	111.1	18.86	17.0	2	300
13.247	111.2	19.11	16.7	3	300
13.23	111.2	18.99	(8.9 ... 9.9)		N

$h$  4666;  $-47^\circ 6456$ ; 7.8

A.R.  $14^h 9^m 0^s$ ; Decl.  $-47^\circ 35'$

13.247	22.5	10.65	17.6	3	300
13.428	23.4	10.66	17.5	2	300
13.34	22.9	10.65	(9.0 ... 9.8)		N

$h$  4669;  $-49^\circ 6888$ ; 9.6

A.R.  $14^h 11^m 28^s$ ; Decl.  $-49^\circ 20'$

13.272	279.8	6.88	12.5	2½	300
13.428	282.7	6.54	17.8	2	300
13.430	279.0	6.56	16.9	2	300
13.38	280.5	6.66	(9.8 ... 10.6)		N

$h$  4672;  $-42^\circ 6626$ ; 7.4

A.R.  $14^h 12^m 19^s$ ; Decl.  $-42^\circ 29'$

13.247	301.5	4.07	17.1	3	300
13.261	302.0	3.94	11.9	3	300
13.294	302.5	4.07	11.5	2	300
13.27	302.0	4.03	(6.3 ... 8.6)		F

$\Delta$  159 = Rii 19;  $-57^\circ 6619$ ; 6.5

A.R.  $14^h 13^m 41^s$ ; Decl.  $-57^\circ 53'$

13.091	160.4	9.61	13.3	2½	300
13.123	160.9	9.46	11.8	2½	300
13.178	160.1	9.73	12.7	2	666
13.13	160.5	9.60	(6.4 ... 7.8)		F

$h$  4673;  $-51^\circ 6793$ ; 9.1

A.R.  $14^h 14^m 9^s$ ; Decl.  $-51^\circ 51'$

17.272	143.9	12.17	13.3	3	370
17.332	143.2	12.11	17.0	2	370
17.30	143.6	12.14	(10.2 ... 11.0)		N

Rus 244;  $-47^\circ 6483$ ; 6.6

A.R.  $14^h 14^m 29^s$ ; Decl.  $-47^\circ 45'$

13.272	120.7	4.83	12.7	2½	300
13.274	120.1	4.73	12.3	2	300
13.430	121.8	4.63	17.2	2	300
13.33	120.9	4.73	(6.9 ... 9.7)		M

$h$  4675;  $-54^\circ 5998$ ; 9.5

A.R.  $14^h 17^m 11^s$ ; Decl.  $-54^\circ 14'$

13.178	337.4	8.84	13.0	2	666
13.195	337.2	8.90	13.0	2	300
13.313	340.9	8.69	18.1	3	300
13.23	338.5	8.81	(9.8 ... 10.2)		20

$\Delta$  160;  $\tau^1$  Lupi;  $4.4 + 9.4$

A.R.  $14^h 18^m 8^s$ ; Decl.  $-44^\circ 39'$

13.450	204.2	158.11	17.0	2	300
13.471	204.1	158.55	16.0	2½	300
13.512	204.0	158.01	17.0	2	300
13.48	204.1	158.22	(4.5 ... 8.5)		N

*h* 4677;  $-48^{\circ} 6453$ ; 9.1:

A.R.  $14^{\text{h}} 18^{\text{m}} 31^{\text{s}}$ ; Decl.  $-48^{\circ} 28'$

13.272	157.4	12.18	12.8	3	300
13.428	156.9	11.96	18.0	2	300
13.35	157.2	12.07	(9.8 ... 10.2)		N

*h* 4676;  $-59^{\circ} 5578 + 7$ ; 8.9 + 8.9

A.R.  $14^{\text{h}} 18^{\text{m}} 37^{\text{s}}$ ; Decl.  $-59^{\circ} 4'$

17.463	261.8	20.52	17.6	3	370
17.471	261.5	20.52	18.1	2	370
17.47	261.7	20.52	(8.3 ... 8.8)		F?

BC; C = 10.8

17.463	116.3	8.71	17.7	3	370
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BD; D = 11.5

17.463	252.5	13.89	17.8	2½	370 N
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BE; E = 12.2

17.463	218.9	5.73	17.9	2½	370 N
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*h* 4681;  $-55^{\circ} 6027$ ; 8.4

A.R.  $14^{\text{h}} 21^{\text{m}} 43^{\text{s}}$ ; Decl.  $-55^{\circ} 14'$

13.123	356.0	14.40	12.0	2½	300
13.313	355.2	14.14	18.3	2½	300
13.315	356.2	13.99	17.9	2½	300
13.25	355.8	14.18	(8.4 ... 12.1)		N

HdA.;  $-48^{\circ} 6496$ ; 5.8

A.R.  $14^{\text{h}} 22^{\text{m}} 1^{\text{s}}$ ; Decl.  $-48^{\circ} 58'$

13.272	18.9	22.08	13.0	3	300
13.430	17.9	22.14	17.6	2	300
13.35	18.4	22.11	(5.9 ... 12.0)		F

$\Delta$  162;  $-45^{\circ} 6895$ ; 8.0

A.R.  $14^{\text{h}} 25^{\text{m}} 42^{\text{s}}$ ; Decl.  $-45^{\circ} 55'$

13.471	241.6	72.24	18.1	2	300
13.512	241.3	72.17	17.4	2	300
13.49	241.4	72.20	(7.7 ... 10.5)		N

*h* 4685;  $-45^{\circ} 6902$ ; 8.9

A.R.  $14^{\text{h}} 26^{\text{m}} 41^{\text{s}}$ ; Decl.  $-45^{\circ} 37'$

13.299	79.2	2.43	12.3	3	300
13.472	81.0	2.38	18.5	2	300
13.512	77.9	2.31	17.8	2	300
13.43	79.4	2.37	(9.6 ... 9.9)		D

Rus 248;  $-46^{\circ} 6869$ ; 8.0

A.R.  $14^{\text{h}} 27^{\text{m}} 33^{\text{s}}$ ; Decl.  $-46^{\circ} 8'$

13.067	291.1	5.58	12.6	2	300
13.431	290.9	5.69	17.9	2	300
13.25	291.0	5.63	(8.6 ... 9.9)		F

*h* 4690; *a* Lupi; 7.5 + 8.2

A.R.  $14^{\text{h}} 29^{\text{m}} 10^{\text{s}}$ ; Decl.  $-45^{\circ} 35'$

13.299	24.4	19.25	12.1	2	300
13.450	25.3	19.36	17.5	2	300
13.472	24.8	19.55	18.7	2	300
13.41	24.8	19.39	(6.6 ... 8.8)		F

*h* 4691;  $-55^{\circ} 6094$ ; 8.6

A.R.  $14^{\text{h}} 30^{\text{m}} 15^{\text{s}}$ ; Decl.  $-55^{\circ} 10'$

13.149	274.2	12.37	12.6	3	300
13.313	272.9	12.20	18.5	3	300
13.23	273.6	12.29	(9.1 ... 9.6)		M

( $\Delta$  165);  $\alpha$  Centauri; 2.1

A.R.  $14^{\text{h}} 30^{\text{m}} 59^{\text{s}}$ ; Decl.  $-60^{\circ} 19'$

13.031	217.5	18.67	11.4	2½	300
13.039	216.8	18.74	11.9	3	300
13.091	217.0	18.55	13.6	2½	300
13.157	217.0	18.45	12.8	2½	300
13.209	217.4	18.34	17.4	2	300
13.214	217.1	18.52	17.3	2	300
16.669	219.4	16.96	20.0	2	370
16.672	219.6	17.02	19.5	2	370
16.705	221.4	16.13	19.6	2	370
17.376	220.3	15.93	15.9	2½	370
17.605	220.6	15.86	17.7	3	650
17.718	220.3	15.89	18.8	2	370
13.12	217.1	18.55			
16.68	220.1	16.70			
17.57	220.4	15.89	(0.7 ... 1.4)		B

Delavan 7;  $-54^{\circ} 6102$ ; 8.9

A.R.  $14^{\text{h}} 31^{\text{m}} 30^{\text{s}}$ ; Decl.  $-54^{\circ} 50'$

14.394	327.5	9.80	11.3	3	370
14.397	328.0	9.93	13.6	3	370
14.400	325.6	9.67	19.8	2½	370
14.40	327.0	9.80	(9.5 ... 10.1)		7

*h* 5445;  $-54^{\circ} 6106$ ; 9.4

A.R.  $14^{\text{h}} 32^{\text{m}} 1^{\text{s}}$ ; Decl.  $-54^{\circ} 26'$

13.313	73.0	16.34	18.7	3	300
13.316	72.8	16.36	18.2	3	300
13.31	72.9	16.35	(10.7 ... 10.9)		95

$\lambda$  209;  $-45^{\circ} 6954$ ; 7.1

A.R.  $14^{\text{h}} 32^{\text{m}} 9^{\text{s}}$ ; Decl.  $-45^{\circ} 15'$

13.299	240.8	11.97	12.6	2½	300
13.512	240.9	11.96	18.1	2	300
13.41	240.8	11.97	(6.8 ... 12.7)		

*h* 4692;  $-42^{\circ} 6748$ ; 8.5A.R.  $14^{\text{h}} 32^{\text{m}} 31^{\text{s}}$ ; Decl.  $-42^{\circ} 8'$ 

13.261	296.7	10.93	12.7	3	300
13.294	296.0	11.07	12.3	$2\frac{1}{2}$	300
13.28	296.4	11.00	(9.2 ... 9.5)		D†

 $\Delta$  168;  $-54^{\circ} 6120$ ; 7.6A.R.  $14^{\text{h}} 33^{\text{m}} 51^{\text{s}}$ ; Decl.  $-54^{\circ} 39'$ 

13.123	202.3	5.91	12.4	3	300
13.313	202.2	5.88	18.9	2	300
13.22	202.3	5.90	(8.0 ... 8.2)		F

 $\Delta$  169;  $-55^{\circ} 6150 + 2$ ; 6.8 + 8.3A.R.  $14^{\text{h}} 36^{\text{m}} 11^{\text{s}}$ ; Decl.  $-55^{\circ} 4'$ 

13.123	106.2	68.62	12.8	$2\frac{1}{2}$	300
13.181	106.2	68.43	12.8	3	666
13.15	106.2	68.52	(7.0 ... 7.9)		96

*h* 4696;  $-44^{\circ} 6947$ ; 7.4A.R.  $14^{\text{h}} 37^{\text{m}} 47^{\text{s}}$ ; Decl.  $-44^{\circ} 20'$ 

13.512	205.7	35.57	18.2	2	300
13.548	206.2	35.08	17.0	2	300
13.583	206.3	35.35	17.3	2	300
13.586	206.4	35.08	18.0	2	300
13.56	206.1	35.28	(7.5 ... 12.0)		97

*h* 4698; *b* Lupi; 7.2A.R.  $14^{\text{h}} 38^{\text{m}} 18^{\text{s}}$ ; Decl.  $-51^{\circ} 51'$ 

17.272	259.5	9.03	13.5	$3\frac{1}{2}$	370
17.343	259.0	8.87	14.2	2	370
17.477	262.8	9.25	17.3	3	370
17.36	260.4	9.05	(5.8 ... 12.8)		F

*h* 4699;  $-58^{\circ} 5719 + 21$ ; 8.5 + 9.0A.R.  $14^{\text{h}} 39^{\text{m}} 47^{\text{s}}$ ; Decl.  $-58^{\circ} 53'$ 

17.463	125.2	37.24	18.1	$2\frac{1}{2}$	370
17.471	125.2	37.33	18.4	2	370
17.47	125.2	37.28	(7.6 ... 9.2)		F

*h* 4705;  $-51^{\circ} 7207$ ; 8.6A.R.  $14^{\text{h}} 41^{\text{m}} 35^{\text{s}}$ ; Decl.  $-51^{\circ} 5'$ 

17.272	182.8	12.22	13.7	3	370
17.343	182.7	12.04	14.6	2	370
17.31	182.8	12.13	(9.2 ... 11.8)		51

*h* 4706;  $-46^{\circ} 7046$ ; 8.2A.R.  $14^{\text{h}} 42^{\text{m}} 52^{\text{s}}$ ; Decl.  $-46^{\circ} 53'$ 

13.266	219.0	6.76	12.3	$2\frac{1}{2}$	300
13.272	219.7	6.91	13.2	3	300
13.431	219.0	6.98	18.3	2	300
13.32	219.2	6.88	(7.9 ... 8.9)		F

*h* 4707;  $-65^{\circ} 2914$ ; 7.9A.R.  $14^{\text{h}} 43^{\text{m}} 38^{\text{s}}$ ; Decl.  $-65^{\circ} 54'$ 

14.394	85.3	0.83	11.9	3	650
14.399	87.0	0.75	13.0	3	650
14.416	87.8	0.88	15.8	3	370
14.40	86.7	0.82	(8.4 ... 8.9)		P

Dawson 16;  $-51^{\circ} 7245$ ; 8.4A.R.  $14^{\text{h}} 43^{\text{m}} 47^{\text{s}}$ ; Decl.  $-51^{\circ} 8'$ 

17.272	211.1	3.45	14.0	3	370
17.343	208.0	3.81	14.4	2	370
17.477	213.5	3.47	17.6	3	370
17.35	210.9	3.58	(8.7 ... 12.3)		

*h* 4709;  $-55^{\circ} 6233$ ; 8.8A.R.  $14^{\text{h}} 44^{\text{m}} 46^{\text{s}}$ ; Decl.  $-55^{\circ} 42'$ 

13.178	225.2	21.22	13.4	2	666
13.316	225.0	21.29	18.5	$2\frac{1}{2}$	300
13.25	225.1	21.26	(9.0 ... 10.8)		98

 $\Delta$  171;  $-45^{\circ} 7082$ ; 7.2A.R.  $14^{\text{h}} 45^{\text{m}} 3^{\text{s}}$ ; Decl.  $-45^{\circ} 20'$ 

13.261	225.8	17.51	13.0	3	300
13.294	226.2	17.49	12.5	2	300
13.28	226.0	17.50	(7.2 ... 8.6)		F†

*h* 4712;  $-54^{\circ} 6214$ ; 8.2A.R.  $14^{\text{h}} 46^{\text{m}} 18^{\text{s}}$ ; Decl.  $-54^{\circ} 55'$ 

13.313	226.7	7.30	19.3	$2\frac{1}{2}$	300
13.316	226.1	7.32	18.7	2	300
13.329	226.4	7.55	11.4	$2\frac{1}{2}$	300
13.32	226.4	7.39	(8.5 ... 9.1)		D

 $\Delta$  174 = *h* 4715;  $-47^{\circ} 6786$ ; 6.7A.R.  $14^{\text{h}} 48^{\text{m}} 2^{\text{s}}$ ; Decl.  $-47^{\circ} 22'$ 

13.266	278.6	2.87	12.4	$2\frac{1}{2}$	300
13.458	277.4	2.77	18.7	2	666
13.461	277.6	2.94	17.8	$2\frac{1}{2}$	666
13.40	277.9	2.86	(7.3 ... 8.2)		99

*h* 4719;  $-58^{\circ} 5777 + 8$ ; 8.6 + 8.9A.R.  $14^{\text{h}} 50^{\text{m}} 37^{\text{s}}$ ; Decl.  $-58^{\circ} 26'$ 

17.463	39.6	23.62	18.3	2	370
17.471	40.3	23.67	18.6	$1\frac{1}{2}$	370
17.47	39.9	23.64	(8.6 ... 8.8)		F†



*h* 4723;  $-51^{\circ} 7432$ ; 8.4

A.R.  $14^{\text{h}} 53^{\text{m}} 5^{\text{s}}$ ; Decl.  $-51^{\circ} 25'$

17.272	168.4	5.45	14.2	3	370
17.332	169.9	5.38	17.3	2	370
17.343	168.9	5.20	14.7	2	370
17.32	169.1	5.34	(7.5 ... 11.5)		A

*h* 4725;  $-45^{\circ} 7172$ ; 9.2

A.R.  $14^{\text{h}} 54^{\text{m}} 33^{\text{s}}$ ; Decl.  $-45^{\circ} 3'$

13.548	254.5	13.87	17.7	$1\frac{1}{2}$	300
13.583	253.6	14.23	17.7	2	300
13.586	253.9	13.92	18.7	2	300
13.57	254.0	14.01	(9.5 ... 10.9)		100

*h* 4726;  $-49^{\circ} 7656$ ; 8.8

A.R.  $14^{\text{h}} 55^{\text{m}} 41^{\text{s}}$ ; Decl.  $-49^{\circ} 15'$

13.266	98.9	6.79	12.8	3	300
13.431	100.0	6.60	18.5	2	300
13.461	99.1	6.75	18.3	$2\frac{1}{2}$	300
13.39	99.3	6.71	(9.8 ... 10.0)		N

*h* 4728;  $\pi$  Lupi; 4.7

A.R.  $14^{\text{h}} 56^{\text{m}} 38^{\text{s}}$ ; Decl.  $-46^{\circ} 34'$

13.266	84.7	1.57	12.5	$2\frac{1}{2}$	666
13.447	83.4	1.40	17.7	2	666
13.458	85.6	1.81	18.8	2	666
13.461	82.9	1.82	18.0	2	666
13.472	85.3	1.57	19.2	2	300
13.507	87.2	1.54	14.0	3	666
13.44	84.8	1.61	(5.1 ... 5.2)		P

*h* 4732;  $-47^{\circ} 6921$ ; 9.0

A.R.  $15^{\text{h}} 0^{\text{m}} 0^{\text{s}}$ ; Decl.  $-47^{\circ} 50'$

13.266	68.2	9.31	13.0	3	300
13.431	68.3	9.34	18.9	2	300
13.461	69.2	9.23	18.4	$2\frac{1}{2}$	300
13.39	68.6	9.29	(9.8 ... 10.1)		N

*h* 4734;  $-54^{\circ} 6367$ ; 7.4

A.R.  $15^{\text{h}} 1^{\text{m}} 58^{\text{s}}$ ; Decl.  $-54^{\circ} 52'$

13.313	249.1	[11.61]	19.5	2	300
13.329	246.8	11.22	11.6	2	300
13.331	247.0	11.25	11.8	2	300
13.33	247.3	11.23	(7.0 ... 11.8)		A

*h* 4735;  $-59^{\circ} 5852$ ; 8.4

A.R.  $15^{\text{h}} 2^{\text{m}} 48^{\text{s}}$ ; Decl.  $-59^{\circ} 55'$

17.477	29.9	7.09	18.0	3	370
17.512	32.2	7.37	17.6	2	370
17.551	31.5	7.30	18.0	$2\frac{1}{2}$	370
17.51	31.3	7.25	(8.2 ... 12.3)		F

$\Delta$  178;  $-44^{\circ} 7220 + 18$ ; 7.8 + 8.1

A.R.  $15^{\text{h}} 3^{\text{m}} 10^{\text{s}}$ ; Decl.  $-44^{\circ} 48'$

13.299	269.1	34.42	12.8	$2\frac{1}{2}$	300
13.512	269.1	34.35	18.5	2	300
13.41	269.1	34.39	(7.4 ... 7.6)		101

*h* 4739; Véase la nota; See note. 101

$\Delta$  177;  $\alpha$  Lupi; 4.2

A.R.  $15^{\text{h}} 3^{\text{m}} 14^{\text{s}}$ ; Decl.  $-48^{\circ} 16'$

13.266	143.7	27.12	13.2	3	300
13.274	143.6	26.85	12.8	2	300
13.395	143.7	27.10	12.8	2	300
13.21	143.7	27.02	(5.2 ... 6.5)		F

$\Delta$  176;  $\zeta$  Lupi; 4.9 + 8.0

A.R.  $15^{\text{h}} 3^{\text{m}} 19^{\text{s}}$ ; Decl.  $-51^{\circ} 37'$

14.403	248.8	72.01	18.2	2	370
14.531	249.1	71.70	18.9	2	370
14.533	249.3	71.97	16.0	2	370
14.49	249.1	71.89	(3.9 ... 7.8)		F

I 238;  $-44^{\circ} 7223$ ; 7.8

A.R.  $15^{\text{h}} 3^{\text{m}} 40^{\text{s}}$ ; Decl.  $-44^{\circ} 32'$

13.299	139.7	3.45	13.0	3	300
13.709	138.9	3.65	19.4	2	300
13.717	139.1	3.06	19.1	$2\frac{1}{2}$	300
14.162	138.8	2.84	13.0	$2\frac{1}{2}$	475
14.337	138.7	3.17	13.4	3	370
13.84	139.0	3.23	(8.4 ... 11.5)		

Có. 39;  $-59^{\circ} 5866$ ; 8.6

A.R.  $15^{\text{h}} 4^{\text{m}} 46^{\text{s}}$ ; Decl.  $-59^{\circ} 21'$

17.463	288.4	12.22	18.5	2	370
17.477	288.4	12.19	18.1	3	370
17.47	288.4	12.20	(8.1 ... 9.7)		102

*h* 4746;  $-58^{\circ} 5866$ ; 8.1

A.R.  $15^{\text{h}} 5^{\text{m}} 36^{\text{s}}$ ; Decl.  $-58^{\circ} 36'$

17.477	349.1	12.54	18.6	2	370
17.513	349.0	12.77	18.7	2	370
17.49	349.0	12.66	(8.1 ... 11.5)		F?

AC

17.477	311.4	18.07	18.5	2	370
17.513	311.7	18.16	18.5	2	370
17.49	311.5	18.11	(8.1 ... 11.5)		N

AD

17.477	265.6	13.50	18.3	$2\frac{1}{2}$	370
17.513	266.1	13.72	18.2	2	370
17.49	265.8	13.61	(8.1 ... 12.2)		103

I 228;  $-43^{\circ} 6926$ ; 7.4A.R.  $15^{\text{h}} 5^{\text{m}} 39^{\text{s}}$ ; Decl.  $-43^{\circ} 19'$ 

13.261	33.5	1.37	13.2	3	666
13.299	33.6	1.40	13.2	3	666
13.709	34.5	1.37	19.5	2	300
13.42	33.9	1.38	(8.2 ... 8.4)		

 $h$  4747 = Rus 259;  $-55^{\circ} 6451, 50$ ; 9.2, 9.7A.R.  $15^{\text{h}} 6^{\text{m}} 3^{\text{s}}$ ; Decl.  $-55^{\circ} 16'$ 

13.313	342.3	17.08	19.7	$2\frac{1}{2}$	300
13.329	340.8	17.40	11.9	$2\frac{1}{2}$	300
13.331	341.1	16.98	12.0	2	300
13.32	341.4	17.15	(9.4 ... 10.0)	104	

 $\Delta$  179;  $-42^{\circ} 6963$ ; 7.3A.R.  $15^{\text{h}} 6^{\text{m}} 11^{\text{s}}$ ; Decl.  $-42^{\circ} 55'$ 

13.261	51.1	19.41	13.4	3	300
13.299	51.2	19.48	13.3	3	300
13.28	51.1	19.44	(8.4 ... 10.8)	20	

 $h$  4749;  $-56^{\circ} 6661$ ; 8.6A.R.  $15^{\text{h}} 7^{\text{m}} 11^{\text{s}}$ ; Decl.  $-56^{\circ} 55'$ 

13.329	255.0	7.06	12.2	2	300
13.331	255.0	7.18	12.3	2	300
13.348	254.8	6.94	11.6	2	300
13.34	254.9	7.06	(9.2 ... 9.8)	N	

 $h$  4750;  $-47^{\circ} 6987$ ; 7.5A.R.  $15^{\text{h}} 7^{\text{m}} 12^{\text{s}}$ ; Decl.  $-47^{\circ} 36'$ 

13.266	19.6	13.35	13.5	3	300
13.431	18.5	13.30	19.1	2	300
13.35	19.1	13.33	(7.0 ... 10.4)	C	

Hargrave 113 = Cape 44;  $-59^{\circ} 5889$ ; 8.2A.R.  $15^{\text{h}} 8^{\text{m}} 12^{\text{s}}$ ; Decl.  $-59^{\circ} 54'$ 

17.551	341.6	3.60	18.2	3	370
17.605	341.7	3.62	18.0	3	650
17.627	341.0	3.54	18.9	2	370
17.59	341.4	3.59	(9.2 ... 9.8)	105	

 $h$  4753;  $\mu$  Lupi; 5.1A.R.  $15^{\text{h}} 9^{\text{m}} 50^{\text{s}}$ ; Decl.  $-47^{\circ} 25'$ 

13.266	152.2	1.57	13.7	3	666
13.431	152.7	1.82	19.4	2	300
13.447	151.9	1.67	18.8	$2\frac{1}{2}$	300
13.38	152.3	1.69	(6.6 ... 6.7)	P	

AC =  $\Delta$  180

13.266	130.8	24.30	13.6	3	300
13.274	130.7	24.21	13.2	2	300
13.431	130.8	24.33	19.3	2	300
13.32	130.8	24.28	(6.6 ... 7.4)	D†	

 $h$  4754;  $-57^{\circ} 7024$ ; 9.4A.R.  $15^{\text{h}} 11^{\text{m}} 59^{\text{s}}$ ; Decl.  $-57^{\circ} 32'$ 

13.332	307.2	6.30	12.5	2	300
13.348	307.5	6.57	11.9	2	300
13.359	308.8	6.30	11.9	2	300
13.35	307.8	6.39	(9.8 ... 10.0)	N	

 $h$  4757;  $\gamma$  Circini; 5.3A.R.  $15^{\text{h}} 13^{\text{m}} 24^{\text{s}}$ ; Decl.  $-58^{\circ} 52'$ 

17.463	68.4	1.11	18.8	3	650
17.551	68.2	1.02	18.4	3	475
17.605	68.2	—	18.2	3	650
17.627	69.5	1.15	19.1	2	650
17.56	68.6	1.09	(5.9 ... 6.0)	P	

Sellors 20 = I 38;  $-47^{\circ} 7081$ ; 7.8A.R.  $15^{\text{h}} 13^{\text{m}} 58^{\text{s}}$ ; Decl.  $-47^{\circ} 28'$ 

14.380	205.5	1.02	14.1	3	370
14.400	202.8	—	20.2	$2\frac{1}{2}$	650
14.421	204.3	1.15	13.8	3	650
14.424	206.3	1.05	12.2	3	370
14.41	204.7	1.07	(9.0 ... 9.1)	P	

Copeland = Gale 3;  $\epsilon$  Lupi; 4.2A.R.  $15^{\text{h}} 14^{\text{m}} 12^{\text{s}}$ ; Decl.  $-44^{\circ} 14'$ 

13.299	272.1	1.23	13.7	$2\frac{1}{2}$	666
13.717	270.2	1.05	19.3	$2\frac{1}{2}$	666
14.337	277.8	1.19	13.6	3	370
14.347	277.4	1.49	13.0	$3\frac{1}{2}$	650
13.93	274.4	1.24	(4.1 ... 5.5)	P	

AC =  $\Delta$  182

13.299	173.3	26.56	13.5	$2\frac{1}{2}$	666
13.709	173.1	26.73	19.6	2	300
13.717	173.3	26.51	19.2	$2\frac{1}{2}$	300
13.58	173.2	26.60	(4.1 ... 8.5)	F	

Dawson 17;  $-54^{\circ} 6484$ ; 10.2A.R.  $15^{\text{h}} 15^{\text{m}} 9^{\text{s}}$ ; Decl.  $-54^{\circ} 30'$ 

13.332	87.2	4.21	13.1	2	300
13.348	88.1	4.43	13.0	2	300
13.359	87.1	4.58	12.1	2	300
13.365	89.0	4.31	12.6	$2\frac{1}{2}$	300
13.35	87.8	4.38	(10.5 ... 11.0)		

 $h$  4763;  $-54^{\circ} 6486$ ; 9.6A.R.  $15^{\text{h}} 15^{\text{m}} 16^{\text{s}}$ ; Decl.  $-54^{\circ} 56'$ 

13.329	321.6	11.74	13.5	3	300
13.332	322.1	12.00	12.9	2	300
13.348	322.0	11.81	12.7	2	300
13.34	321.9	11.85	(9.7 ... 9.9)	F†	

*h* 4766;  $-42^{\circ} 7044$ ; 8.2  
 A.R.  $15^{\text{h}} 17^{\text{m}} 53^{\text{s}}$ ; Decl.  $-42^{\circ} 25'$

13.261	106.4	16.46	13.6	3	300
13.299	107.0	16.44	13.8	3	300
13.28	106.7	16.45	(8.8 ... 9.4)		M

$\Delta$  186;  $-57^{\circ} 7081 + 3$ ; 8.8 + 8.8  
 A.R.  $15^{\text{h}} 23^{\text{m}} 13^{\text{s}}$ ; Decl.  $-57^{\circ} 46'$

13.157	115.5	39.61	14.0	3	300
13.329	115.7	39.49	14.1	3	300
13.24	115.6	39.55	(8.6 ... 8.6)		F

$\Delta$  185 =  $\lambda$  234;  $-51^{\circ} 8065$ ; 7.4  
 A.R.  $15^{\text{h}} 19^{\text{m}} 21^{\text{s}}$ ; Decl.  $-51^{\circ} 10'$

17.272	32.1	13.27	14.3	3	370
17.332	32.7	13.17	17.5	2	370
17.30	32.4	13.22	(7.0 ... 13.1)		F

*h* 4781;  $-42^{\circ} 7082$ ; 9.2  
 A.R.  $15^{\text{h}} 23^{\text{m}} 50^{\text{s}}$ ; Decl.  $-42^{\circ} 31'$

13.737	193.4	12.01	19.2	1½	300
14.321	193.8	12.23	17.6	2	370
14.03	193.6	12.12	(9.5 ... 10.5)		N

Cape 16;  $-57^{\circ} 7066$ ; 7.4  
 A.R.  $15^{\text{h}} 19^{\text{m}} 40^{\text{s}}$ ; Decl.  $-57^{\circ} 55'$

13.157	24.8	2.43	13.8	3	300
13.313	23.2	2.42	20.0	3	300
13.329	23.8	2.37	13.6	3	666
13.27	23.9	2.41	(7.8 ... 8.4)		23

*h* 4784;  $-47^{\circ} 7207 + 6$ ; 7.5 + 9.4  
 A.R.  $15^{\text{h}} 24^{\text{m}} 46^{\text{s}}$ ; Decl.  $-47^{\circ} 7'$

13.274	230.0	28.96	13.5	2	300
13.461	230.0	28.78	18.7	2	300
13.37	230.0	28.87	(7.6 ... 9.6)		R

*h* 4772;  $-50^{\circ} 8086$ ; 7.8  
 A.R.  $15^{\text{h}} 20^{\text{m}} 26^{\text{s}}$ ; Decl.  $-50^{\circ} 57'$

17.272	278.0	8.21	14.4	3	370
17.332	277.2	8.12	17.7	2	370
17.343	275.7	7.76	15.0	2	370
17.430	279.8	8.00	16.7	2	370
17.34	277.7	8.02	(7.7 ... 12.6)		R

$\lambda$  239;  $-46^{\circ} 7520$ ; 8.0  
 A.R.  $15^{\text{h}} 25^{\text{m}} 44^{\text{s}}$ ; Decl.  $-46^{\circ} 48'$

13.461	7.9	13.64	18.9	2½	300
13.472	7.6	13.40	19.5	2	300
13.47	7.8	13.52	(7.8 ... 11.0)		F

*h* 4771;  $-57^{\circ} 7070$ ; 7.9  
 A.R.  $15^{\text{h}} 20^{\text{m}} 42^{\text{s}}$ ; Decl.  $-57^{\circ} 40'$

13.157	186.9	5.37	13.6	3	300
13.329	187.2	5.32	13.8	3	300
13.332	187.4	5.36	13.6	2½	300
13.27	187.2	5.37	(8.5 ... 8.8)		D?

*h* 4786;  $\gamma$  Lupi; 4.2  
 A.R.  $15^{\text{h}} 26^{\text{m}} 49^{\text{s}}$ ; Decl.  $-40^{\circ} 45'$

14.397	90.8	0.23	19.4	4	1125
14.572	79.4	0.23	16.9	4	1125
17.272	77.6	0.21	15.1	3	1125
17.477	73.3	—	16.7	3½	1125
17.608	80.5	—	17.9	3	1125
14.48	85.1	0.23			
17.45	77.1	—	(4.0 ... 4.3)		B

*h* 4777;  $-56^{\circ} 6787$ ; 7.6  
 A.R.  $15^{\text{h}} 22^{\text{m}} 54^{\text{s}}$ ; Decl.  $-56^{\circ} 59'$

13.157	299.7	5.96	13.4	2½	300
13.329	297.1	5.75	14.0	3	300
13.332	297.8	5.71	13.8	2	300
13.27	298.2	5.81	(8.2 ... 9.1)		D

*h* 4788;  $d$  Lupi; 5.3  
 A.R.  $15^{\text{h}} 27^{\text{m}} 17^{\text{s}}$ ; Decl.  $-44^{\circ} 32'$

13.709	360.0	2.89	19.7	2	300
13.717	360.2	2.41	19.5	3	300
14.162	361.8	2.45	13.4	2½	475
14.321	358.9	2.73	17.8	2	370
13.98	360.2	2.62	(5.4 ... 7.5)		M

*h* 4778;  $-52^{\circ} 8475 + 4$ ; 8.4 + 8.6  
 A.R.  $15^{\text{h}} 23^{\text{m}} 12^{\text{s}}$ ; Decl.  $-52^{\circ} 26'$

14.403	205.1	12.83	18.6	2	370
14.531	204.1	13.01	19.2	2	370
14.47	204.6	12.92	(8.6 ... 9.0)		F?

*h* 4789;  $-54^{\circ} 6599$ ; 8.4  
 A.R.  $15^{\text{h}} 27^{\text{m}} 45^{\text{s}}$ ; Decl.  $-54^{\circ} 5'$

14.403	89.3	13.88	18.9	2	370
14.531	89.9	13.60	19.7	2	370
14.534	89.5	13.43	17.6	2	370
14.49	89.6	13.64	(9.0 ... 9.3)		F

$\Delta 189; -51^\circ 83'20'' + 19; 5.8 + 9.6$

A.R.  $15^h 29^m 32^s$ ; Decl.  $-51^\circ 58'$

14.403	278.7	53.46	19.1	2	370
14.531	279.5	53.37	19.4	2	370
14.533	279.6	53.25	16.3	2	370
14.49	279.3	53.36	(5.8 ... 9.7)		F

BC = I 88

14.531	353.7	2.98	19.5	2	370
14.533	355.4	2.97	16.5	2	370
14.536	354.7	2.91	14.4	2	370
14.53	354.6	2.95	(9.7 ... 10.1)		M

$h 4791; -48^\circ 77'65''; 8.6$

A.R.  $15^h 31^m 24^s$ ; Decl.  $-48^\circ 1'$

13.461	128.2	10.48	19.2	2	300
13.485	127.9	10.24	18.3	3	300
14.350	128.0	10.58	14.2	2	370
13.77	128.0	10.43	(9.9 ... 10.3)		N

$\Delta 190; -57^\circ 71'55''; 8.5$

A.R.  $15^h 32^m 58^s$ ; Decl.  $-57^\circ 43'$

13.157	92.1	5.64	14.2	3	300
13.329	92.9	5.78	14.3	3	300
13.332	92.5	5.80	13.9	2	300
13.27	92.5	5.74	(8.6 ... 10.2)		106

I 542 = Ward 57;  $-45^\circ 75'60''; 8.4$

A.R.  $15^h 32^m 59^s$ ; Decl.  $-45^\circ 7'$

13.717	188.3	2.72	19.8	2½	300
14.321	185.6	2.72	18.0	2	370
14.337	186.3	2.80	13.7	3	370
14.12	186.7	2.75	(9.1 ... 9.9)		142

$h 4793; -47^\circ 73'08''; 7.8$

A.R.  $15^h 33^m 8^s$ ; Decl.  $-47^\circ 53'$

13.461	15.7	19.35	19.3	2	300
13.485	15.6	19.47	18.5	2	300
13.47	15.6	19.41	(8.9 ... 11.2)		N

$h 4794; -51^\circ 84'48''; 8.2$

A.R.  $15^h 34^m 13^s$ ; Decl.  $-51^\circ 26'$

17.272	147.3	12.70	14.6	3	370
17.343	149.2	12.77	15.3	2	370
17.430	148.2	12.24	16.6	2	370
17.35	148.2	12.57	(8.8 ... 10.3)		N

$h 4795; -58^\circ 62'43''; 8.0$

A.R.  $15^h 34^m 49^s$ ; Decl.  $-58^\circ 43'$

17.463	222.5	7.53	19.1	2½	370
17.627	222.2	7.57	19.3	2	370
17.718	224.1	7.40	19.2	2	370
17.60	222.9	7.50	(8.1 ... 10.9)		F?

AC; C = 12.0

17.627	136.1	20.89	19.4	2	370 N
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AD; D =  $-58^\circ 62'44''; 9.7$

17.627	177.1	45.26	19.6	1½	370 N
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DE

17.463	233.8	7.95	19.3	2	370
17.718	234.1	7.98	19.4	2	370
17.59	233.9	7.96	(10.2 ... 11.2)		N

$h 4797; -49^\circ 84'96''; 7.6$

A.R.  $15^h 35^m 3^s$ ; Decl.  $-49^\circ 49'$

13.461	255.2	22.66	19.5	2½	300
13.507	254.8	22.41	14.8	3	300
14.421	254.5	22.26	14.0	2½	370
13.80	254.8	22.44	(7.0 ... 10.8)		N

$\Delta 191 = h 4796; -58^\circ 62'52'' + 50; 8.4 + 8.2$

A.R.  $15^h 35^m 8^s$ ; Decl.  $-58^\circ 17'$

17.463	296.9	32.41	19.5	2	370
17.551	296.6	32.72	18.9	2	370
17.718	297.3	32.55	19.6	2	370
17.58	296.9	32.56	(8.4 ... 8.7)		D?

$h 4800; -45^\circ 75'88''; 8.4$

A.R.  $15^h 35^m 51^s$ ; Decl.  $-45^\circ 23'$

13.717	10.3	6.67	19.7	2½	300
14.321	9.7	6.62	18.2	2	370
14.337	9.3	6.46	13.9	2½	370
14.12	9.8	6.58	(9.6 ... 9.7)		F

I 546;  $-55^\circ 66'89''; 7.9$

A.R.  $15^h 35^m 54^s$ ; Decl.  $-55^\circ 35'$

13.324	264.5	0.76	13.3	4	666
13.329	266.4	0.83	14.6	3	666
13.365	264.2	—	13.0	2	666
14.299	266.6	0.97	15.1	3	475
13.58	265.4	0.85	(8.6 ... 9.4)		

$h 4802; -42^\circ 71'83''; 9.4$

A.R.  $15^h 38^m 53^s$ ; Decl.  $-42^\circ 11'$

14.449	283.6	4.73	17.3	2	370
14.451	280.9	4.87	13.7	2½	370
14.462	282.8	5.00	13.4	2	370
14.45	282.4	4.87	(10.4 ... 11.8)		N

$h$  4806;  $-54^\circ 6705$ ; 8.6

A.R.  $15^h 40^m 32^s$ ; Decl.  $-54^\circ 22'$

13.157	326.0	15.24	14.5	3	300
13.332	327.3	15.07	14.1	2	300
13.348	326.5	15.07	13.3	2	300
13.28	326.6	15.13	(8.8 ... 9.5)		N

$h$  4805;  $-52^\circ 8944$ ; 6.8

A.R.  $15^h 40^m 39^s$ ; Decl.  $-52^\circ 49'$

17.272	127.0	28.31	14.7	3	370
17.343	127.7	28.44	15.6	2	370
17.31	127.3	28.37	(6.1 ... 11.8)		N

$\Delta$  193;  $-54^\circ 6711$ ; 6.7

A.R.  $15^h 41^m 25^s$ ; Decl.  $-54^\circ 40'$

13.157	17.2	19.74	14.7	3	300
13.332	17.5	19.63	14.3	2	300
13.24	17.3	19.69	(7.3 ... 9.3)		M

$h$  4808;  $-44^\circ 7624$ ; 9.6

A.R.  $15^h 41^m 46^s$ ; Decl.  $-44^\circ 2'$

14.449	58.4	8.89	17.5	1½	370
14.462	57.5	8.74	13.7	2	370
14.476	59.0	8.74	13.1	2	370
14.46	58.3	8.79	(10.9 ... 11.1)		107

$h$  4810;  $-46^\circ 7745$ ; 8.4

A.R.  $15^h 42^m 21^s$ ; Decl.  $-46^\circ 6'$

14.462	64.0	17.23	13.9	2	370
14.476	63.8	16.95	13.2	2	370
14.531	64.2	16.90	19.9	2	370
14.49	64.0	17.03	(8.9 ... 10.0)		F

$h$  4811;  $-42^\circ 7208$ ; 9.2

A.R.  $15^h 42^m 35^s$ ; Decl.  $-42^\circ 2'$

14.451	62.7	8.86	13.8	3	370
14.462	62.6	8.86	13.6	2	370
14.46	62.7	8.86	(10.1 ... 11.1)		D?

Sellers 11;  $-60^\circ 6191$ ; 6.5

A.R.  $15^h 44^m 19^s$ ; Decl.  $-60^\circ 22'$

17.720	91.7	1.36	19.2	2	370
17.731	96.2	1.32	20.5	1½	370
17.761	94.9	1.33	20.3	2	370
17.74	94.3	1.34	(7.0 ... 8.5)		D

(Sigue Continued.)

$AC + AD = \Delta 194 = h$  4809

$AC$ ;  $C = -60^\circ 6187$ ; 8.5

17.720	257.4	48.01	18.8	2	370
17.731	257.0	48.27	20.2	1½	370
17.73	257.2	48.14	(7.0 ... 8.8)		M

$AD$ ;  $D = -60^\circ 6192$ ; 9.0

17.720	48.8	44.79	19.0	2	370
17.731	48.0	45.29	20.4	1½	370
17.73	48.4	45.04	(7.0 ... 9.1)		M

$h$  4813;  $-59^\circ 6428$ ; 6.5

A.R.  $15^h 45^m 5^s$ ; Decl.  $-59^\circ 48'$

17.720	100.6	3.91	19.4	2	370
17.731	101.2	3.90	20.6	1½	370
17.761	99.7	3.85	20.4	2	370
17.74	100.5	3.89	(6.7 ... 9.4)		20

$\Delta$  195;  $-49^\circ 8731$ ; 7.2

A.R.  $15^h 45^m 39^s$ ; Decl.  $-49^\circ 58'$

13.447	9.6	11.79	19.1	2	300
13.507	9.7	11.93	15.0	3	300
13.48	9.7	11.86	(8.0 ... 8.5)		F

$h$  4817;  $-45^\circ 7721$ ; 9.6:

A.R.  $15^h 46^m 15^s$ ; Decl.  $-45^\circ 38'$

14.476	294.0	12.79	13.4	2	370
14.531	294.6	—	20.1	2	370
14.534	293.9	12.86	17.8	2	370
14.51	294.2	12.83	(10.9 ... 11.7)		N

BC

14.476	323.5	9.87	13.5	2	370
14.534	324.5	9.83	18.0	2	370
14.51	324.0	9.85	(11.7 ... 12.1)		N

BD

14.476	274.6	10.72	13.6	2	370
14.534	276.2	11.02	18.3	2	370
14.51	275.4	10.88	(11.7 ... 13.0)		N

$h$  4818;  $-45^\circ 7723$ ; 9.8

A.R.  $15^h 46^m 17^s$ ; Decl.  $-45^\circ 39'$

14.476	115.0	12.22	13.7	2	370
14.534	114.0	12.61	18.5	2	370
14.536	114.0	12.59	14.6	2½	370
14.52	114.3	12.48	(11.2 ... 11.4)		N

*h* 4823;  $-43^{\circ} 74'13''$ ; 8.1A.R.  $15^{\text{h}} 51^{\text{m}} 41^{\text{s}}$ ; Decl.  $-43^{\circ} 28'$ 

13.709	228.9	34.10	19.9	2	300
14.102	229.8	33.96	13.6	2	475
13.94	229.4	34.03	(7.8 ... 12.5)		N

 $\lambda$  254;  $-46^{\circ} 78'08''$ ; 7.9A.R.  $15^{\text{h}} 52^{\text{m}} 16^{\text{s}}$ ; Decl.  $-46^{\circ} 11'$ 

13.463	196.2	1.44	19.1	$2\frac{1}{2}$	666
14.380	197.5	1.31	14.7	$3\frac{1}{2}$	370
14.421	196.5	1.72	14.2	$2\frac{1}{2}$	370
14.424	197.3	1.67	12.4	3	370
14.17	196.9	1.53	(7.8 ... 9.2)		D?

*h* 4824;  $-45^{\circ} 77'63''$ ; 8.7A.R.  $15^{\text{h}} 52^{\text{m}} 50^{\text{s}}$ ; Decl.  $-45^{\circ} 55'$ 

13.717	245.5	10.04	19.9	$2\frac{1}{2}$	300
14.321	245.5	9.82	18.4	2	370
14.02	245.5	9.93	(9.4 ... 10.6)		A?

*h* 4825;  $\gamma$  Normae; 5.5A.R.  $15^{\text{h}} 53^{\text{m}} 23^{\text{s}}$ ; Decl.  $-57^{\circ} 25'$ 

13.365	247.6	10.90	13.5	2	300
13.422	248.3	10.63	13.1	2	300
13.545	247.3	11.10	18.7	2	300
13.44	247.7	10.84	(5.2 ... 8.0)		108

*h* 4827;  $-43^{\circ} 74'34''$ ; 8.8A.R.  $15^{\text{h}} 55^{\text{m}} 18^{\text{s}}$ ; Decl.  $-43^{\circ} 4'$ 

13.717	166.0	17.08	20.1	3	300
14.321	165.6	17.25	18.7	2	370
14.02	165.8	17.17	(10.1 ... 10.8)		D?

*h* 4828;  $-42^{\circ} 72'77''$ ; 8.6A.R.  $15^{\text{h}} 55^{\text{m}} 59^{\text{s}}$ ; Decl.  $-42^{\circ} 60'$ 

13.717	89.6	8.87	20.3	$2\frac{1}{2}$	300
14.162	90.7	8.71	13.8	2	475
14.321	90.9	9.00	18.9	2	370
14.07	90.4	8.86	(8.9 ... 10.9)		N

*h* 4829;  $-59^{\circ} 66'07''$ ; 8.6A.R.  $15^{\text{h}} 56^{\text{m}} 40^{\text{s}}$ ; Decl.  $-59^{\circ} 47'$ 

17.627	349.7	7.28	20.3	2	370
17.720	348.4	7.46	19.6	2	370
17.731	350.5	7.51	20.7	$1\frac{1}{2}$	370
17.69	350.5	7.42	(8.8 ... 8.9)		109

Dawson 18;  $-59^{\circ} 66'08''$ ; 8.8A.R.  $15^{\text{h}} 56^{\text{m}} 48^{\text{s}}$ ; Decl.  $-59^{\circ} 45'$ 

17.74	AB	205.0	6.5	(9.2 ... 12.0)	
17.74	BC	210	3.0	(12.0 ... 12.5)	110

Dawson 19;  $-31^{\circ} 43'14''$ ; 8.8A.R.  $15^{\text{h}} 59^{\text{m}} 23^{\text{s}}$ ; Decl.  $-31^{\circ} 15'$ 

14.503	45.6	1.30	14.8	2	370
14.531	43.9	1.33	18.6	$2\frac{1}{2}$	370
14.536	44.6	1.25	14.8	3	370
14.52	44.7	1.29	(9.7 ... 9.9)		111

*h* 4833;  $-45^{\circ} 78'08''$ ; 9.4A.R.  $16^{\text{h}} 0^{\text{m}} 20^{\text{s}}$ ; Decl.  $-45^{\circ} 60'$ 

13.272	138.8	7.47	13.5	3	300
13.294	137.9	7.40	14.0	$2\frac{1}{2}$	300
13.447	137.6	[8.06]	19.5	$2\frac{1}{2}$	300
13.463	139.0	7.43	19.3	3	300
13.37	138.3	7.43	(9.9 ... 10.0)		N

Brisbane;  $-32^{\circ} 40'87''$ ; 7.4A.R.  $16^{\text{h}} 1^{\text{m}} 34^{\text{s}}$ ; Decl.  $-32^{\circ} 19'$ 

14.479	85.7	7.84	19.9	2	370
14.490	85.0	7.75	13.6	$2\frac{1}{2}$	370
14.48	85.3	7.79	(6.8 ... 7.2)		D?

C6. 44;  $-56^{\circ} 74'11''$ ; 8.0A.R.  $16^{\text{h}} 3^{\text{m}} 20^{\text{s}}$ ; Decl.  $-56^{\circ} 5'$ 

13.157	130.0	3.23	15.0	3	300
13.176	130.7	3.24	13.6	2	666
13.365	129.7	3.35	13.7	2	300
13.23	130.1	3.27	(8.6 ... 9.7)		

*h* 4835;  $-53^{\circ} 74'00''$ ; 8.5A.R.  $16^{\text{h}} 3^{\text{m}} 30^{\text{s}}$ ; Decl.  $-53^{\circ} 55'$ 

16.718	81.0	9.65	20.1	2	370
16.726	81.2	9.51	20.6	$2\frac{1}{2}$	370
16.729	81.2	9.66	20.1	3	370
16.72	81.1	9.61	(8.8 ... 9.3)		F

*h* 4837;  $-43^{\circ} 74'76''$ ; 8.4A.R.  $16^{\text{h}} 3^{\text{m}} 41^{\text{s}}$ ; Decl.  $-43^{\circ} 19'$ 

14.449	253.2	9.03	18.0	$1\frac{1}{2}$	370
14.462	254.1	9.20	14.3	$2\frac{1}{2}$	370
14.476	254.2	9.20	13.9	2	370
14.46	253.8	9.14	(8.9 ... 9.0)		F

*h* 4838;  $-49^{\circ} 90'38'' + 9''$ ; 8.2 + 9.6A.R.  $16^{\text{h}} 4^{\text{m}} 57^{\text{s}}$ ; Decl.  $-49^{\circ} 46'$ 

13.272	138.8	24.17	13.8	3	300
13.294	138.6	24.15	14.2	3	300
13.28	138.7	24.16	(8.5 ... 9.4)		F

I 558;  $-56^{\circ} 7473$ ; 8.4

A.R.  $16^h 5^m 26^s$ ; Decl.  $-56^{\circ} 22'$

13.365	50.0	1.67	14.3	3	300
14.299	54.2	1.77	15.4	3	475
14.328	54.0	1.82	13.5	$2\frac{1}{2}$	370
14.00	52.7	1.75	(8.5 ... 10.1)		112

*h* 4841;  $\gamma^2$  Normae; 6.7 + 9.8

A.R.  $16^h 10^m 30^s$ ; Decl.  $-49^{\circ} 51'$

13.294	3.4	42.04	14.4	$2\frac{1}{2}$	300
13.428	3.9	42.46	19.1	$1\frac{1}{2}$	300
13.463	3.3	42.26	19.5	$2\frac{1}{2}$	300
13.40	3.5	42.25	(4.7 ... 9.4)		R

*h* 4842;  $-46^{\circ} 7891 + 90$ ; 7.9 + 9.2

A.R.  $16^h 10^m 44^s$ ; Decl.  $-46^{\circ} 55'$

13.294	199.9	20.01	14.8	3	300
13.428	199.3	19.77	19.3	$1\frac{1}{2}$	300
13.463	199.6	19.65	19.7	$2\frac{1}{2}$	300
13.40	199.6	19.81	(8.4 ... 9.4)		N

$\Delta$  200;  $-43^{\circ} 7520 + 19$ ; 7.3 + 9.7

A.R.  $16^h 13^m 40^s$ ; Decl.  $-43^{\circ} 37'$

14.449	195.7	40.68	18.2	$1\frac{1}{2}$	370
14.462	195.8	40.64	14.4	$2\frac{1}{2}$	370
14.46	195.8	40.66	(6.4 ... 9.5)		D?

*h* 4844;  $-59^{\circ} 6729$ ; 9.1

A.R.  $16^h 14^m 54^s$ ; Decl.  $-59^{\circ} 8'$

17.513	64.7	6.90	19.0	2	370
17.627	64.4	6.89	20.5	2	370
17.761	65.0	6.65	20.7	2	370
17.63	64.7	6.81	(9.8 ... 10.1)		N

*h* 4846;  $-47^{\circ} 7648$ ; 8.6

A.R.  $16^h 15^m 24^s$ ; Decl.  $-47^{\circ} 56'$

13.266	147.6	11.81	14.0	3	300
13.447	146.9	11.49	19.8	2	300
13.463	147.9	11.46	19.9	3	300
13.39	147.5	11.59	(8.9 ... 9.6)		M

C6. 45;  $-48^{\circ} 8449$ ; 7.6

A.R.  $16^h 16^m 1^s$ ; Decl.  $-48^{\circ} 51'$

13.266	186.3	1.81	14.2	3	666
13.464	185.0	1.61	20.1	3	300
13.507	183.9	1.82	15.3	$2\frac{1}{2}$	666
14.347	183.0	1.71	13.4	3	650
13.65	184.5	1.74	(8.0 ... 8.1)		P

(*Sigue* *Continued.*)

AC

13.266	104.3	11.57	14.1	3	300
13.464	102.6	11.93	20.2	$2\frac{1}{2}$	300
14.347	104.7	12.09	13.6	3	370
13.69	103.9	11.86	(8.0 ... 11.1)		R

*h* 4853;  $\varepsilon$  Normae; 5.1

A.R.  $16^h 18^m 1^s$ ; Decl.  $-47^{\circ} 16'$

13.266	334.6	22.91	14.5	3	300
13.447	335.3	23.06	20.4	2	300
13.36	334.9	22.98	(5.0 ... 8.0)		F

*h* 4857;  $-46^{\circ} 8038$ ; 7.9

A.R.  $16^h 21^m 58^s$ ; Decl.  $-46^{\circ} 12'$

13.472	70.4	6.64	19.9	2	300
13.507	70.2	6.76	15.6	$2\frac{1}{2}$	300
13.509	68.6	6.56	13.9	2	300
13.50	69.7	6.65	(8.0 ... 9.1)		20

*h* 4856;  $-52^{\circ} 9934$ ; 9.4

A.R.  $16^h 22^m 4^s$ ; Decl.  $-52^{\circ} 20'$

16.729	237.9	8.17	20.3	3	370
16.732	239.2	8.09	20.2	2	370
16.737	238.1	8.26	20.8	2	370
16.73	238.4	8.17	(9.8 ... 11.1)		N

$\Delta$  203;  $-60^{\circ} 6550 + 48$ ; 8.2 + 8.4

A.R.  $16^h 22^m 5^s$ ; Decl.  $-60^{\circ} 38'$

17.513	259.5	28.65	19.2	2	370
17.551	259.0	28.61	19.1	2	370
17.761	259.0	28.69	20.8	2	370
17.61	259.2	28.65	(8.2 ... 8.3)		R

*h* 4861;  $-47^{\circ} 7765$ ; 6.9

A.R.  $16^h 24^m 39^s$ ; Decl.  $-47^{\circ} 50'$

13.509	359.0	36.60	14.1	2	300
13.513	[358.7]	—	19.3	1	300
14.394	358.8	35.91	15.2	2	370
13.95	358.9	36.25	(7.5 ... 13.2)		N

*h* 4862;  $-61^{\circ} 5746$ ; 8.0

A.R.  $16^h 26^m 16^s$ ; Decl.  $-61^{\circ} 18'$

17.551	179.2	11.10	19.3	2	370
17.761	178.3	11.06	21.0	2	370
17.66	178.7	11.08	(8.9 ... 9.5)		D†

I 374;  $-50^{\circ} 9525$ ; 7.6A.R.  $16^h 26^m 30^s$ ; Decl.  $-50^{\circ} 59'$ 

16.729	297.9	2.78	20.7	3	370
16.732	296.6	2.77	20.3	2	370
16.737	299.3	2.86	21.0	2	370
16.73	297.9	2.80	(7.8 ... 11.9)		23

h 4863;  $-53^{\circ} 8091$ ; 8.2A.R.  $16^h 27^m 26^s$ ; Decl.  $-53^{\circ} 31'$ 

16.718	119.7	3.94	20.6	2	370
16.726	120.7	4.19	20.8	2½	370
16.729	120.7	4.18	20.5	3½	370
16.72	120.4	4.10	(9.0 ... 9.4)		F

h 4866;  $-56^{\circ} 7804$ ; 7.5A.R.  $16^h 29^m 22^s$ ; Decl.  $-56^{\circ} 44'$ 

13.157	124.4	3.94	15.2	3	300
13.178	124.2	3.95	13.9	2	666
13.187	126.7	3.99	14.1	2	280
13.17	125.1	3.96	(7.8 ... 8.1)		F

h 4867;  $-43^{\circ} 7635$ ; 6.6A.R.  $16^h 29^m 36^s$ ; Decl.  $-43^{\circ} 9'$ 

14.449	294.4	16.63	18.5	2	370
14.462	294.8	16.31	14.7	2	370
14.476	293.5	16.29	14.0	2	370
14.46	294.2	16.41	(6.6 ... 9.9)		21

h 4873;  $-49^{\circ} 9498 + 9502$ ; 8.6 + 9.5A.R.  $16^h 30^m 19^s$ ; Decl.  $-49^{\circ} 6'$ 

13.509	71.8	31.12	14.7	2	300
14.440	70.8	31.06	14.6	2	370
14.481	71.2	30.92	14.3	2	370
14.14	71.3	31.03	(9.1 ... 9.3)		F

## AC

13.509	170.7	13.38	14.5	2	300
14.440	169.2	13.43	14.8	2	370
14.481	168.8	13.49	14.5	2	370
14.14	169.6	13.43	(9.1 ... 12.0)		N

## BD

14.440	36.6	8.57	14.9	2	370
14.481	34.5	8.68	14.7	2	370
14.46	35.6	8.62	(9.3 ... 13.0)		N

I 405;  $-46^{\circ} 8112$ ; 8.4A.R.  $16^h 30^m 26^s$ ; Decl.  $-46^{\circ} 24'$ 

14.424	133.6	2.70	12.6	3	370
14.438	137.2	2.54	13.6	3	370
14.441	134.8	2.78	20.3	2	370
14.43	135.2	2.67	(9.2 ... 9.4)		

Sellors 12;  $-47^{\circ} 7811$ ; 7.8A.R.  $16^h 30^m 42^s$ ; Decl.  $-47^{\circ} 32'$ 

14.424	175.6	1.31	13.1	2½	370
14.438	176.9	1.31	13.9	3	370
14.441	172.7	1.36	20.4	2	370
14.43	175.1	1.33	(8.2 ... 8.3)		F

AC = h 4871; C =  $-47^{\circ} 7812$ ; 9.5

14.424	45.1	29.52	13.2	2½	370
14.438	44.2	29.91	14.0	2½	370
14.441	44.2	30.25	20.5	2	370
14.462	44.9	30.21	15.1	2	370
14.44	44.6	29.97	(8.2 ... 10.5)		M

C6. 46;  $-47^{\circ} 7818$ ; 7.9A.R.  $16^h 31^m 29^s$ ; Decl.  $-47^{\circ} 25'$ 

14.424	99.5	2.90	13.4	3	370
14.438	101.6	2.78	14.1	2	370
14.441	99.9	2.60	20.7	2	370
14.462	101.2	2.86	15.3	2½	370
14.44	100.5	2.79	(9.0 ... 9.6)		F

Sellors 21;  $-47^{\circ} 7821$ ; 7.3A.R.  $16^h 31^m 50^s$ ; Decl.  $-47^{\circ} 30'$ 

14.424	322.1	1.88	13.5	3	370
14.438	316.5	1.98	14.2	2	370
14.462	319.1	2.10	15.4	2½	370
14.528	316.8	1.93	14.5	2	370
14.46	318.4	1.97	(7.8 ... 9.8)		F

h 4874 = Rus 282;  $-60^{\circ} 6614$ ; 8.0A.R.  $16^h 31^m 53^s$ ; Decl.  $-60^{\circ} 41'$ 

17.551	295.4	3.22	19.5	2	370
17.761	296.8	3.27	21.1	2	370
17.767	297.1	3.21	21.2	2	370
17.69	296.4	3.23	(9.1 ... 9.1)		20

 $-48^{\circ} 8703$ ; 6.8A.R.  $16^h 31^m 59^s$ ; Decl.  $-48^{\circ} 31'$ 

## AB = Melbourne

14.424	15.9	1.93	13.6	3	370
14.536	12.4	1.82	15.5	3	370
14.572	12.7	1.67	16.6	4	370
14.51	13.7	1.80	(6.3 ... 9.0)		F

AC =  $\Delta$  206 = h 4876 AB

14.424	265.3	9.76	13.8	2½	370
14.476	266.0	9.83	14.3	2	370
14.569	265.9	9.85	18.0	2	370
14.49	265.7	9.81	(6.3 ... 7.2)		F

(Sigue Continued.)



AD = h 4876 AC = I 96

14.424	160.8	13.37	13.9	2½	370
14.536	159.8	13.34	15.7	3	370
14.48	160.3	13.35	(6.3 ... 10.0)		N

h 4877; -48° 8736 + 8; 9.0 + 10.0

A.R. 16<sup>h</sup> 32<sup>m</sup> 57<sup>s</sup>; Decl. -48° 19'

14.424	93.5	19.63	14.1	2½	370
14.438	94.7	19.79	14.4	2	370
14.476	93.8	19.90	14.5	2	370
14.45	94.0	19.77	(9.4 ... 10.1)		I13

h 4881; -47° 7860; 8.4

A.R. 16<sup>h</sup> 34<sup>m</sup> 54<sup>s</sup>; Decl. -47° 14'

14.424	254.0	9.31	13.0	2½	370
14.438	254.1	9.38	13.8	3	370
14.43	254.1	9.35	(9.4 ... 9.9)		N

h 4882; -48° 8773 + 4; 9.4 + 9.5

A.R. 16<sup>h</sup> 35<sup>m</sup> 21<sup>s</sup>; Decl. -48° 46'

14.424	169.6	19.37	14.2	3	370
14.441	169.3	19.59	21.0	2	370
14.43	169.5	19.48	(9.6 ... 9.7)		N

Δ 207 = h 4883; -42° 7482 + 3; 8.8 + 8.9

A.R. 16<sup>h</sup> 35<sup>m</sup> 39<sup>s</sup>; Decl. -42° 9'

14.462	185.2	11.42	14.9	2	370
14.476	185.3	11.58	14.2	2	370
14.47	185.3	11.50	(9.0 ... 9.2)		F

Δ 211; -48° 8811 + 14 + 15; 8.0 + 7.9 + 8.4

A.R. 16<sup>h</sup> 38<sup>m</sup> 15<sup>s</sup>; Decl. -48° 7'

13.395	124.3	106.03	14.7	1½	300
13.490	124.6	106.21	14.3	3	300
13.44	124.5	106.12	(7.1 ... 8.3)		N

AC

13.395	143.5	128.96	14.3	1½	300
13.490	143.5	129.18	14.4	3	300
13.44	143.5	129.07	(7.1 ... 8.3)		N

CD = h 4885

13.395	243.9	4.36	13.8	2	300
13.490	242.4	4.27	14.5	3	300
14.350	242.6	4.19	15.3	3	370
13.74	243.0	4.27	(8.3 ... 9.3)		F?

Δ 210; -55° 7693 + 4; 8.9 + 8.5

A.R. 16<sup>h</sup> 38<sup>m</sup> 30<sup>s</sup>; Decl. -55° 12'

13.187	352.1	75.48	14.5	2	280
13.365	351.8	75.12	14.8	2½	300
13.422	351.9	75.26	13.4	2	300
13.32	351.9	75.29	(8.6 ... 8.7)		I14

C6. 47; -49° 9629; 7.2

A.R. 16<sup>h</sup> 41<sup>m</sup> 3<sup>s</sup>; Decl. -49° 49'

13.490	43.0	2.92	14.7	3	300
14.350	44.1	2.97	15.4	3	370
14.380	43.2	2.80	15.4	4	370
14.07	43.4	2.90	(7.0 ... 7.1)		F

h 4889; -37° 6755; 6.6

A.R. 16<sup>h</sup> 42<sup>m</sup> 35<sup>s</sup>; Decl. -37° 18'

14.350	5.7	6.72	14.8	2½	370
14.391	5.1	6.66	14.3	2½	370
14.394	6.1	6.94	14.9	2	370
14.38	5.6	6.77	(6.7 ... 8.2)		F

h 4890; -46° 8281; 7.8

A.R. 16<sup>h</sup> 44<sup>m</sup> 44<sup>s</sup>; Decl. -46° 42'

13.490	323.3	30.84	14.8	3	300
14.476	324.4	30.72	14.7	1½	370
14.481	324.4	30.87	15.0	2	370
14.15	324.0	30.81	(8.0 ... 8.1)		F

h 4896; -46° 8299; 7.4

A.R. 16<sup>h</sup> 47<sup>m</sup> 0<sup>s</sup>; Decl. -46° 39'

13.490	24.4	4.09	15.1	3	300
14.476	26.8	4.16	14.9	1½	370
14.481	25.3	4.13	15.2	2	370
14.15	25.5	4.13	(7.9 ... 9.2)		F

h 4899; -45° 8225; 8.8

A.R. 16<sup>h</sup> 48<sup>m</sup> 47<sup>s</sup>; Decl. -45° 44'

13.709	272.2	2.69	20.4	2	300
13.717	272.6	2.40	20.7	2½	300
13.737	270.4	2.47	21.2	3	300
13.72	271.7	2.52	(9.3 ... 9.7)		F

h 4900 = h 4897; -59° 6876 + 7; 7.8 + 9.2

A.R. 16<sup>h</sup> 49<sup>m</sup> 2<sup>s</sup>; Decl. -59° 8'

17.551	11.8	26.17	19.7	2	370
17.761	12.1	26.03	21.3	2	370
17.66	12.0	26.10	(8.0 ... 11.0)		N

$h 4901 = \text{Rus } 287; -58^\circ 6960; 7.0$ A.R.  $16^h 50^m 19^s$ ; Decl.  $-58^\circ 39'$ 

17.551	128.8	2.77	19.9	2	370
17.606	130.7	2.87	20.5	3	650
17.761	130.2	2.84	21.5	1½	370
17.64	129.9	2.83	(8.0 ... 8.1)		F

Holden 131;  $-56^\circ 7940; 6.9$ A.R.  $16^h 50^m 42^s$ ; Decl.  $-56^\circ 22'$ 

13.365	133.6	2.64	15.5	2½	300
13.545	134.4	2.43	19.0	2	300
14.328	131.5	2.60	13.7	2	370
13.75	133.2	2.56	(7.5 ... 9.8)		F

I 997;  $-58^\circ 6975; 7.8$ A.R.  $16^h 52^m 21^s$ ; Decl.  $-58^\circ 22'$ 

17.606	163.5	0.68	20.3	3	650
17.783	168.3	0.69	21.9	2½	370
17.69	165.9	0.68	(8.4 ... 8.5)		142

 $h 4905; -54^\circ 7986; 10.1$ A.R.  $16^h 52^m 43^s$ ; Decl.  $-54^\circ 52'$ 

13.422	59.6	34.39	13.8	1½	300
13.545	59.4	34.34	19.3	2	300
13.48	59.5	34.36	(9.1 ... 10.0)		115

Hargrave (288);  $-48^\circ 8968; 8.6$ A.R.  $16^h 52^m 54^s$ ; Decl.  $-48^\circ 44'$ 

13.509	50.7	2.60	15.1	2	300
14.421	52.6	2.77	14.8	2	370
14.424	51.9	2.60	14.4	3	370
14.12	51.7	2.66	(9.0 ... 9.5)		F

AC =  $h 4906$ 

13.509	235.5	15.48	15.2	2	300
14.421	236.6	15.49	14.9	2	370
13.97	236.1	15.49	(9.0 ... 10.8)		F

C6. 48;  $-49^\circ 9727; 7.5$ A.R.  $16^h 53^m 17^s$ ; Decl.  $-49^\circ 58'$ 

14.421	234.6	8.07	14.5	2	370
14.424	233.1	8.01	14.5	3	370
14.440	234.4	8.06	15.1	2	370
14.43	234.0	8.05	(7.6 ... 8.4)		F

C6. 49;  $-46^\circ 8360; 8.3$ A.R.  $16^h 53^m 42^s$ ; Decl.  $-46^\circ 34'$ 

13.509	46.1	3.62	15.3	2	300
14.424	44.3	3.72	14.6	3	370
14.440	46.0	3.75	15.3	2	370
14.12	45.8	3.70	(8.8 ... 9.3)		D?

 $\Delta 212 = h 4909; -50^\circ 9813; 8.0$ A.R.  $16^h 54^m 18^s$ ; Decl.  $-50^\circ 54'$ 

16.718	284.4	16.07	20.8	2	370
16.726	284.2	16.24	20.9	2	370
16.72	284.3	16.16	(8.5 ... 8.8)		116

Dawson 20;  $-36^\circ 7109; 7.5$ A.R.  $16^h 54^m 30^s$ ; Decl.  $-36^\circ 41'$ 

14.299	242.5	1.50	14.5	3	475
14.309	238.9	1.49	15.2	3	650
14.326	239.3	1.55	15.5	2	370
14.31	240.2	1.51	(8.5 ... 9.4)		111

 $h 4913; -47^\circ 8019; 8.1$ A.R.  $16^h 55^m 45^s$ ; Decl.  $-47^\circ 4'$ 

13.509	234.9	3.68	15.5	2	300
14.424	235.6	3.37	14.7	3	370
14.440	236.0	3.46	15.4	2	370
14.12	235.5	3.50	(8.8 ... 9.2)		F

 $h 4916; -49^\circ 9764; 8.4$ A.R.  $16^h 58^m 58^s$ ; Decl.  $-49^\circ 18'$ 

14.424	277.5	10.07	14.9	3	370
14.440	277.1	9.93	15.5	2	370
14.43	277.7	10.00	(8.8 ... 9.1)		F?

 $h 4917; -54^\circ 8046; 8.4$ A.R.  $16^h 59^m 35^s$ ; Decl.  $-54^\circ 10'$ 

13.545	358.4	12.00	19.5	2	300
14.328	359.6	12.68	14.1	2	370
14.334	359.4	11.83	14.8	2	370
14.07	359.1	12.17	(8.8 ... 12.0)		A

 $h 4918; -42^\circ 7648; 8.3$ A.R.  $16^h 59^m 47^s$ ; Decl.  $-42^\circ 32'$ 

13.709	291.4	13.89	20.9	2	300
13.718	290.6	13.72	20.8	3	300
13.737	290.0	13.60	21.3	2	300
13.72	290.7	13.74	(8.7 ... 11.5)		N

 $\Delta 213; -46^\circ 8423; 7.1$ A.R.  $17^h 1^m 4^s$ ; Decl.  $-46^\circ 34'$ 

13.272	167.0	8.21	14.7	3	300
13.447	166.3	8.03	14.5	2	300
13.490	167.0	8.01	15.2	3	300
13.40	166.8	8.08	(7.5 ... 8.7)		F

*h* 4920;  $-58^{\circ} 70'14''$ ; 7.0  
 A.R.  $17^{\text{h}} 2^{\text{m}} 10^{\text{s}}$ ; Decl.  $-58^{\circ} 26'$

17.606	328.0	2.96	20.7	3	370
17.767	324.0	3.14	21.5	2	370
17.783	325.9	3.33	22.0	2	370
17.72	326.0	3.14	(7.3 ... 10.2)		F

Rus 294;  $-54^{\circ} 8'10.5''$ ; 9.3:  
 A.R.  $17^{\text{h}} 3^{\text{m}} 33^{\text{s}}$ ; Decl.  $-54^{\circ} 16'$

13.179	115.6	14.67	14.7	2	666
13.187	117.1	14.55	14.8	2	280
13.18	116.4	14.61	(9.5 ... 9.7)		F

*h* 4927;  $-50^{\circ} 9'54''$ ; 9.2  
 A.R.  $17^{\text{h}} 8^{\text{m}} 4^{\text{s}}$ ; Decl.  $-50^{\circ} 59'$

16.726	144.3	10.98	21.1	2	370
16.729	144.5	10.95	20.8	3	370
16.73	144.4	10.96	(9.9 ... 10.1)		N

*h* 4929;  $-45^{\circ} 8'41''$ ; 8.2  
 A.R.  $17^{\text{h}} 8^{\text{m}} 53^{\text{s}}$ ; Decl.  $-45^{\circ} 57'$

13.737	224.4	10.85	21.6	2½	300
14.162	224.9	10.70	14.1	2	370
13.95	224.6	10.77	(9.1 ... 10.4)		N

*h* 4930;  $-54^{\circ} 8'19.3''$ ; 8.3  
 A.R.  $17^{\text{h}} 9^{\text{m}} 17^{\text{s}}$ ; Decl.  $-54^{\circ} 13'$

13.493	42.5	8.67	15.2	3	300
13.545	43.2	8.80	19.9	2	300
14.328	43.2	8.89	14.4	2	370
13.79	43.0	8.79	(8.7 ... 10.3)		F?

Brisbane = Rus 297;  $-46^{\circ} 8'51.3''$ ; 7.3  
 A.R.  $17^{\text{h}} 9^{\text{m}} 35^{\text{s}}$ ; Decl.  $-46^{\circ} 30'$

13.490	144.6	2.47	15.4	3	300
13.509	142.4	3.01	15.6	2	300
14.350	145.0	2.70	15.6	3	370
14.375	146.2	2.86	15.8	2	370
13.93	144.6	2.76	(6.1 ... 8.3)		B

*h* 4931;  $-59^{\circ} 6'69.9''$ ; 7.3  
 A.R.  $17^{\text{h}} 9^{\text{m}} 37^{\text{s}}$ ; Decl.  $-59^{\circ} 18'$

17.551	253.5	0.96	20.2	2	475
17.606	256.2	1.15	21.2	3	650
17.767	258.8	1.09	21.7	2	370
17.783	255.6	1.17	20.8	2½	370
17.67	256.0	1.11	(8.4 ... 8.5)		F

*h* 4938;  $-56^{\circ} 8'15.4'' + 5''$ ; 8.6 + 8.8  
 A.R.  $17^{\text{h}} 10^{\text{m}} 12^{\text{s}}$ ; Decl.  $-56^{\circ} 17'$

13.493	110.1	25.30	15.4	3	300
13.545	109.6	25.18	20.1	2½	300
13.52	109.9	25.24	(8.7 ... 8.7)		F

*h* 4936;  $-46^{\circ} 5'52.6''$ ; 8.8  
 A.R.  $17^{\text{h}} 10^{\text{m}} 49^{\text{s}}$ ; Decl.  $-46^{\circ} 2'$

13.272	77.1	7.57	14.9	2	300
13.447	77.6	7.62	14.7	3	300
13.490	77.3	7.54	15.5	3	300
13.40	77.3	7.58	(9.0 ... 9.5)		F

*h* 4939;  $-56^{\circ} 8'16.5''$ ; 8.3  
 A.R.  $17^{\text{h}} 11^{\text{m}} 1^{\text{s}}$ ; Decl.  $-56^{\circ} 20'$

13.187	224.8	30.35	15.2	2	280
13.493	224.6	30.08	15.5	3	300
13.545	224.6	30.11	20.3	2½	300
13.41	224.7	30.18	(8.7 ... 9.3)		21

*h* 4934;  $-58^{\circ} 7'07.8'' + 7''$ ; 9.3 + 9.4  
 A.R.  $17^{\text{h}} 11^{\text{m}} 11^{\text{s}}$ ; Decl.  $-58^{\circ} 54'$

17.606	269.7	13.42	21.0	3	370
17.767	270.1	13.30	21.9	2	370
17.69	269.9	13.36	(9.6 ... 9.7)		N

Có.;  $-58^{\circ} 7'08.6''$ ; 7.5  
 A.R.  $17^{\text{h}} 11^{\text{m}} 58^{\text{s}}$ ; Decl.  $-58^{\circ} 20'$

17.606	282.8	9.42	20.8	3	370
17.627	282.9	9.41	21.0	1½	370
17.62	282.8	9.42	(7.3 ... 9.9)		11

*h* 4941;  $-51^{\circ} 10'32.8''$ ; 9.1  
 A.R.  $17^{\text{h}} 14^{\text{m}} 1^{\text{s}}$ ; Decl.  $-51^{\circ} 47'$

16.726	314.7	5.81	21.3	2	370
16.729	316.7	5.70	21.0	3½	370
16.732	316.8	5.82	20.5	2	370
16.73	316.1	5.78	(9.7 ... 10.1)		N

*h* 4942;  $\gamma$  Arae; 4.0  
 A.R.  $17^{\text{h}} 14^{\text{m}} 54^{\text{s}}$ ; Decl.  $-56^{\circ} 15'$

13.493	327.8	17.86	15.8	3	300
13.545	328.0	18.00	20.4	2	300
13.52	327.9	17.93	(3.4 ... 10.0)		F

AC

13.493	65.7	41.33	15.6	3	300
13.545	65.7	41.65	20.6	2	300
14.378	66.1	41.88	15.1	2½	370
13.81	65.8	41.62	(3.4 ... 11.2)		N

$h$  4944;  $-47^\circ 8268 + 9$ ;  $9.0 + 9.0$

A.R.  $17^h 15^m 13^s$ ; Decl.  $-47^\circ 2'$

13.272	164.5	13.48	15.1	$2\frac{1}{2}$	300
13.274	164.7	13.43	14.4	2	300
13.447	164.6	13.55	14.8	2	300
13.33	164.6	13.49	(9.6 ... 9.6)		A

$h$  4945;  $-47^\circ 8280$ ; 8.4

A.R.  $17^h 16^m 1^s$ ; Decl.  $-47^\circ 47'$

13.272	111.8	6.61	15.4	3	300
13.274	112.1	6.62	14.5	2	300
13.447	112.3	6.62	15.0	2	300
13.33	112.1	6.62	(9.4 ... 9.8)		D?

$h$  4949;  $-45^\circ 8580$ ; 6.2

A.R.  $17^h 17^m 39^s$ ; Decl.  $-45^\circ 44'$

13.709	263.2	[3.18]	21.5	2	300
13.737	261.1	2.70	21.9	3	300
14.331	259.5	2.58	15.5	3	370
14.334	262.8	2.54	15.8	3	370
14.03	261.6	2.61	(6.5 ... 7.2)		A

AC =  $\Delta$  216; C =  $-45^\circ 8574$ ; 7.1

13.709	312.4	102.77	21.4	2	300
13.737	312.5	103.19	21.7	$2\frac{1}{2}$	300
14.331	312.6	102.74	15.4	3	370
13.93	312.5	102.90	(6.5 ... 7.2)		F

$h$  4950;  $-57^\circ 8577$ ; 9.6

A.R.  $17^h 19^m 22^s$ ; Decl.  $-57^\circ 27'$

14.391	306.0	10.40	15.1	2	370
14.394	307.4	10.55	15.5	2	370
14.39	306.7	10.47	(10.2 ... 11.1)		21

$h$  4952; Véase la nota. See note. 117

$h$  4951;  $\varepsilon$  Arae; 4.1

A.R.  $17^h 19^m 49^s$ ; Decl.  $-60^\circ 35'$

17.761	312.8	47.34	21.8	$1\frac{1}{2}$	370
17.783	312.8	47.49	21.6	$2\frac{1}{2}$	370
17.77	312.8	47.42	(3.5 ... 11.8)		N

$\Delta$  217;  $-43^\circ 8092$ ; 7.1

A.R.  $17^h 19^m 59^s$ ; Decl.  $-43^\circ 52'$

13.709	169.4	13.59	21.3	2	300
13.737	169.3	13.42	22.0	$2\frac{1}{2}$	300
13.72	169.3	13.50	(6.5 ... 7.9)		F

$h$  4955;  $\alpha$  Arae; 4.3

A.R.  $17^h 22^m 11^s$ ; Decl.  $-49^\circ 46'$

13.275	173.0	55.58	14.7	2	300
13.447	172.9	55.59	15.2	2	300
13.36	173.0	55.58	(2.7 ... 10.0)		N

$h$  4957;  $-46^\circ 8708$ ; 8.6

A.R.  $17^h 23^m 4^s$ ; Decl.  $-46^\circ 32'$

13.275	264.3	3.18	15.1	$2\frac{1}{2}$	300
13.447	265.3	3.28	15.3	2	300
13.477	266.1	3.26	20.7	3	300
13.40	265.2	3.24	(9.4 ... 9.5)		D

$h$  4959;  $-55^\circ 8221 + 2$ ;  $9.2 + 9.2$

A.R.  $17^h 25^m 44^s$ ; Decl.  $-55^\circ 32'$

17.343	295.5	19.45	15.8	$1\frac{1}{2}$	370
17.718	294.3	19.70	20.8	2	370
17.720	294.7	19.56	21.2	$1\frac{1}{2}$	370
17.59	294.8	19.57	(9.1 ... 9.2)		5

$h$  4961;  $-59^\circ 7088 + 9$ ;  $9.4 + 9.4$

A.R.  $17^h 27^m 18^s$ ; Decl.  $-59^\circ 51'$

17.606	153.4	17.10	21.4	$2\frac{1}{2}$	370
17.718	153.8	17.14	21.0	2	370
17.66	153.6	17.12	(10.3 ... 10.5)		F?

$h$  4965;  $-51^\circ 10479$ ; 8.0:

A.R.  $17^h 29^m 22^s$ ; Decl.  $-51^\circ 7'$

16.727	231.2	13.58	21.5	2	370
16.729	231.4	13.32	21.2	$3\frac{1}{2}$	370
16.73	231.3	13.45	(8.6 ... 8.8)		F?

$h$  4967;  $-53^\circ 8722?$ ; 9.8

A.R.  $17^h 30^m 38^s$ ; Decl.  $-53^\circ 35'$

16.727	50.1	5.04	21.6	2	370
16.729	48.3	5.03	21.3	3	370
16.732	50.5	5.04	20.7	2	370
16.73	49.6	5.04	(10.7 ... 10.9)		N

$h$  4968; Véase la nota. See note. 118

$h$  4969;  $-53^\circ 8733 + 4$ ;  $10.0 + 9.5$

A.R.  $17^h 31^m 34^s$ ; Decl.  $-53^\circ 58'$

16.697	48.8	17.54	20.1	2	370
16.718	47.4	17.58	22.0	2	370
16.71	48.1	17.56	(9.2 ... 9.4)		21

*h* 4970;  $-48^{\circ} 9406$ ; 8.0

A.R.  $17^{\text{h}} 32^{\text{m}} 42^{\text{s}}$ ; Decl.  $-48^{\circ} 34'$

13.275	68.7	8.11	15.4	2½	300
13.464	69.8	8.20	20.6	2	300
13.477	69.2	8.18	20.9	2½	300
13.41	69.2	8.16	(8.0 ... 8.8)		D?

Rus 303;  $-54^{\circ} 8468$ ; 7.5

A.R.  $17^{\text{h}} 34^{\text{m}} 50^{\text{s}}$ ; Decl.  $-54^{\circ} 4'$

13.493	110.2	3.53	16.0	3	300
14.309	108.3	3.55	15.4	3	370
14.328	110.1	3.52	14.7	2	370
16.718	107.1	3.47	21.7	2½	370
16.727	108.3	3.40	21.8	2	370
16.729	108.3	3.45	21.4	3	370
14.04	109.5	3.53			F
16.72	107.9	3.44	(8.0 ... 9.1)		23

*h* 4973 = *h* 4989;  $-45^{\circ} 8830$ ; 8.0

A.R.  $17^{\text{h}} 35^{\text{m}} 47^{\text{s}}$ ; Decl.  $-45^{\circ} 8'$

14.443	26.4	12.99	14.6	2	370
14.451	26.6	13.27	14.9	2	370
14.476	26.3	12.96	15.1	2	370
14.46	26.4	13.07	(8.2 ... 9.0)		119

*h* 4971;  $-55^{\circ} 8295$ ; 8.8

A.R.  $17^{\text{h}} 36^{\text{m}} 21^{\text{s}}$ ; Decl.  $-55^{\circ} 58'$

14.394	196.5	5.85	15.9	2	370
14.400	196.3	5.63	15.3	3	370
14.424	196.1	5.84	15.0	3	370
14.41	196.3	5.77	(10.2 ... 11.1)		N

Cape 24;  $-44^{\circ} 8775$ ; 8.5

A.R.  $17^{\text{h}} 39^{\text{m}} 26^{\text{s}}$ ; Decl.  $-44^{\circ} 59'$

14.443	329.6	4.16	14.8	2	370
14.476	329.5	4.22	15.3	2	370
14.481	328.0	4.16	15.4	2	370
14.47	329.0	4.18	(9.1 ... 10.0)		

*h* 4978;  $-53^{\circ} 8799$ ; 6.5

A.R.  $17^{\text{h}} 40^{\text{m}} 18^{\text{s}}$ ; Decl.  $-53^{\circ} 34'$

16.727	268.6	12.49	22.0	2	370
16.729	268.3	12.31	21.5	3	370
16.73	268.4	12.40	(6.6 ... 9.4)		F

*h* 4981;  $-50^{\circ} 10391$ ; 8.8

A.R.  $17^{\text{h}} 40^{\text{m}} 28^{\text{s}}$ ; Decl.  $-50^{\circ} 15'$

16.754	16.5	2.52	21.0	2	370
16.759	17.3	2.37	21.9	2	370
16.762	17.4	2.43	21.0	3	370
16.76	17.1	2.44	(9.6 ... 9.7)		51

*h* 4979;  $-60^{\circ} 6953$ ; 7.9

A.R.  $17^{\text{h}} 40^{\text{m}} 47^{\text{s}}$ ; Decl.  $-60^{\circ} 21'$

17.606	239.8	10.51	21.5	3	370
17.718	240.3	10.39	21.3	2	370
17.66	240.0	10.45	(8.0 ... 11.0)		F

*h* 4982;  $-48^{\circ} 9516 + 18$ ;  $7.7 + 9.6$

A.R.  $17^{\text{h}} 40^{\text{m}} 58^{\text{s}}$ ; Decl.  $-48^{\circ} 14'$

13.275	58.7	41.80	15.6	2	300
13.464	58.7	42.06	21.0	2	300
13.37	58.7	41.93	(7.2 ... 9.4)		F

*h* 4980;  $-65^{\circ} 3516$ ; 8.8

A.R.  $17^{\text{h}} 42^{\text{m}} 27^{\text{s}}$ ; Decl.  $-65^{\circ} 10'$

17.783	99.0	7.58	22.2	2	370
17.805	100.6	7.51	22.9	2	370
17.808	101.7	7.47	22.7	2	370
17.80	100.4	7.52	(9.0 ... 11.8)		N

*h* 4984;  $-52^{\circ} 10900$ ; 7.8:

A.R.  $17^{\text{h}} 42^{\text{m}} 40^{\text{s}}$ ; Decl.  $-52^{\circ} 26'$

16.729	8.7	12.39	21.5	3	370
16.732	8.5	12.42	20.8	2	370
16.73	8.6	12.40	(8.3 ... 9.5)		F?

*h* 4985;  $-62^{\circ} 5742$ ; 8.6

A.R.  $17^{\text{h}} 43^{\text{m}} 39^{\text{s}}$ ; Decl.  $-62^{\circ} 58'$

17.783	263.3	21.27	22.3	2	370
17.805	263.1	21.30	23.0	2	370
17.79	263.2	21.28	(8.8 ... 10.0)		D?

*h* 4992;  $-57^{\circ} 8803$ ; 8.0

A.R.  $17^{\text{h}} 46^{\text{m}} 43^{\text{s}}$ ; Decl.  $-57^{\circ} 38'$

14.394	15.1	4.20	16.0	2	370
14.400	15.6	4.21	15.4	3	370
14.424	15.1	4.19	15.1	2½	370
14.41	15.3	4.20	(8.6 ... 9.2)		M

Rü 22 = Rus 304 = Cape 18;  $-55^{\circ} 8375$ ; 7.3

A.R.  $17^{\text{h}} 46^{\text{m}} 48^{\text{s}}$ ; Decl.  $-55^{\circ} 21'$

13.493	94.5	2.65	16.2	3	300
14.328	93.5	2.90	14.9	2½	370
14.334	92.7	2.69	15.2	3	370
14.05	93.6	2.75	(7.7 ... 8.8)		A

*h* 4994;  $-52^{\circ} 10926 + 7$ ;  $9.2 + 9.1$

A.R.  $17^{\text{h}} 47^{\text{m}} 16^{\text{s}}$ ; Decl.  $-52^{\circ} 11'$

16.729	209.2	14.00	21.6	3	370
16.732	208.7	14.16	20.9	2	370
16.73	209.0	14.08	(9.1 ... 9.3)		F

$h$  4996;  $-62^\circ 57'60$ ; 8.0A.R.  $17^h 49^m 2^s$ ; Decl.  $-62^\circ 9'$ 

17.783	250.7	6.03	22.5	2	370
17.805	250.5	5.81	23.2	2	370
17.808	251.2	6.04	22.9	2	370
17.80	250.8	5.96	(8.5 ... 11.5)		F

I 1112;  $-45^\circ 9'13$ ; 8.3A.R.  $17^h 51^m 57^s$ ; Decl.  $-45^\circ 49'$ 

13.709	233.8	19.87	22.0	$1\frac{1}{2}$	300
14.331	232.1	19.70	16.0	$2\frac{1}{2}$	370
14.02	232.9	19.78	(8.1 ... 11.3)		23

AC =  $h$  5005; C =  $-45^\circ 9'14$ ; 9.0

13.709	26.4	26.82	21.9	2	300
14.331	26.5	26.59	15.9	3	370
14.02	26.5	26.70	(8.1 ... 9.8)		142

AD; D = 11.5

13.709	58.0	20.07	22.1	2	300 N
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 $h$  5004;  $-42^\circ 8'203$ ; 9.0:A.R.  $17^h 53^m 39^s$ ; Decl.  $-42^\circ 4'$ 

13.299	296.6	12.86	14.9	3	300
14.331	296.9	12.98	16.3	2	370
13.82	296.8	12.92	(9.0 ... 10.0)		88

 $h$  5006;  $-59^\circ 7'218$ ; 7.2A.R.  $17^h 53^m 41^s$ ; Decl.  $-59^\circ 12'$ 

17.006	335.3	28.91	21.8	$2\frac{1}{2}$	370
17.720	335.8	28.84	21.4	2	370
17.66	335.5	28.88	(7.1 ... 12.6)		N

 $\lambda$  345;  $-43^\circ 8'402$ ; 7.7A.R.  $17^h 54^m 0^s$ ; Decl.  $-43^\circ 28'$ 

13.299	141.1	16.04	15.3	2	300
14.331	141.5	15.98	16.4	2	370
13.82	141.3	16.01	(7.5 ... 12.0)		

 $h$  5014;  $-43^\circ 8'434$ ; 6.2A.R.  $17^h 57^m 47^s$ ; Decl.  $-43^\circ 26'$ 

13.710	53.3	1.89	22.2	2	300
14.331	52.3	1.90	16.6	2	370
14.334	54.8	1.53	16.0	3	475
14.337	54.3	1.67	14.4	3	370
14.348	55.1	1.59	15.2	3	650
16.672	51.8	1.93	19.9	2	370
16.686	51.4	1.75	21.3	$2\frac{1}{2}$	370
16.697	53.8	1.49	20.4	2	650
16.705	54.6	1.81	20.1	2	650
14.21	54.0	1.72			
16.69	52.9	1.74	(6.1 ... 6.2)		B

 $h$  5015;  $-45^\circ 9'95$ ; 6.7A.R.  $17^h 59^m 14^s$ ; Decl.  $-45^\circ 47'$ 

13.299	260.4	4.00	15.5	2	300
13.441	259.9	4.28	14.8	2	300
14.334	260.5	3.93	16.2	3	475
14.348	258.8	3.95	15.4	2	370
13.86	259.9	4.04	(6.7 ... 11.0)		F

 $h$  5017;  $-48^\circ 9'677 + 6$ ;  $8.7 + 9.6$ A.R.  $18^h 0^m 22^s$ ; Decl.  $-48^\circ 53'$ 

13.275	319.0	23.76	15.9	2	300
13.277	318.8	23.81	15.5	2	300
13.28	318.9	23.78	(9.0 ... 9.4)		N

 $h$  5018; Anon.A.R.  $18^h 1^m 6^s$ ; Decl.  $-59^\circ 52'$ 

16.754	259.0	11.10	21.6	2	370
16.759	259.4	11.13	22.0	2	370
16.76	259.2	11.11	(9.8 ... 11.0)		N

 $h$  5021;  $-56^\circ 8'656$ ; 7.8A.R.  $18^h 1^m 28^s$ ; Decl.  $-56^\circ 27'$ 

13.365	325.4	4.48	16.0	3	300
13.564	325.4	4.90	16.0	2	300
13.567	326.5	4.87	21.7	2	300
14.378	324.6	4.54	15.6	$2\frac{1}{2}$	370
13.72	325.5	4.70	(7.6 ... 13.5)		N

 $h$  5020; Anon.A.R.  $18^h 1^m 30^s$ ; Decl.  $-59^\circ 56'$ 

16.754	8.9	14.68	21.5	2	370
16.759	8.6	14.55	22.1	2	370
16.76	8.8	14.62	(10.0 ... 11.1)		N

 $h$  5022;  $-52^\circ 11'024$ ; 9.1A.R.  $18^h 1^m 54^s$ ; Decl.  $-52^\circ 6'$ 

A,BC

16.729	107.8	6.08	21.8	3	370
16.735	105.9	6.86	22.8	2	370
16.737	106.7	6.31	21.2	$2\frac{1}{2}$	370
16.754	107.2	6.41	21.1	2	370
16.74	106.9	6.41	(9.4 ... 11.7)		N

BC = Dawson 21

16.729	104.1	1.69	21.9	3	370
16.737	103.5	1.53	21.3	$2\frac{1}{2}$	370
16.754	99.0	1.62	21.3	2	370
16.74	102.2	1.61	(12.3 ... 12.6)		

*h* 5023; —40° 8488; 7.8

A.R. 18<sup>h</sup> 2<sup>m</sup> 1<sup>s</sup>; Decl. —40° 27'

14.397	276.3	8.88	16.5	3	370
14.424	276.6	8.78	16.0	3	370
14.438	276.7	8.90	15.3	2	370
14.42	276.5	8.85	(8.5 ... 8.8)		21

*h* 5027; —54° 8761; 8.4

A.R. 18<sup>h</sup> 3<sup>m</sup> 29<sup>s</sup>; Decl. —54° 24'

13.329	116.6	12.35	15.7	3	300
13.365	117.4	12.37	16.2	3	300
13.35	117.0	12.36	(9.0 ... 9.7)		R

*h* 5024; —63° 4343 + 4; 7.1 + 9.4

A.R. 18<sup>h</sup> 3<sup>m</sup> 48<sup>s</sup>; Decl. —63° 5'

17.783	7.5	42.04	22.7	2	370
17.805	7.8	42.11	23.4	1½	370
17.79	7.6	42.07	(5.8 ... 11.2)		F

*h* 5029; —57° 8940; 8.0

A.R. 18<sup>h</sup> 4<sup>m</sup> 18<sup>s</sup>; Decl. —57° 53'

13.329	107.6	2.45	15.9	3	300
13.365	107.5	2.25	17.0	2½	300
13.493	107.5	2.38	16.4	2½	666
13.40	107.5	2.36	(8.6 ... 8.8)		P

*h* 5031; —47° 8766 + 7; 8.6 + 9.2

A.R. 18<sup>h</sup> 5<sup>m</sup> 13<sup>s</sup>; Decl. —47° 24'

13.266	79.4	26.55	15.5	2½	300
13.275	80.2	26.41	16.3	2	300
13.277	79.8	26.65	16.0	2	300
13.27	79.8	26.54	(8.5 ... 9.3)		R

*h* 5453; —53° 9025; 9.0

A.R. 18<sup>h</sup> 5<sup>m</sup> 48<sup>s</sup>; Decl. —53° 35'

16.729	270.2	14.39	22.0	2½	370
16.732	269.6	14.39	21.5	2	370
16.73	269.9	14.39	(9.4 ... 10.8)		N

BC

16.729	219.4	8.08	22.1	2½	370
16.732	218.7	7.93	21.6	2	370
16.73	219.1	8.01	(10.8 ... 12.2)		N

*h* 5033; —48° 9714 + 15; 7.8 + 9.6

A.R. 18<sup>h</sup> 5<sup>m</sup> 51<sup>s</sup>; Decl. —48° 53'

13.277	64.0	27.73	15.8	2	300
13.377	64.1	27.97	15.3	2	300
13.441	64.8	27.93	15.8	2	300
13.37	64.3	27.88	(7.0 ... 9.7)		R†

(*Sigue* *Continued.*)

AC

13.277	114.3	17.25	15.9	2	300
13.377	115.6	17.18	15.4	2	300
13.441	115.7	17.45	16.0	1½	300
13.37	115.2	17.29	(7.0 ... 9.8)		A

AD

13.277	9.2	18.27	15.6	2	300
13.441	9.9	18.22	15.7	2	300
13.36	9.5	18.25	(7.0 ... 11.2)		N

*h* 5034; —46° 9202; 7.8

A.R. 18<sup>h</sup> 6<sup>m</sup> 54<sup>s</sup>; Decl. —46° 4'

13.266	94.0	2.52	15.7	3	300
13.461	94.7	2.57	21.2	2½	300
13.464	94.1	2.67	21.3	2	300
13.40	94.3	2.59	(7.7 ... 8.6)		20

*h* 5038; —71° 2299; 8.2:

A.R. 18<sup>h</sup> 11<sup>m</sup> 39<sup>s</sup>; Decl. —71° 51'

17.811	301.3	11.94	22.2	2	370
17.816	302.1	11.90	22.2	2½	370
17.81	301.7	11.92	(8.8 ... 9.8)		F

Δ 220; —55° 8629 + 30; 8.0 + 8.2

A.R. 18<sup>h</sup> 11<sup>m</sup> 41<sup>s</sup>; Decl. —55° 37'

13.329	178.3	31.04	16.2	3	300
13.354	178.2	31.23	16.4	3	300
13.34	178.2	31.14	(8.2 ... 8.4)		F

*h* 5040; —48° 9768; 10.4

A.R. 18<sup>h</sup> 14<sup>m</sup> 19<sup>s</sup>; Decl. —48° 19'

13.477	304.2	7.03	21.2	2	300
13.488	305.4	7.16	15.6	2	300
13.490	304.7	7.00	15.8	3	300
13.48	304.8	7.06	(11.2 ... 11.4)		N

BC

13.477	359.1	4.97	21.4	2	300
13.488	358.1	4.98	15.8	2	300
13.490	361.1	4.83	15.9	3	300
13.48	359.4	4.93	(11.4 ... 12.1)		N

Δ 221; —44° 9116; 5.7

A.R. 18<sup>h</sup> 15<sup>m</sup> 12<sup>s</sup>; Decl. —44° 10'

13.710	164.0	75.11	22.8	2	300
14.337	163.8	—	14.7	2½	370
14.350	163.8	75.49	16.0	2½	370
14.03	163.9	75.30	(5.9 ... 10.0)		120

$h\ 5042; -46^\circ\ 9293; 8.3$ A.R.  $18^h\ 15^m\ 33^s$ ; Decl.  $-46^\circ\ 0'$ 

13.710	176.8	15.93	23.0	2	300
14.334	177.2	16.12	16.3	3	370
14.02	177.0	16.03	(8.5 ... 11.1)		N

 $h\ 5041; -53^\circ\ 9112; 7.3$ A.R.  $18^h\ 15^m\ 39^s$ ; Decl.  $-53^\circ\ 43'$ 

14.375	261.1	2.91	16.2	2½	370
14.481	260.2	2.85	15.6	2	370
14.531	260.3	2.89	17.0	2	370
14.46	260.5	2.88	(7.6 ... 8.9)		F

HdA.;  $-57^\circ\ 9063; 7.2$ A.R.  $18^h\ 19^m\ 11^s$ ; Decl.  $-57^\circ\ 36'$ 

13.545	119.4	34.08	16.3	2	300
13.562	119.8	33.63	21.5	1	300
13.564	120.4	34.17	16.2	2	300
13.567	119.4	33.76	21.8	2	300
13.56	119.8	33.91	(6.2 ... 10.6)		142

I 1113;  $-55^\circ\ 8704; 9.0$ A.R.  $18^h\ 20^m\ 33^s$ ; Decl.  $-55^\circ\ 37'$ 

13.329	23.6	3.68	16.4	3	300
13.354	25.3	3.65	16.6	2½	300
13.542	24.2	3.57	16.2	2½	300
13.41	24.4	3.64	(9.4 ... 10.4)		23

 $h\ 5044; -55^\circ\ 8710 + 09; 9.4 + 9.4$ A.R.  $18^h\ 20^m\ 55^s$ ; Decl.  $-55^\circ\ 36'$ 

13.329	356.6	14.38	16.6	2½	300
13.354	355.0	14.35	16.8	2½	300
13.542	356.0	14.33	16.5	3	300
13.41	355.9	14.35	(9.8 ... 10.0)		F?

 $h\ 5045; -48^\circ\ 9828; 7.4$ A.R.  $18^h\ 21^m\ 28^s$ ; Decl.  $-48^\circ\ 6'$ 

13.266	23.5	8.38	15.9	3	300
13.441	23.9	8.20	16.4	1½	300
13.461	22.9	8.20	21.4	2	300
13.39	23.4	8.26	(7.2 ... 9.9)		F

 $h\ 5046; -48^\circ\ 9830; 9.0$ A.R.  $18^h\ 21^m\ 48^s$ ; Decl.  $-48^\circ\ 26'$ 

13.266	75.1	7.65	16.1	2½	300
13.441	77.2	7.72	16.6	2	300
13.461	77.2	7.57	21.5	2	300
13.39	76.5	7.65	(10.0 ... 10.3)		20

I 1024;  $-50^\circ\ 10739; 8.6$ A.R.  $18^h\ 24^m\ 12^s$ ; Decl.  $-50^\circ\ 48'$ 

14.375	97.3	3.06	16.4	3	370
14.481	98.6	2.96	16.1	2	370
14.536	97.0	2.99	15.9	3	370
14.46	97.6	3.00	(9.6 ... 9.7)		142

 $\Delta\ 222; \alpha\ Coronae\ Australis; 7.0 + 7.4$ A.R.  $18^h\ 24^m\ 46^s$ ; Decl.  $-38^\circ\ 49'$ 

13.474	358.7	21.44	16.3	3½	300
14.378	358.5	21.67	16.3	2	370
13.93	358.6	21.55	(6.5 ... 6.9)		F

 $h\ 5047; -48^\circ\ 9862 + 3; 8.2 + 8.6$ A.R.  $18^h\ 25^m\ 22^s$ ; Decl.  $-48^\circ\ 6'$ 

13.461	173.0	42.82	21.7	2	300
13.464	172.8	42.72	21.5	2	300
13.46	172.9	42.77	(8.4 ... 8.5)		N

 $h\ 5049; -47^\circ\ 8961; 7.2$ A.R.  $18^h\ 28^m\ 2^s$ ; Decl.  $-47^\circ\ 10'$ 

13.461	263.6	19.90	22.0	2	300
13.464	263.5	19.92	21.8	2	300
13.46	263.6	19.91	(7.4 ... 11.2)		N

 $h\ 5048; \zeta\ Pavonis; 6.0$ A.R.  $18^h\ 28^m\ 25^s$ ; Decl.  $-71^\circ\ 32'$ 

17.811	356.0	55.50	22.4	2	370
17.816	356.0	55.68	22.4	2	370
17.81	256.0	55.59	(4.5 ... 11.5)		D

 $h\ 5050; -57^\circ\ 9126; 9.0$ A.R.  $18^h\ 28^m\ 39^s$ ; Decl.  $-57^\circ\ 30'$ 

13.526	106.5	12.76	16.5	1½	300
13.545	106.2	12.32	16.6	2½	300
13.562	105.5	12.30	21.8	1	300
13.564	106.2	12.39	16.4	2	300
13.55	106.1	12.44	(9.8 ... 10.2)		N

Rus 309;  $-56^\circ\ 8914; 8.2$ A.R.  $18^h\ 32^m\ 10^s$ ; Decl.  $-56^\circ\ 0'$ 

13.493	215.3	2.75	16.6	3	300
13.526	216.0	2.97	16.0	1½	300
13.545	215.7	2.77	16.7	2½	300
13.52	215.7	2.83	(8.5 ... 9.3)		121



$h$  5053 =  $h$  5056 = Rus 310;  $-55^{\circ} 8807$ ; 8.1

A.R.  $18^h 33^m 0^s$ ; Decl.  $-55^{\circ} 53'$

13.526	197.5	32.65	16.2	$1\frac{1}{2}$	300
13.545	197.4	32.58	16.8	2	300
13.567	197.0	32.61	22.0	$2\frac{1}{2}$	300
13.55	197.3	32.61	(8.3 ... 9.5) 121		

$h$  5054;  $-47^{\circ} 9010$ ; 8.0

A.R.  $18^h 33^m 9^s$ ; Decl.  $-47^{\circ} 47'$

13.461	327.8	16.09	22.2	2	300
13.464	327.9	16.22	22.0	$2\frac{1}{2}$	300
13.46	327.9	16.16	(8.7 ... 9.6) F?		

$h$  5055;  $-52^{\circ} 11213$ ; 7.9

A.R.  $18^h 33^m 21^s$ ; Decl.  $-52^{\circ} 59'$

14.481	76.3	7.67	15.8	2	370
14.531	75.8	7.53	17.2	2	370
14.536	76.5	7.58	16.0	3	370
14.52	76.2	7.59	(8.3 ... 8.7) F		

Hargrave;  $-54^{\circ} 9044$ ; 8.6

A.R.  $18^h 34^m 38^s$ ; Decl.  $-54^{\circ} 1'$

13.545	309.6	3.48	17.0	3	300
13.564	310.1	3.40	16.6	$2\frac{1}{2}$	300
13.567	308.5	3.46	22.2	3	300
13.56	309.4	3.45	(9.2 ... 9.2) 122		

$h$  5057;  $-54^{\circ} 9055$ ; 10.0

A.R.  $18^h 35^m 20^s$ ; Decl.  $-54^{\circ} 3'$

13.564	81.0	10.83	16.9	2	300
13.568	80.8	10.95	22.3	3	300
13.57	80.9	10.89	(10.2 ... 10.7) A?		

$h$  5058;  $-50^{\circ} 10727$ ; 8.8

A.R.  $18^h 37^m 36^s$ ; Decl.  $-50^{\circ} 58'$

16.727	315.3	12.64	22.3	2	370
16.732	315.4	12.88	21.7	2	370
16.73	315.4	12.88	(8.9 ... 12.5) N		

$h$  5059;  $-49^{\circ} 10737$ ; 7.0

A.R.  $18^h 37^m 47^s$ ; Decl.  $-49^{\circ} 46'$

13.488	239.0	[26.39]	16.1	2	300
13.490	238.0	25.48	16.4	$2\frac{1}{2}$	300
13.509	238.0	25.75	16.5	$1\frac{1}{2}$	300
14.375	238.9	25.54	17.0	2	370
13.72	238.5	25.59	(7.2 ... 11.9) N		

(Sigue Continued.)

AC

13.488	201.3	32.21	15.9	2	300
13.490	201.6	31.92	16.3	3	300
13.509	200.8	32.02	16.6	$1\frac{1}{2}$	300
14.375	200.7	31.89	16.8	2	370
13.72	201.1	32.01	(7.2 ... 11.5) N		

Dawson 22;  $-50^{\circ} 10840$ ; 9.0

A.R.  $18^h 39^m 45^s$ ; Decl.  $-50^{\circ} 51'$

16.727	13.6	6.10	22.6	2	370
16.729	12.9	6.07	22.4	2	370
16.732	13.8	6.08	21.8	2	370
16.73	13.4	6.08	(9.2 ... 9.9) 123		

$h$  5062;  $\lambda$  Pavonis; 4.1

A.R.  $18^h 40^m 37^s$ ; Decl.  $-62^{\circ} 20'$

17.805	205.6	63.15	23.6	$1\frac{1}{2}$	370
17.808	205.9	63.03	23.2	$1\frac{1}{2}$	370
17.81	205.8	63.09	(4.2 ... 12.0) N		

$h$  5065;  $-58^{\circ} 7510 + 11$ ; 7.9 + 9.1

A.R.  $18^h 41^m 10^s$ ; Decl.  $-58^{\circ} 4'$

13.564	21.5	22.61	17.3	2	300
13.568	21.5	22.47	22.6	$2\frac{1}{2}$	300
13.57	21.5	22.54	(7.8 ... 9.4) 124		

$h$  5067;  $-51^{\circ} 11043$ ; 8.8

A.R.  $18^h 43^m 44^s$ ; Decl.  $-51^{\circ} 5'$

16.727	276.4	3.90	22.8	2	370
16.729	278.9	3.81	22.5	$1\frac{1}{2}$	370
16.732	276.4	3.85	22.0	$2\frac{1}{2}$	370
16.73	277.2	3.85	(9.4 ... 9.7) D?		

$h$  5068;  $-54^{\circ} 9142$ ; 8.8

A.R.  $18^h 43^m 52^s$ ; Decl.  $-54^{\circ} 30'$

13.526	4.8	11.36	16.9	$1\frac{1}{2}$	300
13.545	4.1	11.30	17.1	$2\frac{1}{2}$	300
13.54	4.4	11.33	(8.8 ... 9.6) F?		

I 112;  $-47^{\circ} 9096$ ; 7.3

A.R.  $18^h 44^m 41^s$ ; Decl.  $-47^{\circ} 25'$

13.490	184.2	1.71	16.6	3	300
14.350	183.8	1.90	16.2	$2\frac{1}{2}$	370
14.375	184.9	1.81	17.1	3	370
14.07	184.3	1.81	(7.4 ... 9.0) D?		

AB,C =  $\Delta$  224; C =  $-47^{\circ} 9097$ ; 7.3

13.461	63.0	84.10	22.4	2	300
13.464	62.9	84.11	22.2	2	300
13.46	62.9	84.11	(7.3 ... 7.5) D?		

*h* 5069;  $-61^{\circ} 6282$ ; 7.3A.R.  $18^{\text{h}} 44^{\text{m}} 54^{\text{s}}$ ; Decl.  $-61^{\circ} 58'$ 

16.754	82.0	0.86	22.0	2	475
16.759	82.5	0.76	22.3	2	475
16.762	81.0	0.85	21.4	$2\frac{1}{2}$	650
16.76	81.8	0.82	(8.4 ... 8.6)		F?

## AB,C

16.754	92.5	15.17	21.7	2	370
16.762	91.5	15.18	21.2	$2\frac{1}{2}$	370
16.76	92.0	15.18	(7.7 ... 11.6)		A?

Dawson 23;  $-52^{\circ} 11299$ ; 7.6A.R.  $18^{\text{h}} 46^{\text{m}} 39^{\text{s}}$ ; Decl.  $-52^{\circ} 26'$ 

16.737	38.1	1.96	21.7	3	370
16.754	40.7	1.97	22.3	2	370
16.759	39.2	2.07	22.6	2	370
16.75	39.3	2.00	(8.3 ... 12.1)		

*h* 5075;  $-63^{\circ} 4469$ ; 6.9A.R.  $18^{\text{h}} 52^{\text{m}} 12^{\text{s}}$ ; Decl.  $-63^{\circ} 58'$ 

17.783	110.7	2.73	22.9	2	370
17.789	111.9	1.81	23.9	$2\frac{1}{2}$	370
17.808	111.9	1.00	23.4	2	370
17.79	111.5	1.85	(7.5 ... 7.5)		F

C6. 52;  $-44^{\circ} 9427$ ; 8.9A.R.  $18^{\text{h}} 52^{\text{m}} 37^{\text{s}}$ ; Decl.  $-44^{\circ} 17'$ 

13.737	343.7	2.96	22.2	3	300
14.334	340.9	3.13	17.1	3	370
14.378	343.3	2.96	16.5	3	370
14.15	342.6	3.02	(9.2 ... 9.3)		F

*h* 5076; Anon.A.R.  $18^{\text{h}} 53^{\text{m}} 0^{\text{s}}$ ; Decl.  $-63^{\circ} 12'$ 

17.783	214.8	11.93	23.0	2	370
17.789	216.5	11.89	0.0	2	370
17.79	215.7	11.91	(9.9 ... 10.8)		N

Hargrave (317);  $-45^{\circ} 9582$ ; 7.0:A.R.  $18^{\text{h}} 53^{\text{m}} 54^{\text{s}}$ ; Decl.  $-45^{\circ} 53'$ 

13.710	283.3	1.79	23.9	2	300
13.792	284.5	1.50	23.4	2	300
14.334	282.3	1.44	16.9	$3\frac{1}{2}$	475
14.350	282.3	1.68	16.4	$2\frac{1}{2}$	370
14.05	283.1	1.60	(8.2 ... 8.8)		F

AC = *h* 5078

13.710	213.6	19.20	23.8	2	300
13.792	213.3	18.92	23.3	2	300
14.334	212.8	18.94	17.0	3	370
13.95	213.5	19.02	(7.7 ... 8.7)		125

*h* 5079;  $-48^{\circ} 10023$ ; 9.6:A.R.  $18^{\text{h}} 54^{\text{m}} 12^{\text{s}}$ ; Decl.  $-48^{\circ} 23'$ 

13.461	237.3	16.71	22.7	2	300
13.464	238.0	16.69	22.5	3	300
13.46	237.7	16.70	(9.7 ... 10.2)		F

*h* 5081;  $-53^{\circ} 9460 + 61$ ; 9.4 + 9.5A.R.  $18^{\text{h}} 55^{\text{m}} 29^{\text{s}}$ ; Decl.  $-53^{\circ} 58'$ 

13.564	167.0	16.29	17.5	2	300
13.568	167.9	16.35	22.4	3	300
13.57	167.5	16.32	(9.5 ... 9.9)		22

*h* 5084;  $\gamma$  Coronae Australis; 5.5A.R.  $18^{\text{h}} 57^{\text{m}} 58^{\text{s}}$ ; Decl.  $-37^{\circ} 14'$ 

13.474	285.0	2.16	16.1	4	666
14.334	281.0	2.22	16.6	4	475
14.378	281.2	2.19	16.0	3	475
16.669	96.9	2.23	20.5	2	370
16.672	94.5	[2.65]	20.0	2	370
16.686	98.4	2.20	21.6	$2\frac{1}{2}$	370
16.697	98.7	2.30	20.8	2	370
17.272	276.6	2.10	16.6	3	650
17.332	275.7	2.28	18.4	2	650
17.540	276.6	2.29	20.3	3	370
17.606	276.0	2.06	19.9	3	650
14.06	282.4	2.19			
16.68	277.1	2.24			
17.44	276.2	2.18	(5.4 ... 5.5)		B

*h* 5085;  $-60^{\circ} 7269$ ; 7.4A.R.  $18^{\text{h}} 59^{\text{m}} 34^{\text{s}}$ ; Decl.  $-60^{\circ} 14'$ 

16.754	241.3	2.93	22.5	2	370
16.762	240.4	2.91	21.5	$2\frac{1}{2}$	370
16.765	241.7	2.93	21.8	2	370
16.76	241.1	2.92	(7.9 ... 9.5)		F

*h* 5086;  $-54^{\circ} 9265$ ; 9.4A.R.  $18^{\text{h}} 59^{\text{m}} 45^{\text{s}}$ ; Decl.  $-54^{\circ} 33'$ 

13.526	292.0	16.76	17.2	$1\frac{1}{2}$	300
13.545	291.7	16.56	17.3	$2\frac{1}{2}$	300
13.54	291.8	16.66	(9.7 ... 10.7)		N

*h* 5088a; Anon.A.R.  $18^{\text{h}} 59^{\text{m}} 54^{\text{s}}$ ; Decl.  $-49^{\circ} 50'$ 

14.394	13.5	10.95	17.6	2	370
14.397	10.5	10.85	16.9	$2\frac{1}{2}$	370
14.40	12.0	10.90	(12.0 ... 13.2)		N

*h* 5088d; Anon.A.R.  $18^{\text{h}} 59^{\text{m}} 57^{\text{s}}$ ; Decl.  $-49^{\circ} 45'$ 

14.394	155.1	5.99	17.1	2	370
14.397	159.1	6.45	16.7	$2\frac{1}{2}$	370
14.40	157.1	6.22	(12.3 ... 14.0)		N

*h* 5088*b*; C6D  $-49^{\circ}$  12520; 10

A.R. 18<sup>h</sup> 59<sup>m</sup> 58<sup>s</sup>; Decl.  $-49^{\circ}$  48'

14.394	252.4	14.07	17.3	2	370
14.397	252.1	13.65	17.1	2½	370
14.40	252.2	13.86	(12.2 ... 12.3)		N

*h* 5089;  $-49^{\circ}$  10869; 10.6

A.R. 19<sup>h</sup> 0<sup>m</sup> 0<sup>s</sup>; Decl.  $-49^{\circ}$  47'

14.394	109.2	9.22	17.2	2	370
14.397	109.8	9.15	17.2	2½	370
14.40	109.5	9.19	(10.6 ... 12.8)		N

*h* 5088*c*; Anon.

A.R. 19<sup>h</sup> 0<sup>m</sup> 4<sup>s</sup>; Decl.  $-49^{\circ}$  51'

14.394	207.7	17.58	17.4	2	370
14.397	205.9	17.70	17.4	2½	370
14.40	206.8	17.64	(12.5 ... 12.9)		N

*h* 5087;  $-54^{\circ}$  9269; 8.9

A.R. 19<sup>h</sup> 0<sup>m</sup> 5<sup>s</sup>; Decl.  $-54^{\circ}$  20'

13.526	22.9	16.19	17.3	1½	300
13.545	22.7	16.29	17.4	3	300
13.54	22.8	16.24	(8.9 ... 11.6)		N

Hu—;  $-56^{\circ}$  9110; 8.9

A.R. 19<sup>h</sup> 1<sup>m</sup> 3<sup>s</sup>; Decl.  $-56^{\circ}$  54'

17.819	293.5	6.70	22.4	2	370
17.822	294.4	6.70	21.9	2	370
17.82	294.0	6.70	(9.0 ... 11.4)		126

*h* 5092;  $-47^{\circ}$  9214 + 15; 8.4 + 8.4

A.R. 19<sup>h</sup> 4<sup>m</sup> 38<sup>s</sup>; Decl.  $-47^{\circ}$  34'

13.441	351.0	17.84	16.9	2	300
13.461	351.6	17.83	23.1	2	300
13.45	351.3	17.83	(8.3 ... 8.4)		F

*h* 5093;  $-43^{\circ}$  8940 + 39; 8.6 + 9.6

A.R. 19<sup>h</sup> 4<sup>m</sup> 44<sup>s</sup>; Decl.  $-43^{\circ}$  27'

14.438	213.3	33.58	16.0	2	370
14.443	214.2	—	15.2	2	370
14.462	213.6	33.63	17.0	2½	370
14.45	213.7	33.61	(9.0 ... 9.9)		N

BC

14.438	228.3	11.63	16.2	1½	370
14.462	229.0	11.73	17.1	2½	370
14.45	228.7	11.68	(9.9 ... 10.6)		N

*h* 5099;  $-50^{\circ}$  11021; 7.7

A.R. 19<sup>h</sup> 7<sup>m</sup> 10<sup>s</sup>; Decl.  $-50^{\circ}$  12'

16.727	36.6	13.41	23.0	1½	370
16.729	35.9	13.10	22.7	2	370
16.732	37.0	13.11	22.1	2	370
16.72	36.5	13.21	(8.2 ... 9.7)		F

*h* 5100;  $-56^{\circ}$  9141; 6.8

A.R. 19<sup>h</sup> 8<sup>m</sup> 21<sup>s</sup>; Decl.  $-56^{\circ}$  22'

13.493	150.9	19.31	17.2	3	300
13.513	151.2	19.21	21.2	1½	300
13.545	150.6	19.50	17.5	2½	300
13.52	150.9	19.34	(6.7 ... 10.6)		N

*h* 5102;  $-61^{\circ}$  6369; 9.4

A.R. 19<sup>h</sup> 11<sup>m</sup> 7<sup>s</sup>; Decl.  $-61^{\circ}$  30'

16.754	341.5	14.15	22.6	2	370
16.762	340.8	14.18	21.7	2½	370
16.76	341.1	14.17	(10.4 ... 11.1)		N

*h* 5104;  $-51^{\circ}$  11202 + 3; 8.8 + 8.8

A.R. 19<sup>h</sup> 11<sup>m</sup> 15<sup>s</sup>; Decl.  $51^{\circ}$  17'

16.718	38.4	18.39	22.5	2	370
16.727	37.6	18.22	23.2	2	370
16.729	37.5	18.30	22.8	2	370
16.72	37.8	18.30	(8.9 ... 8.9)		F

*h* 5105;  $-49^{\circ}$  10939; 8.8

A.R. 19<sup>h</sup> 11<sup>m</sup> 18<sup>s</sup>; Decl.  $-49^{\circ}$  45'

13.488	230.5	10.90	17.0	2	300
13.490	231.4	10.78	16.8	3	300
13.49	231.0	10.84	(9.5 ... 10.2)		N

*h* 5103;  $-72^{\circ}$  2377; 8.3

A.R. 19<sup>h</sup> 12<sup>m</sup> 35<sup>s</sup>; Decl.  $-72^{\circ}$  1'

17.811	243.9	12.64	22.8	2	370
17.816	244.4	12.66	23.3	2	370
17.81	244.2	12.65	(8.5 ... 12.4)		N

$\Delta$  226;  $\beta^1$  Sagittarii; 5.0

A.R. 19<sup>h</sup> 13<sup>m</sup> 40<sup>s</sup>; Decl.  $-44^{\circ}$  41'

13.329	77.3	28.49	17.5	3	300
13.792	77.2	28.67	23.5	2	300
14.378	77.6	28.26	16.7	2½	370
14.394	76.9	28.40	18.0	2½	370
13.97	77.3	28.45	(4.3 ... 8.0)		F?

*h* 5108; C6D  $-58^{\circ} 7433$ ; 9.7A.R.  $19^{\text{h}} 16^{\text{m}} 14^{\text{s}}$ ; Decl.  $-58^{\circ} 28'$ 

16.754	49.1	18.21	22.8	2	370
16.762	48.9	18.17	21.9	2½	370
16.76	49.0	18.19	(10.5 ... 11.0)		N

*h* 5109;  $-67^{\circ} 3646 + 7$ ; 7.9 + 8.9A.R.  $19^{\text{h}} 17^{\text{m}} 6^{\text{s}}$ ; Decl.  $-67^{\circ} 33'$ 

17.783	141.5	24.73	23.3	2	370
17.789	141.2	24.73	0.1	2	370
17.79	141.4	24.73	(8.0 ... 9.1)		D?

## AC

17.783	13.4	36.18	23.5	2	370
17.789	13.5	36.51	0.3	2	370
17.79	13.4	36.34	(8.0 ... 9.8)		F

*h* 5114;  $-54^{\circ} 9371 + 69$ ; 7.2 + 7.8A.R.  $19^{\text{h}} 17^{\text{m}} 45^{\text{s}}$ ; Decl.  $-54^{\circ} 34'$ 

AB Véase la nota. See note 127

## AB,C

13.493	254.3	68.80	17.4	3	300
13.513	254.0	69.06	21.4	1½	300
13.545	254.3	69.13	17.7	2½	300
13.52	254.2	69.00	(6.9 ... 8.2)		A

## CD

13.545	190.3	12.06	17.8	2½	300
14.400	191.6	11.65	15.8	2½	370
13.97	191.0	11.85	(8.2 ... 13.0)		N

*l* 650;  $-50^{\circ} 11086$ ; 8.6A.R.  $19^{\text{h}} 19^{\text{m}} 4^{\text{s}}$ ; Decl.  $-50^{\circ} 8'$ 

16.718	271.6	1.74	23.0	2	370
16.729	271.0	1.64	23.0	2	370
16.737	270.2	1.44	21.6	3	370
16.762	269.8	1.64	22.3	2	370
16.74	270.6	1.62	(9.0 ... 11.6)		23

*h* 5117;  $-44^{\circ} 9569$ ; 7.8A.R.  $19^{\text{h}} 19^{\text{m}} 28^{\text{s}}$ ; Decl.  $-44^{\circ} 8'$ 

14.394	263.2	6.30	18.2	3	370
14.397	262.4	6.13	17.5	3	370
14.400	262.7	6.28	16.1	2½	370
14.40	262.8	6.24	(8.0 ... 9.2)		F

*h* 5118;  $-70^{\circ} 2662^{\text{p}}$ ; 10.0A.R.  $19^{\text{h}} 21^{\text{m}} 19^{\text{s}}$ ; Decl.  $-70^{\circ} 55'$ 

17.816	8.8	8.67	23.5	2	370
17.822	8.7	8.71	22.2	2	370
17.827	7.8	8.39	22.7	1½	370
17.832	9.7	8.67	22.5	2	370
17.82	8.8	8.61	(11.0 ... 11.2)		N

*h* 5121;  $-56^{\circ} 9206$ ; 9.8A.R.  $19^{\text{h}} 22^{\text{m}} 31^{\text{s}}$ ; Decl.  $-56^{\circ} 43'$ 

13.513	279.2	14.21	21.6	1½	300
13.568	278.8	14.33	22.9	3	300
13.54	279.0	14.27	(10.0 ... 10.4)		N

*h* 5125;  $-50^{\circ} 11113 + 12$ ; 9.4 + 9.4A.R.  $19^{\text{h}} 23^{\text{m}} 38^{\text{s}}$ ; Decl.  $-50^{\circ} 10'$ 

16.719	291.8	29.47	23.3	2	370
16.729	291.7	[29.88]	23.2	1	370
16.735	291.8	29.56	23.5	2	370
16.73	291.8	29.51	(9.0 ... 9.2)		F

*h* 5123;  $-66^{\circ} 3439 + 8$ ; 9.5 + 9.5A.R.  $19^{\text{h}} 23^{\text{m}} 40^{\text{s}}$ ; Decl.  $-66^{\circ} 41'$ 

17.783	180.6	27.30	23.6	2	370
17.789	180.8	27.25	0.4	2	370
17.79	180.7	27.28	(9.6 ... 9.9)		D?

Anon.;  $-66^{\circ} 3445$ ; 6.7A.R.  $19^{\text{h}} 27^{\text{m}} 30^{\text{s}}$ ; Decl.  $-66^{\circ} 58'$ 

16.822	242.7	19.76	22.9	2	370
16.828	241.0	19.72	23.6	2	370
16.83	241.8	19.74	(7.1 ... 12.5)		

*h* 5129;  $-47^{\circ} 9318$ ; 9.0:A.R.  $19^{\text{h}} 28^{\text{m}} 17^{\text{s}}$ ; Decl.  $-47^{\circ} 2'$ 

13.275	107.8	13.55	16.6	2	300
13.461	107.8	13.47	23.5	2	300
13.37	107.8	13.51	(9.5 ... 9.9)		R?

*h* 5130;  $-50^{\circ} 11143$ ; 9.2A.R.  $19^{\text{h}} 29^{\text{m}} 42^{\text{s}}$ ; Decl.  $-50^{\circ} 8'$ 

16.719	145.2	14.59	23.5	2	370
16.735	145.6	14.37	23.7	1½	370
16.73	145.4	14.48	(8.9 ... 11.9)		N

*h* 5132; —66° 3450; 7.9:

A.R. 19<sup>h</sup> 31<sup>m</sup> 48<sup>s</sup>; Decl. —66° 35'

16.822	308.6	21.49	23.5	2	370
16.828	308.9	21.72	23.8	2	370
16.82	308.7	21.60	(8.0 ... 10.0)	128	

*h* 5135; —55° 9161; 8.0

A.R. 19<sup>h</sup> 32<sup>m</sup> 42<sup>s</sup>; Decl. —55° 46'

13.493	176.6	12.28	17.7	3	300
13.513	175.8	12.44	21.7	1½	300
13.545	177.0	12.49	18.0	2	300
13.52	176.5	12.40	(8.6 ... 10.6)	N	

*h* 5138; —44° 9633; 9.0

A.R. 19<sup>h</sup> 34<sup>m</sup> 53<sup>s</sup>; Decl. —44° 36'

14.438	37.8	16.59	16.3	2	370
14.463	38.3	16.74	17.3	2	370
14.45	38.1	16.67	(9.3 ... 10.9)	N	

*h* 5139; —43° 9057; 9.0

A.R. 19<sup>h</sup> 35<sup>m</sup> 0<sup>s</sup>; Decl. —43° 44'

14.438	129.8	15.97	16.5	1½	370
14.463	130.5	16.20	17.5	2	370
14.476	130.8	15.96	16.2	1½	370
14.46	130.4	16.04	(9.3 ... 12.0)	N	

*h* 5136; Anon.

A.R. 19<sup>h</sup> 35<sup>m</sup> 40<sup>s</sup>; Decl. —67° 26'

16.822	89.6	9.21	23.8	2	370
16.828	92.1	9.04	23.9	2	370
16.82	90.8	9.12	(13.2 ... 13.5)	N	

*h* 5137; —73° 2067; 7.4

A.R. 19<sup>h</sup> 36<sup>m</sup> 40<sup>s</sup>; Decl. —73° 6'

17.816	200.8	29.65	23.7	2	370
17.833	200.6	29.61	23.8	2	370
17.82	200.7	29.63	(7.6 ... 11.4)	N	

AC

17.816	312.6	42.79	23.7	2	370
17.833	312.5	42.85	0.0	2	370
17.82	312.6	42.82	(7.6 ... 10.9)	N	

*h* 5142; —48° 10250; 10.2

A.R. 19<sup>h</sup> 37<sup>m</sup> 30<sup>s</sup>; Decl. —48° 40'

13.275	284.5	9.88	16.8	2	300
13.488	285.2	10.14	17.2	2	300
13.491	284.5	10.22	17.0	3	300
13.42	284.7	10.08	(10.1 ... 11.1)	N	

*h* 5141; —62° 6108; 7.3

A.R. 19<sup>h</sup> 38<sup>m</sup> 0<sup>s</sup>; Decl. —62° 7'

16.822	343.7	13.86	0.3	2	370
16.831	343.7	13.91	22.9	2	370
16.83	343.7	13.88	(8.1 ... 10.5)	129	

*h* 5140; —65° 3825; 7.9

A.R. 19<sup>h</sup> 38<sup>m</sup> 2<sup>s</sup>; Decl. —65° 13'

16.822	262.0	1.89	23.3	2	370
16.828	259.8	1.77	0.1	2	370
16.831	259.5	2.02	22.7	2	370
16.842	261.5	1.84	23.3	2	370
16.83	260.7	1.88	(8.6 ... 8.7)	130	

*h* 5143; —46° 5800; 9.6

A.R. 19<sup>h</sup> 38<sup>m</sup> 50<sup>s</sup>; Decl. —46° 47'

14.476	326.3	7.71	16.5	2	370
14.482	325.0	7.98	17.0	1½	370
14.536	325.1	7.89	16.3	2	370
14.50	325.5	7.86	(9.7 ... 10.2)	20	

Dawson 24; —53° 9688; 10.4

A.R. 19<sup>h</sup> 40<sup>m</sup> 40<sup>s</sup>; Decl. —53° 58'

13.513	180.7	5.46	22.0	1½	300
13.568	181.6	5.64	23.1	2½	300
14.329	183.8	5.51	15.8	2	370
13.80	182.0	5.54	(10.8 ... 11.1)	131	

*h* 5146; —53° 9691; 8.5

A.R. 19<sup>h</sup> 40<sup>m</sup> 47<sup>s</sup>; Decl. —53° 58'

13.513	284.5	8.57	22.2	2	300
13.568	283.2	—	23.3	1½	300
14.329	284.3	8.56	15.9	2	370
13.80	284.0	8.56	(9.4 ... 11.8)	131	

*h* 5148; —45° 9803; 7.0

A.R. 19<sup>h</sup> 41<sup>m</sup> 14<sup>s</sup>; Decl. —45° 41'

13.710	317.8	14.31	0.5	2	300
14.334	318.5	14.38	17.3	3	370
14.02	318.2	14.35	(7.2 ... 12.0)	N	

Δ 227; —55° 9221 + 2; 7.3 + 7.3

A.R. 19<sup>h</sup> 42<sup>m</sup> 40<sup>s</sup>; Decl. —55° 17'

13.329	148.9	23.15	17.1	3	300
13.491	148.9	23.05	17.3	2½	300
13.41	148.9	23.10	(6.5 ... 7.0)	F	

$h$  5150;  $-51^\circ$  11360; 8.6A.R.  $19^h$  42<sup>m</sup> 43<sup>s</sup>; Decl.  $-51^\circ$  34'

16.719	259.5	23.11	23.8	2	370
16.737	259.5	23.09	22.0	3	370
16.73	259.5	23.10	(8.9 ... 11.4)		N

 $h$  5447;  $-54^\circ$  9530; 9.0A.R.  $19^h$  46<sup>m</sup> 25<sup>s</sup>; Decl.  $-54^\circ$  26'

13.513	270.3	9.92	22.5	2	300
13.568	270.6	9.72	23.5	1½	300
14.329	270.2	9.83	16.1	2	370
13.80	270.4	9.82	(9.2 ... 11.3)		N

Dawson 25;  $-57^\circ$  9555; 9.1A.R.  $19^h$  48<sup>m</sup> 7<sup>s</sup>; Decl.  $-57^\circ$  45'

14.583	222.9	3.35	19.6	3	370
14.591	220.3	3.20	18.0	2	370
14.592	222.5	3.33	21.9	2	370
14.59	221.9	3.29	(9.4 ... 10.1)		132

 $h$  5155;  $-61^\circ$  6437; 8.8A.R.  $19^h$  48<sup>m</sup> 50<sup>s</sup>; Decl.  $-61^\circ$  22'

16.754	191.5	4.99	23.3	2	370
16.762	192.0	4.73	22.7	2	370
16.765	192.3	4.84	22.0	1½	370
16.76	191.9	4.85	(9.6 ... 10.0)		142

 $h$  5157;  $-46^\circ$  9854; 9.6A.R.  $19^h$  49<sup>m</sup> 59<sup>s</sup>; Decl.  $-46^\circ$  42'

13.275	281.6	15.90	17.0	2	300
13.488	280.7	16.10	17.4	2	300
13.38	281.1	16.00	(9.6 ... 11.6)		N

 $h$  5160;  $-46^\circ$  9864; 9.3A.R.  $19^h$  52<sup>m</sup> 1<sup>s</sup>; Decl.  $-46^\circ$  34'

13.275	164.0	27.42	17.2	2	300
13.488	163.9	26.92	17.7	2	300
14.394	163.8	27.59	18.8	3	370
13.72	163.9	27.31	(9.6 ... 12.2)		N

 $h$  5161;  $-44^\circ$  9703; 9.4A.R.  $19^h$  52<sup>m</sup> 36<sup>s</sup>; Decl.  $-44^\circ$  43'

14.441	314.5	11.64	17.6	2	370
14.463	314.9	11.57	17.8	2	370
14.45	314.7	11.60	(9.9 ... 11.0)		N

 $h$  5163;  $-63^\circ$  4561; 7.4A.R.  $19^h$  53<sup>m</sup> 58<sup>s</sup>; Decl.  $-63^\circ$  24'

16.822	249.5	1.79	0.4	2½	370
16.842	248.1	1.71	23.5	2	370
16.871	248.5	1.63	23.4	2	370
16.84	248.7	1.71	(8.6 ... 9.0)		130

 $h$  5162;  $-71^\circ$  2535; 8.3A.R.  $19^h$  54<sup>m</sup> 33<sup>s</sup>; Decl.  $-71^\circ$  10'

17.816	291.8	6.65	0.0	2	370
17.833	291.7	6.65	0.2	2	370
17.841	291.4	6.74	23.7	2	370
17.83	291.6	6.68	(8.2 ... 10.5)		D

Dawson 26;  $-47^\circ$  9430; 10.2A.R.  $19^h$  57<sup>m</sup> 1<sup>s</sup>; Decl.  $-47^\circ$  20'

14.397	199.2	3.80	18.0	3	370
14.400	199.4	4.01	16.7	3	370
14.441	201.0	4.55	16.6	2	370
14.482	199.9	4.00	17.3	2	370
14.43	199.9	4.09	(10.8 ... 11.3)		

AC

14.397	238.5	—	18.1	3	370
14.400	240.4	—	16.4	3	370
14.441	244.0	—	16.7	2	370
14.482	240.2	—	17.5	2	370
14.43	240.8	4.21	(10.8 ... 12.6)		133

 $h$  5166;  $-47^\circ$  9432; 10.3A.R.  $19^h$  57<sup>m</sup> 9<sup>s</sup>; Decl.  $-47^\circ$  10'

14.397	248.6	11.42	17.8	3	370
14.440	249.9	11.49	15.8	2	370
14.476	249.3	11.50	16.7	1½	370
14.44	249.3	11.47	(10.1 ... 10.1)		N

 $h$  5169;  $-47^\circ$  9448; 10.0A.R.  $20^h$  0<sup>m</sup> 33<sup>s</sup>; Decl.  $-47^\circ$  3'

14.441	128.4	5.95	17.0	2	370
14.476	129.7	5.98	16.9	1½	370
14.482	131.2	6.06	17.7	2	370
14.47	129.8	6.00	(10.5 ... 11.5)		N

 $h$  5167;  $-63^\circ$  4566; 7.2A.R.  $20^h$  0<sup>m</sup> 37<sup>s</sup>; Decl.  $-63^\circ$  59'

16.822	34.6	7.21	0.5	2½	370
16.842	33.4	7.23	23.7	2	370
16.871	34.5	7.23	23.6	2	370
16.84	34.2	7.22	(8.5 ... 9.5)		F

*h* 5172;  $-47^{\circ} 9458$ ; 8.6

A.R.  $20^{\text{h}} 2^{\text{m}} 55^{\text{s}}$ ; Decl.  $-47^{\circ} 26'$

14.441	5.5	30.42	17.2	$1\frac{1}{2}$	370
14.476	5.5	30.62	17.1	1	370
14.46	5.5	30.52	(9.0 ... 10.1)		N

*h* 5171;  $-64^{\circ} 4035$ ; 6.8:

A.R.  $20^{\text{h}} 3^{\text{m}} 12^{\text{s}}$ ; Decl.  $-64^{\circ} 48'$

16.822	305.2	17.38	0.6	$2\frac{1}{2}$	370
16.828	306.1	17.25	0.6	2	370
16.82	305.6	17.32	(7.7 ... 10.1)		134

AC

16.822	335.5	30.12	0.7	$2\frac{1}{2}$	370
16.828	335.7	30.17	0.7	2	370
16.82	335.6	30.14	(7.7 ... 10.1)		134

*h* 5174;  $-50^{\circ} 11299$ ; 7.8

A.R.  $20^{\text{h}} 3^{\text{m}} 28^{\text{s}}$ ; Decl.  $-50^{\circ} 41'$

16.707	254.0	18.31	19.9	2	370
16.710	252.2	18.36	19.9	2	370
16.71	253.1	18.33	(7.9 ... 11.2)		142

Rü 25 = *h* 5177;  $-57^{\circ} 9635$ ; 7.5

A.R.  $20^{\text{h}} 4^{\text{m}} 54^{\text{s}}$ ; Decl.  $-57^{\circ} 21'$

13.349	28.8	7.72	17.5	2	300
13.491	28.1	7.65	17.6	$2\frac{1}{2}$	300
13.493	28.7	7.65	18.0	3	300
13.44	28.5	7.67	(8.1 ... 8.3)		F

*h* 5176; Anon.

A.R.  $20^{\text{h}} 5^{\text{m}} 55^{\text{s}}$ ; Decl.  $-71^{\circ} 14'$

17.857	129.8	6.20	23.4	3	370
17.876	130.5	6.02	0.0	$1\frac{1}{2}$	370
17.904	131.1	5.83	1.8	2	370
17.88	130.5	6.02	(11.7 ... 11.8)		N

*h* 5179;  $-46^{\circ} 9933$ ; 9.0

A.R.  $20^{\text{h}} 6^{\text{m}} 21^{\text{s}}$ ; Decl.  $-46^{\circ} 26'$

13.275	137.0	6.03	17.8	2	300
14.400	136.4	5.81	18.2	3	370
14.482	135.6	6.01	18.2	2	370
14.05	136.3	5.95	(9.6 ... 9.8)		F?

*h* 5184 = I 378;  $-46^{\circ} 9941$ ; 8.6

A.R.  $20^{\text{h}} 8^{\text{m}} 54^{\text{s}}$ ; Decl.  $-46^{\circ} 20'$

(13.275	170.5)	—	18.1	2	300
14.400	171.9	2.25	18.3	3	370
14.572	172.4	2.37	17.3	4	370
14.49	172.2	2.31	(8.6 ... 13.6)		R

*h* 5185;  $-59^{\circ} 7604$ ; 7.8

A.R.  $20^{\text{h}} 10^{\text{m}} 23^{\text{s}}$ ; Decl.  $-59^{\circ} 7'$

16.754	61.0	18.60	23.7	$1\frac{1}{2}$	370
16.762	60.9	18.51	22.9	2	370
16.76	60.9	18.55	(7.9 ... 11.1)		N

Có. 57;  $-55^{\circ} 9370$ ; 8.6

A.R.  $20^{\text{h}} 12^{\text{m}} 0^{\text{s}}$ ; Decl.  $-55^{\circ} 12'$

13.513	358.3	4.48	22.7	2	300
13.835	358.6	4.24	0.5	$2\frac{1}{2}$	300
13.893	358.8	4.39	1.1	2	420
13.75	358.6	4.37	(8.8 ... 9.5)		F

*h* 5187;  $-54^{\circ} 9673$ ; 8.4

A.R.  $20^{\text{h}} 13^{\text{m}} 1^{\text{s}}$ ; Decl.  $-54^{\circ} 39'$

13.893	322.9	17.76	1.3	2	300
14.400	322.9	17.91	18.5	3	370
14.15	322.9	17.84	(8.1 ... 13.5)		N

*h* 5190;  $\alpha'$  Sagittarii; 6.0

A.R.  $20^{\text{h}} 13^{\text{m}} 59^{\text{s}}$ ; Decl.  $-42^{\circ} 26'$

13.819	307.2	31.70	0.1	3	420
14.441	307.4	31.87	17.8	2	370
14.13	307.3	31.78	(5.8 ... 12.5)		R

AC

14.463	278.4	52.14	18.0	2	370
14.479	277.5	52.31	17.9	2	370
14.47	278.0	52.22	(5.8 ... 11.2)		R

*h* 5193;  $-57^{\circ} 9677$ ; 9.2

A.R.  $20^{\text{h}} 16^{\text{m}} 14^{\text{s}}$ ; Decl.  $-57^{\circ} 8'$

13.513	331.7	17.67	22.8	2	300
14.329	331.6	17.76	16.4	2	370
14.334	331.6	17.72	17.7	$2\frac{1}{2}$	370
14.06	331.6	17.72	(9.2 ... 10.1)		D?

*h* 5196; Anon.

A.R.  $20^{\text{h}} 17^{\text{m}} 50^{\text{s}}$ ; Decl.  $-62^{\circ} 51'$

16.872	278.7	21.81	1.1	2	370
16.885	277.8	22.71	1.1	2	370
16.88	278.2	22.11	(9.5 ... 14.2)		135

*h* 5194;  $-69^{\circ} 3120$ ; 6.8

A.R.  $20^{\text{h}} 17^{\text{m}} 56^{\text{s}}$ ; Decl.  $-69^{\circ} 29'$

17.783	256.8	4.17	23.9	2	370
17.789	256.1	4.41	0.6	2	370
17.805	256.8	—	0.1	1	370
17.808	254.9	4.27	23.7	2	370
17.80	256.1	4.28	(6.8 ... 12.6)		A?

$h$  5197;  $-62^\circ 6160$ ; 8.4A.R.  $20^h 18^m 4^s$ ; Decl.  $-62^\circ 52'$ 

16.842	247.1	44.84	0.0	2	370
16.872	247.1	44.07	0.7	2	370
16.877	247.1	44.11	0.9	1½	370
16.86	247.1	44.34	(8.6 ... 12.8)		N

 $h$  5201;  $-44^\circ 9815$ ; 9.8A.R.  $20^h 20^m 17^s$ ; Decl.  $-44^\circ 27'$ 

14.441	116.7	10.89	18.1	2	370
14.463	116.9	10.88	18.3	2	370
14.45	116.8	10.88	(10.3 ... 11.4)		N

 $h$  5200;  $-68^\circ 3374$ ; 7.4A.R.  $20^h 20^m 52^s$ ; Decl.  $-68^\circ 47'$ 

17.789	136.8	12.04	0.7	2	370
17.808	136.7	12.37	0.0	1½	370
17.80	136.8	12.20	(7.2 ... 10.9)		N

 $h$  5204;  $-45^\circ 9966$ ; 7.5A.R.  $20^h 23^m 30^s$ ; Decl.  $-45^\circ 46'$ 

13.710	35.0	6.59	1.0	2	300
14.441	32.9	6.33	18.0	2	370
14.463	34.9	6.37	18.5	3	370
14.20	34.3	6.43	(8.4 ... 9.5)		F

 $\Delta$  231;  $-71^\circ 2563 + 2$ ; 7.1 + 8.6A.R.  $20^h 23^m 41^s$ ; Decl.  $-71^\circ 30'$ 

17.816	288.6	57.29	0.3	2	370
17.833	288.4	57.17	0.5	2	370
17.82	288.5	57.23	(6.8 ... 8.9)		N

 $h$  5209;  $\alpha$  Indi; 5.8A.R.  $20^h 28^m 47^s$ ; Decl.  $-47^\circ 44'$ 

14.537	199.3	68.02	19.1	2	370
14.561	199.0	66.87	17.1	2	370
14.572	199.9	67.39	17.4	4	370
14.56	199.4	67.43	(2.9 ... 11.5)		R

AC

14.537	343.1	62.11	19.1	2	370
14.572	342.7	62.39	17.6	4	370
14.55	342.9	62.25	(2.9 ... 13.0)		136

 $h$  5211;  $-42^\circ 9126$ ; 7.2A.R.  $20^h 32^m 31^s$ ; Decl.  $-42^\circ 50'$ 

13.710	299.4	20.36	1.2	2	300
13.792	299.3	19.96	0.5	2	300
13.819	299.8	20.12	0.3	2½	420
13.77	299.5	20.14	(6.5 ... 9.3)		137

 $h$  5217; Anon.A.R.  $20^h 38^m 45^s$ ; Decl.  $-64^\circ 54'$ 

16.842	133.4	7.38	0.5	2	370
16.877	135.4	7.54	1.6	1½	370
16.885	135.2	7.20	1.3	2	370
16.87	134.7	7.37	(11.0 ... 12.8)		138

 $h$  5222;  $-44^\circ 9892$ ; 7.5A.R.  $20^h 40^m 18^s$ ; Decl.  $-44^\circ 26'$ 

14.441	276.8	27.23	18.3	2	370
14.463	277.0	27.16	18.7	3	370
14.45	276.9	27.19	(8.1 ... 12.6)		139

 $h$  5221;  $-66^\circ 3506$ ; 9.3A.R.  $20^h 40^m 24^s$ ; Decl.  $-66^\circ 10'$ 

16.842	44.8	10.25	0.9	2	370
16.885	45.0	10.20	1.5	2	370
16.86	44.9	10.22	(10.2 ... 10.5)		140

Rü 26;  $-62^\circ 6180$ ; 5.7A.R.  $20^h 41^m 11^s$ ; Decl.  $-62^\circ 53'$ 

16.822	92.5	2.76	0.9	3	370
16.842	92.7	2.66	1.2	2	370
16.872	91.5	2.53	1.4	2½	370
16.85	92.2	2.65	(6.6 ... 6.9)		A

 $h$  5223 = Rus 325;  $-56^\circ 9555$ ; 8.4A.R.  $20^h 42^m 1^s$ ; Decl.  $-56^\circ 51'$ 

13.513	289.6	9.23	23.3	2	300
13.893	289.6	9.23	1.6	3	300
13.70	289.6	9.23	(9.3 ... 9.4)		F

 $h$  5232;  $-56^\circ 9562 + 3$ ; 9.2 + 9.3A.R.  $20^h 46^m 25^s$ ; Decl.  $-56^\circ 24'$ 

13.513	6.5	26.00	23.6	2	300
13.893	7.1	26.04	1.7	3	300
13.70	6.8	26.02	(9.3 ... 9.8)		M?

 $h$  5231;  $-70^\circ 2812$ ; 7.4A.R.  $20^h 46^m 30^s$ ; Decl.  $-70^\circ 54'$ 

17.841	116.0	7.24	0.1	2	370
17.857	116.0	7.32	23.7	3	370
17.904	116.7	7.35	2.0	2	370
17.87	116.2	7.30	(8.1 ... 8.7)		F?

BC = I 668

17.841	325.6	1.06	0.3	2	370
17.857	324.7	1.01	23.6	3	370
17.904	320.9	1.07	2.1	2	370
17.87	323.7	1.05	(8.7 ... 9.2)		142



*h* 5238;  $-44^{\circ} 9926 + 7$ ;  $9.6 + 9.6$

A.R.  $20^{\text{h}} 52^{\text{m}} 41^{\text{s}}$ ; Decl.  $-44^{\circ} 54'$

14.441	191.9	36.89	18.5	2	370
14.463	192.5	36.80	18.8	3	370
14.45	192.2	36.84	(9.3 ... 9.3)		F

*h* 5237;  $-73^{\circ} 2190$ ;  $10.0$

A.R.  $20^{\text{h}} 53^{\text{m}} 9^{\text{s}}$ ; Decl.  $-73^{\circ} 46'$

17.841	275.0	6.04	0.6	2	370
17.857	274.1	5.70	0.4	3	370
17.904	277.9	5.87	2.3	2	370
17.87	275.7	5.87	(10.3 ... 12.0)		N

$\Delta$  236;  $-43^{\circ} 9359 + 61$ ;  $6.4 + 7.6$

A.R.  $20^{\text{h}} 53^{\text{m}} 55^{\text{s}}$ ; Decl.  $-43^{\circ} 29'$

13.493	73.3	57.79	18.5	3	300
13.710	73.0	57.75	1.4	$1\frac{1}{2}$	300
13.60	73.2	57.77	(6.7 ... 6.9)		D

*h* 5239 = Rus 327;  $-55^{\circ} 9505 + 6$ ;  $8.9 + 9.0$

A.R.  $20^{\text{h}} 54^{\text{m}} 55^{\text{s}}$ ; Decl.  $-55^{\circ} 49'$

13.513	211.6	12.96	23.8	2	300
13.893	211.6	12.71	2.2	3	300
13.70	211.6	12.83	(8.9 ... 9.4)		F

*h* 5240;  $-67^{\circ} 3774$ ;  $9.3$

A.R.  $20^{\text{h}} 57^{\text{m}} 6^{\text{s}}$ ; Decl.  $-67^{\circ} 32'$

17.789	205.8	13.67	0.9	2	370
17.822	206.1	[13.12]	0.8	$1\frac{1}{2}$	370
17.833	206.8	13.49	0.7	2	370
17.81	206.2	13.58	(9.4 ... 11.8)		N

*h* 5241;  $-55^{\circ} 9515$ ;  $9.8$

A.R.  $20^{\text{h}} 57^{\text{m}} 40^{\text{s}}$ ; Decl.  $-55^{\circ} 59'$

13.513	41.5	12.69	23.9	$2\frac{1}{2}$	300
13.893	40.4	12.62	2.3	$2\frac{1}{2}$	300
13.70	41.0	12.65	(10.5 ... 10.9)		N

*h* 5243;  $-57^{\circ} 9793 + 4$ ;  $10.0 + 10.0$

A.R.  $20^{\text{h}} 58^{\text{m}} 22^{\text{s}}$ ; Decl.  $-57^{\circ} 32'$

13.513	95.9	24.58	0.1	2	300
13.893	96.0	24.77	2.4	3	300
13.70	96.0	24.67	(9.6 ... 9.8)		F

*h* 5246;  $-55^{\circ} 9530$ ;  $7.2$

A.R.  $21^{\text{h}} 1^{\text{m}} 16^{\text{s}}$ ; Decl.  $-55^{\circ} 5'$

13.491	125.3	3.23	17.8	2	300
13.513	125.0	3.26	0.3	2	300
13.718	124.9	3.29	1.4	$2\frac{1}{2}$	300
13.57	125.1	3.26	(8.2 ... 8.5)		20

*h* 5247;  $-49^{\circ} 11376 + 7$ ;  $8.4 + 8.6$

A.R.  $21^{\text{h}} 1^{\text{m}} 30^{\text{s}}$ ; Decl.  $-49^{\circ} 21'$

13.275	187.0	28.74	18.3	2	300
13.461	187.6	28.34	23.8	2	300
13.819	187.1	28.39	1.6	3	420
13.833	186.9	28.44	0.6	2	300
13.60	187.1	28.48	(8.6 ... 8.8)		F

*h* 5250;  $-64^{\circ} 4110$ ;  $8.0$

A.R.  $21^{\text{h}} 5^{\text{m}} 6^{\text{s}}$ ; Decl.  $-64^{\circ} 12'$

16.814	305.5	9.58	0.2	$2\frac{1}{2}$	370
16.817	305.5	9.66	0.3	2	370
16.822	305.1	9.56	1.1	3	370
16.82	305.4	9.60	(8.7 ... 10.4)		F

*h* 5257;  $-51^{\circ} 11643$ ;  $8.2$

A.R.  $21^{\text{h}} 10^{\text{m}} 21^{\text{s}}$ ; Decl.  $-51^{\circ} 14'$

16.707	273.7	13.48	20.1	$2\frac{1}{2}$	370
16.710	273.4	13.60	20.0	2	370
16.71	273.6	13.58	(8.8 ... 9.1)		F?

*h* 5256;  $-60^{\circ} 7465 + 4$ ;  $8.8 + 8.8$

A.R.  $21^{\text{h}} 10^{\text{m}} 22^{\text{s}}$ ; Decl.  $-60^{\circ} 49'$

16.754	331.9	26.76	0.0	$1\frac{1}{2}$	370
16.762	332.2	26.72	23.3	2	370
16.76	332.1	26.74	(8.8 ... 8.8)		D?

*h* 5255;  $-67^{\circ} 3791$ ;  $9.2$

A.R.  $21^{\text{h}} 10^{\text{m}} 39^{\text{s}}$ ; Decl.  $-67^{\circ} 26'$

17.789	111.0	26.14	1.2	2	370
17.833	111.2	26.11	1.0	2	370
17.81	111.1	26.12	(9.2 ... 11.0)		128

*h* 5258; 9 Indi;  $4.3$

A.R.  $21^{\text{h}} 10^{\text{m}} 57^{\text{s}}$ ; Decl.  $-53^{\circ} 58'$

13.514	282.4	5.34	0.4	$2\frac{1}{2}$	300
13.893	282.6	5.24	2.6	$2\frac{1}{2}$	420
13.901	283.3	5.19	2.5	2	420
14.394	284.3	5.00	19.1	3	370
14.397	282.4	4.97	19.0	4	370
14.400	283.0	4.91	19.1	3	370
13.30	282.8	5.26			
14.40	283.2	4.96	(5.1 ... 7.4)		M

*h* 5259;  $-47^{\circ} 9670$ ;  $7.0$

A.R.  $21^{\text{h}} 10^{\text{m}} 58^{\text{s}}$ ; Decl.  $-47^{\circ} 35'$

13.275	129.5	27.68	18.5	2	300
13.819	129.8	27.39	1.7	$2\frac{1}{2}$	420
13.833	129.3	27.44	0.8	2	300
13.64	129.5	27.50	(6.8 ... 9.7)		N

$h$  5260;  $-72^\circ 25'9''$ ; 7.0A.R.  $21^h 13^m 20^s$ ; Decl.  $-72^\circ 20'$ 

17.816	270.9	44.82	0.5	$1\frac{1}{2}$	370
17.841	270.7	44.59	0.8	2	370
17.857	270.6	44.39	0.5	3	370
17.84	270.7	44.60	(6.6 ... 12.0)		N

 $h$  5267;  $-46^\circ 10'21.6''$  + 17; 7.4 + 9.5A.R.  $21^h 18^m 21^s$ ; Decl.  $-46^\circ 36'$ 

AB Véase la nota. See note 127

AC

13.819	207.3	22.52	2.1	2	420
14.537	209.1	[22.20]	19.7	1	370
14.569	207.3	23.01	18.7	$2\frac{1}{2}$	370
14.572	208.0	22.93	18.1	$3\frac{1}{2}$	370
14.37	207.9	22.82	(7.7 ... 13.3)		N

AD

13.819	182.2	44.14	2.0	2	420
14.537	182.3	43.83	19.5	1	370
14.561	181.7	44.10	17.3	2	370
14.572	182.4	44.00	18.2	$3\frac{1}{2}$	370
14.37	182.2	44.02	(7.7 ... 9.0)		N

Melbourne =  $\beta$  767;  $-43^\circ 9'45.1''$ ; 5.8A.R.  $21^h 18^m 59^s$ ; Decl.  $-43^\circ 5'$ 

14.463	144.8	2.96	19.0	3	370
14.479	147.1	3.03	18.1	2	370
14.482	144.3	3.13	18.9	2	370
14.47	145.4	3.04	(6.1 ... 8.7)		D

Rus 331;  $-55^\circ 9'52''$  + 3; 8.8 + 9.4A.R.  $21^h 19^m 16^s$ ; Decl.  $-55^\circ 42'$ 

13.513	108.1	31.43	0.7	2	300
13.830	108.0	32.00	2.1	2	420
13.893	107.7	31.61	2.7	3	300
13.75	107.9	31.68	(9.1 ... 9.3)		F

 $h$  5268;  $-74^\circ 19'9.6''$ ; 10.3:A.R.  $21^h 20^m 25^s$ ; Decl.  $-74^\circ 4'$ 

17.904	231.9	14.37	2.5	2	370
17.906	231.7	14.34	1.4	$1\frac{1}{2}$	370
17.90	231.8	14.36	(10.9 ... 11.6)		N

 $h$  5270;  $-60^\circ 7'48.1''$ ; 7.8A.R.  $21^h 20^m 56^s$ ; Decl.  $-60^\circ 45'$ 

16.760	54.1	27.64	1.5	2	370
16.762	54.0	27.58	23.6	2	370
16.76	54.0	27.61	(8.2 ... 11.6)		N

 $h$  5272;  $-41^\circ 9'63.7''$ ; 9.4A.R.  $21^h 21^m 18^s$ ; Decl.  $-41^\circ 58'$ 

14.463	302.7	23.85	19.1	3	370
14.482	301.7	23.61	19.1	2	370
14.47	302.2	23.73	(9.0 ... 13.0)		N

 $h$  5273;  $-48^\circ 10'59.0''$ ; 9.4A.R.  $21^h 22^m 36^s$ ; Decl.  $-48^\circ 54'$ 

14.575	95.3	7.47	0.1	$2\frac{1}{2}$	370
14.583	95.9	7.51	20.0	$2\frac{1}{2}$	370
14.58	95.6	7.49	(10.0 ... 10.6)		A

 $h$  5277;  $-53^\circ 10'10.3''$ ; 9.3A.R.  $21^h 26^m 35^s$ ; Decl.  $-53^\circ 51'$ 

16.707	49.2	13.93	20.6	2	370
16.710	47.4	13.79	20.2	2	370
16.716	49.0	14.24	20.1	$2\frac{1}{2}$	370
16.71	48.5	13.99	(9.1 ... 12.7)		N

 $h$  5276?; Anon.A.R.  $21^h 26^m 52^s$ ; Decl.  $-56^\circ 0'$ 

16.707	36.5	13.51	20.9	2	370
16.710	36.8	—	20.3	2	370
16.716	37.2	13.82	20.2	$2\frac{1}{2}$	370
16.71	36.8	13.67	(10.6 ... 10.6)		141

 $h$  5281; Anon.A.R.  $21^h 30^m 30^s$ ; Decl.  $-68^\circ 8'$ 

17.789	37.7	[44.60]	1.4	2	370
17.833	37.8	43.80	1.2	2	370
17.857	37.8	43.84	0.7	$2\frac{1}{2}$	370
17.83	37.8	43.82	(9.4 ... 12.2)		N

BC

17.789	29.2	7.67	1.5	2	370
17.833	31.8	7.97	1.3	2	370
17.857	32.0	7.78	0.7	$2\frac{1}{2}$	370
17.83	31.0	7.81	(12.2 ... 12.4)		N

 $h$  5286;  $-58^\circ 7'88.6''$ ; 8.4A.R.  $21^h 34^m 29^s$ ; Decl.  $-58^\circ 28'$ 

16.760	87.5	7.98	1.8	2	370
16.762	87.5	8.04	0.0	2	370
16.765	87.3	8.20	22.4	2	370
16.76	87.4	8.07	(9.1 ... 10.9)		A†

*h* 5294;  $-60^{\circ} 7503$ ; 9.4

A.R.  $21^{\text{h}} 35^{\text{m}} 8^{\text{s}}$ ; Decl.  $-60^{\circ} 47'$

16.760	12.01	8.52	1.6	2½	370
16.762	13.1	8.64	23.8	2	370
16.765	12.5	8.60	22.2	2	370
16.76	12.6	8.59	(10.2 ... 10.4)		F

*h* 5287; Anon.

A.R.  $21^{\text{h}} 35^{\text{m}} 50^{\text{s}}$ ; Decl.  $-74^{\circ} 49'$

17.904	319.3	5.50	2.8	2	370
17.906	321.6	5.69	1.6	2	370
17.909	320.4	5.63	1.2	2½	370
17.91	320.4	5.61	(10.5 ... 10.8)		N

*h* 5290;  $-54^{\circ} 9934$ ; 9.0

A.R.  $21^{\text{h}} 35^{\text{m}} 51^{\text{s}}$ ; Decl.  $-54^{\circ} 42'$

13.513	290.5	11.05	0.8	3	300
13.830	290.9	11.19	2.3	2	300
13.912	291.8	11.14	2.8	2	300
13.75	291.1	11.13	(9.3 ... 10.4)		N

Brisbane;  $-47^{\circ} 9758$ ; 6.7

A.R.  $21^{\text{h}} 40^{\text{m}} 8^{\text{s}}$ ; Decl.  $-47^{\circ} 52'$

14.537	357.8	50.11	19.8	1	370
14.561	357.4	50.26	17.9	2	370
14.55	357.6	50.19	(6.5 ... 9.2)		R

*h* 5295;  $-75^{\circ} 1736 + 5$ ; 9.4 + 9.6

A.R.  $21^{\text{h}} 40^{\text{m}} 43^{\text{s}}$ ; Decl.  $-75^{\circ} 29'$

17.906	203.5	21.82	1.9	2	370
17.909	203.4	21.64	1.3	2½	370
17.91	203.4	21.73	(9.4 ... 10.3)		22

*h* 5297; Anon.

A.R.  $21^{\text{h}} 46^{\text{m}} 0^{\text{s}}$ ; Decl.  $-73^{\circ} 10'$

17.857	313.7	8.78	0.9	2½	370
17.909	312.7	8.86	1.9	2½	370
17.918	311.5	8.71	1.9	2	370
17.89	312.6	8.78	(10.8 ... 12.0)		N

*h* 5300;  $-59^{\circ} 7742 + 3$ ; 8.4 + 10.1

A.R.  $21^{\text{h}} 47^{\text{m}} 25^{\text{s}}$ ; Decl.  $-59^{\circ} 57'$

16.760	19.2	26.39	2.0	2	370
16.762	20.3	26.64	0.2	2	370
16.765	20.0	26.53	22.6	2	370
16.76	19.8	26.52	(8.5 ... 10.8)		N

BC

16.760	271.8	7.09	2.1	2	370
16.762	272.5	7.23	0.4	2	370
16.765	273.8	7.36	22.7	2	370
16.76	272.7	7.23	(10.8 ... 11.8)		N

*h* 5302;  $-53^{\circ} 10200$ ; 7.6

A.R.  $21^{\text{h}} 48^{\text{m}} 6^{\text{s}}$ ; Decl.  $-53^{\circ} 38'$

16.707	351.93	12.38	21.2	2	370
16.719	351.3	12.27	0.8	3	370
16.71	351.3	12.32	(8.6 ... 11.1)		F?

*h* 5303;  $-43^{\circ} 9552$ ; 8.6

A.R.  $21^{\text{h}} 48^{\text{m}} 16^{\text{s}}$ ; Decl.  $-43^{\circ} 10'$

13.710	50.2	28.26	1.8	2	300
13.792	50.5	28.02	1.1	3	300
13.75	50.4	28.14	(8.5 ... 9.2)		M?

*h* 5309;  $-51^{\circ} 11755$ ; 9.0

A.R.  $21^{\text{h}} 48^{\text{m}} 58^{\text{s}}$ ; Decl.  $-51^{\circ} 40'$

16.707	347.8	8.89	21.3	2½	370
16.717	348.3	8.99	20.5	3	370
16.719	349.1	9.00	0.6	2½	370
16.71	348.4	8.96	(9.8 ... 9.9)		51

*h* 5308;  $-46^{\circ} 10321 + 20$ ; 9.4 + 9.6

A.R.  $21^{\text{h}} 49^{\text{m}} 22^{\text{s}}$ ; Decl.  $-46^{\circ} 1'$

14.463	314.1	18.69	19.5	3	370
14.542	314.4	18.76	19.7	1½	370
14.50	314.2	18.72	(9.2 ... 9.3)		F

*h* 5301;  $-77^{\circ} 1528$ ; 7.7

A.R.  $21^{\text{h}} 49^{\text{m}} 31^{\text{s}}$ ; Decl.  $-77^{\circ} 54'$

17.909	204.0	10.63	1.5	3	370
17.926	203.5	10.51	2.2	2	370
17.931	203.6	10.52	2.2	2½	370
17.92	203.7	10.55	(8.0 ... 10.2)		F

Anon. 3' nf. *h* 5301

A.R.  $21^{\text{h}} 49^{\text{m}} 40^{\text{s}}$ ; Decl.  $-77^{\circ} 52'$

17.926	277.0	6.57	2.4	2	370
17.931	274.7	6.65	2.3	2	370
17.93	275.8	6.61	(11.6 ... 13.0)		N

*h* 5306;  $-76^{\circ} 1542$ ; 6.0

A.R.  $21^{\text{h}} 50^{\text{m}} 45^{\text{s}}$ ; Decl.  $-76^{\circ} 43'$

17.909	71.8	34.62	1.7	2½	370
17.926	71.5	34.51	2.6	2	370
17.92	71.7	34.57	(6.2 ... 10.1)		N

*h* 5312;  $-71^{\circ} 2656?$ ; 10.0

A.R.  $21^{\text{h}} 53^{\text{m}} 58^{\text{s}}$ ; Decl.  $-71^{\circ} 39'$

17.857	358.7	25.60	1.1	2½	370
17.909	358.9	25.47	2.2	2	370
17.88	358.8	25.54	(10.4 ... 10.8)		88

$h$  5313;  $-54^\circ 10006$ ; 9.8A.R.  $21^h 56^m 6^s$ ; Decl.  $-54^\circ 27'$ 

13.901	90.9	11.61	2.8	2	300
13.912	91.6	11.52	2.9	2	300
13.91	91.2	11.56	(10.2 ... 11.5)		N

 $h$  5314;  $-43^\circ 9578$ ; 8.0A.R.  $21^h 56^m 37^s$ ; Decl.  $-43^\circ 20'$ 

13.792	56.2	13.10	1.3	3	300
14.463	56.3	12.83	19.9	$2\frac{1}{2}$	370
14.542	56.2	12.82	19.9	$1\frac{1}{2}$	370
14.27	56.2	12.92	(8.8 ... 11.3)		N

 $h$  5316;  $-59^\circ 7765$ ; 8.4A.R.  $21^h 58^m 18^s$ ; Decl.  $-59^\circ 44'$ 

16.707	138.7	3.86	21.5	2	370
16.716	138.1	3.88	20.7	3	370
16.719	139.5	3.87	1.1	3	370
16.71	138.8	3.87	(8.8 ... 10.1)		F?

 $h$  5317;  $-59^\circ 7773 + 4$ ; 8.8 + 9.6A.R.  $22^h 3^m 6^s$ ; Decl.  $-59^\circ 27'$ 

16.707	99.8	14.42	21.7	2	370
16.716	100.3	14.37	20.8	3	370
16.71	100.0	14.39	(8.8 ... 9.1)		51

C6. 62;  $-49^\circ 11560$ ; 8.0A.R.  $22^h 5^m 5^s$ ; Decl.  $-49^\circ 40'$ 

14.542	354.1	5.55	19.5	$1\frac{1}{2}$	370
14.569	354.1	5.47	19.0	$2\frac{1}{2}$	370
14.56	354.1	5.51	(8.0 ... 11.0)		D?

 $h$  5320;  $-56^\circ 9838$ ; 8.7A.R.  $22^h 5^m 18^s$ ; Decl.  $-56^\circ 5'$ 

13.901	275.5	17.83	3.0	2	300
13.920	276.9	17.72	2.9	2	300
13.91	276.2	17.77	(9.1 ... 12.8)		N

 $h$  5321; Anon.A.R.  $22^h 7^m 10^s$ ; Decl.  $-77^\circ 18'$ 

17.909	99.3	5.97	2.6	2	370
17.926	100.3	6.00	2.9	$1\frac{1}{2}$	370
17.931	99.0	6.10	2.5	$2\frac{1}{2}$	370
17.92	99.5	6.02	(10.7 ... 12.3)		N

 $h$  5323;  $-61^\circ 6640 + 39$ ; 8.2 + 8.4A.R.  $22^h 10^m 50^s$ ; Decl.  $-61^\circ 25'$ 

16.759	204.5	26.52	23.1	2	370
16.762	204.6	26.61	0.6	2	370
16.76	204.5	26.56	(8.5 ... 8.8)		F

 $h$  5325;  $-73^\circ 2253 + 2$ ; 7.9 + 8.1A.R.  $22^h 13^m 21^s$ ; Decl.  $-73^\circ 26'$ 

17.833	267.5	19.01	2.0	2	370
17.857	267.5	18.90	1.4	$2\frac{1}{2}$	370
17.860	267.2	19.01	2.1	2	370
17.84	267.4	18.97	(7.8 ... 8.2)		F?

AC

17.860	99.0	32.31	2.2	2	370
17.909	98.8	32.54	2.4	2	370
17.88	98.9	32.43	(7.8 ... 11.3)		N

 $h$  5327;  $-65^\circ 4027 + 8$ ; 9.0 + 9.8A.R.  $22^h 14^m 4^s$ ; Decl.  $-65^\circ 47'$ 

16.814	128.8	25.51	0.5	$2\frac{1}{2}$	370
16.817	128.2	25.56	0.5	2	370
16.822	128.6	25.52	1.3	3	370
16.82	128.5	25.53	(9.3 ... 10.1)		128

 $\Delta$  238;  $-75^\circ 1738$ ; 6.6A.R.  $22^h 14^m 55^s$ ; Decl.  $-75^\circ 39'$ 

17.909	81.5	20.04	3.0	2	370
17.926	80.9	20.20	3.2	$1\frac{1}{2}$	370
17.92	81.2	20.12	(6.4 ... 9.0)		D?

 $h$  5328;  $-65^\circ 4033$ ; 10.2A.R.  $22^h 15^m 17^s$ ; Decl.  $-65^\circ 45'$ 

16.814	294.8	9.15	0.8	2	370
16.817	295.4	9.25	0.7	$1\frac{1}{2}$	370
16.822	295.6	9.27	1.4	3	370
16.82	295.3	9.22	(10.8 ... 12.3)		N

Jacob 230;  $-42^\circ 9433 + 4$ ; 7.4 + 8.2A.R.  $22^h 17^m 11^s$ ; Decl.  $-42^\circ 4'$ 

13.493	79.1	31.04	18.7	3	300
13.792	78.9	31.04	1.4	$2\frac{1}{2}$	300
14.463	78.1	30.74	20.1	3	370
13.92	78.7	30.94	(6.9 ... 7.9)		

 $h$  5331;  $-62^\circ 6335 + 6$ ; 10.2 + 10.2A.R.  $22^h 17^m 33^s$ ; Decl.  $-62^\circ 35'$ 

16.814	176.6	18.79	1.7	2	370
16.817	176.9	18.93	1.0	$1\frac{1}{2}$	370
16.82	176.7	18.86	(10.4 ... 10.4)		M

 $h$  5332;  $-42^\circ 9436$ ; 8.6A.R.  $22^h 17^m 33^s$ ; Decl.  $-42^\circ 40'$ 

13.792	244.4	12.67	1.5	3	300
14.463	244.5	12.57	20.3	$2\frac{1}{2}$	370
14.13	244.4	12.62	(8.5 ... 9.8)		N

*h* 5335; —45° 10294; 9.6

A.R. 22<sup>h</sup> 18<sup>m</sup> 1<sup>s</sup>; Decl. —45° 56'

14.542	69.7	9.38	20.1	1½	370
14.569	69.0	9.44	19.2	2½	370
14.572	67.7	9.52	18.4	4	370
14.56	68.8	9.45	(9.9 ... 10.3)		N

*h* 5333; Anon.

A.R. 22<sup>h</sup> 18<sup>m</sup> 25<sup>s</sup>; Decl. —62° 42'

16.814	251.2	16.79	1.5	2	370
16.823	252.2	16.52	1.6	3	370
16.842	252.8	16.55	1.5	2	370
16.83	252.1	16.62	(10.4 ... 11.9)		N

*h* 5334; δ Tucanae; 5.0

A.R. 22<sup>h</sup> 18<sup>m</sup> 25<sup>s</sup>; Decl. —65° 36'

16.814	282.3	7.06	1.2	2	370
16.817	281.5	6.89	0.8	2	370
16.822	283.2	7.05	1.5	3	370
16.82	282.3	7.00	(4.2 ... 10.1)		F

*h* 5337; C6D —45° 14700; 9.6

A.R. 22<sup>h</sup> 19<sup>m</sup> 44<sup>s</sup>; Decl. —45° 31'

14.542	25.0	14.37	20.3	1	370
14.569	23.5	14.44	19.3	2	370
14.572	23.9	14.32	18.6	4	370
14.56	24.1	14.38	(10.2 ... 10.7)		N

*h* 5336; Anon.

A.R. 22<sup>h</sup> 20<sup>m</sup> 30<sup>s</sup>; Decl. —74° 31'

17.931	22.0	13.51	3.1	2½	370
17.940	22.8	13.59	2.5	2	370
17.94	22.4	13.55	(10.6 ... 12.4)		N

*h* 5338; —52° 12028; 7.8

A.R. 22<sup>h</sup> 20<sup>m</sup> 30<sup>s</sup>; Decl. —52° 25'

16.702	182.5	30.23	20.0	3	370
16.705	182.8	30.35	20.4	2	370
16.70	182.6	30.29	(7.2 ... 10.4)		142

*h* 5340; —62° 6344; 9.6

A.R. 22<sup>h</sup> 23<sup>m</sup> 22<sup>s</sup>; Decl. —62° 3'

16.707	308.2	5.97	21.8	2	370
16.716	309.2	6.22	20.9	3	370
16.727	307.3	6.12	1.5	2	370
16.814	307.4	5.97	2.1	2	370
16.74	308.0	6.07	(10.2 ... 10.4)		N

*h* 5341; —46° 10417; 9.1

A.R. 22<sup>h</sup> 24<sup>m</sup> 19<sup>s</sup>; Decl. —46° 57'

14.575	92.3	5.11	1.2	3	370
14.583	93.0	5.23	20.1	2	370
14.586	92.4	5.20	20.4	2	370
14.58	92.6	5.18	(10.4 ... 10.6)		D?

*h* 5339; Anon.

A.R. 22<sup>h</sup> 24<sup>m</sup> 20<sup>s</sup>; Decl. —74° 32'

17.931	130.4	14.64	3.2	2½	370
17.940	130.2	14.70	2.8	2	370
17.94	130.3	14.67	(10.4 ... 11.4)		N

*h* 5342; —66° 3682?; 10.0

A.R. 22<sup>h</sup> 26<sup>m</sup> 40<sup>s</sup>; Decl. —66° 44'

16.872	255.3	8.54	2.0	2	370
16.874	256.5	8.33	2.2	2	370
16.885	255.0	8.25	1.9	2	370
16.88	255.6	8.37	(10.4 ... 11.5)		N

*h* 5348; —59° 7821; 8.0

A.R. 22<sup>h</sup> 31<sup>m</sup> 2<sup>s</sup>; Decl. —59° 27'

16.707	273.6	4.30	22.0	2	370
16.716	274.9	4.41	21.0	3	370
16.727	272.3	4.32	1.7	2	370
16.72	273.6	4.34	(8.8 ... 12.2)		142

*h* 5349; —53° 10326; 6.6

A.R. 22<sup>h</sup> 31<sup>m</sup> 24<sup>s</sup>; Decl. —53° 20'

16.702	118.5	33.41	20.2	2½	370
16.705	118.6	33.47	20.5	2	370
16.70	118.5	33.44	(6.6 ... 11.4)		142

*h* 5351; —48° 10791; 10.4

A.R. 22<sup>h</sup> 31<sup>m</sup> 48<sup>s</sup>; Decl. —48° 16'

14.575	336.0	8.12	1.4	2½	370
14.583	335.6	8.24	20.4	2	370
14.586	333.5	8.23	20.8	2	370
14.58	335.0	8.20	(10.3 ... 10.9)		N

AC

14.575	223.5	6.81	1.3	2½	370
14.583	220.7	7.12	20.3	2	370
14.586	220.5	7.05	20.6	2	370
14.58	221.6	6.99	(10.3 ... 11.5)		N

*h* 5352; —45° 10317; 9.6

A.R. 22<sup>h</sup> 31<sup>m</sup> 54<sup>s</sup>; Decl. —45° 41'

14.569	263.4	13.80	19.6	2	370
14.572	263.2	13.60	18.7	4	370
14.57	263.3	13.70	(9.7 ... 12.3)		N

(Sigue Continued.)

## AC

14.569	247.6	26.02	19.7	2	370
14.572	247.0	25.81	18.8	4	370
14.57	247.3	25.91	(9.7 ... 9.8)		N

$h$  5354;  $-58^\circ 7981$ ; 8.2

A.R.  $22^h 32^m 29^s$ ; Decl.  $-58^\circ 29'$

16.707	75.3	27.47	22.2	2*	370
16.716	76.5	27.30	21.2	2	370
16.727	75.7	27.36	2.0	2	370
16.72	75.8	27.38	(9.0 ... 9.4)		F?

$h$  5357;  $-58^\circ 7987$ ; 9.3

A.R.  $22^h 34^m 52^s$ ; Decl.  $-58^\circ 30'$

16.707	135.5	17.48	22.3	2	370
16.716	135.6	17.51	21.6	2	370
16.71	135.5	17.49	(9.2 ... 10.9)		N

$h$  5358;  $-60^\circ 7594 + 5$ ; 8.2 + 8.8

A.R.  $22^h 36^m 36^s$ ; Decl.  $-60^\circ 46'$

16.716	91.2	31.29	21.8	2	370
16.737	91.0	31.37	22.4	3	370
16.73	91.1	31.33	(8.6 ... 9.8)		N

Cruls 140 = I 139;  $\gamma$  Gruis; 5.8

A.R.  $22^h 37^m 57^s$ ; Decl.  $-54^\circ 9'$

13.901	184.4	24.47	3.3	2	300
13.920	184.3	24.06	3.2	2	300
13.926	184.5	24.10	3.3	2	300
13.92	184.4	24.21	(5.5 ... 11.4)		

$h$  5360;  $-59^\circ 7828$ ; 8.4

A.R.  $22^h 38^m 58^s$ ; Decl.  $-59^\circ 23'$

16.716	86.6	9.62	21.9	2	370
16.738	86.6	9.66	22.6	3	370
16.73	86.6	9.64	(9.4 ... 10.9)		N

$h$  5361;  $-66^\circ 3709$ ; 7.6

A.R.  $22^h 39^m 10^s$ ; Decl.  $-66^\circ 13'$

16.872	41.3	80.65	2.1	2	370
16.874	41.6	80.53	2.4	2	370
16.87	41.4	80.59	(7.2 ... 10.8)		N

$h$  5362 =  $\lambda$  477;  $-47^\circ 9903$ ; 7.1

A.R.  $22^h 39^m 20^s$ ; Decl.  $-47^\circ 36'$

14.575	139.8	10.60	1.5	2	370
14.583	139.8	10.61	20.5	2½	370
14.58	139.8	10.61	(7.0 ... 9.6)		20

$h$  5364;  $-57^\circ 10150$ ; 9.0

A.R.  $22^h 42^m 45^s$ ; Decl.  $-57^\circ 9'$

13.526	98.5	10.80	19.7	2	300
13.803	99.0	10.66	3.1	2	300
13.66	98.8	10.73	(9.7 ... 10.2)		F?

$h$  5366;  $-43^\circ 9666$ ; 7.5

A.R.  $22^h 45^m 20^s$ ; Decl.  $-43^\circ 27'$

14.572	251.7	14.77	19.2	4	370
14.575	251.1	14.88	0.6	2½	370
14.57	251.4	14.82	(8.4 ... 8.7)		F

## CD

14.572	110.0	12.2	19.4	3½	370
14.575	112.9	13.8	0.8	2½	370
14.57	111.4	13.0	(13.7 ... 13.9)		N

$h$  5369;  $-72^\circ 2738$ ; 10.0

A.R.  $22^h 50^m 17^s$ ; Decl.  $-72^\circ 58'$

17.833	9.9	21.77	2.4	2	370
17.857	10.8	21.70	1.7	2½	370
17.860	9.7	21.68	2.3	2	370
17.85	10.1	21.72	(10.4 ... 11.2)		N

$h$  5370;  $-61^\circ 6700 + 2$ ; 8.8 + 9.4

A.R.  $22^h 50^m 29^s$ ; Decl.  $-61^\circ 51'$

16.716	142.5	18.88	22.0	2	370
16.738	141.4	18.82	22.7	3	370
16.73	141.9	18.85	(10.0 ... 10.2)		N

$h$  5372;  $-54^\circ 10176$ ; 9.4

A.R.  $22^h 51^m 53^s$ ; Decl.  $-54^\circ 2'$

13.920	300.5	18.16	3.7	2	300
13.926	300.0	18.11	3.6	2½	300
13.92	300.2	18.13	(9.5 ... 11.1)		N

$h$  5373;  $-64^\circ 4309 + 10$ ; 7.3 + 9.6

A.R.  $22^h 54^m 17^s$ ; Decl.  $-64^\circ 58'$

16.814	95.4	47.56	2.5	2	370
16.823	95.6	47.12	1.9	3	370
16.842	95.5	47.04	1.8	2	370
16.83	95.5	47.24	(8.0 ... 10.1)		A

$h$  5374; Anon.

A.R.  $22^h 54^m 20^s$ ; Decl.  $-73^\circ 58'$

17.833	237.5	13.91	2.6	2	370
17.857	238.0	14.11	2.0	2½	370
17.85	237.8	14.01	(10.8 ... 11.0)		D?

*h* 5375; Anon.

A.R. 22<sup>h</sup> 55<sup>m</sup> 5<sup>s</sup>; Decl. -77° 0'

17.931	124.2	9.49	3.7	2	370
17.942	123.6	9.89	3.0	2	370
17.945	122.9	9.84	2.4	2½	370
17.94	123.6	9.74	(10.8 ... 11.1)		N

*h* 5376; -72° 2747; 8.8:

A.R. 22<sup>h</sup> 55<sup>m</sup> 52<sup>s</sup>; Decl. -72° 3'

17.833	351.1	8.90	2.8	2	370
17.857	351.3	8.96	2.3	2½	370
17.860	350.9	8.94	2.6	2	370
17.85	351.1	8.93	(9.4 ... 10.6)		N

*h* 5379; -56° 9990 + 1; 9.4 + 9.4

A.R. 22<sup>h</sup> 56<sup>m</sup> 8<sup>s</sup>; Decl. -56° 58'

13.920	325.7	12.44	4.0	2	300
13.926	327.7	12.22	3.8	2	300
13.92	326.7	12.33	(9.7 ... 10.2)		21

Có. 64; -46° 10486; 7.4

A.R. 22<sup>h</sup> 56<sup>m</sup> 49<sup>s</sup>; Decl. -46° 50'

14.583	108.0	3.28	20.7	3	370
14.586	108.1	3.25	21.0	2	370
14.58	108.0	3.27	(8.2 ... 9.3)		F

Sellers 27; -75° 1770; 8.1

A.R. 22<sup>h</sup> 56<sup>m</sup> 59<sup>s</sup>; Decl. -75° 26'

17.931	70.6	3.62	3.3	2	370
17.940	71.5	3.87	3.0	2	370
17.942	70.4	3.47	2.3	2	370
17.945	70.8	3.49	2.2	2½	370
17.94	70.8	3.61	(8.5 ... 11.2)		F

AC

17.931	320.0	18.69	3.5	2	370
17.942	320.0	18.78	2.5	2	370
17.94	320.0	18.73	(8.5 ... 12.4)		N

*h* 5380 = *h* 5377; -68° 3556; 8.9

A.R. 22<sup>h</sup> 57<sup>m</sup> 1<sup>s</sup>; Decl. -68° 7'

16.872	94.8	12.57	2.9	3	370
16.874	95.6	12.56	2.7	2	370
16.87	95.2	12.57	(9.2 ... 10.7)		N

*h* 5382; -52° 12108; 8.2

A.R. 22<sup>h</sup> 57<sup>m</sup> 42<sup>s</sup>; Decl. -52° 2'

16.697	50.1	7.64	21.1	2	370
16.702	50.7	7.73	20.5	2½	370
16.705	51.7	7.82	20.7	2	370
16.70	50.8	7.73	(9.4 ... 9.4)		F

*h* 5381; -75° 1771; 8.5

A.R. 22<sup>h</sup> 58<sup>m</sup> 20<sup>s</sup>; Decl. -75° 41'

17.860	49.4	4.54	3.8	2	370
17.909	51.5	4.56	3.3	2	370
17.931	49.4	4.35	3.6	2	370
17.942	49.2	4.49	2.7	2	370
17.92	49.9	4.49	(9.3 ... 9.6)		D?

Jacob 238 = β 751; θ Gruis; 5.6

A.R. 22<sup>h</sup> 59<sup>m</sup> 49<sup>s</sup>; Decl. -44° 12'

14.572	37.8	1.90	19.6	3	370
14.575	33.5	1.78	0.9	3	370
14.583	38.5	1.80	20.8	3	370
14.58	36.6	1.83	(4.7 ... 7.0)		P

Δ 246; -51° 11908; 6.4

A.R. 23<sup>h</sup> 0<sup>m</sup> 1<sup>s</sup>; Decl. -51° 22'

16.697	257.6	8.38	21.2	2	370
16.702	258.3	8.55	20.7	2½	370
16.705	258.4	8.47	20.8	2	370
16.70	258.1	8.47	(6.7 ... 7.3)		F

Δ 245; -60° 7635; 7.3

A.R. 23<sup>h</sup> 1<sup>m</sup> 2<sup>s</sup>; Decl. -60° 24'

16.707	290.6	13.67	22.4	2½	370
16.716	290.6	13.77	22.1	2	370
16.71	290.6	13.72	(8.0 ... 9.5)		D

*h* 5389; -67° 3954; 8.6

A.R. 23<sup>h</sup> 7<sup>m</sup> 52<sup>s</sup>; Decl. -67° 51'

16.872	250.8	8.62	3.0	3	370
16.875	250.1	8.52	3.3	1½	370
16.885	251.0	8.52	2.1	2	370
16.88	250.6	8.55	(8.7 ... 12.0)		N

*h* 5390; -45° 10408; 7.0

A.R. 23<sup>h</sup> 9<sup>m</sup> 41<sup>s</sup>; Decl. -45° 10'

13.690	44.3	23.07	20.4	2	300
13.710	43.9	23.05	2.3	2	300
13.70	44.1	23.06	(6.5 ... 10.9)		N

Δ 247; -61° 6735 + 4; 7.6 + 7.8

A.R. 23<sup>h</sup> 10<sup>m</sup> 32<sup>s</sup>; Decl. -61° 41'

16.708	286.2	43.12	22.7	3	370
16.716	286.0	43.15	22.3	2	370
16.71	286.1	43.13	(7.6 ... 9.0)		R?

$h$  5392 = Rus 343;  $-58^\circ 8064 + 3$ ;  $7.8 + 8.5$

A.R.  $23^h 11^m 16^s$ ; Decl.  $-58^\circ 59'$

16.716	327.5	24.72	22.7	2	370
16.738	327.3	24.72	22.9	3	370
16.73	327.4	24.72	(8.1 ... 9.1)		R

$\Delta$  248;  $-50^\circ 11802$ ; 5.9

A.R.  $23^h 13^m 48^s$ ; Decl.  $-50^\circ 59'$

16.697	210.6	16.66	21.4	2	370
16.702	209.9	16.76	20.8	$2\frac{1}{2}$	370
16.70	210.2	16.71	(6.4 ... 8.8)		F

$h$  5396; C6D  $-47^\circ 14548$ ; 9.9

A.R.  $23^h 15^m 42^s$ ; Decl.  $-47^\circ 41'$

14.583	147.0	12.37	21.1	$2\frac{1}{2}$	370
14.586	148.5	12.18	21.2	2	370
14.591	147.3	12.45	19.8	2	370
14.59	147.6	12.33	(10.2 ... 11.0)		N

$\Delta$  249 = Rus 344;  $\psi$  Gruis;  $6.4 + 6.8$

A.R.  $23^h 16^m 49^s$ ; Decl.  $-54^\circ 30'$

13.718	212.3	26.56	1.6	3	300
13.803	211.8	26.53	3.3	2	300
13.833	211.3	26.78	2.8	2	300
13.78	211.8	26.62	(6.5 ... 6.9)		F

$\Delta$  250;  $-50^\circ 11819 + 20$ ;  $8.3 + 9.0$

A.R.  $23^h 20^m 13^s$ ; Decl.  $-50^\circ 58'$

16.792	88.5	38.84	22.8	$2\frac{1}{2}$	370
16.795	88.5	38.86	22.2	$2\frac{1}{2}$	370
16.79	88.5	38.85	(7.8 ... 8.9)		R

$h$  5401;  $-55^\circ 10033 + 4$ ;  $9.4 + 9.8$

A.R.  $23^h 23^m 2^s$ ; Decl.  $-55^\circ 0'$

13.833	42.0	13.45	3.1	2	300
13.920	42.9	13.38	4.2	2	300
13.88	42.4	13.42	(9.8 ... 9.9)		F?

I 690;  $-74^\circ 2071$ ; 8.2

A.R.  $23^h 23^m 14^s$ ; Decl.  $-74^\circ 49'$

17.931	249.6	1.95	4.1	$1\frac{1}{2}$	370
17.945	247.0	1.92	2.6	$2\frac{1}{2}$	370
17.904	245.6	1.82	3.4	2	370
17.95	247.4	1.90	(8.4 ... 11.1)		142

AC =  $h$  5400

17.931	187.4	32.85	4.0	2	370
17.945	188.3	32.92	3.0	2	370
17.964	187.1	32.81	3.6	2	370
17.95	187.6	32.86	(8.4 ... 12.1)		N

$h$  5402;  $-69^\circ 3325 + 4$ ;  $6.8 + 9.0$

A.R.  $23^h 23^m 31^s$ ; Decl.  $-69^\circ 46'$

16.872	198.1	36.34	3.3	3	370
16.875	198.3	36.28	3.6	2	370
16.87	198.2	36.31	(7.6 ... 9.4)		F

$h$  5403;  $-65^\circ 4148 + 9$ ;  $7.5 + 9.2$

A.R.  $23^h 28^m 4^s$ ; Decl.  $-65^\circ 23'$

16.823	45.1	37.74	2.1	3	370
16.842	44.8	37.60	2.3	2	370
16.83	45.0	37.67	(7.6 ... 9.8)		M

Dawson 27;  $-50^\circ 11833$ ; 9.5

A.R.  $23^h 28^m 39^s$ ; Decl.  $-50^\circ 54'$

16.708	355.7	3.77	23.2	3	370
16.716	352.9	3.86	23.0	2	370
16.738	353.7	3.72	23.0	3	370
16.72	354.1	3.78	(10.1 ... 10.4)		

$h$  5407;  $-64^\circ 4363$ ; 9.0

A.R.  $23^h 29^m 22^s$ ; Decl.  $-64^\circ 47'$

16.814	19.8	10.04	2.8	$1\frac{1}{2}$	370
16.823	19.7	9.91	2.3	3	370
16.842	20.3	9.82	2.5	2	370
16.83	19.9	9.92	(9.4 ... 10.4)		A

$h$  5408; Anon.

A.R.  $23^h 29^m 50^s$ ; Decl.  $-50^\circ 21'$

16.708	306.6	6.99	23.0	3	370
16.738	307.4	7.32	23.3	3	370
16.740	305.2	7.32	21.2	2	370
16.73	306.4	7.21	(12.1 ... 12.2)		N

$h$  5409; Anon.

A.R.  $23^h 30^m 10^s$ ; Decl.  $-71^\circ 30'$

17.857	48.3	7.14	2.6	2	370
17.860	48.3	7.12	2.8	2	370
17.909	48.1	7.29	3.6	2	370
17.88	48.2	7.18	(10.7 ... 11.3)		143

$\Delta$  251 = Rii 27; 0 Phoenicis; 6.6

A.R.  $23^h 32^m 46^s$ ; Decl.  $-47^\circ 20'$

14.542	273.6	4.15	20.6	2	370
14.578	273.0	4.12	22.1	$2\frac{1}{2}$	370
14.583	273.0	4.19	21.3	3	370
14.57	273.2	4.15	(6.8 ... 7.6)		F



*h* 5415;  $-71^{\circ} 2770$ ; 7.9

A.R.  $23^{\text{h}} 36^{\text{m}} 8^{\text{s}}$ ; Decl.  $-71^{\circ} 31'$

17.857	125.7	38.18	2.8	2	370
17.909	126.1	38.14	4.0	2	370
17.88	125.9	38.16	(7.5 ... 11.2)		N

Dawson 28;  $-47^{\circ} 10031$ ; 6.7

A.R.  $23^{\text{h}} 36^{\text{m}} 26^{\text{s}}$ ; Decl.  $-47^{\circ} 0'$

14.578	75.1	3.90	22.4	3	370
14.586	77.0	3.83	21.5	2	370
14.591	76.5	3.77	21.3	2	370
14.58	76.2	3.83	(6.7 ... 12.6)		

AC = *h* 5416

14.542	214.5	45.26	20.7	$1\frac{1}{2}$	370
14.578	215.0	45.13	22.3	$2\frac{1}{2}$	370
14.586	214.7	45.31	21.3	2	370
14.57	214.7	45.23	(6.7 ... 10.4)		N

Có. 67;  $-45^{\circ} 10467$ ; 8.2

A.R.  $23^{\text{h}} 38^{\text{m}} 9^{\text{s}}$ ; Decl.  $-45^{\circ} 56'$

14.542	305.8	4.16	20.9	2	370
14.578	306.0	4.13	22.6	3	370
14.583	305.6	4.38	21.5	3	370
14.57	305.8	4.22	(9.6 ... 10.0)		F

*h* 5418;  $-45^{\circ} 10469$ ; 8.8

A.R.  $23^{\text{h}} 39^{\text{m}} 8^{\text{s}}$ ; Decl.  $-45^{\circ} 21'$

14.542	133.5	7.87	21.0	$1\frac{1}{2}$	370
14.578	132.9	8.03	22.7	3	370
14.583	134.4	8.35	21.6	$2\frac{1}{2}$	370
14.57	133.6	8.08	(9.1 ... 13.2)		N

*h* 5419;  $-72^{\circ} 2781 + 2$ ;  $9.8 + 10.4$

A.R.  $23^{\text{h}} 39^{\text{m}} 28^{\text{s}}$ ; Decl.  $-72^{\circ} 40'$

17.860	95.3	21.24	3.1	3	370
17.909	95.6	20.91	4.3	2	370
17.931	95.9	21.19	4.3	2	370
17.90	95.6	21.11	(9.8 ... 10.0)		21

*h* 5420;  $-53^{\circ} 10523$ ; 9.2

A.R.  $23^{\text{h}} 39^{\text{m}} 41^{\text{s}}$ ; Decl.  $-53^{\circ} 58'$

13.833	40.5	9.87	3.3	2	300
13.885	41.4	9.51	4.7	$2\frac{1}{2}$	300
13.893	42.3	9.63	3.9	3	300
13.87	41.4	9.67	(9.2 ... 10.6)		F

Cape 25;  $-45^{\circ} 10474$ ; 8.2

A.R.  $23^{\text{h}} 40^{\text{m}} 8^{\text{s}}$ ; Decl.  $-45^{\circ} 45'$

14.542	343.9	2.59	21.2	2	370
14.578	346.1	2.48	22.8	3	370
14.583	344.8	2.46	21.7	$2\frac{1}{2}$	370
14.57	344.9	2.51	(9.5 ... 9.6)		142

*h* 5421; Anon.

A.R.  $23^{\text{h}} 40^{\text{m}} 45^{\text{s}}$ ; Decl.  $-55^{\circ} 17'$

13.833	227.3	15.87	3.7	2	300
13.885	226.5	16.12	4.9	$2\frac{1}{2}$	300
13.893	227.5	15.97	4.1	3	300
13.87	227.1	15.99	(10.9 ... 11.6)		N

*h* 5422;  $-44^{\circ} 10373$ ; 9.0

A.R.  $23^{\text{h}} 42^{\text{m}} 54^{\text{s}}$ ; Decl.  $-44^{\circ} 9'$

14.542	349.6	6.83	21.3	$2\frac{1}{2}$	370
14.583	349.0	6.88	21.9	$2\frac{1}{2}$	370
14.56	349.3	6.86	(9.8 ... 10.0)		42

*h* 5424;  $-56^{\circ} 10166$ ; 9.0

A.R.  $23^{\text{h}} 43^{\text{m}} 38^{\text{s}}$ ; Decl.  $-56^{\circ} 34'$

13.833	56.1	11.56	3.9	$2\frac{1}{2}$	300
13.885	55.0	11.90	5.1	$2\frac{1}{2}$	300
13.893	56.9	11.68	4.3	3	300
13.87	56.0	11.71	(9.5 ... 11.2)		N

*h* 5425;  $-61^{\circ} 6769$ ; 9.6

A.R.  $23^{\text{h}} 43^{\text{m}} 38^{\text{s}}$ ; Decl.  $-61^{\circ} 48'$

16.740	276.6	13.73	21.5	2	370
16.751	277.4	13.76	21.4	2	370
16.75	277.0	13.74	(10.8 ... 10.9)		N

*h* 5426;  $-45^{\circ} 10482$ ; 9.4

A.R.  $23^{\text{h}} 46^{\text{m}} 4^{\text{s}}$ ; Decl.  $-45^{\circ} 13'$

14.542	335.0	13.06	21.5	$2\frac{1}{2}$	370
14.583	336.1	13.44	22.1	$2\frac{1}{2}$	370
14.586	335.2	13.49	21.8	2	370
14.57	335.4	13.33	(9.8 ... 11.1)		N

*h* 5427;  $-72^{\circ} 2788$ ; 8.9

A.R.  $23^{\text{h}} 46^{\text{m}} 46^{\text{s}}$ ; Decl.  $-72^{\circ} 53'$

17.833	61.7	9.19	3.1	$2\frac{1}{2}$	370
17.860	61.2	9.16	3.2	3	370
17.909	64.3	8.96	4.7	2	370
17.87	62.4	9.10	(9.4 ... 9.7)		F

$h$  5428;  $-66^\circ 38'10''$ ; 7.4A.R.  $23^h 47^m 0^s$ ; Decl.  $-66^\circ 39'$ 

16.872	114.00	12.30	3.5	$1\frac{1}{2}$	370
16.885	113.9	12.44	2.4	2	370
16.88	113.9	12.37	(7.5 ... 12.8)		N

 $h$  5431;  $-52^\circ 12'25''$ ; 9.4A.R.  $23^h 48^m 2^s$ ; Decl.  $-52^\circ 16'$ 

16.697	146.7	33.79	22.0	2	370
16.702	147.2	34.10	21.0	$2\frac{1}{2}$	370
16.705	147.0	33.93	21.0	2	370
16.70	147.0	33.94	(9.6 ... 10.0)		N

 $h$  5430; Anon.A.R.  $23^h 48^m 5^s$ ; Decl.  $-77^\circ 30'$ 

17.931	58.2	20.78	4.7	$1\frac{1}{2}$	370
17.940	57.2	20.26	3.7	2	370
17.942	57.6	20.33	3.3	$1\frac{1}{2}$	370
17.94	57.7	20.46	(10.0 ... 10.6)		M

 $h$  5449; Anon.A.R.  $23^h 48^m 40^s$ ; Decl.  $-70^\circ 3'$ 

16.872	352.6	7.87	3.4	$2\frac{1}{2}$	370
16.875	353.6	7.97	3.8	2	370
16.885	353.2	8.09	2.6	2	370
16.88	353.1	7.98	(10.5 ... 11.1)		N

 $h$  5432;  $-59^\circ 7'38'' + 9$ ; 9.3 + 9.6A.R.  $23^h 48^m 48^s$ ; Decl.  $-59^\circ 27'$ 

16.740	33.4	20.33	21.6	$2\frac{1}{2}$	370
16.751	33.9	20.34	21.5	2	370
16.75	33.6	20.33	(9.2 ... 10.0)		M

 $h$  5434;  $-71^\circ 27'80''$ ; 9.0A.R.  $23^h 49^m 39^s$ ; Decl.  $-71^\circ 34'$ 

17.860	51.98	19.96	3.4	$3\frac{1}{2}$	370
17.931	52.6	20.12	4.4	$1\frac{1}{2}$	370
17.90	52.2	20.04	(9.1 ... 11.6)		N

 $h$  5436;  $-61^\circ 6'88''$ ; 9.6A.R.  $23^h 52^m 23^s$ ; Decl.  $-61^\circ 46'$ 

16.740	258.0	32.55	22.8	$2\frac{1}{2}$	370
16.751	258.7	33.16	21.7	2	370
16.760	258.8	32.63	0.0	2	370
16.75	258.5	32.78	(9.4 ... 11.3)		144

 $h$  5437;  $-53^\circ 10'565''$ ; 6.8A.R.  $23^h 54^m 6^s$ ; Decl.  $-53^\circ 48'$ 

13.833	302.1	2.75	4.2	3	420
13.893	301.0	2.67	4.5	3	420
13.918	299.3	2.91	4.2	$2\frac{1}{2}$	300
13.88	300.8	2.78	(6.3 ... 9.9)		20

 $h$  5438;  $-57^\circ 10'404''$ ; 9.6A.R.  $23^h 55^m 22^s$ ; Decl.  $-57^\circ 56'$ 

13.918	320.4	—	4.6	2	300
13.926	316.0	10.98	4.2	2	300
14.578	320.1	11.72	23.1	3	370
14.14	318.8	11.35	(9.8 ... 13.5)		N

 $h$  5439;  $-73^\circ 23'42''$ ; 9.0A.R.  $23^h 55^m 48^s$ ; Decl.  $-73^\circ 19'$ 

17.860	80.6	9.58	3.5	3	370
17.931	79.9	9.88	4.5	$1\frac{1}{2}$	370
17.940	79.7	9.55	3.3	2	370
17.91	80.1	9.67	(9.3 ... 11.5)		N

STARS NORTH OF  $-31^\circ$  ESTRELLAS AL NORTE DE  $-31^\circ$

Hu 1203; SD  $-18^\circ 68$ ; 9.0

A.R.  $0^h 23^m 10^s$ ; Decl.  $-18^\circ 29'$

17.778	193.8	1.77	0.8	$3\frac{1}{2}$	370
17.961	195.3	1.82	2.9	$2\frac{1}{2}$	370
18.011	194.7	1.89	4.0	$2\frac{1}{2}$	370
17.92	194.6	1.83	(9.5 ... 10.0)		

Hu 1204;  $-21^\circ 65$ ; 8.2

A.R.  $0^h 39^m 40^s$ ; Decl.  $-21^\circ 34'$

17.778	268.8	1.42	1.1	$3\frac{1}{2}$	370
18.011	271.9	1.46	4.2	2	370
18.013	272.7	—	4.8	2	370
17.93	271.1	1.44	(8.8 ... 12.8)		

Hu 1205;  $-19^\circ 93$ ; 8.7

A.R.  $0^h 45^m 34^s$ ; Decl.  $-19^\circ 10'$

17.778	112.4	0.51	1.4	$3\frac{1}{2}$	650
(9.5 ... 9.8) A?					

Hu 1206;  $-20^\circ 120$ ; 9.8

A.R.  $0^h 49^m 23^s$ ; Decl.  $-20^\circ 47'$

17.778	102.1	1.97	1.6	$3\frac{1}{2}$	650
17.961	101.6	1.70	3.3	2	370
18.011	103.3	1.48	4.6	2	475
18.024	100.7	1.59	5.3	2	370
17.94	101.9	1.68	(9.6 ... 10.4) F		

Hu 1211;  $-20^\circ 212$ ; 8.0

A.R.  $1^h 39^m 4^s$ ; Decl.  $-20^\circ 45'$

17.778	111.9	3.55	2.2	$2\frac{1}{2}$	370
17.959	114.8	3.53	5.6	3	370
17.961	113.3	3.83	3.6	2	370
18.011	115.3	3.39	4.8	2	370
17.93	113.8	3.57	(8.7 ... 12.3) D		

Hu 1212;  $-24^\circ 206$ ; 8.4

A.R.  $1^h 44^m 44^s$ ; Decl.  $-24^\circ 22'$

17.959	197.0	—	5.8	3	370
18.011	198.0	[5.20]	5.1	2	370
18.038	198.8	4.60	5.8	3	370
18.043	198.4	4.61	4.9	2	370
18.01	198.1	4.61	(8.5 ... 14.1) F		

Hu 1561;  $-24^\circ 321$ ; 8.6

A.R.  $2^h 42^m 0^s$ ; Decl.  $-24^\circ 11'$

18.011	315.9	1.02	5.4	2	475
18.013	316.0	1.12	5.2	2	475
18.024	317.2	1.23	6.0	$2\frac{1}{2}$	475
18.02	316.4	1.12	(9.5 ... 9.8)		

Olivier 1; SD  $-14^\circ 762$ ; 9.3

A.R.  $3^h 46^m 13^s$ ; Decl.  $-14^\circ 7'$

18.011	278.5	3.31	5.7	$2\frac{1}{2}$	475
18.024	279.7	3.10	6.7	2	475
18.038	277.9	3.11	6.2	3	370
18.02	278.7	3.17	(9.8 ... 10.1)		

Hu 1363;  $-22^\circ 458$ ; 6.8

A.R.  $4^h 1^m 46^s$ ; Decl.  $-22^\circ 19'$

18.038	110±	0.2±	(7.5 ... 8.2)		
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Hu 1374;  $-24^\circ 691$ ; 8.8

A.R.  $4^h 38^m 11^s$ ; Decl.  $-24^\circ 44'$

18.025	268.1	—	7.7	2	650
18.038	261.8	0.60	7.0	$3\frac{1}{2}$	650
18.043	271.8	0.48	5.2	$2\frac{1}{2}$	475
18.04	267.2	0.54	(9.6 ... 9.9) N		

Olivier 2;  $-21^\circ 649$ ; 7.8

A.R.  $4^h 41^m 4^s$ ; Decl.  $-21^\circ 41'$

18.025	222.2	4.44	7.0	2	475
18.038	224.5	4.42	6.7	$3\frac{1}{2}$	370
18.043	225.4	4.55	5.5	$2\frac{1}{2}$	370
18.04	224.0	4.47	(8.6 ... 11.9) D		

Olivier 3;  $-23^\circ 615$ ; 7.7

A.R.  $4^h 41^m 30^s$ ; Decl.  $-23^\circ 0'$

17.959	61.1	1.60	4.8	3	650
18.011	62.1	1.62	6.4	$2\frac{1}{2}$	370
18.025	61.4	1.70	7.3	2	475
18.00	61.5	1.64	(8.4 ... 9.5)		

Anon.; Cód —23° 2343; 9.8

A.R. 4<sup>h</sup> 56<sup>m</sup> 54<sup>s</sup>; Decl. —23° 53'

18.038	72.06	3.44	7.3	3	475
18.044	72.1	3.55	5.7	2	370
18.04	72.4	3.49	(10.2 ... 12.0)		147

AC; C = 12.0

18.044	119.2	13.09	5.9	2	370
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Hu 1385; —23° 679; 9.4

A.R. 4<sup>h</sup> 57<sup>m</sup> 26<sup>s</sup>; Decl. —23° 56'

17.959	326.0	1.08	5.1	3	650
18.038	323.6	0.99	7.6	3½	475
18.044	324.6	0.95	6.2	2	475
18.01	324.8	1.01	(9.9 ... 10.1)		148

Σ 668; β Orionis; 1

A.R. 5<sup>h</sup> 8<sup>m</sup> 47<sup>s</sup>; Decl. —8° 20'

13.075	200.5	9.68	6.7	2½	300
13.113	202.6	9.73	8.0	2½	300
13.151	202.6	9.65	8.8	2	300
13.11	201.9	9.69	(1.0 ... 8.8)		149

Olivier 4; —21° 887; 9.2

A.R. 5<sup>h</sup> 34<sup>m</sup> 34<sup>s</sup>; Decl. —21° 41'

18.025	253.6	2.01	8.9	2	475
18.038	253.8	1.77	9.4	3	475
18.044	254.6	1.99	6.4	2½	475
18.04	254.0	1.92	(9.8 ... 10.0)		

Fox 12; —19° 1888; 9.2

A.R. 7<sup>h</sup> 8<sup>m</sup> 1<sup>s</sup>; Decl. —19° 49'

17.091	258.4	3.87	9.1	2	370
17.266	258.1	3.70	9.6	3	370
17.354	257.8	3.55	9.8	2	370
17.24	258.1	3.71	(10.1 ... 11.3)		142

Roe 26; SD —15° 1715; 9.2

A.R. 7<sup>h</sup> 8<sup>m</sup> 59<sup>s</sup>; Decl. —15° 7'

17.091	119.3	10.11	9.3	2	370
17.266	119.4	10.01	9.8	3	370
17.18	119.4	10.06	(8.8 ... 12.2)		150

Anon.; —19° 2666; 10.4

A.R. 7<sup>h</sup> 41<sup>m</sup> 49<sup>s</sup>; Decl. —19° 15'

17.354	332.6	3.97	10.3	2	370
18.025	333.8	3.75	9.2	2	475
17.69	333.2	3.86	(10.8 ... 11.4)		151

Olivier 5; Véase la nota. See note 151

Dawson 29; SD —18° 2051; 8.9

A.R. 7<sup>h</sup> 45<sup>m</sup> 30<sup>s</sup>; Decl. —18° 36'

17.354	190.06	5.71	10.2	2	370
18.025	190.4	5.56	9.4	2½	475
18.038	190.3	5.72	10.2	2	370
17.81	190.4	5.66	(9.2 ... 9.4)		151

Pettit; —19° 4039; 9.4:

A.R. 9<sup>h</sup> 10<sup>m</sup> 2<sup>s</sup>; Decl. —19° 46'

17.343	259.0	12.45	11.8	2½	370
17.351	258.8	12.62	11.2	2	370
17.35	258.9	12.53	(10.4 ... 10.9)		D?

Alvan Clark 5; γ Sextantis; 6.0

A.R. 9<sup>h</sup> 46<sup>m</sup> 34<sup>s</sup>; Decl. —7° 32'

17.340	66.5	0.60	11.2	3	650
17.343	70.0	0.61	12.1	2	650
17.373	67.6	0.67	12.3	2½	650
17.35	68.0	0.63	(5.7 ... 6.0)		B

β 411; —26° 4360; 7.0

A.R. 10<sup>h</sup> 30<sup>m</sup> 25<sup>s</sup>; Decl. —26° 3'

17.340	272.1	0.75	11.6	3	650
17.343	271.8	0.87	12.3	2	650
17.540	271.1	0.68	14.4	3	650
17.41	271.7	0.77	(7.4 ... 8.5)		M

h 4456; —23° 5207; 7.5

A.R. 11<sup>h</sup> 30<sup>m</sup> 46<sup>s</sup>; Decl. —23° 46'

13.277	122.8	17.27	9.5	2	300
			(7.5 ... 11.0)		D?

h 4479; —23° 5311; 8.1

A.R. 11<sup>h</sup> 47<sup>m</sup> 15<sup>s</sup>; Decl. —23° 55'

13.277	91.3	7.37	9.8	3	300
			(9.2 ... 9.8)		F

Hu 1489; Véase la nota. See note 152

h 4549; —23° 5599; 9.4:

A.R. 12<sup>h</sup> 39<sup>m</sup> 34<sup>s</sup>; Decl. —23° 46'

13.258	116.6	12.71	10.4	3	300
13.277	116.4	12.59	10.8	3	300
13.27	116.5	12.65	(9.5 ... 10.2)		N

*h* 4551;  $-24^{\circ} 4920$ ; 8.8:

A.R.  $12^{\text{h}} 41^{\text{m}} 50^{\text{s}}$ ; Decl.  $-24^{\circ} 9'$

13.258	313.0	12.44	10.3	3	300
13.277	313.9	12.44	10.8	3	300
13.27	313.5	12.44	(8.9 ... 9.5)		N

Hu 1502;  $-25^{\circ} 5153$ ; 8.8

A.R.  $13^{\text{h}} 13^{\text{m}} 8^{\text{s}}$ ; Decl.  $-25^{\circ} 15'$

17.542	31.2	1.08	15.8	$2\frac{1}{2}$	370
			(9.2 ... 9.7)		A

*h* 2655;  $-22^{\circ} 5613$ ; 9.1

A.R.  $13^{\text{h}} 23^{\text{m}} 52^{\text{s}}$ ; Decl.  $-22^{\circ} 52'$

13.258	273.6	14.16	11.3	$2\frac{1}{2}$	300
			(9.0 ... 10.2)		N

*h* 4606;  $-22^{\circ} 5641$ ; 6.9

A.R.  $13^{\text{h}} 34^{\text{m}} 53^{\text{s}}$ ; Decl.  $-22^{\circ} 50'$

13.258	352.2	31.09	11.4	2	300
			(6.8 ... 9.5)		F

*h* 2671;  $-24^{\circ} 5125$ ; 8.5

A.R.  $13^{\text{h}} 36^{\text{m}} 38^{\text{s}}$ ; Decl.  $-24^{\circ} 22'$

13.258	70.3	27.81	11.8	$2\frac{1}{2}$	300
			(8.8 ... 9.2)		F

Hough 383;  $-22^{\circ} 5659$ ; 8.8

A.R.  $13^{\text{h}} 40^{\text{m}} 33^{\text{s}}$ ; Decl.  $-22^{\circ} 52'$

13.258	166.3	16.20	11.7	2	300
			(8.2 ... 12.0)		D?

Hu 1262;  $-21^{\circ} 5633$ ; 7.1

A.R.  $13^{\text{h}} 47^{\text{m}} 52^{\text{s}}$ ; Decl.  $-21^{\circ} 39'$

17.474	291.2	1.17	16.1	3	650
17.540	293.8	1.03	15.6	3	650
17.51	292.5	1.10	(6.9 ... 11.5)		D

$\Sigma$  1788; SD  $-7^{\circ} 3728$ ; 6.0

A.R.  $13^{\text{h}} 48^{\text{m}} 41^{\text{s}}$ ; Decl.  $-7^{\circ} 28'$

17.343	82.2	3.16	12.8	2	370
17.474	83.4	3.03	16.6	3	370
17.608	82.6	2.95	18.1	3	650
17.48	82.7	3.05	(6.8 ... 8.1)		P

*h* 4670;  $-25^{\circ} 5392$ ; 8.6

A.R.  $14^{\text{h}} 11^{\text{m}} 30^{\text{s}}$ ; Decl.  $-25^{\circ} 39'$

13.258	23.2	18.11	12.2	3	300
13.277	23.4	18.18	12.0	$2\frac{1}{2}$	300
13.27	23.3	18.14	(9.0 ... 11.2)		F?

Hough 386;  $-22^{\circ} 5772$ ; 8.0

A.R.  $14^{\text{h}} 21^{\text{m}} 36^{\text{s}}$ ; Decl.  $-22^{\circ} 28'$

17.540	325.5	4.43	16.0	$2\frac{1}{2}$	370
17.542	325.6	4.31	16.5	$2\frac{1}{2}$	370
17.54	325.6	4.37	(8.2 ... 12.8)		D?

Morgan; Véase la nota. See note 153

*h* 2723;  $-23^{\circ} 5930$ ; 8.8

A.R.  $14^{\text{h}} 25^{\text{m}} 24^{\text{s}}$ ; Decl.  $-23^{\circ} 30'$

13.277	138.2	27.22	12.2	$2\frac{1}{2}$	300
			(9.0 ... 10.2)		F

*h* 4694; Véase la nota. See note 154

Sh 184; m Hydrae; 5.6

A.R.  $14^{\text{h}} 39^{\text{m}} 4^{\text{s}}$ ; Decl.  $-24^{\circ} 56'$

14.336	127.2	8.90	13.0	3	370
14.394	128.3	8.82	13.1	2	370
14.403	127.4	8.81	17.7	$2\frac{1}{2}$	370
14.38	127.6	8.84	(5.8 ... 7.8)		C

Hu 1511;  $-24^{\circ} 5376$ ; 9.2

A.R.  $14^{\text{h}} 41^{\text{m}} 18^{\text{s}}$ ; Decl.  $-24^{\circ} 7'$

17.540	309.6	1.09	16.2	$2\frac{1}{2}$	650
17.542	313.9	0.91	16.8	$2\frac{1}{2}$	370
17.54	311.8	1.00	(9.8 ... 10.0)		142

Hu 1512;  $-23^{\circ} 5987$ ; 8.6

A.R.  $14^{\text{h}} 42^{\text{m}} 20^{\text{s}}$ ; Decl.  $-23^{\circ} 11'$

17.540	48.8	1.16	16.3	$2\frac{1}{2}$	650
17.542	50.4	1.15	16.9	$2\frac{1}{2}$	370
17.54	49.6	1.16	(9.2 ... 9.3)		142

Hu 1271; SD  $-18^{\circ} 3920$ ; 8.8

A.R.  $14^{\text{h}} 45^{\text{m}} 34^{\text{s}}$ ; Decl.  $-18^{\circ} 56'$

17.343	42.6	0.88	13.2	2	650
17.474	40.6	0.77	16.3	3	650
17.540	38.6	0.98	16.5	2	650
17.45	40.6	0.88	(8.8 ... 10.5)		

*h* 4716;  $-24^{\circ} 5406$ ; 9.1

A.R.  $14^{\text{h}} 49^{\text{m}} 22^{\text{s}}$ ; Decl.  $-24^{\circ} 11'$

13.258	358.9	3.18	12.8	3	300
13.277	359.1	3.09	12.8	3	300
13.27	359.0	3.14	(9.6 ... 10.0)		F

$\beta$  239;  $-27^\circ 50'2''$ ; 6.4A.R.  $14^h 51^m 33^s$ ; Decl.  $-27^\circ 10'$ 

14.394	321.8	0.81	13.3	$2\frac{1}{2}$	650
14.399	319.8	0.91	13.5	3	650
14.421	323.5	0.89	13.3	3	650
14.40	321.7	0.87	(6.2 ... 6.4)		P

Fox 16;  $-19^\circ 56'8''$ ; 9.4A.R.  $14^h 55^m 33^s$ ; Decl.  $-19^\circ 5'$ 

17.343	234.4	49.68	13.4	2	370
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BC

17.343	106.9	1.74	13.5	2	370
17.540	108.6	1.88	16.6	2	370
17.543	111.6	1.82	17.2	$2\frac{1}{2}$	370
17.48	109.0	1.81	(11.0 ... 11.6)		155

Hu 1515;  $-24^\circ 55'01''$ ; 8.4A.R.  $15^h 13^m 10^s$ ; Decl.  $-24^\circ 32'$ 

17.540	153.5	1.99	16.8	$2\frac{1}{2}$	370
			(9.0 ... 12.5)		142

Hu 1516;  $-22^\circ 60'64''$ ; 8.8A.R.  $15^h 37^m 18^s$ ; Decl.  $-22^\circ 57'$ 

17.540	246.3	1.65	16.9	3	650
17.543	243.3	1.46	17.5	3	370
17.54	244.8	1.56	(8.9 ... 11.6)		142

Hu 1274;  $-19^\circ 59'26''$ ; 6.0A.R.  $15^h 48^m 4^s$ ; Decl.  $-19^\circ 2'$ 

17.540	110±	$\frac{1}{4}$ ±	(6.5 ... 7.5)		A?
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Burg;  $\alpha$  Scorpii; 4.2A.R.  $16^h 22^m 3^s$ ; Decl.  $-26^\circ 10'$ 

13.438	272.0	3.51	15.5	2	300
13.474	275.2	3.35	15.6	4	666
13.507	275.2	3.40	14.5	3	666
14.348	274.9	3.20	14.8	$2\frac{1}{2}$	650
14.399	272.7	2.98	13.8	3	650
13.83	274.0	3.29	(1.0 ... 6.5)		C

h 1294;  $-24^\circ 57'45''$ ; 8.3A.R.  $16^h 40^m 56^s$ ; Decl.  $-24^\circ 19'$ 

13.277	131.6	25.16	14.3	$2\frac{1}{2}$	300
			(7.5 ... 12.5)		F

h 4891;  $-24^\circ 57'59''$ ; 10.0A.R.  $16^h 45^m 6^s$ ; Decl.  $-24^\circ 30'$ 

13.277	311.5	10.97	14.4	3	300
			(10.0 ... 10.2)		F

Argelander 78; Véase la nota. See note 156

Doolittle; SD  $-18^\circ 44'21''$ ; 9.0A.R.  $17^h 1^m 8^s$ ; Decl.  $-18^\circ 17'$ 

17.299	188.3	3.32	17.3	$3\frac{1}{2}$	650
17.302	189.4	3.19	16.4	2	370
17.474	187.9	3.08	17.2	3	370
17.540	187.7	3.24	17.4	3	650
17.40	188.3	3.21	(9.5 ... 10.5)		

Hu 1280;  $-19^\circ 61'23''$ ; 8.6A.R.  $17^h 1^m 12^s$ ; Decl.  $-19^\circ 38'$ 

17.299	355.0	—	17.2	4	650
17.608	353.5	0.30	18.5	$3\frac{1}{2}$	1125
17.45	354.3	0.30	(9.8 ... 9.9)		A

AB,C; C = 10.8

17.299	3.1	8.68	17.0	4	370 F
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Hu 1522;  $-25^\circ 59'47''$ ; 8.8A.R.  $17^h 4^m 6^s$ ; Decl.  $-25^\circ 10'$ 

17.543	91.0	1.20	18.2	3	650
17.789	94.7	1.09	21.0	$2\frac{1}{2}$	370
17.67	92.8	1.15	(9.6 ... 10.0)		142

A 2238; SD  $-18^\circ 44'62''$ ; 9.4A.R.  $17^h 7^m 23^s$ ; Decl.  $-18^\circ 52'$ 

17.299	195.3	0.73	17.4	$3\frac{1}{2}$	650
17.540	195.5	0.85	17.5	$2\frac{1}{2}$	650
17.608	197.3	0.84	18.9	3	650
17.48	196.0	0.81	(10.4 ... 11.2)		

I 591;  $-19^\circ 61'87''$ ; 8.7A.R.  $17^h 11^m 47^s$ ; Decl.  $-19^\circ 7'$ 

17.543	217.5	1.14	18.6	$2\frac{1}{2}$	650
17.608	216.9	1.11	18.8	3	650
17.789	217.4	1.06	21.1	$2\frac{1}{2}$	370
17.65	217.3	1.10	(9.5 ... 9.6)		

A 2240;  $-19^\circ 61'94''$ ; 8.8A.R.  $17^h 12^m 47^s$ ; Decl.  $-19^\circ 33'$ 

17.299	200.0	1.34	17.6	3	370
17.302	199.6	1.28	16.6	2	370
17.608	200.8	1.44	19.1	$3\frac{1}{2}$	370
17.60	200.1	1.35	(9.3 ... 12.7)		F

A 2241; Véase la nota. See note 152

A 2242; SD  $-17^{\circ} 4792$ ; 9.0

A.R.  $17^{\text{h}} 16^{\text{m}} 9^{\text{s}}$ ; Decl.  $-18^{\circ} 0'$

17.299	289.4	2.98	17.7	3	370
17.302	291.2	2.99	16.8	2	370
17.543	292.2	3.14	18.9	3	370
17.38	290.9	3.04	(8.9 ... 12.2)		

A 2244; Véase la nota. See note 157

A 2250; SD  $-18^{\circ} 4634$ ; 8.5

A.R.  $17^{\text{h}} 37^{\text{m}} 54^{\text{s}}$ ; Decl.  $-18^{\circ} 36'$

17.299	212.8	1.85	17.9	3	370
17.608	214.1	1.71	19.8	3	370
17.45	213.4	1.78	(8.2 ... 13.5)		F

A 2251; SD  $-18^{\circ} 4637$ ; 8.8

A.R.  $17^{\text{h}} 38^{\text{m}} 43^{\text{s}}$ ; Decl.  $-18^{\circ} 29'$

17.299	257.9	2.46	18.0	3½	370
17.302	257.8	2.41	17.2	2	370
17.540	257.0	2.66	17.9	2½	370
17.38	257.6	2.51	(9.5 ... 10.2)		F

Hu 1524;  $-22^{\circ} 6446$ ; 9.0

A.R.  $17^{\text{h}} 40^{\text{m}} 45^{\text{s}}$ ; Decl.  $-22^{\circ} 38'$

17.543	344.6	1.18	19.8	3	370
17.608	346.7	1.21	19.4	3	650
17.789	344.4	1.09	21.4	2½	370
17.65	345.2	1.16	(9.8 ... 9.9)		N

Dawson 30;  $-22^{\circ} 6450$ ; 9.2

A.R.  $17^{\text{h}} 41^{\text{m}} 16^{\text{s}}$ ; Decl.  $-22^{\circ} 35'$

17.543	131.8	0.97	19.6	3	370
17.608	130.2	0.94	19.5	3	650
17.789	132.9	0.98	21.6	2½	370
17.65	131.6	0.96	(10.0 ... 10.1)		

A 2252; SD  $-18^{\circ} 4650$ ; 9.0

A.R.  $17^{\text{h}} 41^{\text{m}} 36^{\text{s}}$ ; Decl.  $-18^{\circ} 51'$

17.299	217.1	3.75	18.1	3½	370
17.540	218.3	3.87	18.1	2½	370
17.543	218.2	[3.44]	19.3	3	370
17.608	216.8	3.83	20.0	3	370
17.50	217.6	3.82	(9.1 ... 12.3)		F

Fox 24;  $-24^{\circ} 6154$ ; 8.4

A.R.  $17^{\text{h}} 56^{\text{m}} 54^{\text{s}}$ ; Decl.  $-24^{\circ} 15'$

17.543	21.5	3.97	20.2	3	370
17.789	21.0	3.88	21.8	2½	370
17.67	21.3	3.93	(9.0 ... 11.2)		A?

SD  $-18^{\circ} 4794$ ; 9.0

A.R.  $18^{\text{h}} 0^{\text{m}} 9^{\text{s}}$ ; Decl.  $-18^{\circ} 55'$

AB = O. Stone

17.540	256.3	18.90	18.5	3	370
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BC = A 2259

17.299	217.2	1.06	18.3	3½	370
17.540	214.7	1.04	18.6	2½	650
17.42	216.0	1.05	(10.0 ... 10.8)		

I 625;  $-18^{\circ} 384$ ; 9.1

A.R.  $18^{\text{h}} 1^{\text{m}} 19^{\text{s}}$ ; Decl.  $-18^{\circ} 57'$

17.299	46.4	1.77	18.4	3½	370
17.540	41.8	1.97	18.8	2½	650
17.42	44.1	1.87	(9.5 ... 10.1)		D

§ 245 = Hd 149;  $-30^{\circ} 5314$ ; 7.4

A.R.  $18^{\text{h}} 2^{\text{m}} 21^{\text{s}}$ ; Decl.  $-30^{\circ} 45'$

14.397	352.4	4.12	16.3	3	370
14.424	352.1	4.18	15.8	3	370
14.438	352.8	4.20	15.1	2	370
14.42	352.4	4.17	(5.6 ... 7.8)		F

Argelander 82; Véase la nota. See note 156

Jonekheere 482; Véase la nota. See note 158

§ 138; SD  $-14^{\circ} 5333$ ; 7.8

A.R.  $19^{\text{h}} 6^{\text{m}} 37^{\text{s}}$ ; Decl.  $-14^{\circ} 39'$

17.540	304.2	1.39	19.8	2½	370
17.608	304.2	1.53	20.7	2½	650
17.57	304.2	1.46	(7.8 ... 11.0)		M

A 2094; SD  $-18^{\circ} 5346$ ; 8.5

A.R.  $19^{\text{h}} 17^{\text{m}} 16^{\text{s}}$ ; Decl.  $-18^{\circ} 1'$

17.540	129.7	2.11	20.5	3	370
17.608	128.1	2.05	20.8	2½	650
17.778	129.3	2.11	22.9	3	370
17.64	129.0	2.09	(8.6 ... 11.5)		

Fox 28;  $-19^{\circ} 7540$ ; 9.4

A.R.  $19^{\text{h}} 29^{\text{m}} 14^{\text{s}}$ ; Decl.  $-19^{\circ} 20'$

17.540	263.9	3.58	20.9	2½	370
17.608	264.2	3.54	21.0	2½	370
17.778	263.5	3.47	23.1	3	370
17.64	263.9	3.53	(9.9 ... 10.7)		142

## Fox 42; Anon.

A.R. 21<sup>h</sup> 11<sup>m</sup> 0<sup>s</sup>; Decl. -21° 49'

17.608	101.2	1.75	21.3	3	650
17.778	102.3	1.74	23.5	3	370
17.789	99.5	1.83	23.0	2½	370
17.76	101.0	1.77	(10.8 ... 11.3)		142

## Hu 1312; -20° 8150; 8.7

A.R. 21<sup>h</sup> 17<sup>m</sup> 27<sup>s</sup>; Decl. -20° 18'

17.608	80.3	2.92	21.5	2½	650
17.778	80.2	2.94	23.7	3½	370
17.789	81.0	2.83	23.2	2½	370
17.76	80.5	2.90	(8.9 ... 9.4)		F

## Hu 1313; SD -18° 5951; 8.9

A.R. 21<sup>h</sup> 24<sup>m</sup> 19<sup>s</sup>; Decl. -18° 12'

17.778	246.2	0.43	0.0	3	650
					(9.7 ... 9.8)

## Fox 45; -23° 8125; 9.1

A.R. 22<sup>h</sup> 7<sup>m</sup> 22<sup>s</sup>; Decl. -23° 44'

17.778	153.6	4.42	0.4	4	370
17.789	153.3	4.41	23.5	2½	370
17.78	153.5	4.42	(9.8 ... 10.9)		142

## AC

17.778	80.3	29.86	0.5	4	370
17.789	81.9	30.08	23.7	2	370
17.78	81.1	29.97	(9.8 ... 10.6)		142

## NOTES

1. In cluster 47 G. Tucanae. There is no pair prominent above the others as in Herschel's Plate III, fig. 1. The place given is that of the cluster.
2. Magnitude estimates, 9.8 ... 12.5, 11.0 ... 12.2. « A » variable?
3. 1916.823, Certainly less than 0"3 if double.
4. Herschel and others make the quadrant south preceding.
5. 1° south of Herschel's place.
6. In field with preceding star.
7. Noted as double at the Gautier meridian circle.
8. Seen by averted vision only. Too faint to measure. 1° south of Herschel's place, but identity certain.
9. Perhaps a mistaken wire in Herschel's R.A.
10. Called Δ 7 by Herschel. Refraction in distance included in the mean.
11. Noted as double in *Uranometría Argentina* (1879).
12. The Decl. of *h* 3525 errs 1°. The following of the two stars is I 386, but seeing was too poor to measure.
13. Herschel's star fixed. Innes' star noted independently. Herschel's place correct.
14. Herschel's place of Δ 10 is erroneous.
15. This was measured by Hargrave in 1879, Fixed.
16. Southern of two, 1' apart. No other measures.
17. Not found. 1" prec. Herschel's place is a 7.3 mag. star, but without companion.

## NOTAS

1. En el cúmulo 47 G Tucanae. No hay pareja sobresaliente como en el dibujo en Results. Las coordenadas son las del cúmulo.
2. Magnitudes apreciadas 9.8 ... 12.5, 11.0 ... 12.2. ¿Es variable la A?
3. 1916.823. Si es doble, distancia seguramente menos de 0"3.
4. Herschel y otros ponen la compañera al sur precedente.
5. 1° al sur de la posición asignada por Herschel.
6. En el mismo campo visual con la estrella anterior.
7. Notada como doble con el círculo meridiano Gautier.
8. Visible solamente con mirada indirecta. Demasiado débil para medir. Estoy seguro de que es la estrella anotada por Herschel, aunque está 1° al sur de la posición asignada por él.
9. Tal vez la A.R. de Herschel tiene error del hilo.
10. Herschel la llama Δ 7. El promedio incluye la refracción en distancia.
11. Anotada como doble en la *Uranometría Argentina*, (1879).
12. La declinación de *h* 3525 tiene error de 1°. La siguiente de las dos estrellas es I 386, pero no la pude medir.
13. La posición dada por Herschel es correcta y su estrella no presenta cambio. Noté la estrella de Innes independientemente.
14. La posición de Δ 10, según Herschel, es errónea.
15. Fue medida por Hargrave en 1879. Fija.
16. La más austral de dos distantes 1'. No hay otras medidas.
17. No he podido encontrar *h* 3590. 1' precediendo la posición dada por Herschel hay una estrella de magnitud 7.3, pero sin compañera.



18. Principal star has been recorded as  $\lambda$  30. Not seen double.
19. R.A. of  $h$  3639 needs  $-5^m$ .
20. Previous measures discordant.
21. Fixed. Some error in Hargrave's measure.
22. No other measures. Hargrave's measure purporting to be of this is of another pair.
23. Picked up independently.
24. Principal star fainter than given by Herschel, and not in C.P.D. Variable?
25. Nebula easily seen with low power,  $333^\circ 62''$  from «A».
26. Measured by mistake for  $h$  3726, which is  $14'$  south,  $59^s$  prec.
27. Lacaille's R.A. is correct.
28. Fixed. Principal star is I 345; suspected independently, but not measurable.
29. The principal «star» is a small round nebula.
30.  $h$  3774 not found. A pair 11.0 and 13.5,  $31^\circ 9'9''$  measured one night. Nothing else within a degree of the place.
31. Place and identification refer to the star mentioned in the original observation.
32.  $-67^\circ 509$  is near and similar to  $h$  3701 and liable to be mistaken for it.
33. Principal star is Hu 1415.
34. Herschel observed AB, Hargrave, AC, both noting a star south following. My estimates of magnitude are,
- |        |       |        |        |
|--------|-------|--------|--------|
| 17.108 | A 9.5 | B 12.0 | C 11.5 |
| 17.156 | 9.2   | 11.5   | 9.7    |
35. Not found. Probably at R.A.  $6^h 41^m 40^s$  and = Hu 1416.
36. 1875.0 191 $\circ$ 1 130 $\prime$ 1 4 $n$  A.G.C. Probably fixed.
37. «B» variable? Magnitudes 8.2 ... 8.5, 8.5 ... 10.0.
38.  $\Delta$  45 has been measured by Hargrave and Tebbutt for  $h$  3960 and Innes continues this error in I. R. C. But Herschel said «the preceding of two» (cf. Results  $h$  3960). Both pairs fixed.
39. Rus 76 is BC of this triple.
40. Distance AC depends on angle of BC,  $166^\circ 4$ ,  $167^\circ 6$ .
41. Greater R.A. correct.
42. Lesser R.A. correct.
43. Principal star is I 1070 = Hu 1432, not measured.
44.  $12'$  north of Herschel's place.
45. Probably also =  $h$  4042 thru a misidentification of the latter by Herschel.

18. La estrella principal se ha anotado como doble ( $\lambda$  30) pero me pareció simple.
19. La A.R. de  $h$  3639 necesita una corrección de  $5^m$ .
20. Las medidas anteriores son discordantes.
21. Fija. La medida de Hargrave tiene algún error.
22. No hay otras medidas. La de Hargrave notada como de esta estrella es de otra.
23. Fué encontrada independientemente.
24. La estrella principal parece más débil de lo que la estimó Herschel, y no está en la C. P. D. ¿Será variable?
25. La nebulosa es fácil de ver con poco aumento. Está a  $62''$  en  $333^\circ$  de A.
26. Observada en vez de  $h$  3726 que está  $14'$  al sur y  $59^s$  precedente.
27. La A.R. de Lacaille es correcta.
28. Fija. La estrella principal es I 345; la noté independientemente pero no la pude medir.
29. La «estrella» principal es una pequeña nebulosa redonda.
30. No he podido encontrar  $h$  3774. La única pareja dentro de  $1^\circ$  de la posición es 11.0 y 13.5,  $31^\circ 9'9''$ .
31. La posición y la identificación son de la estrella mencionada en la observación original.
32.  $-67^\circ 509$  es semejante a  $h$  3701 y está tan cerca que habría caso de confundirlas.
33. La estrella principal es Hu 1415.
34. Herschel observó AB y Hargrave observó AC, ambos notaron una estrella al sur siguiente. Mis apreciaciones de magnitud son:
- |        |       |        |         |
|--------|-------|--------|---------|
| 17.108 | A 9.5 | B 12.0 | C 11.5, |
| 17.156 | 9.2   | 11.5   | 9.7.    |
35. No la he podido encontrar. Me parece probable que esté en A.R.  $6^h 41^m 40^s$  y que sea entonces igual a Hu 1416.
36. 1875.0 191 $\circ$ 1 130 $\prime$ 1 4 $n$ , C. G. A. Probablemente fija.
37. Magnitudes, 8.2 ... 8.5, 8.5 ... 10.0. ¿Variable la B?
38.  $\Delta$  45 ha sido medida por Hargrave y por Tebbutt en vez de  $h$  3960, e Innes mantiene este error en I. R. C. Pero Herschel anotó su 3960 como la *precedente* de las dos y  $\Delta$  45 es la siguiente. Ambas parejas fijas.
39. Rus 76 es BC de esta triple.
40. La distancia de AC depende de observaciones del ángulo de BC;  $166^\circ 4$ ,  $167^\circ 6$ .
41. La A.R. mayor es la correcta.
42. La A.R. menor es la correcta.
43. La estrella principal es I 1070 = Hu 1432.
44. Está  $12'$  al norte de la posición dada por Herschel.
45. Me parece probable que sea también igual a  $h$  4042 por un error en la identificación de ésta por Herschel.

46. 1913.07 220°0 41'02 2n A. J. Chaves. Fixed.  
 47. Measured for *h* 4066. This is 10' south of his place and differs considerably, but may be the star. No other pair near here.  
 48. 1913.07 251°8 33'30 1n A. J. Chaves. Angle decreasing.  
 49. No other measures. See's measure is of a star 7' north.  
 50. Apparently fixed. Herschel's angle needs + 100° and Hargrave's, + 180°.  
 51. 1<sup>m</sup> preceding Herschel's place.  
 52. No other measures. Many other stars in the field, but none near « A ».  
 53. Measured for *h* 4123, whose place is 1<sup>m</sup> following. Nothing in Herschel's place and no likelier pair near.  
 54. Other stars noted are : (single settings).

11.5	75°	75'0
10.5	145	77.2
9.2	166	71.0
10.0	178	38.6
9.5	178	75.4
9.8	247	33.9
10.5	268	83.8
8.8	268	55.2
10.2	339	98.4

55. Herschel's R.A. of *h* 4142 needs -6<sup>m</sup>. Some change in angle.  
 56. Herschel corrects his R.A. in the errata, Results, p. 452B. First distance of AC is deduced from a measure of the angle BC.  
 57. HdA. star not seen either night.  
 58. No other measures. 2' south is a pair 11.8 + 13.0, 270° 3'3.  
 59. AB, 1913.09 258°3 13'40 3n A. J. Chaves.  
 60. No other measures except 1913.15 134°0 3'06 2n Hu.  
 61. No other measures. A 9.2 mag. star in 199° 49'.  
 62. This is the star measured by Herschel. Probably 2 rev. error in each of Dunlop's measures.  
 63. See measures this star and calls it Jacob 121, whereas Jacob 121 = *h* 4220.  
 64. Magnitudes 10.5 ... 12.0. Nothing else near place of *h* 4243.  
 65. 1913.15 249°9 18'57 1n A. J. Chaves.  
 66. 1882.35, 83.1, 5.40 1n Hargrave.  
 67. *h* 4252 is not  $\nu$  Argûs, but a pair (= Gilliss 117) south following it, as is shown by Herschel's place and description.  $\nu$  Argûs itself is Rû 11 (= Gilliss 116), but has been called *h* 4252 by practically all observers since Herschel.

46. 1913.07 220°0 41'02 2n, A. J. Chaves. Fija.  
 47. Medida por *h* 4066. Esta está 10' al sur de su posición y no corresponde a su descripción, pero no hay otra pareja en la región.  
 48. 1913.07 251°8 33'30 1n, A. J. Chaves. Ángulo disminuyendo.  
 49. No hay otras medidas. La medida de See es de alguna otra.  
 50. Parece fija. El ángulo de Herschel necesita + 100° y el de Hargrave, + 180°.  
 51. 1<sup>m</sup> precedente de la posición de Herschel.  
 52. No hay otras medidas. Muchas otras estrellas alrededor, pero ninguna cerca de A.  
 53. Medida como *h* 4123, cuya posición está 1<sup>m</sup> siguiente. Nada en la posición misma y nada más probable alrededor.  
 54. Otras estrellas alrededor son :

11.5	75°	75'0
10.5	145	77.2
9.2	166	71.0
10.0	178	38.6
9.5	178	75.4
9.8	247	33.9
10.5	268	83.8
8.8	268	55.2
10.2	339	98.4

55. La A.R. de *h* 4142 necesita una corrección de - 6<sup>m</sup>. El ángulo ha cambiado algo.  
 56. En sus Erratas (Results, página 452B), Herschel da una corrección para la A.R. La primera distancia AC depende de una medida del ángulo BC.  
 57. No pude ver la compañera HdA. en ninguna de las noches.  
 58. No hay otras medidas. 2' al sur hay una pareja 11.8 y 13.0, 270° 3'3.  
 59. AB, 1913.09 258°3 13'40 3n, A. J. Chaves.  
 60. Las únicas medidas anteriores son : 1913.15 134°0 3'06 2n, Hu.  
 61. No hay otras medidas. Una estrella de mag. 9.2 está a 49' en 199°.  
 62. Esta es la estrella que midió Herschel. Probablemente hay 2 rev. de error en ambas medidas de Dunlop.  
 63. See midió ésta y la llamó Jacob 121, mientras Jacob 121 = *h* 4220.  
 64. Magnitudes 10.5 ... 12.0. La única cerca de la posición de *h* 4243.  
 65. 1913.15 249°9 18'57 1n, A. J. Chaves.  
 66. 1882.35 83.1 5.40 1n, Hargrave.  
 67. *h* 4252 no es  $\nu$  Argûs sino una pareja al sud siguiente de ella, como muestran la posición y la descripción de Herschel.  $\nu$  Argûs es Rû 11, pero casi todos los observadores después de Herschel la han llamado *h* 4252.

68. 1913.09 120°1 13"16 1n P. T. Delavan.  
 69. Hargrave's measure purporting to be of this is really of Rii 12.  
 70. Many other faint pairs near, some of them somewhat less wide.  
 71. 1913.07 162°7 40"70 2n A. J. Chaves.  
 72. 1° north of Herschel's place.  
 73. Measured by See in 1897. (M. N. R. A. S. lvii, 541).  
 74. *h* 4358 and *h* 4359 are so mixed in the lists of Herschel and others that choice of numbers is difficult. I have used them in the order of the R.A.'s. in the C. G. A. (page 627).  
 75. The famous variable; estimated magnitude 7.9. Innes' closer stars not looked for. Some change in these wide ones.  
 76. Adjusted means, using all the measures.  
 77. No other measures. A 12 mag. star measured:  
                   1913.077    133°8    10"85  
 78. CB from these measures is 105° 3"5.  
 79. 1875.3 13°2 63"7; 200°7 153"6, 5n A. G. C.  
 79a. Noticed as double by Aguilar. Hussey's identification erroneous.  
 80. No other measures. A 13 mag. star in 343° 18".  
 81. 278° 160" from —59° 2923.  
 82. Magnitude estimates 9.8 ... 11.8, 11.2 ... 12.0. « A » variable?  
 83. Herschel's R.A. of 4458 needs — 4<sup>m</sup>. No other measures.  
 84. This agrees with Herschel's place, but not with his description.  
 85. Rus 175 and Rus 176 are in Russell's diagram, Plate IV, and are mentioned in connection with *h* 4475. The measure of 1881.6 by Hargrave set down to *h* 4475 (Sydney edition) is of *h* 4468 and the star measured by Russell for *h* 4475 (Sydney edition) is set down as Rus 176 in the Mem. R. A. S. edition. This was remeasured by Hargrave and Innes, but is also not Herschel's star. Innes and I have concurred in calling it Rus 176a. *h* 4475 has no other measures but is probably fixed.  
 86. This has never been seen sharply defined and may be nebulous.  
 87. Refraction in AB, 0"09, in AC, 0"07, not applied. The close star suspected by See was not seen. Other faint stars were noted as follows:

11.5	14°	76"7
11.0	117	117.8
9.5	159	188.2
12.5	159	92.4
12.0	294	99.6

11.5	14°	76"7
11.0	117	117.8
9.5	159	188.2
12.5	159	92.4
12.0	294	99.6

88. 1<sup>m</sup> following Herschel's place.  
 88a. A faint companion recorded as  $\lambda$  159 was not seen.  
 89. 1914.347 « Certainly less than 0".2 if double »; many other times noted as single. It seems quite probable that the star really observed by Herschel is the one rediscovered as Sellors 18.  
 90. No other measures; D not seen by Herschel. C and D are variable.  
 91. 1913.07 67°9 3"16 1n A. J. Chaves. Fixed.  
 92. Herschel's angle should probably be 324"0. The star measured by Hargrave is closely south following, but very faint.  
 93. No star in Herschel's place of 4646. Dawson 15 is in this same group.  
 94. C. P. D. printed mag. (9.6) corrected in vol. III.  
 95. A measure of this is called  $h$  5444 on pp. 258 and 280 of Results.  
 96. Called triple within 30" by HdA., but nothing closer noticed.  
 97. Original record probably erroneous, 4 for 40.  
 98. 10' south of Herschel's place.  
 99. Fixed. Dunlop's place has an error of 1°.  
 100. Herschel's angle should probably be 253°3. No other measures.  
 101. There is no star in or near Herschel's place of 4739. It is barely possible that, by a mistake of 2°,  $\Delta$  178 =  $h$  4739. Dunlop's measures are inconsistent but indicate some change.  
 102. Cf. note in Union Obs. Circular 4, page 35. I also cannot find See's star.  
 103. Additional stars noted (letters correspond to Russell's):

$e$	11.8	44°	25"
$f$	11.8	41	31
$g$	12.3	352	31
$h$	12.4	341	47
$i$	12.4	332	74
$j$	12.6	54	66
$k$	11.1	255	68
—	13.6	267	30

104. Herschel's place agrees exactly with that of the star answering Russell's description.  
 105. The identification of Hargrave 113 in I. R. C. was erroneous, and tho later corrected by Innes, he had already also recorded the star as Cape 44.  
 106. Another companion recorded as I 372 was not seen.  
 107. Magnitude estimates 12.2 ... 11.8, 10.8 ... 11.0, 9.8 ... 10.5. One or both variable?  
 108. Principal star is  $\lambda$  258 and was seen elongated but not measurable.

88. 1<sup>m</sup> siguiente de la posición de Herschel.  
 88a. No he visto la pequeña compañera notada como  $\lambda$  159.  
 89. 1914.347. Si es doble, distancia seguramente menos de 0".2; notada varias veces como simple. Parece bien probable que la estrella que realmente observó Herschel sea la que se conoce como Sellors 18.  
 90. No hay otras medidas. Herschel no vió la D. La C y la D son variables.  
 91. 1913.07. 67°9 3"16 1n, A. J. Chaves. Fija.  
 92. Parece que el ángulo dado por Herschel debe ser 324"0. La estrella medida por Hargrave está cerca al sur siguiente, pero es muy débil.  
 93. No hay estrella en la posición de Herschel para su 4646. Dawson 15 está en este mismo grupo.  
 94. La magnitud (9.6) impresa en la C. P. D. se corrige en el tomo III de la misma obra.  
 95. Una medida de ésta está publicada como de  $h$  5444 en páginas 258 y 280 de Results.  
 96. Los de HdA notaron « dos ó más compañeras dentro de 30" » pero no he visto compañera más cerca que ésta.  
 97. Parece que la observación original debe leerse 40 en vez de 4.  
 98. 10' al sur de la posición de Herschel.  
 99. Fija. La posición de Dunlop tiene un error de 1°.  
 100. No hay otras medidas, pero parece que el ángulo de Herschel debe ser 253°3.  
 101. No hay estrella ni en la posición de  $h$  4739 ni alrededor. Es apenas posible que por un error de 2° sea igual a  $\Delta$  178. Las medidas de Dunlop no están de acuerdo entre sí, pero indican algún cambio.  
 102. Véase la nota en Unión Obs. Circular 4, página 35. Yo tampoco encuentro la estrella de See.  
 103. Estrellas adicionales (las letras son las de Russell):

$e$	11.8	44°	25"
$f$	11.8	41	31
$g$	12.3	352	31
$h$	12.4	341	47
$i$	12.4	332	74
$j$	12.6	54	66
$k$	11.1	255	68
—	13.6	267	30

104. La posición de Herschel coincide con la de la estrella que corresponde a la descripción de Russell.  
 105. La identificación de Hargrave 113 en I. R. C. fué errónea, y aunque Innes la corrigió después, ya había vuelto á notar la estrella como Cape 44.  
 106. Otra compañera notada como I 372 no fué vista.  
 107. Magnitudes apreciadas, 12.2 ... 11.8, 10.8 ... 11.0, 9.8 ... 10.5  $\frac{1}{2}$  Son variables las dos o una de ellas?  
 108. La estrella principal es  $\lambda$  258 y pareció alargada, pero no se pudo medir.

109. Herschel has difference of magnitude 1.5. This with redness suggests variability.
110. In field with  $h$  4829. Mean of two careful estimates, the seeing being too poor for a measure.
111. Used as a comparison star with (704) Interamnia.
112. This is perhaps the star measured by Russell for  $h$  4854.
113. No other measures. A 9.2 mag. star is 2' north preceding, and north of that a faint pair.
114. 1836.39 173°9 — 1n Herschel. No measures of distance.
115. Some change in angle. Larger star very red and C. P. D. star may be the companion.
116. Other stars noted :

C	9.8	204°	60"6	
D	10.2	152	28.2	
E	10.3	256	41.9	
F	11.0	243	13.4	
G	13.0	158	10	from F.
H	13.5	228	7	from F.

117. At R.A. 17<sup>h</sup> 19<sup>m</sup> 37<sup>s</sup>; Decl. —58° 51' is a small pair, largest of several, none of which are worth measuring. Nothing at all in Herschel's place which is 1<sup>m</sup> following.
118. Cannot find anything in any part of the cluster answering Herschel's description of 4968.
119. Herschel's R.A. of 4973 is 1<sup>m</sup> large and that of 4989, 10<sup>m</sup> large.
120. I am practically certain that there is no closer companion.
121. The preceding of these stars, called both  $h$  5053 and Rus 309 by Russell, was new. The following of the two was called  $h$  5053 by Hargrave and both  $h$  5056 and Rus 310 by Russell. Herschel's places are both rough, being with the equatorial.
122. This is the star measured by Hargrave for  $h$  5057.
123. Picked up hunting  $h$  5060, which I could not find.
124. A 10.5 mag star is 3' north following and has a companion 13 mag. in 265° 8".
125. Fixed. Herschel's angle needs —100°.
126. Noted with the meridian circle by Aguilar, but had previously been seen by Hussey.
127. Carefully examined each night, but no sign of duplicity.
128. Herschel's angle needs  $\pm$ 180°.
129. Principal star is I 120 and was seen elongated but unmeasurable.

109. Herschel notó magnitud y media de diferencia. Esto con el color rojo hace pensar en variabilidad.
110. En el mismo campo visual con  $h$  4829. Los valores son promedios de dos apreciaciones, porque las condiciones no permitían medidas.
111. Ésta fué usada como estrella de comparación con (704) Interamnia.
112. Ésta puede ser la estrella que midió Russell por  $h$  4854.
113. No hay otras medidas. Una estrella de magnitud 9.2 está 2' norte precedente y más allá una pareja débil.
114. 1836.39 173°9 — 1n, Herschel. No hay medidas de distancia.
115. Algún cambio en el ángulo. La estrella mayor es muy roja y la estrella de la C. P. D. puede ser la compañera.
116. Estrellas adicionales :

C	9.8	204°	60"6	
D	10.2	152	28.2	
E	10.3	256	41.9	
F	11.0	243	13.4	
G	13.0	158	10	desde la F.
H	13.5	228	7	desde la F.

117. En A.R. 17<sup>h</sup>19<sup>m</sup>37<sup>s</sup>; Decl. — 58°51' hay una pequeña pareja, la mayor de varias, ninguna de las cuales vale la pena de medir. No hay nada en la posición de Herschel, 1<sup>m</sup> siguiente.
118. No puedo encontrar pareja que corresponda a la descripción de  $h$  4968 en ninguna parte del cúmulo.
119. La A.R. de Herschel para su 4973 necesita — 1<sup>m</sup> y la para su 4989, — 10<sup>m</sup>.
120. Estoy casi seguro que no hay compañera más cercana.
121. La precedente de estas estrellas fué anotada como  $h$  5053 y también como Rus 309 por Russell, y en realidad era nueva. La siguiente fué anotada como  $h$  5053 por Hargrave y como  $h$  5056 y Rus 310 por Russell, y es la observada por Herschel. Ambas posiciones de Herschel fueron determinadas con su ecuatorial y son meras aproximaciones.
122. Esta es la estrella que midió Hargrave para  $h$  5057.
123. Encontrada en busca de  $h$  5060, que no pude encontrar.
124. Una estrella de magnitud 10.5 esta 3' al norte siguiente y tiene compañera de mag. 13 á 8" en 265°.
125. Fija. El ángulo de Herschel necesita —100°.
126. Notada con el círculo meridiano por Aguilar, pero ya había sido notada por Hussey.
127. La he examinado cuidadosamente cada noche sin notar indicación de duplicidad.
128. El ángulo de Herschel necesita  $\pm$  180°.
129. La estrella principal es I 120 y pareció alargada pero no se pudo medir.

130. Probably fixed, but previous distance measures are very erratic.
131. Herschel mentions « 2 others near » to his 5146; one of them is a small pair.
132. Discovered thru a clerical error. Aguilar communicated this star (which he did not observe) instead of  $-56^{\circ} 9555$ , ( $h$  5223).
133. Distance AC depends on angle BC,  $308^{\circ}1$ , mean of three nights.
134. Apparently fixed with  $10^{\circ}$  error in Russell's measure.
135. Second distance noted « Hardly better than a guess ».
136. Dunlop's companion ( $\Delta$  234) not seen. C was noted by Sellors. Principal star perfectly round.
137. I 1121 was noted independently but not measured.
138. Herschel's angle needs  $-100^{\circ}$  if there be no decided change.
139. No other measures. The Sydney measures credited to this star are of Rii 26.
140. Herschel's angle seems to need  $+100^{\circ}-180^{\circ}$ .
141. No other pair near. Change?
142. The only measures are too recent to warrant comparison.
143. Gilliss 286 is not this star but one  $20'$  south following. This is in Herschel's place but shows considerable change.
144.  $25^s$  preceding Herschel's place.
145.  $h$  4628,  $\zeta$  Centauri. 1913.07 Single 3n.
146. C6. 30, Definitely single, 1917.27.
147. In field with Hu 1385.
148. Hussey's identification erroneous. No other measures.
149. These measures are of A, BC. Seeing would not permit measures of  $BC = \beta$  555.
150. No other measures of distance; angle constant.
151. Could not find Olivier 5 on 3 nights. Two small pairs picked up near Olivier's place.
152. Could not see companion on 3 nights in 1917.
153. 1917.54 Single. 2n.
154. 1913.28 Single. 1n.
155. What I call A, B, C, were called, respectively, C, A, B, by Fox.
156. 1917. Certainly not double in any sense that could have been seen with Argelander's instruments.
157. Could not separate on two good nights in 1917. Less than  $\frac{1}{4}''$  if double.
158. Could not find this star in or near Jonckheere's place.
130. Probablemente fija, pero las medidas anteriores de distancia están en desacuerdo.
131. Herschel menciona dos otras cerca de su 5146; una de ellas es una pareja pequeña.
132. Encontrado por un error de copia. Aguilar me comunicó esta estrella (que no figura en su programa) en vez de  $-56^{\circ} 9555$ .
133. La distancia de AC depende del ángulo BC,  $308^{\circ}1$ , promedio de tres noches.
134. Parece fija con error de  $10^{\circ}$  en la medida de Russell.
135. Noté la segunda distancia como « poco mejor que una estimación ».
136. La compañera de Dunlop ( $\Delta$  234) invisible. C fué notada por Sellors. La estrella principal pareció perfectamente redonda.
137. I 1121 fué notada independientemente pero no medida.
138. El ángulo de Herschel necesita  $-100^{\circ}$  si no hay cambio fuerte.
139. No hay otras medidas. Las en Sydney notadas como de ésta son de Rii 26.
140. El ángulo de Herschel parece necesitar  $+100^{\circ}-180^{\circ}$ .
141. No hay otra pareja cerca. ¿ Ha cambiado ?
142. Las únicas medidas son demasiado recientes para justificar comparación.
143. Gilliss 286 no es esta estrella sino una  $20'$  al sur siguiente. Ésta está en la posición de Herschel, pero pare haber cambiado.
144. Está  $25^s$  precediendo la posición de Herschel.
145.  $h$  4628,  $\zeta$  Centauri. 1913.07. Sin compañera, 3n.
146. C6. 30, 1917.07. Definitivamente simple.
147. En el mismo campo visual con Hu 1385.
148. La identificación de Hussey es errónea. No hay otras medidas.
149. Estas medidas son de A, BC. Condiciones atmosféricas no permitían medidas de  $BC = \beta$  555.
150. No hay otras medidas de distancia; el ángulo es constante.
151. No pude encontrar Olivier 5 en tres noches, pero noté dos parejas pequeñas cerca de su posición.
152. No pude ver la compañera en tres noches en 1917.
153. 1917.54 Simple. 2n.
154. 1913.28. Sin compañera. 1n.
155. Mis A, B, C fueron designadas C, A, B, respectivamente, por Fox.
156. 1917. Seguramente no ha podido ser vista doble con los instrumentos de Argelander.
157. No la pude separar en dos noches buenas de 1917. Distancia menos de  $\frac{1}{4}''$  si es doble.
158. No pude encontrar esta estrella ni en la posición de Jonckheere ni alrededor.

INDEXES ÍNDICES

A. CONSTELLATION NAMED STARS. ESTRELLAS CON LETRA

<p><b>Ara</b></p> <p><math>\alpha</math> 17<sup>h</sup> 22<sup>m</sup> 11<sup>s</sup>  <math>\gamma</math> 17 14 54  <math>\delta</math> 17 19 49</p> <p><b>Argo</b></p> <p><math>\gamma</math> 8 5 40  <math>\delta</math> 8 41 17  <math>\eta</math> 10 40 13  <math>\sigma</math> 7 25 16  <math>\nu</math> Note 67  <math>\psi</math> 9 25 47</p> <p><b>Carina</b></p> <p><math>C</math> 8 13 22  <math>b^1</math> 8 53 55  <math>c</math> 8 52 12  <math>t^2</math> 10 34 0  <math>u</math> 10 48 24  <math>y</math> 11 7 12</p> <p><b>Centaurus</b></p> <p><math>\alpha</math> 14 30 59  <math>\gamma</math> 12 34 38  <math>\delta</math> 12 1 53  <math>\xi</math> Note 145  <math>\xi^2</math> 12 59 38  <math>\sigma^1</math> 11 26 0  <math>D</math> 12 7 31  <math>Q</math> 13 33 45  <math>f</math> 12 59 3</p> <p><b>Circinus</b></p> <p><math>\gamma</math> 15 13 24</p> <p><b>Corona Austr.</b></p> <p><math>\gamma</math> 18 57 58</p>	<p><b>Corona Austr.</b></p> <p><math>\alpha</math> 18<sup>h</sup> 24<sup>m</sup> 46<sup>s</sup></p> <p><b>Crux</b></p> <p><math>\alpha</math> 12 19 38  <math>\gamma</math> 12 24 14  <math>\mu</math> 12 47 16</p> <p><b>Dorado</b></p> <p><math>\alpha</math> 4 31 19</p> <p><b>Eridanus</b></p> <p><math>\varphi</math> 2 12 2  <math>\chi</math> 1 51 7  <math>p</math> 1 35 4</p> <p><b>Grus</b></p> <p><math>\eta</math> 22 37 57  <math>\theta</math> 22 59 49  <math>\psi</math> 23 16 49</p> <p><b>Hydra</b></p> <p><math>m</math> *14 39 4</p> <p><b>Indus</b></p> <p><math>\alpha</math> 20 28 47  <math>\theta</math> 21 10 57</p> <p><b>Lupus</b></p> <p><math>\gamma</math> 15 26 49  <math>\varepsilon</math> 15 14 12  <math>\zeta</math> 15 3 19  <math>\alpha</math> 15 3 14  <math>\mu</math> 15 9 50  <math>\pi</math> 14 56 38</p>	<p><b>Lupus</b></p> <p><math>\tau^1</math> 14<sup>h</sup> 18<sup>m</sup> 8<sup>s</sup>  <math>a</math> 14 29 10  <math>b</math> 14 38 18  <math>d</math> 15 27 17</p> <p><b>Musca</b></p> <p><math>\beta</math> 12 38 38</p> <p><b>Norma</b></p> <p><math>\gamma^2</math> 16 10 30  <math>\varepsilon</math> 16 18 1  <math>\iota^1</math> 15 53 23</p> <p><b>Orion</b></p> <p><math>\beta</math> *5 8 47</p> <p><b>Pavo</b></p> <p><math>\alpha</math> 18 28 25  <math>\lambda</math> 18 40 37</p> <p><b>Phoenix</b></p> <p><math>\beta</math> 1 0 30  <math>\zeta</math> 1 3 8  <math>\eta</math> 0 37 42  <math>\theta</math> 23 32 46  <math>\xi</math> 0 36 4</p> <p><b>Pictor.</b></p> <p><math>\theta</math> 5 21 56  <math>\iota</math> 4 48 9  <math>\mu</math> 6 30 6</p> <p><b>Puppis</b></p> <p><math>L^2</math> 7 9 44  <math>P</math> 7 45 26</p>	<p><b>Reticulum</b></p> <p><math>\alpha</math> 4<sup>h</sup> 12<sup>m</sup> 48<sup>s</sup>  <math>\theta</math> 4 16 17  <math>\alpha</math> 3 27 12</p> <p><b>Sagittarius</b></p> <p><math>\beta^1</math> 19 13 40  <math>\alpha^1</math> 20 13 59</p> <p><b>Scorpius</b></p> <p><math>\alpha</math> *16 22 3</p> <p><b>Sextans</b></p> <p><math>\gamma</math> *9 46 34</p> <p><b>Tucana</b></p> <p><math>\beta</math> 0 25 49  <math>\delta</math> 22 18 25  <math>\alpha</math> 1 11 31  <math>\lambda</math> 0 47 40</p> <p><b>Vela</b></p> <p><math>\Delta</math> 8 25 8  <math>J</math> 10 16 17  <math>\Gamma</math> 10 26 30  <math>b</math> 8 36 29  <math>d</math> 8 39 57  <math>t</math> 10 27 41  <math>u</math> 9 45 6  <math>z</math> 9 9 45</p> <p><b>Volans</b></p> <p><math>\gamma</math> 7 9 46  <math>\zeta</math> 7 43 20  <math>\iota</math> 8 23 9  <math>\theta</math> 8 38 35</p>
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NOTE. — The asterisk indicates that the corresponding star is in the second list, pp. 109-114.

NOTA. — El asterisco indica que la estrella correspondiente se encuentra en la segunda lista, páginas 109 a 114.

## B. STARS OF OBSERVERS OTHER THAN HERSCHEL

## ESTRELLAS DE OTROS OBSERVADORES

Aguilar	$\beta$ = Burnham	Có. = Córdoba	$\Delta$ = Dunlop
1 0 <sup>h</sup> 51 <sup>m</sup> 10 <sup>s</sup>	751 22 <sup>h</sup> 59 <sup>m</sup> 49 <sup>s</sup>	— 11 <sup>h</sup> 48 <sup>m</sup> 43 <sup>s</sup>	1 0 <sup>h</sup> 25 <sup>m</sup> 49 <sup>s</sup>
2 3 12 30	767 21 18 59	— 12 53 58	2 0 47 40
3 7 30 49		— 13 50 36	4 1 33 58
4 8 11 11	Cape	— 17 11 58	5 1 35 4
5 8 11 30			6 2 12 2
6 8 41 58	13 12 53 8		7 2 36 20
7 9 6 28	16 15 19 40	Cruis	10 3 0 38
8 9 31 2	18 17 46 48		12 3 13 12
9 10 19 51	20 7 44 3	140 22 37 57	14 3 35 41
10 10 57 56	23 6 11 10		18 4 48 9
11 13 35 39	24 17 39 26	$\delta$ = Dawson	20 5 21 56
	25 23 40 8		21 5 26 44
A = Aitken	32 13 18 30	1 2 24 15	22 5 27 17
	44 15 8 12	2 4 40 32	26 6 11 53
2094 *19 17 16		3 4 45 34	27 6 14 34
2238 *17 7 23	A. C. = Alvan Clark	4 7 23 33	34 6 41 40
2240 *17 12 47		5 10 32 40	38 7 0 8
2241 Note 152	5 * 9 46 34	6 10 39 13	40 7 6 50
2242 *17 16 9		7 10 39 28	42 7 9 46
2244 Note 157	Copeland	8 10 39 34	45 7 17 55
2250 *17 37 54		9 10 42 24	51 7 25 16
2251 *17 38 43	— 9 25 47	10 10 43 29	55 7 40 51
2252 *17 41 36	— 15 14 12	11 10 59 59	57 7 43 20
2259 *18 0 9		12 11 41 52	60 7 58 21
	Có. = Córdoba	13 12 50 14	62 8 2 55
Argelander		14 13 50 36	63 8 5 34
78 Note 156	29 12 57 52	15 13 59 36	65 8 5 40
82 Note 156	30 Note 146	16 14 43 47	73 8 52 41
	32 13 57 23	17 15 15 9	74 8 53 55
	39 15 4 46	18 15 56 48	76 9 23 55
Brisbane	44 16 3 20	19 15 59 23	77 9 24 37
1973 8 14 48	45 16 16 1	20 16 54 30	79 9 29 12
2018 8 20 10	46 16 31 29	21 18 1 54	80 9 40 29
2168 8 38 50	47 16 41 3	22 18 39 45	83 9 57 35
3190 10 39 18	48 16 53 17	23 18 46 39	85 10 24 30
3194 10 39 45	49 16 53 42	24 19 40 40	94 10 34 0
3574 11 19 15	52 18 52 37	25 19 48 7	95 10 34 24
3594 11 22 34	57 20 12 0	26 19 57 1	98 10 40 13
4042 12 18 0	62 22 5 5	27 23 28 39	99 10 40 34
4839 14 7 48	64 22 56 49	28 23 36 26	102 10 48 24
5613 16 1 34	67 23 38 9	29 * 7 45 30	103 10 48 24
6021 17 9 35	72 13 3 56	30 *17 41 16	105 10 59 45
7080 21 40 8	77 8 28 34		122 12 19 38
	— 2 34 41	Delavan	123 12 19 38
	— 7 44 9		124 12 24 14
	— 7 57 57	1 4 6 27	126 12 47 16
	— 9 23 29	2 6 11 49	127 12 52 26
Antares *16 22 3	— 9 46 12	3 9 3 47	128 12 59 38
	— 10 25 56	4 12 6 11	141 13 33 45
$\beta$ = Burnham	— 10 35 48	5 13 9 32	144 13 41 50
138 *19 6 37	— 10 39 4	6 14 31 30	150 13 48 53
239 *14 51 33	— 10 40 22		151 13 49 0
245 *18 2 21	— 10 42 21	Doo = Doolittle	155 13 59 26
411 *10 30 25	— 10 42 24		159 14 13 41
746 4 27 2	— 10 49 47	— *17 1 8	160 14 18 8
	— 11 0 14		162 14 35 42





J = Jonckheere	Pollock	Rus = Russell	Sellers
482 Note 158	— 1 <sup>h</sup> 33 <sup>m</sup> 26 <sup>s</sup>	140 10 <sup>h</sup> 14 <sup>m</sup> 26 <sup>s</sup>	1 1 <sup>h</sup> 0 <sup>m</sup> 30 <sup>s</sup>
Lacaille	— 14 3 1	146 10 21 34	8 8 28 37
— 3 <sup>h</sup> 59 <sup>m</sup> 45 <sup>s</sup>	$\rho$ = Roe	153 10 34 14	11 15 44 19
$\lambda$ = Lowell Obs.	26 * 7 8 59	155 10 41 24	12 16 30 42
24 3 20 24	Rü = Rümker	156 10 41 20	18 13 15 27
30 Note 18	1 0 47 40	161 10 44 27	19 13 59 37
93 7 54 39	2 1 3 8	165 11 7 19	20 15 13 58
112 9 23 55	3 4 16 17	171 11 19 45	21 16 31 50
122 10 37 25	4 4 21 46	172 11 23 32	23 7 16 59
123 10 39 10	6 7 17 20	173 11 31 25	25 3 8 2
159 Note 88a	8 8 13 22	175 11 35 30	27 22 56 59
209 14 32 9	9 8 42 7	176 11 35 36	
234 15 19 21	11 Note 67	176a 11 42 38	Sh=South and Herschel
239 15 25 44	12 Note 69	177 11 39 26	184 *14 39 4
254 15 52 16	13 10 16 17	199 12 20 3	Ormond Stone
258 Note 108	14 12 7 31	204 12 31 12	41 *18 0 9
345 17 54 0	15 12 19 38	206 12 37 10	$\Sigma$ = W. Struve
477 22 39 20	19 14 13 41	207 12 38 38	668 * 5 8 47
Melbourne	22 17 46 48	208 12 39 54	1788 *13 48 41
1 0 36 19	25 20 4 54	216 13 8 24	N.Z. = Ward.
6 21 18 59	26 20 41 11	218 13 20 45	35 13 7 44
8 16 31 59	27 23 32 46	223 13 29 57	57 15 32 59
Morgan	Rus = Russell	238 13 59 5	Anonymae
— (*14 22)	3 0 22 33	239 13 58 53	— 0 47 13
Note 153	4 0 29 20	244 14 14 29	— 5 3 59
Olivier	12 1 51 18	248 14 27 33	— 5 46 29
1 * 3 46 13	16 2 16 51	259 15 6 3	— 7 31 20
2 * 4 41 4	74 7 17 37	282 16 31 53	— 7 45 25
3 * 4 41 30	75 7 18 56	287 16 50 19	— 8 17 12
4 5 34 34	76 Note 39	288 16 52 54	— 9 37 30
5 Note 151	82 8 13 22	294 17 3 33	— 19 27 30
Pettit	83 8 15 21	297 17 9 35	— 21 49 40
— 9 10 2	107 9 13 9	303 17 34 50	— * 4 56 54
	123 9 29 33	304 17 46 48	— * 7 41 49
	125 9 31 54	309 18 32 10	
	129 9 38 38	310 18 33 0	
		317 18 53 54	
		325 20 42 1	
		327 20 54 55	
		331 21 19 16	
		343 23 11 16	
		344 23 16 49	

C. HERSCHEL STARS OUT OF THE REGULAR ORDER  
ESTRELLAS DE HERSCHEL FUERA DEL ORDEN NUMÉRICO

h1294 *16 <sup>h</sup> 40 <sup>m</sup> 56 <sup>s</sup>	3748 4 <sup>h</sup> 13 <sup>m</sup> 10 <sup>s</sup>	4551 *12 <sup>h</sup> 41 <sup>m</sup> 50 <sup>s</sup>	5294 21 <sup>h</sup> 35 <sup>m</sup> 8 <sup>s</sup>
2655 *13 23 52	4042 Note 45	4606 *13 34 53	5445 14 32 1
2671 *13 36 38	4142 8 37 41	4670 *14 11 30	5447 19 46 25
2723 *14 25 24	4456 *11 30 46	4694 Note 154	5449 23 48 40
3639 4 8 35	4458 11 26 40	4716 *14 49 22	5450 5 11 40
3685 4 40 54	4479 *11 47 15	4891 *16 45 6	5452 9 16 53
3701 5 46 44	4549 *12 39 34	4989 17 35 47	5453 18 5 48

## CONNECTIONS OF CLUSTER STARS

## CONEXIONES DE ESTRELLAS DE CÚMULOS

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The following connections of stars, chiefly in milky way clusters, were made in correlation with and complementary to the work of the Gautier meridian circle in the zones from  $52^{\circ}$  to  $57^{\circ}$  and from  $57^{\circ}$  to  $62^{\circ}$  of south declination. Lists of stars for observation with the equatorial were communicated by the meridian observers, and these stars were then observed differentially, using as points of reference stars already determined by the meridian circle. The instrument used thruout the work has been the 17 inch Gautier equatorial with Warner and Swasey filar micrometer using an eyepiece of 150 power and twelve minute field.

A night's observations began with the determination of parallel at several hour angles in the zone to be observed, followed by the measurement of the difference of declination of several stars, then the difference of right ascension of these stars and others, the difference of declination of these last and yet others and so on successively, taking a minimum of eight settings in each coordinate and recording also the sidereal time at the middle of the group of settings. It was considered advisable to keep the work within five hours of the meridian, and observation was usually stopped on reaching that hour angle, but

Las siguientes conexiones de estrellas, en su mayoría pertenecientes a cúmulos en la vía láctea, fueron hechas para completar el trabajo con el círculo meridiano Gautier en las zonas de  $52^{\circ}$  a  $57^{\circ}$  y de  $57^{\circ}$  a  $62^{\circ}$  de declinación austral. Las estrellas a observar con la ecuatorial me fueron indicadas por los observadores con el círculo meridiano y las observaciones fueron hechas diferencialmente, refiriéndolas a otras estrellas ya determinadas con el círculo meridiano. El instrumento empleado para todo el trabajo ha sido la ecuatorial Gautier de 433 mm. de abertura, con el micrómetro filar Warner and Swasey, usando un ocular que da aumento de ciento cincuenta veces y campo de vista de doce minutos de arco.

Las observaciones de una noche consistían: 1<sup>o</sup>, en la determinación del paralelo en varios ángulos horarios de la zona a observar; 2<sup>o</sup>, la observación de las diferencias de declinación de varias estrellas, seguida por la observación de las diferencias de ascensión recta de éstas y varias otras, las diferencias de declinación de estas últimas y otras, y así sucesivamente, tomando como mínimo ocho lecturas en cada coordenada y anotando también la hora sidérea del medio del grupo de lecturas. (He considerado conveniente observar en ángulos horarios menores de cinco horas, y así generalmente limité las observaciones a esa región.

the few measures made a little beyond have been retained. Checking the parallel and a determination of coincidence with a higher power eyepiece closed the series. Coincidence was sometimes determined at the beginning of the night's work as well.

In the reduction of the observations the reading of coincidence is applied to the means of the settings to obtain the differential coördinates in terms of the screw. These are then multiplied by

$$R = 11''.5786$$

to reduce to arc of a great circle. These apparent coördinates are then differentially reduced to mean place by coefficients computed for each night, and corrected for differential refraction by tables similar to those of Washington (*Publications, Second Series, Vol. IV, App. III, 1905*), but computed for our latitude and methods of observing. The difference of declination thus obtained is reduced to minutes of arc and half of it, with the proper sign, applied to the declination of the comparison star to obtain the middle declination for the formula :

$$\Delta z^s = \frac{1}{15} \Delta \alpha'' \sec \frac{1}{2} (\delta_1 + \delta_2).$$

Mr. L. V. Garbarino assisted in the reductions.

In the zone from  $-57^\circ$  to  $-62^\circ$  each star was observed at least twice, against different comparison stars when possible, on different nights when but one comparison star was available. In many cases several intermediate stars were compared with the same two reference stars, leading to several independent values of the relative position of these latter, which not only gave a check on the observations and reductions, but also supplied material for a discussion of the accuracy of the observations. From a consider-

Las pocas observaciones hechas con ángulo horario un poco mayor no se han desechado); 3°, una comprobación del paralelo, y 4°, una determinación de coincidencia con ocular de mayor aumento. Algunas veces la coincidencia se ha determinado también al principio de la noche.

En la reducción de las observaciones la lectura de coincidencia se aplica al promedio de las lecturas para obtener las coordenadas diferenciales en vueltas del tornillo, las cuales se multiplican por

$$R = 11''.5786$$

para reducir a arco de círculo máximo. Estas coordenadas aparentes se reducen diferencialmente a lugares medios mediante coeficientes calculados para cada noche y se corrigen para la refracción diferencial con tablas semejantes a las de Washington (*Publications, Second Series, Vol. IV, App. III, 1905*) pero calculadas para nuestra latitud y manera de observar. La diferencia de declinación así obtenida se reduce a minutos de arco y la mitad, con su signo correspondiente, se aplica a la declinación de la estrella de comparación para tener la declinación media de la fórmula :

$$\Delta \alpha^s = \frac{1}{15} \Delta \alpha'' \sec \frac{1}{2} (\delta_1 + \delta_2).$$

El señor L. V. Garbarino ha ayudado en las reducciones.

En la zona de  $-57^\circ$  a  $-62^\circ$  cada estrella se observaba dos veces como mínimo, con estrellas distintas de referencia cuando era posible, y cuando no, en dos noches distintas. En muchos casos varias estrellas intermedias se han observado con las mismas dos de referencia, conduciendo así a varios valores de la posición relativa de éstas, lo que no sólo da comprobación de las observaciones y reducciones, sino también suministra material para una investigación de los errores de observación. De una consideración de todos los

ation of all cases in which three or more intermediate stars were observed with the same pair the following mean errors of a simple measure were deduced :

$$\varepsilon_1 \text{ in } \Delta\alpha, \pm 0^{\circ}036; \quad \varepsilon_1 \text{ in } \Delta\delta, \pm 0''26;$$

from which the probable error of the mean of two connections (neglecting the errors of the comparison stars themselves), would be :

$$r_0 \text{ in } \Delta\alpha, \pm 0^{\circ}017; \quad r_0 \text{ in } \Delta\delta, \pm 0''12$$

In the zone from  $-52^{\circ}$  to  $-57^{\circ}$ , in accordance with instructions from Mr. Delavan, some of the stars were left with but a single observation. As there was no other check, these single observations were reduced in duplicate, to insure against errors of reduction.

The data resulting from these connections are presented in the following table. The first two columns give the C. P. D. number and magnitude of the star observed and the third and fourth its approximate place for 1917.0 based on the C. P. D. place. The following group of columns contains, in order; the date in decimals of a year; the estimated visual magnitude; the observed difference of right ascension in revolutions of the screw and with no corrections applied; the hour angle of the observation of  $\Delta\alpha$ ; the difference of declination, similarly uncorrected, and the hour angle of the observation of  $\Delta\delta$ . The last three columns give the corrected differential coördinates reduced to the mean equinox of 1917.0 and the C. P. D. number of the star to which they refer.

casos en que tres o más estrellas intermedias fueron observadas con un mismo par de referencia resultan los siguientes errores medios de una observación simple :

$$\varepsilon_1 \text{ en } \Delta\alpha, \pm 0^{\circ}036; \quad \varepsilon_1 \text{ en } \Delta\delta, \pm 0''26;$$

de donde se deduce el error probable del promedio de dos conexiones (fuera de los errores de las estrellas de referencia)

$$r_0 \text{ en } \Delta\alpha, \pm 0^{\circ}017; \quad r_0 \text{ en } \Delta\delta, \pm 0''12.$$

En la zona de  $-52^{\circ}$  a  $-57^{\circ}$ , conforme con las indicaciones del señor Delavan, algunas de las estrellas se han dejado con una sola observación. Estas observaciones, únicas de sus estrellas, se han reducido en duplicado para evitar errores de cálculo, no habiendo otra comprobación.

Los datos resultantes de estas conexiones están presentados en la tabla siguiente. Las primeras dos columnas dan el número en la C. P. D. de la estrella observada y su magnitud según esta obra; las dos siguientes dan su posición aproximada para 1917.0, a base de la posición de la C. P. D. Las columnas del próximo grupo dan, en orden; la fecha, en fracción decimal del año; la magnitud visual apreciada; la diferencia de ascensión recta observada, en vueltas del tornillo y sin ninguna corrección; el ángulo horario de la observación de  $\Delta\alpha$ ; la diferencia observada de declinación, también sin corrección, y el ángulo horario de la observación de  $\Delta\delta$ . Las últimas tres columnas contienen las coordenadas diferenciales corregidas, reducidas al equinoccio medio de 1917.0, y el número en la C. P. D. de la estrella a que refieren.

# CONEXIONES DE ESTRELLAS

CON EL MICRÓMETRO FILAR DE LA ECUATORIAL GRANDE

C. P. D.		1917		Aparentes						1917.0		* Ref. C. P. D.
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	
- 60° 925	9 <sup>m</sup> .1	7 <sup>h</sup> 53 <sup>m</sup> 58 <sup>s</sup>	- 60° 22' 18"	.167	8 <sup>m</sup> .5	1 <sup>m</sup> 59.2	+ 2 <sup>m</sup> 25 <sup>m</sup>	16 <sup>m</sup> 84.8	+ 2 <sup>m</sup> 17 <sup>m</sup>	+ 2 <sup>m</sup> 48	- 3' 15".1	- 60° 924
				.167	—	43.709	2 46	23.467	3 22	- 68.21	- 4 31.8	60 935
60 930	8.2	54 27	60 14.8	.167	8.2	27.948	2 31	26.838	2 2	+ 43.54	+ 5 10.9	60 924
				.167	—	17.532	2 53	20.169	3 9	- 27.30	+ 3 53.6	60 935
60 933	9.0	54 40	60 18.2	.167	9.2	35.624	2 35	7.165	2 8	+ 55.56	+ 1 23.0	60 924
				.167	—	9.805	3 2	0.553	3 14	- 15.28	+ 0 6.4	60 935
60 939	8.4	54 59	60 34.7	.282	8.6	15.900	4 25	4.186	4 10	- 25.00	+ 0 48.5	60 944
				.285	8.6	38.513	2 15	10.912	1 40	- 60.50	- 2 6.4	60 953
60 942	9.1	55 17	60 33.1	.282	9.0	4.329	4 28	12.119	4 14	- 6.80	+ 2 20.4	60 944
				.285	9.0	26.994	2 18	3.046	1 45	- 42.38	- 0 35.3	60 953
60 945	8.0	7 55 26	60 37.0	.282	8.1	1.434	+ 4 31	8.016	+ 4 21	+ 2.26	- 1 32.8	60 944
				.285	8.3	21.159	2 21	25.141	1 49	- 33.26	- 4 28.1	60 953
60 948	8.7	55 38	60 33.6	.282	8.8	9.015	4 34	9.853	4 17	+ 14.17	+ 1 54.1	60 944
				.285	9.0	13.560	2 24	5.263	1 52	- 21.29	- 1 1.0	60 953
60 949	8.8	55 51	60 39.8	.282	8.7	16.658	4 44	22.727	4 48	+ 26.23	- 4 23.2	60 944
				.285	8.9	21.833	2 44	11.325	2 49	- 34.43	+ 2 11.1	60 967
60 952	8.3	55 58	60 35.1	.282	8.5	21.946	4 39	1.025	4 53	- 34.51	+ 0 11.9	60 944
				.285	8.4	0.682	2 27	14.145	1 55	- 1.07	- 2 43.8	60 953
60 954	9.0	56 7	60 36.8	.285	8.9	5.045	2 31	22.517	2 1	+ 7.93	- 4 20.8	60 953
				.285	9.0	24.753	4 46	18.827	4 39	- 38.91	- 3 38.1	60 979
60 955	8.2	7 56 8	60 24.3	.170	8.8	19.770	+ 0 11	5.288	- 0 3	- 30.90	- 1 1.2	60 976
				.176	—	11.281	- 0 27	16.278	0 43	- 17.65	+ 3 8.5	60 969
60 961	8.2	56 17	60 40.9	.307	—	4.708	+ 2 40	5.403	+ 2 34	- 7.42	+ 1 2.6	60 967
				.307	8.2	22.013	2 42	11.103	2 37	- 34.69	- 2 8.6	60 985
60 964	8.5	56 20	60 24.3	.170	9.0	12.510	0 14	5.145	0 0	- 19.55	- 0 59.6	60 976
				.176	—	4.028	- 0 24	16.401	- 0 38	- 6.30	+ 3 10.0	60 969
60 966	7.8	56 23	60 23.0	.170	7.5	9.736	+ 0 17	1.455	+ 0 4	- 15.21	+ 0 16.7	60 976
				.176	—	1.225	- 0 21	23.006	- 0 34	- 1.92	+ 4 26.5	60 969
60 968	8.2	56 24	60 36.0	.285	8.4	16.016	+ 2 36	18.071	+ 2 5	+ 25.17	- 3 29.3	60 953
				.285	8.7	13.813	4 48	14.415	4 43	- 21.71	- 2 47.0	60 979
60 970	8.4	7 56 26	60 35.3	.285	8.7	17.475	+ 2 38	14.782	+ 2 9	+ 27.46	- 2 51.2	60 953
				.296	8.4	12.434	2 39	11.146	2 14	- 19.54	- 2 9.1	60 979
60 971	8.8	56 26	60 29.7	.285	8.9	0.430	3 38	11.716	3 0	+ 0.67	- 2 15.7	60 969
				.285	8.8	12.054	4 9	18.242	4 24	- 18.92	+ 3 31.3	60 979
60 973	8.6	56 35	60 31.8	.285	8.6	5.456	3 40	22.928	3 30	+ 8.55	- 4 25.5	60 969
				.285	8.7	6.956	4 12	7.121	4 33	- 10.92	+ 1 22.5	60 979
60 974	8.8	56 35	60 30.7	.285	8.8	5.484	3 44	16.812	3 23	+ 8.60	- 3 14.7	60 969
				.285	8.9	6.959	4 15	13.144	4 29	- 10.93	+ 2 32.2	60 979
60 975	8.2	56 36	60 37.1	.296	8.1	6.047	2 41	20.434	2 16	- 9.51	- 3 56.7	60 979
				.296	8.3	9.570	3 7	8.595	3 43	- 15.07	+ 1 39.5	60 985

C. P. D.		1917		Aparentes						1917.0		* Ref.	
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	C. P. D.	
- 60	978	8 <sup>m</sup> 3	7 <sup>h</sup> 56 41	- 60°35'2	.296	7 <sup>m</sup> 9	3R374	+2 <sup>b</sup> 44	10R143	+2 <sup>b</sup> 18	- 5 <sup>s</sup> 29	- 1' 57 <sup>s</sup> 5	-60° 979
					.296	8.1	6.892	3 18	18.907	3 33	- 10.85	+ 3 39.0	60 985
60	980	7.6	56 47	60 35.3	.296	6.2	1.168	2 50	11.298	2 22	+ 1.83	- 2 10.9	60 979
					.296	6.0	2.364	3 14	17.713	3 38	- 3.72	+ 3 25.1	60 985
					.296	6.1	25.872	4 18	1.970	3 53	- 40.69	+ 0 22.8	60 1006
60	981	8.8	56 49	60 38.3	.296	9.0	1.625	3 10	2.508	3 44	- 2.56	+ 0 29.0	60 985
					.296	9.0	25.109	4 20	13.251	3 55	- 39.52	- 2 33.5	60 1006
60	982	7.4	56 51	60 34.4	.296	7.0	3.136	2 53	6.425	2 25	+ 4.93	- 1 14.4	60 979
					.296	6.5	0.417	3 20	22.622	3 30	- 0.66	+ 4 22.0	60 985
					.285	8.9	16.248	+3 50	12.874	+3 5	+ 25.46	- 2 29.1	60 969
					.285	8.8	3.868	4 19	17.089	4 25	+ 6.07	+ 3 17.9	60 979
60	989	8.4	57 2	60 38.8	.296	9.0	7.006	3 25	0.259	3 48	+ 11.04	- 0 3.0	60 985
					.296	9.0	16.463	4 23	15.996	3 58	- 25.91	- 3 5.3	60 1006
60	990	7.8	57 4	60 34.4	.296	7.8	12.260	2 56	6.518	2 28	+ 19.26	- 1 15.5	60 979
					.296	7.9	14.809	4 26	6.725	4 3	- 23.29	+ 1 17.9	60 1006
60	991	8.7	57 6	60 28.1	.285	8.7	25.768	3 54	3.933	3 9	+ 40.36	- 0 45.5	60 969
					.307	8.6	17.368	2 47	25.454	2 50	+ 27.17	- 4 54.8	60 976
60	993	8.0	57 7	60 30.0	.285	8.0	26.599	3 58	13.771	3 18	+ 41.68	- 2 39.5	60 969
					.296	8.0	14.130	2 58	16.210	2 32	+ 22.17	+ 3 7.8	60 979
					.307	8.6	20.249	+3 0	14.748	+3 2	+ 31.57	+ 2 50.8	60 976
60	995	8.5	7 57 10	60 20.5	.307	8.6	25.314	3 45	5.481	3 7	- 39.51	+ 1 3.4	60 1012
					.307	8.6	22.309	2 57	12.393	2 54	+ 34.88	- 2 23.5	60 976
60	1000	8.6	57 18	60 25.7	.315	8.6	23.216	3 2	21.596	3 18	- 36.28	- 4 10.2	60 1012
					.285	7.4	34.608	4 3	5.067	3 13	+ 54.21	- 0 58.6	60 969
60	1003	7.4	57 20	60 28.4	.296	7.2	22.155	3 1	24.891	2 35	+ 34.75	+ 4 48.3	60 979
					.315	7.5	19.303	3 8	35.756	3 13	- 30.19	- 6 54.2	60 1012
					.307	8.8	13.733	3 39	5.100	3 19	- 21.45	- 0 59.1	60 1012
60	1008	8.6	57 29	60 22.5	.307	—	28.355	3 58	—	—	- 44.28	- 1 0—	60 1018
					.321	8.6	28.220	4 3	5.323	3 58	- 44.07	- 1 1.7	60 1018
					.296	9.1	15.843	+4 13	13.343	+4 4	+ 24.93	- 2 34.5	60 1006
60	1013	9.0	7 57 53	60 38.1	.296	—	3.555	4 11	16.391	4 7	- 5.59	- 3 9.8	60 1015
					.296	—	3.800	4 29	6.012	4 40	+ 5.97	+ 1 9.6	60 1015
60	1017	8.5	58 5	60 33.9	.296	9.0	18.958	4 32	15.708	4 35	- 29.76	- 3 2.0	60 1022
					.315	8.9	4.580	2 55	26.315	2 42	+ 7.16	- 5 4.8	60 1018
60	1019	8.6	58 20	60 26.4	.315	8.7	8.902	+2 50	23.154	+2 45	- 13.95	+ 4 28.2	60 1022
					.170	8.7	28.990	-0 31	12.195	-0 19	+ 39.33	+ 2 21.2	55 1869
55	1878	9.0	8 56 49	55 17.8	.176	8.7	40.303	1 15	28.576	1 12	- 54.72	+ 5 31.0	55 1886
					.178	8.5	13.938	-1 1	24.641	-1 4	+ 19.81	- 4 45.4	56 1956
56	1963	8.8	8 58 5	57 8.2	.178	—	1.165	0 59	—	—	+ 1.65	- 9 8—	56 1962
					.176	—	41.694	1 7	12.904	1 10	+ 56.70	- 2 29.5	55 1886
55	1896	9.0	58 40	55 25.6	.176	9.1	21.181	1 4	32.441	1 1	- 28.78	- 6 15.7	55 1900
					.178	8.8	32.140	0 54	5.670	0 45	+ 44.54	+ 1 5.7	55 1898
55	1903	9.0	59 27	56 8.0	.178	—	36.964	0 51	18.808	0 48	- 51.17	- 3 37.8	55 1910
					.178	8.7	14.491	0 35	31.034	0 37	+ 20.30	+ 5 59.4	56 1970
56	1973	9.0	59 37	56 30.8	.176	8.5	36.144	0 52	19.469	1 0	- 49.19	+ 3 45.5	55 1957
55	1945	8.4	9 3 21	55 24.3	.176	—	25.614	0 54	32.829	0 57	- 34.88	+ 6 20.2	55 1951
					.176	8.7	24.881	-0 44	6.349	-0 36	+ 33.97	- 1 13.5	55 1939
55	1946	9.0	9 3 34	55 34.7	.176	—	17.105	0 42	25.527	0 39	+ 23.39	+ 4 55.7	55 1943
					.178	9.1	33.242	0 33	22.243	0 27	+ 45.25	+ 4 17.6	55 1957
55	1969	9.0	4 56	55 24.8	.178	—	44.251	0 30	6.001	0 24	- 60.20	+ 1 9.5	55 1976
					.178	8.8	25.856	0 11	1.165	0 21	+ 36.78	+ 0 13.5	56 2010
56	2016	9.0	5 39	57 7.5	.176	8.7	33.750	0 6	11.539	0 18	+ 47.94	+ 2 13.6	56 2010
56	2017	8.4	5 46	57 3.3	.176	8.6	30.325	0 9	22.865	0 14	+ 43.14	+ 4 24.8	56 2010
56	2020	8.9	5 51	57 5.5	.178	8.7	47.395	+0 5	15.257	0 17	- 64.58	+ 2 56.7	55 2031
55	2015	8.6	10 25	55 27.8	.178	—	23.323	0 1	2.108	0 11	- 31.76	+ 0 24.4	55 2024

C. P. D.		1917		Aparentes						1917.0		* Ref.
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	C. P. D.
- 55°2025	8.9	9 <sup>h</sup> 10 <sup>m</sup> 58 <sup>s</sup>	- 55°30'16"	.178	8.8	1.055	-0 <sup>h</sup> 6 <sup>m</sup>	12.398	-0 <sup>h</sup> 15 <sup>m</sup>	+ 1.44	- 2' 23.6"	-55°2024
				.178	—	23.019	0 4	0.812	0 9	- 31.38	+ 0 9.4	55 2031
55 2032	9.0	11 33	55 14.8	.167	9.2	6.344	+2 42	15.443	+2 21	+ 8.58	- 2 58.9	55 2028
				.167	—	13.435	2 48	6.130	2 24	- 18.20	- 1 11.0	55 2035
55 2033	8.2	11 34	55 20.1	.167	8.0	11.938	3 1	33.798	2 29	- 16.19	- 6 31.4	55 2035
				.167	—	33.585	2 55	11.893	2 36	- 45.58	- 2 17.7	55 2037
55 2034	9.0	11 42	55 44.8	.195	8.5	37.066	-0 36	8.266	-0 46	- 50.82	- 1 35.7	55 2039
				.195	—	39.929	0 39	12.933	0 44	- 54.74	- 2 29.8	55 2040
56 2060	8.8	12 28	56 52.6	.195	8.8	13.725	0 31	4.636	0 8	+ 19.39	+ 0 53.7	56 2058
				.195	—	6.623	0 28	44.986	0 11	- 9.34	- 8 41.0	56 2062
56 2066	9.0	9 13 7	56 38.4	.195	9.0	20.600	-0 24	29.013	-0 15	+ 28.96	+ 5 36.0	56 2062
				.195	—	22.882	0 22	11.701	0 19	- 32.14	+ 2 15.5	56 2069
56 2070	9.0	13 52	56 20.6	.195	9.1	19.139	0 3	18.278	0 4	- 26.68	+ 3 31.7	56 2078
56 2083	9.0	14 50	56 51.6	.195	9.0	26.322	+0 6	18.929	+0 15	- 37.14	- 3 39.1	56 2091
				.195	—	—	—	18.075	0 12	- 69.—	+ 3 29.4	56 2095
56 2112	8.8	18 44	56 55.1	.195	8.3	15.018	0 21	3.777	0 18	+ 21.24	- 0 43.7	56 2109
55 2126	8.8	20 24	55 22.8	.195	8.7	5.001	1 26	27.064	1 2	+ 6.78	- 5 13.5	55 2125
				.195	—	48.506	1 18	10.484	1 5	- 65.94	+ 2 1.5	55 2144
55 2133	9.0	9 20 46	55 42.8	.195	9.1	4.482	+0 44	18.891	+0 39	+ 6.15	+ 3 38.8	55 2130
				.195	—	6.129	0 53	22.979	0 57	+ 8.39	- 4 26.2	55 2129
55 2138	8.7	20 55	55 29.7	.195	8.7	24.945	1 20	26.123	1 8	- 34.04	+ 5 2.6	55 2144
				.195	—	47.732	1 15	12.971	1 10	- 65.02	- 2 30.2	55 2148
55 2159	9.0	23 14	56 10.7	.195	8.8	28.672	1 28	19.316	1 32	- 39.74	+ 3 43.7	55 2167
56 2160	9.0	23 33	56 53.9	.195	8.2	22.891	1 38	32.736	1 35	+ 32.41	+ 6 19.2	55 2154
56 2169	9.0	24 2	56 38.1	.285	9.2	47.556	3 47	1.576	4 6	- 66.76	- 0 18.3	56 2202
				.285	—	26.709	3 51	21.406	4 10	- 37.46	- 4 7.9	56 2184
55 2171	8.8	24 4	55 41.6	.178	9.1	27.147	-0 2	11.386	0 8	+ 37.20	+ 2 11.9	55 2163
				.178	—	3.596	+0 1	29.421	0 6	- 4.92	- 5 40.8	55 2175
55 2176	8.9	9 24 9	55 34.5	.178	8.5	0.859	+0 3	7.354	+0 10	+ 1.17	+ 1 25.2	55 2175
56 2186	8.7	24 45	56 31.6	.285	—	3.680	3 39	16.659	4 15	+ 5.16	+ 3 12.9	56 2184
				.285	8.7	17.230	3 43	36.460	4 13	- 24.16	+ 7 2.3	56 2202
56 2215	9.6	25 31	56 39.1	.285	—	37.037	3 54	22.425	4 3	+ 51.97	- 4 19.7	56 2184
				.285	8.8	16.114	3 57	2.629	3 59	+ 22.63	- 0 30.4	56 2202
56 2258	9.0	28 0	56 45.9	.285	—	30.058	4 28	30.602	4 18	- 42.29	- 5 54.4	56 2270
				.285	9.0	7.607	4 25	26.494	4 22	- 10.73	+ 5 6.8	56 2261
56 2276	9.0	29 2	56 36.9	.195	9.1	13.938	1 45	16.575	1 49	+ 19.57	+ 3 12.0	56 2270
				.195	—	14.300	1 48	2.155	1 53	- 20.07	+ 0 25.0	56 2282
56 2313	9.0	9 30 56	57 6.0	.195	9.1	36.511	+2 12	16.727	+2 15	+ 51.94	+ 3 13.7	56 2296
56 2323	9.0	31 23	56 29.2	.195	9.0	19.422	2 23	4.883	2 18	- 27.15	- 0 56.5	56 2330
56 2382	9.0	35 27	56 29.4	.176	8.5	28.390	-0 10	19.138	-0 20	- 39.67	- 3 41.6	56 2398
				.176	—	1.535	0 12	29.216	0 17	- 2.15	+ 5 38.4	56 2383
56 2407	9.0	36 49	57 8.8	.176	8.7	39.594	0 31	3.528	0 27	+ 56.35	+ 0 40.8	56 2393
56 2416	9.0	37 17	56 53.6	.176	9.0	48.491	0 7	3.736	+0 2	- 68.53	- 0 43.2	56 2435
				.176	—	3.722	0 4	10.680	-0 2	+ 5.27	+ 2 3.7	56 2415
57 3486	9.0	10 32 20	57 46.3	.425	9.0	8.196	+3 54	2.976	+3 5	- 11.86	- 0 34.5	57 3499
				.427	9.0	7.292	+4 0	3.074	3 12	- 10.56	+ 0 35.6	57 3500
57 3502	9.0	10 32 35	57 48.9	.425	8.0	1.291	+3 56	16.237	+3 7	+ 1.87	- 3 8.0	57 3499
				.427	7.3	2.188	4 15	10.182	3 37	+ 3.17	- 1 57.9	57 3500
57 3504	9.0	32 35	57 46.4	.427	7.8	43.101	4 32	16.147	3 53	- 62.53	+ 3 7.0	57 3563
				.425	9.2	2.176	4 0	4.273	3 23	+ 3.15	- 0 49.5	57 3499
57 3506	8.1	32 37	57 48.4	.427	9.2	3.019	4 1	1.785	3 13	+ 4.37	+ 0 20.7	57 3500
				.425	8.2	3.191	3 58	13.620	3 11	+ 4.62	- 2 37.7	57 3499
57 3507	9.0	32 38	57 46.8	.427	8.3	4.053	4 13	7.553	3 29	+ 5.87	- 1 27.5	57 3500
				.425	9.0	4.242	4 2	5.058	3 21	+ 6.14	- 0 58.6	57 3499
				.427	8.9	5.142	4 3	0.989	3 16	+ 7.45	+ 0 11.5	57 3500



C. P. D.		1917		Aparentes						1917.0		* Ref. C. P. D.
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	
— 57°3508	7 <sup>m</sup> 3	10 <sup>h</sup> 32 <sup>m</sup> 39 <sup>s</sup>	— 57°47'6"	.425	7 <sup>m</sup> 1	5 <sup>R</sup> 024	+4 <sup>h</sup> 4 <sup>m</sup>	9 <sup>R</sup> 712	+3 <sup>h</sup> 18 <sup>m</sup>	+ 7.27	— 1' 52 <sup>''</sup> 5	—57°3499
				.427	7.0	5.903	4 11	3.667	3 27	+ 8.55	— 0 42.5	57 3500
				.427	7.0	39.356	4 34	22.642	3 50	— 57.08	+ 4 22.2	57 3563
57 3515	8.8	32 45	57 47.2	.425	8.9	8.877	4 12	7.255	3 31	+ 12.85	— 1 24.0	57 3499
				.427	8.8	9.722	4 7	1.192	3 21	+ 14.08	— 0 13.8	57 3500
57 3516	8.7	32 45	57 49.6	.425	8.7	8.444	4 7	20.051	3 51	+ 12.24	— 3 52.2	57 3499
				.427	8.6	9.319	4 24	13.972	3 46	+ 13.51	— 2 41.8	57 3500
57 3517	9.0	32 45	57 49.0	.425	9.0	8.046	4 10	16.649	3 46	+ 11.66	— 3 12.8	57 3499
				.427	9.0	8.911	4 19	10.617	3 40	+ 12.91	— 2 3.0	57 3500
57 3521	8.6	10 32 46	57 48.8	.425	8.4	10.009	+4 16	15.517	+3 42	+ 14.50	— 2 59.7	57 3499
				.427	8.4	10.888	4 21	9.531	3 34	+ 15.78	— 1 50.4	57 3500
57 3523	8.3	32 47	57 47.5	.425	8.3	10.773	4 19	9.110	3 36	+ 15.60	— 1 45.5	57 3499
				.427	8.2	11.618	4 9	3.064	3 25	+ 16.83	— 0 35.5	57 3500
57 3524	8.5	32 48	57 46.6	.425	8.8	11.372	4 21	4.910	3 28	+ 16.46	— 0 56.9	57 3499
				.427	8.6	12.229	4 5	1.114	3 18	+ 17.71	+ 0 12.9	57 3500
57 3526	8.2	32 49	57 48.5	.425	8.5	11.611	4 23	14.785	3 39	+ 16.82	— 2 51.2	57 3499
				.427	8.5	12.486	4 23	8.708	3 31	+ 18.09	— 1 40.8	57 3500
57 3527	8.8	32 53	57 49.3	.425	8.8	13.476	4 26	18.494	3 49	+ 19.53	— 3 34.2	57 3499
				.427	8.7	14.406	4 25	12.442	3 44	+ 20.88	— 2 24.1	57 3500
57 3533	8.8	10 32 57	57 47.2	.425	8.7	18.014	+4 28	7.668	+3 33	+ 26.09	— 1 28.8	57 3499
				.427	8.6	18.890	4 27	1.611	3 23	+ 27.36	— 0 18.6	57 3500
57 3540	8.4	33 6	57 50.7	.427	8.3	24.280	4 29	20.043	3 48	+ 35.20	— 3 52.1	57 3500
				.427	8.3	20.998	4 36	6.352	3 56	— 30.48	+ 1 13.5	57 3563
58 2949	8.7	58 42	58 20.7	.373	8.8	9.697	3 28	9.708	2 52	— 14.26	— 1 52.4	58 2953
				.381	8.9	9.745	2 55	9.674	2 49	— 14.33	— 1 52.0	58 2953
58 2963	8.8	59 16	58 22.3	.373	8.9	12.648	3 34	18.329	3 6	+ 18.60	— 3 32.3	58 2953
				.381	8.8	19.151	3 0	22.482	3 8	— 28.22	+ 4 20.4	58 2979
58 2968	8.6	10 59 23	58 15.4	.373	8.5	16.837	+3 38	18.178	+3 19	+ 24.73	+ 3 30.5	58 2953
				.381	8.7	42.276	3 53	19.384	4 31	— 62.10	+ 3 44.5	58 2995
57 4133	9.0	59 41	58 3.6	.373	9.0	8.836	3 47	7.635	4 3	+ 12.89	— 1 28.4	57 4127
				.373	9.0	29.278	4 49	15.684	4 12	— 42.78	+ 3 1.6	57 4156
57 4141	8.6	59 42	57 56.6	.373	8.7	22.982	3 55	29.173	4 8	+ 33.48	+ 5 37.9	57 4127
				.373	8.7	28.620	4 45	1.286	4 18	— 41.65	+ 0 14.9	57 4170
58 2986	8.9	11 0 0	58 20.3	.381	8.8	16.004	3 58	6.458	3 33	— 23.53	— 1 14.8	58 2995
				.381	8.8	33.446	4 12	5.296	3 36	— 49.19	— 1 1.3	58 3005
58 2987	8.9	0 2	58 18.5	.381	8.8	15.030	4 2	3.445	3 14	— 22.09	+ 0 39.9	58 2995
				.381	8.8	32.519	4 16	4.648	3 19	— 47.81	+ 0 53.8	58 3005
58 2993	8.7	11 0 15	58 20.5	.381	8.7	5.937	+4 6	6.899	+3 42	— 8.73	— 1 19.6	58 2995
				.381	8.7	23.360	4 22	5.748	3 45	— 34.36	— 1 6.6	58 3005
58 2999	8.9	0 27	58 24.7	.389	9.0	2.196	2 12	29.740	1 50	+ 3.23	— 5 44.4	58 2995
				.389	9.0	15.324	2 17	28.499	1 54	— 22.56	— 5 30.1	58 3005
58 3000	8.9	0 32	58 25.5	.389	—	5.714	2 13	32.933	1 55	+ 8.41	— 6 21.4	58 2995
				.389	8.9	11.701	2 19	31.746	1 58	— 17.23	— 6 7.7	58 3005
58 3003	8.4	0 43	58 16.9	.389	7.7	13.077	2 22	11.522	3 13	+ 19.21	+ 2 13.4	58 2995
				.389	7.7	4.422	2 26	12.719	3 15	— 6.50	+ 2 27.3	58 3005
57 4181	8.7	11 0 44	58 1.0	.373	8.3	14.003	+4 40	21.321	+4 23	+ 20.40	— 4 6.9	57 4170
				.373	8.3	27.327	4 35	29.831	4 29	+ 39.89	+ 5 45.5	57 4156
58 3014	8.4	1 4	58 14.8	.389	7.8	9.800	2 31	23.396	3 18	+ 14.40	+ 4 31.0	58 3005
				.389	7.8	15.238	4 41	8.888	4 3	— 22.35	— 1 42.9	57 4208
58 3016	8.4	1 5	58 18.5	.389	7.8	11.241	2 33	4.306	3 35	+ 16.52	+ 0 49.9	58 3005
				.389	7.8	13.663	4 45	28.040	4 22	— 20.05	— 5 24.7	57 4208
				.392	7.7	27.445	2 40	8.417	3 21	— 40.34	+ 1 37.5	58 3056
				.389	8.8	13.385	2 37	26.212	3 21	+ 19.66	+ 5 3.6	58 3005
58 3019	8.5	1 8	58 14.2	.389	9.0	11.573	4 48	6.091	4 7	— 16.97	— 1 10.5	57 4208

C. P. D.		1917		Aparentes				1917.0		* Ref. C. P. D.		
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	
- 58°3020	9.0	11 <sup>b</sup> 1 <sup>m</sup> 9 <sup>s</sup>	-58°22.6	.389	9.0	13.093	+2 <sup>h</sup> 8 <sup>m</sup>	17.204	+2 <sup>h</sup> 2 <sup>m</sup>	+ 19.26	- 3' 19.3	-58°3005
				.392	9.0	25.457	2 44	12.986	3 27	- 37.46	- 2 30.4	58 3056
58 3027	8.8	1 14	58 14.9	.389	8.7	16.875	2 45	22.995	3 24	+ 24.78	+ 4 26.3	58 3005
				.389	8.7	8.096	4 50	9.338	4 10	- 11.87	- 1 48.2	57 4208
58 3028	8.3	1 15	58 15.4	.389	8.4	17.271	2 48	20.916	3 26	+ 25.37	+ 4 2.2	58 3005
				.389	8.5	7.646	4 52	11.401	4 13	- 11.21	- 2 12.0	57 4208
58 3031	9.0	1 19	58 16.3	.389	8.0	20.794	2 52	16.297	3 28	+ 30.55	+ 3 8.8	58 3005
				.389	8.2	4.177	4 54	16.007	4 16	- 6.13	- 3 5.4	57 4208
57 4206	8.2	1 24	58 6.2	.411	8.2	25.386	4 5	21.942	2 59	- 37.14	+ 4 14.1	57 4235
				.417	8.2	25.335	3 37	21.888	3 41	- 37.05	+ 4 13.5	57 4235
58 3036	9.0	11 1 24	58 16.4	.389	9.1	23.480	+2 56	15.830	+3 30	+ 34.50	+ 3 3.3	58 3005
				.389	9.1	1.463	4 56	16.501	4 19	- 2.14	- 3 11.1	57 4208
58 3037	8.2	1 25	58 18.1	.389	8.3	24.134	3 2	6.261	3 33	+ 35.47	+ 1 12.5	58 3005
				.389	8.3	0.763	4 58	26.005	4 25	- 1.11	- 5 1.2	57 4208
58 3038	8.4	1 28	58 20.7	.392	8.2	14.547	2 47	10.462	3 24	- 21.38	+ 2 1.2	58 3056
				.389	8.5	26.140	3 6	7.856	3 28	+ 38.44	- 1 31.0	58 3005
58 3040	8.8	1 29	58 21.3	.392	8.3	12.542	2 52	3.612	3 30	- 18.45	- 0 41.8	58 3056
				.389	9.0	27.309	3 9	10.310	3 41	+ 40.17	- 1 59.4	58 3005
				.392	9.0	11.310	2 56	6.158	3 33	- 16.64	- 1 11.3	58 3056
58 3043	8.7	11 1 32	58 15.5	.389	8.8	4.002	+5 5	11.716	+4 28	+ 5.88	- 2 15.7	57 4208
				.411	9.0	19.620	3 58	25.252	3 2	- 28.76	- 4 52.5	57 4235
58 3044	8.8	1 33	58 14.3	.389	9.0	4.603	5 3	6.086	4 33	+ 6.75	- 1 10.5	57 4208
				.411	9.0	19.035	4 1	19.631	3 5	- 27.90	- 3 47.4	57 4235
58 3048	8.6	1 37	58 33.9	.392	8.8	5.683	2 35	0.480	2 25	+ 8.41	+ 0 5.6	58 3039
				.406	8.7	5.674	2 39	0.434	2 30	+ 8.40	+ 0 5.0	58 3039
58 3049	8.7	1 38	58 19.8	.392	8.8	5.909	2 59	1.359	3 34	- 8.69	+ 0 15.7	58 3056
				.406	8.7	5.886	2 45	1.356	3 36	- 8.66	+ 0 15.7	58 3056
				.409	8.7	5.885	3 27	1.344	3 25	- 8.65	+ 0 15.6	58 3056
58 3050	8.9	11 1 38	58 22.8	.392	8.8	5.850	+3 3	23.777	+3 37	- 8.62	- 4 35.4	58 3056
				.406	8.9	5.867	3 56	23.748	3 44	- 8.64	- 4 35.0	58 3056
58 3051	9.5	1 42	58 23.0	.406	8.8	2.907	3 58	25.174	3 48	- 4.28	- 4 51.6	58 3056
				.417	8.9	2.957	3 49	25.215	3 46	- 4.35	- 4 52.0	58 3056
58 3053	8.8	1 44	58 23.7	.392	8.7	2.347	3 8	18.282	3 43	- 3.46	- 3 31.7	58 3056
				.406	8.8	2.306	4 1	18.259	3 52	- 3.39	- 3 31.5	58 3056
58 3055	8.7	1 45	58 37.9	.392	8.7	11.236	2 32	19.974	2 29	+ 16.65	- 3 51.3	58 3039
				.406	8.7	11.107	2 36	20.063	2 33	+ 16.46	- 3 52.4	58 3039
58 3057	8.8	11 1 48	58 19.5	.406	8.8	1.177	+2 49	3.965	+3 31	+ 1.73	+ 0 45.9	58 3056
				.409	8.8	1.191	3 29	3.963	3 23	+ 1.75	+ 0 45.9	58 3056
58 3058	8.9	1 48	58 13.8	.389	8.9	15.163	5 0	3.300	4 36	+ 22.24	- 0 38.2	57 4208
				.411	8.9	8.403	3 55	16.831	3 9	- 12.31	- 3 14.9	57 4235
58 3066	8.7	2 2	58 17.0	.406	8.5	10.867	2 52	16.635	3 25	+ 15.97	+ 3 12.7	58 3056
				.409	8.8	37.941	3 35	17.331	4 24	- 55.68	- 3 20.7	58 3112
58 3069	8.6	2 5	58 19.4	.406	8.6	12.905	2 55	4.483	3 29	+ 18.96	+ 0 51.9	58 3056
				.406	8.7	25.104	4 33	23.106	5 10	- 36.95	+ 4 27.6	58 3103
58 3073	8.8	2 10	58 17.0	.406	8.5	16.058	3 1	16.338	3 22	+ 23.60	+ 3 9.2	58 3056
				.409	8.7	32.742	3 38	17.594	4 26	- 48.05	- 3 23.8	58 3112
58 3075	8.3	11 2 12	58 23.3	.406	8.5	17.300	+3 7	16.289	+3 15	+ 25.46	- 3 8.6	58 3056
				.406	8.5	20.599	4 36	2.372	5 1	- 30.35	+ 0 27.5	58 3103
58 3077	8.7	2 15	58 13.7	.409	8.3	29.420	3 42	0.891	4 36	- 43.14	- 0 10.3	58 3112
				.411	8.5	9.579	3 52	17.086	3 18	+ 14.03	- 3 17.9	57 4235
58 3079	8.7	2 17	58 22.9	.406	8.8	21.102	3 10	14.750	3 18	+ 31.05	- 2 50.8	58 3056
				.406	8.7	16.786	4 39	3.922	5 3	- 24.73	+ 0 45.4	58 3103
57 4247	9.0	2 18	58 5.7	.411	8.9	11.825	3 47	25.196	3 31	+ 17.29	+ 4 51.8	57 4235
				.417	8.9	11.815	3 53	25.166	3 43	+ 17.28	+ 4 51.5	57 4235

C. P. D.		1917		Aparentes						1917.0		* Ref. C. P. D.
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	
- 58°3080	8 <sup>m</sup> .9	11 <sup>h</sup> 2 <sup>m</sup> 18 <sup>s</sup>	-58°15'5	.409	8 <sup>m</sup> .9	26 <sup>m</sup> 81 <sup>s</sup> 2	+3 <sup>h</sup> 44 <sup>m</sup>	8 <sup>m</sup> 884	+4 <sup>h</sup> 38 <sup>m</sup>	- 39 <sup>s</sup> .33	- 1' 42 <sup>s</sup> .9	-58°3112
				.419	9.0	31.306	2 8	12.638	1 17	- 45.96	+ 2 26.4	58 3120
58 3081	8.6	2 19	58 16.9	.409	8.8	25.798	3 47	17.550	4 28	- 37.86	- 3 23.3	58 3112
				.419	9.0	30.282	2 10	3.879	1 34	- 44.47	+ 0 44.9	58 3120
57 4253	8.4	2 22	58 12.9	.409	8.6	24.128	3 51	3.767	4 50	- 35.37	+ 0 43.6	58 3112
				.411	8.6	14.897	3 44	12.390	3 24	+ 21.82	- 2 23.5	57 4235
58 3085	8.8	2 24	58 13.7	.409	8.8	23.284	3 53	0.117	4 42	- 34.14	- 0 1.4	58 3112
				.411	9.0	15.739	3 41	16.335	3 20	+ 23.05	- 3 9.2	57 4235
58 3087	8.8	2 25	58 14.7	.409	8.9	22.003	3 55	5.524	4 44	- 32.27	- 1 4.0	58 3112
				.419	8.9	26.523	2 12	15.991	1 21	- 38.93	+ 3 5.2	58 3120
58 3090	8.6	11 2 27	58 16.7	.409	8.0	20.522	+3 57	15.545	+4 30	- 30.12	- 3 0.0	58 3112
				.419	8.0	24.994	2 14	5.912	1 31	- 36.71	+ 1 8.5	58 3120
58 3092	8.6	2 33	58 14.5	.409	7.8	17.132	3 59	4.010	4 46	- 25.13	- 0 46.5	58 3112
				.411	7.7	21.863	3 37	20.204	3 13	+ 32.04	- 3 54.0	57 4235
				.419	7.5	21.646	2 17	17.470	1 23	- 31.77	+ 3 22.3	58 3120
57 4257	8.8	2 36	58 11.5	.409	8.7	14.724	4 2	11.311	4 51	- 21.58	+ 2 11.0	58 3112
				.411	8.8	24.306	3 35	4.881	3 28	+ 35.60	- 0 56.5	57 4235
58 3097	8.3	2 37	58 26.7	.406	8.3	3.415	4 42	14.999	4 54	- 5.03	- 2 53.7	58 3103
				.409	8.4	42.577	5 7	4.541	5 1	- 62.85	+ 0 52.6	58 3147
58 3099	8.4	11 2 39	58 14.9	.409	9.2	12.534	+4 5	6.926	+4 19	- 18.39	- 1 20.2	58 3112
				.419	8.9	17.018	2 19	14.617	1 26	- 24.98	+ 2 49.3	58 3120
58 3102	8.3	2 40	58 17.5	.409	8.8	11.134	4 7	19.602	4 31	- 16.34	- 3 47.0	58 3112
				.419	8.3	15.595	2 22	1.844	1 36	- 22.91	+ 0 21.4	58 3120
58 3104	8.6	2 42	58 21.7	.419	8.6	15.045	2 24	20.658	1 46	- 22.12	- 3 59.3	58 3120
				.425	8.6	27.642	4 50	5.442	4 32	- 40.68	- 1 3.0	58 3132
58 3107	8.8	2 52	58 14.8	.409	9.1	3.918	4 10	6.251	4 17	- 5.75	- 1 12.4	58 3112
				.419	9.0	8.429	2 27	15.238	2 4	- 12.36	+ 2 56.5	58 3120
57 4272	9.0	11 2 55	58 4.7	.417	8.9	24.084	+3 56	19.724	+4 26	- 35.14	- 3 48.4	57 4293
				.417	8.9	29.369	4 8	0.048	4 17	- 42.89	+ 0 0.5	57 4296
58 3108	8.8	2 55	59 11.6	.430	8.8	4.897	4 12	22.178	3 49	- 7.37	- 4 16.9	58 3108
				.430	8.8	15.781	4 14	22.800	3 52	- 23.82	+ 4 24.0	59 3045
58 3110	8.6	2 56	58 18.8	.419	8.6	5.686	2 30	5.882	1 43	- 8.36	- 1 8.1	58 3120
				.425	8.8	18.392	4 54	9.347	4 37	- 27.05	+ 1 48.2	58 3132
58 3114	8.6	2 57	58 21.5	.406	8.6	10.642	4 50	12.143	5 6	+ 15.67	+ 2 20.6	58 3103
				.425	8.6	17.139	4 52	3.746	4 35	- 25.22	- 0 43.4	58 3132
58 3123	8.8	3 5	58 24.7	.406	9.0	16.212	4 47	5.160	4 57	+ 23.90	- 0 59.7	58 3103
				.409	8.9	22.916	5 10	14.427	5 4	- 33.81	+ 2 47.1	58 3147
57 4279	9.4	11 3 12	58 8.3	.417	8.7	12.078	+3 59	37.568	+4 23	- 17.64	- 7 15.1	57 4293
				.417	8.7	17.388	4 11	17.909	4 14	- 25.41	- 3 27.4	57 4296
58 3128	8.4	3 18	58 17.7	.419	8.5	9.150	2 34	0.598	1 39	+ 13.44	+ 0 6.9	58 3120
				.425	8.5	3.575	4 56	15.874	4 39	- 5.26	+ 3 3.8	58 3132
58 3131	8.4	3 19	58 15.6	.409	8.6	14.791	4 12	9.848	4 15	+ 21.70	- 1 54.1	58 3112
				.419	8.5	10.297	2 36	11.671	1 50	+ 15.12	+ 2 15.2	58 3120
58 3133	9.0	3 23	58 19.3	.419	9.0	12.777	2 38	7.819	1 56	+ 18.77	- 1 30.5	58 3120
				.425	9.1	0.120	4 58	7.462	4 45	+ 0.17	+ 1 26.4	58 3132
58 3140	8.5	11 3 29	59 13.1	.430	8.5	7.818	+4 17	14.754	+3 55	+ 11.80	+ 2 50.9	59 3045
				.430	8.5	28.240	4 19	0.877	3 57	- 42.61	+ 0 10.1	58 3163
57 4295	9.0	3 36	57 56.5	.417	9.0	4.531	4 1	22.864	4 27	+ 6.60	+ 4 24.8	57 4293
				.417	8.9	0.805	4 4	42.520	4 20	- 1.17	+ 8 12.4	57 4296
58 3144	8.2	3 36	58 16.1	.417	8.3	22.593	5 9	12.429	4 48	- 33.20	+ 2 23.9	58 3161
				.419	8.2	21.735	2 39	8.706	1 52	+ 31.92	+ 1 40.8	58 3120
				.425	8.4	8.954	4 59	23.995	4 43	+ 13.16	+ 4 37.9	58 3132
58 3145	9.0	3 39	58 21.9	.417	9.1	20.702	5 7	18.466	4 52	- 30.45	- 3 33.9	58 3161
				.425	9.0	10.953	5 0	6.898	4 46	+ 16.12	- 1 19.9	58 3132

C. P. D.		1917		Aparentes						1917.0		* Ref. C. P. D.
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	
- 58°3168	9.0	11 <sup>h</sup> 4 <sup>m</sup> 18 <sup>s</sup>	- 58°30'11"	.409	9.1	25.686	+5 <sup>h</sup> 12"	14.498	+5 <sup>h</sup> 16'	+ 37.95	- 2' 47.9	-58°3147
				.419	9.0	30.497	2 45	6.204	3 45	- 45.07	+ 1 11.8	58 3189
58 3174	8.6	4 27	58 23.9	.417	8.7	12.308	5 4	28.746	4 56	+ 18.12	- 5 32.9	58 3161
				.419	8.8	19.447	2 58	12.066	3 56	- 28.66	+ 2 19.7	58 3186
57 4322	8.8	4 30	58 3.0	.417	8.9	36.346	4 35	8.347	4 30	+ 53.06	+ 1 36.7	57 4296
				.417	8.9	18.029	4 38	21.463	4 41	- 26.28	- 4 8.6	57 4335
58 3175	8.9	4 33	58 33.0	.419	8.9	20.148	2 46	8.711	3 48	- 29.80	- 1 40.9	58 3189
				.419	8.9	15.588	2 49	35.519	4 13	- 23.03	- 6 51.4	58 3186
58 3178	8.6	4 42	58 29.5	.419	8.6	13.680	2 51	10.212	3 51	- 20.22	+ 1 58.3	58 3189
				.419	8.7	9.226	2 54	16.634	3 58	- 13.62	- 3 12.7	58 3186
58 3181	9.0	11 4 51	59 6.4	.430	9.1	25.149	+4 5	35.798	+3 59	+ 37.88	+ 6 54.6	58 3163
				.430	9.1	1.632	4 8	44.678	4 2	- 2.45	- 8 30.5	58 3184
58 3183	8.6	4 52	58 22.7	.417	8.6	28.772	5 1	21.499	4 58	+ 42.34	- 4 9.0	58 3161
				.419	8.5	2.983	2 59	19.429	4 5	- 4.40	+ 3 45.0	58 3186
58 3198	8.6	5 20	58 22.7	.419	8.7	16.558	3 2	18.081	4 1	+ 24.40	+ 3 29.4	58 3186
				.428	8.6	31.857	4 48	1.904	4 40	- 46.96	+ 3 40.5	58 3217
58 3199	8.7	5 26	58 30.5	.419	8.7	19.875	3 8	21.812	4 8	+ 29.34	- 4 12.6	58 3186
				.419	8.7	15.326	3 13	4.990	3 27	+ 22.65	+ 0 57.8	58 3189
58 3219	8.5	11 6 11	58 15.2	.425	8.5	22.697	+4 1	7.141	+4 18	+ 33.32	+ 1 22.7	58 3203
				.425	8.5	2.189	4 5	42.291	4 15	+ 3.22	+ 8 9.8	58 3217
58 3228	8.7	6 29	58 24.3	.425	8.8	15.045	4 8	5.373	4 20	+ 22.17	- 1 2.2	58 3217
				.428	8.8	15.044	4 55	5.400	4 45	+ 22.17	- 1 2.5	58 3217
58 3229	8.4	6 35	59 1.9	.430	8.4	5.377	3 18	8.656	3 13	- 8.07	+ 1 40.2	58 3231
				.430	8.4	6.118	3 20	16.429	3 15	- 9.19	+ 3 10.3	58 3232
58 3233	9.0	6 46	58 28.1	.425	9.0	26.250	4 9	25.432	4 11	+ 38.71	- 4 54.5	58 3217
				.428	9.0	26.236	4 52	25.445	4 47	+ 38.70	- 4 54.7	58 3217
58 3243	9.0	7 17	59 7.9	.430	9.1	22.054	3 27	22.445	3 31	+ 33.15	- 4 19.9	58 3231
				.430	9.1	21.290	3 29	14.645	3 34	+ 32.01	- 2 49.6	58 3232
58 3244	9.0	11 7 21	59 5.7	.430	8.9	25.103	+3 23	10.200	+3 36	+ 37.72	- 1 58.1	58 3231
				.430	8.9	24.353	3 25	2.379	3 38	+ 36.60	- 0 27.5	58 3232
58 3255	9.0	7 54	58 46.5	.430	8.5	25.447	4 22	10.475	4 24	+ 37.89	- 2 1.3	58 3242
				.430	8.5	0.892	4 37	37.471	4 27	+ 1.32	+ 7 14.0	58 3253
58 3262	8.9	8 8	58 48.7	.430	9.1	0.693	4 39	39.695	4 31	+ 1.03	+ 7 39.7	58 3261
				.430	9.1	10.903	4 35	25.823	4 33	+ 16.27	+ 4 59.1	58 3253
58 3307	8.7	9 37	59 10.4	.430	8.9	18.863	4 41	11.253	4 49	+ 28.44	+ 2 10.3	59 3193
				.430	8.9	11.537	4 44	7.054	4 46	- 17.38	- 1 21.7	58 3314
60 3094	8.8	11 30 44	61 7.1	.493	7.8	1.324	+4 20	5.449	+3 17	- 2.12	- 1 3.1	60 3095
				.493	7.8	6.496	4 46	7.981	3 46	- 10.39	+ 1 32.4	60 3102
60 3096	9.0	31 46	61 1.8	.515	7.7	26.811	4 16	27.004	3 14	- 42.93	+ 5 12.8	60 3155
				.469	9.0	0.830	4 43	22.331	4 24	+ 1.32	+ 4 18.6	60 3095
60 3098	8.4	31 51	61 10.7	.493	9.0	4.330	4 42	35.747	3 59	- 6.92	+ 6 54.0	60 3102
				.501	8.6	1.971	3 49	9.832	4 40	- 3.16	- 1 53.9	60 3102
60 3108	9.0	31 58	61 9.8	.515	8.6	22.274	4 20	9.208	3 19	- 35.70	+ 1 46.7	60 3155
				.501	9.0	3.464	3 53	5.586	4 50	+ 5.54	- 1 4.7	60 3102
				.515	9.1	16.811	4 24	13.453	3 25	- 26.94	+ 2 35.8	60 3155
60 3112	8.4	11 32 2	61 7.8	.493	8.1	10.730	+4 25	9.015	+3 30	+ 17.15	- 1 44.4	60 3095
				.501	8.1	5.579	2 43	4.429	2 36	+ 8.93	+ 0 51.3	60 3102
60 3116	9.0	32 3	61 7.2	.515	8.1	14.794	4 28	23.453	3 30	- 23.69	+ 4 31.6	60 3155
				.493	9.2	10.971	4 22	6.134	3 23	+ 17.54	- 1 11.0	60 3095
60 3122	8.8	32 6	61 11.1	.493	8.2	5.800	4 49	7.338	4 8	+ 9.28	+ 1 25.0	60 3102
				.501	8.9	7.742	3 59	12.450	4 37	+ 12.40	- 2 24.2	60 3102
60 3126	8.5	32 8	61 10.1	.515	9.0	12.571	4 31	6.572	3 38	- 20.15	+ 1 16.1	60 3155
				.501	8.4	9.065	4 3	7.399	4 43	+ 14.51	- 1 25.7	60 3102
				.515	8.4	11.251	4 35	11.594	3 45	- 18.03	+ 2 14.3	60 3155

C. P. D.		1917		Aparentes						1917.0		* Ref.
Nº	Mag.	A. R.	Decl.	1917 +	Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.	Δ Decl.	C. P. D.
- 60°3128	8 <sup>m</sup> 3	11 <sup>h</sup> 32 <sup>m</sup> 9 <sup>s</sup>	- 61° 8' 2"	.493	8 <sup>m</sup> 3	15 <sup>R</sup> 267	+4 <sup>h</sup> 37 <sup>m</sup>	11 <sup>R</sup> 392	+3 <sup>h</sup> 38 <sup>m</sup>	+ 24.41	- 2' 11".9	-60°3095
				.501	8.1	10.123	4 6	2.069	4 56	+ 16.20	+ 0 24.0	60 3102
				.515	8.2	10.254	4 38	21.058	3 52	- 16.42	+ 4 3.9	60 3155
60 3129	8.7	32 9	61 5.1	.469	9.2	15.575	4 47	4.671	4 38	+ 24.89	+ 0 54.1	60 3095
				.493	9.1	10.402	4 52	18.057	3 50	+ 16.63	+ 3 29.1	60 3102
60 3133	8.9	32 12	61 10.0	.501	8.9	11.466	4 10	7.041	4 46	+ 18.36	- 1 21.6	60 3102
				.515	8.9	8.887	4 42	11.935	3 58	- 14.24	+ 2 18.2	60 3155
60 3136	8.4	32 15	61 0.3	.469	8.5	18.386	4 51	29.115	4 27	+ 29.49	+ 5 37.2	60 3095
				.518	8.6	46.603	3 16	5.464	3 35	- 74.26	+ 1 3.3	60 3195
60 3145	8.4	11 32 18	61 11.5	.501	8.5	15.782	+4 13	14.576	+4 34	+ 25.27	- 2 48.8	60 3102
				.515	8.4	4.493	4 47	4.426	4 3	- 7.20	+ 0 51.3	60 3155
60 3147	9.0	32 19	61 7.7	.493	9.0	15.954	4 56	5.129	4 12	+ 25.53	+ 0 59.4	60 3102
				.518	9.0	4.319	2 18	23.121	2 39	- 6.91	+ 4 27.8	60 3155
60 3148	8.6	32 19	61 8.1	.501	8.4	16.367	4 17	3.077	4 59	+ 26.19	+ 0 35.6	60 3102
				.518	8.8	3.915	2 22	22.060	2 44	- 6.26	+ 4 15.5	60 3155
60 3157	8.4	32 28	61 6.9	.493	8.3	22.226	5 0	9.362	4 3	+ 35.56	+ 1 48.4	60 3102
				.518	8.5	1.952	2 26	28.455	2 48	+ 3.13	+ 5 29.6	60 3155
60 3161	8.9	11 32 32	61 9.0	.501	8.2	24.241	+4 20	1.779	+4 52	+ 38.80	- 0 20.6	60 3102
				.515	8.0	3.914	4 50	17.187	4 8	+ 6.27	+ 3 19.0	60 3155
				.518	7.8	3.997	2 29	17.208	2 52	+ 6.40	+ 3 19.3	60 3155
60 3168	8.7	32 38	61 4.0	.469	8.9	33.765	4 54	10.495	4 31	+ 53.94	+ 2 1.6	60 3095
				.518	8.4	31.191	3 23	13.130	3 39	- 49.76	- 2 32.1	60 3195
60 3175	8.6	32 47	61 12.5	.501	8.7	33.860	4 25	19.525	4 29	+ 54.24	- 3 46.1	60 3102
				.518	8.7	13.577	3 6	0.538	2 59	+ 21.77	- 0 6.2	60 3155
60 3191	8.8	33 18	60 58.3	.518	8.8	6.783	3 28	15.617	3 48	- 10.80	+ 3 0.9	60 3195
				.518	9.0	11.486	4 2	46.960	3 56	+ 18.23	- 9 3.9	60 3182
60 6319	8.8	15 55 58	60 11.5	.469	9.0	8.645	+2 12	5.352	+2 0	- 13.43	- 1 2.0	60 6326
				.469	9.0	4.399	3 24	6.186	4 8	+ 6.83	+ 1 11.6	60 6317
60 6325	8.6	56 11	60 9.0	.469	8.5	12.063	2 36	13.863	1 36	+ 18.70	- 2 40.6	59 6555
				.469	8.5	0.879	2 16	8.181	1 56	- 1.36	+ 1 34.8	60 6326
60 6332	9.0	56 18	60 16.4	.469	9.0	17.700	3 31	18.954	4 12	+ 27.54	- 3 39.5	60 6317
				.469	9.0	14.357	3 49	1.572	4 30	- 22.36	- 0 18.2	60 6348
59 6562	9.0	56 21	60 5.7	.469	9.0	18.635	2 39	2.537	1 18	+ 28.87	+ 0 29.4	59 6555
				.469	9.2	5.657	2 19	24.542	1 45	+ 8.78	+ 4 44.2	60 6326
60 6334	8.9	15 56 22	60 8.8	.469	8.7	19.170	+2 43	13.044	+1 29	+ 29.72	- 2 31.1	59 6555
				.469	8.7	6.205	2 24	8.966	1 53	+ 9.63	+ 1 43.8	60 6326
60 6338	8.4	56 25	60 15.3	.469	8.3	22.201	3 35	13.694	4 15	+ 34.54	- 2 38.6	60 6317
				.469	8.2	9.893	3 52	3.711	4 34	- 15.40	+ 0 43.0	60 6348
				.469	8.2	9.150	3 45	25.234	4 22	+ 14.22	- 4 52.3	60 6326
60 6339	9.0	56 26	60 12.5	.469	9.0	9.922	2 27	10.263	2 7	+ 15.41	- 1 58.9	60 6326
				.469	9.1	9.146	3 55	18.779	4 27	- 14.23	+ 3 37.5	60 6348
59 6563	8.8	11 56 30	60 6.3	.469	8.9	24.799	+2 45	0.533	+1 21	+ 38.42	- 0 6.2	59 6555
				.469	8.9	11.837	2 30	21.467	1 48	+ 18.36	+ 4 8.6	60 6326
60 6349	8.4	56 40	60 17.0	.469	8.5	32.011	3 38	21.986	4 18	+ 49.82	- 4 14.6	60 6317
				.469	8.5	*	3 59	4.591	4 36	+ 0.04	- 0 53.2	60 6348
53 7744	8.8	16 13 20	53 23.3	.778	8.9	4.999	5 47	24.007	5 42	+ 6.49	- 4 38.1	53 7737
				.786	8.9	5.029	4 54	24.026	4 48	+ 6.51	- 4 38.2	53 7737
55 8539	8.5	18 5 24	55 30.6	.778	8.6	27.153	4 13	41.058	4 31	+ 36.97	- 7 55.5	55 8536
				.778	8.5	32.440	4 20	37.364	4 25	- 44.31	+ 7 12.7	55 8545

\* P = 180°36.

# OBSERVATIONS OF COMETS AND OF (704) INTERAMNIA

## OBSERVACIONES DE COMETAS Y DE (704) INTERAMNIA

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The following observations were made with the 17 inch Gautier refractor described on pages 39 to 45 of volume I of these Publications, in connection with the micrometers there described and again mentioned on pages 4 and 5 of the present volume. The eyepieces used were as follows, each having the lowest power and largest field of those available at the time.

Power 300, field 5.0 until March, 1913.

Power 280, field 8.2 from March, 1913 to Feb. 9, 1914.

Power 150, field 12.5, since Feb. 11, 1914.

Whenever possible, the observations have been made by the method of direct micrometer measurement. In the few cases in which the method of transits was used, the letter «t» is added in the column of number of comparisons. On and after Oct. 31, 1913, the observations of difference of right ascension by the method of transits have been chronographically recorded; before that date they were made by eye and ear.

The observed differences of right ascension and declination have all been corrected for differential refraction. The parallax factors have been computed partly with the constants

$$\begin{aligned} \frac{1}{15} 8''.80 \rho \cos \varphi' &= [9.68272] \\ \tan \varphi' &= [9.84080n] \\ 8''.80 \rho \sin \varphi' &= [0.69961n] \end{aligned}$$

Las observaciones siguientes fueron hechas con el refractor Gautier de 433 mm. de abertura, descrito en páginas 39 a 45 del primer tomo de estas publicaciones, en conexión con los dos micrómetros ahí mencionados y también notados en páginas 4 y 5 del presente tomo. Los oculares empleados fueron los siguientes, teniendo cada uno el menor aumento y el mayor campo de vista de los disponibles en las épocas correspondientes.

Aumento 300, campo 5.0, hasta marzo de 1913.

Aumento 280, campo 8.2, desde marzo de 1913 hasta el 9 de febrero de 1914.

Aumento 150, campo 12.5, después del 11 de febrero de 1914.

Cuando era posible, se hacían las observaciones con el método de medidas micrométricas directas. En los casos en que se ha empleado el método de pasajes el hecho se indica con una *t* en la columna del número de comparaciones. En el 31 de octubre de 1913 y después, las observaciones de diferencia de ascensión recta hechas con este método fueron registradas cronográficamente; las anteriores fueron hechas a ojo y oído.

Las diferencias observadas de ascensión recta y de declinación han sido corregidas para refracción diferencial. Una parte de los factores de paralaje ha sido calculada con las constantes

$$\begin{aligned} \frac{1}{15} 8''.80 \rho \cos \varphi' &= [9.68272] \\ \tan \varphi' &= [9.84080n] \\ 8''.80 \rho \sin \varphi' &= [0.69961n] \end{aligned}$$

and partly from tables based on them. The reductions to apparent place have been computed with the independent star numbers of the *American Ephemeris and Nautical Almanac*, including short period terms except  $f'$

The provisional value of the longitude of this Observatory,

3<sup>h</sup> 51<sup>m</sup> 44.<sup>s</sup>9 west of Greenwich,

given on page 65 of volume I of these Publications is sufficiently accurate for the reduction of the times of observation to any standard meridian.

Some comet observations made in 1912, 1913 and 1914 have already been published in volume I of this series.

Several notes of physical appearance, etc., are omitted. They will be gladly communicated upon request.

y la otra con tablas basadas en los mismos valores. Las reducciones a lugar aparente han sido calculadas con los números independientes del *American Ephemeris and Nautical Almanac*, teniendo en cuenta los términos lunares con la excepción de  $f'$ .

El valor provisorio de la longitud de este observatorio,

3<sup>h</sup> 51<sup>m</sup> 44.<sup>s</sup>9 oeste de Greenwich,

publicado en página 65 del primer tomo de estas publicaciones es bastante exacto para la reducción de las horas de observación a cualquier meridiano fundamental.

Algunas observaciones de cometas hechas en 1912, 1913 y 1914 ya han aparecido en el primer tomo de esta serie.

Varias notas sobre aspecto físico, etc., se han omitido. Tendré mucho gusto en comunicarlas a quien las pida.

OBSERVATIONS

OBSERVACIONES

T.M. La Plata	*	Comp.	Cometa—Estrella		Pos. Aparente del Cometa		Log. p <sup>o</sup> Δ	
			Δ A.R.	Δ Decl.	A.R.	Decl.	en A.R.	en Decl.
			h m s	° ' "	h m s	° ' "		
<b>Cometa Neujmín, 1913c</b>								
1913 Sept.								
9 10 58 51	1	10,10	+0 10.85	-3 13.9	23 48 7.52	+ 0 55 36.4	9.2882n	0.7087n
9 11 46 20	2	10,10	+0 13.38	-4 40.6	23 48 6.19	+ 0 56 31.3	8.9972n	0.7095n
<b>Cometa Zinner-Giacobini, 1913e</b>								
Oct.								
28 9 6 50	3	8,8	-0 7.70	-0 2.1	19 6 12.14	- 9 18 38.1	9.6523	0.6516n
29 9 2 0	5	8,8	-0 0.79	+0 29.2	19 11 14.73	-10 15 55.5	9.6485	0.6426n
30 8 37 21	7	8,8	-0 20.77	-0 55.7	19 16 20.08	-11 13 13.3	9.6240	0.6219n
31 8 22 59	8	8,8	+0 11.69	+2 32.6	19 21 34.57	-12 11 29.2	9.6062	0.6042n
Nov.								
1 8 38 38	10	8,8	+0 15.60	+1 2.6	19 27 3.56	-13 11 42.8	9.6255	0.6037n
2 8 5 58	12	8,8	-0 9.02	+1 4.3	19 32 28.84	-14 10 29.3	9.5805	0.5703n
5 9 39 58	14	10,10	+0 17.01	+0 4.4	19 50 15.76	-17 16 39.5	9.6812	0.6151n
6 8 21 2	15	8,8	+0 12.67	-2 42.9	19 55 59.82	-18 14 22.3	9.6008	0.5262n
7 8 26 53	16	8,8	-0 0.32	-2 55.6	20 2 12.30	-19 15 34.6	9.6087	0.5165n
8 8 33 1	18	8,8	+0 9.86	-4 58.1	20 8 33.27	-20 16 33.2	9.6168	0.5071n
16 9 13 8	20	11,-t	+1 56.45	...	21 3 40.37	...	9.6643	...
16 9 35 24	21	8,8	+0 0.57	+3 8.2	21 3 46.93	-27 57 17.3	9.6680	0.4635n
17 8 50 10	22	8,8	-0 4.59	-4 1.1	21 10 54.32	-28 47 7.9	9.6322	0.3448n
17 9 6 40	24	8,8	-0 21.61	+4 36.3	21 10 59.31	-28 47 39.4	9.6555	0.3823n
18 8 21 25	25	8,8	-0 4.03	-1 27.3	21 18 12.22	-29 35 30.7	9.5791	0.2442n
19 8 36 40	27	8,8	+0 21.75	+2 19.5	21 25 49.33	-30 24 7.8	9.6049	0.2517n

T.M. La Plata	*	Comp.	Cometa—Estrella		Pos. Aparente del Cometa		Log. $p \cdot \Delta$		
			$\Delta$ A.R.	$\Delta$ Decl.	A.R.	Decl.	en A.R.	en Decl.	
			h m s	° ' "	h m s	° ' "			
<b>Cometa Zinner-Giacobini, 1913e</b>									
1913									
Nov.	22 14 1 14	29	8,8	+0 2.96	+2 36.2	21 49 29.75	-32 38 50.6	9.7500	0.5441n
	25 9 1 6	30	10,10	+0 10.05	+2 50.2	22 12 7.76	-34 25 32.1	9.6276	0.1218n
	29 8 29 32	31	10,10	+0 1.63	+0 49.1	22 42 59.21	-36 17 34.1	9.5340	9.7237n
	29 9 13 41	32	10,-t	-3 42.44	...	22 43 13.41	...	9.6328	...
Dic.	2 9 15 24	33	10,10	+0 12.14	-3 7.9	23 6 4.75	-37 17 11.0	9.6206	9.9109n
	4 9 25 44	34	10,10	-0 20.82	-1 56.3	23 21 0.97	-37 45 3.2	9.6298	9.9032n
	4 9 57 4	35	16,-t	+1 21.95	...	23 21 10.38	...	9.6827	...
	5 9 35 3	36	12,-t	+4 6.75	...	23 28 21.82	...	9.6420	...
	5 10 37 27	37	10,10	+0 2.38	-0 5.5	23 28 40.51	-37 56 6.2	9.7296	0.2620n
	15 8 42 52	38	10,10	+0 12.23	+1 26.3	0 34 48.99	-38 1 22.1	9.4292	8.7227
	15 9 20 8	39	16,-t	-1 6.13	...	0 34 58.16	...	9.5489	...
	20 11 18 23	40	10,10	+0 10.80	-2 13.0	1 3 56.09	-37 10 29.7	9.7301	0.2983n
	20 12 12 30	41	12,-t	-2 58.43	...	1 4 8.22	...	9.7687	...
<b>Cometa Kritzinger, 1914a</b>									
1914									
Abril	1 14 25 27	42	8,8	-0 15.48	-5 32.5	16 21 26.62	-7 49 18.7	9.2049n	0.6056n
	2 15 19 36	44	8,8	-0 17.69	+5 33.8	16 24 45.77	-7 12 57.7	8.6690n	0.6090n
	3 14 3 27	46	8,8	+0 2.27	+4 39.1	16 27 50.64	-6 38 56.7	9.3015n	0.6245n
<b>Cometa Zlatinsky, 1914b</b>									
Junio	9 7 18 20	48	8,8	+0 17.48	+4 59.8	8 48 51.42	+3 48 31.1	9.5962	0.7220n
	10 6 19 41	50	8,8	+0 9.39	-8 33.0	8 52 15.76	+2 34 47.1	9.4937	0.7202n
	10 6 55 43	51	8,8	+0 25.03	+5 17.3	8 52 20.69	+2 33 2.5	9.5628	0.7170n
	12 6 26 26	52	8,8	+0 27.30	+3 55.8	8 58 27.33	+0 15 49.7	9.5111	0.7017n
<b>(704) Interamnia</b>									
Feb.	27 12 11 38	54	8,8	+0 14.26	-2 44.3	16 41 20.20	-35 2 34.9	9.7696n	0.6150n
	27 12 29 47	55	8,8	-0 8.43	-3 54.5	16 41 20.75	-35 2 36.1	9.7684n	0.5789n
	27 13 49 20	56	8,8	+0 37.64	-1 53.7	16 41 23.53	-35 2 42.8	9.7297n	0.3802n
	28 13 37 51	56	8,8	-0 11.39	-4 45.5	16 42 12.60	-35 5 34.6	9.7366n	0.4036n
Mar.	6 13 20 26	57	8,8	+0 28.81	-3 7.2	16 46 46.91	-35 22 0.5	9.7370n	0.3951n
	7 13 47 28	58	8,9	-0 15.74	-5 38.1	16 47 29.92	-35 24 38.4	9.7087n	0.2973n
	8 13 18 43	58	8,10	+0 25.48	-8 14.0	16 48 11.18	-35 27 14.5	9.7336n	0.3794n
	19 13 16 12	59	10,10	-0 27.75	-5 10.9	16 54 26.44	-35 53 28.9	9.7010n	0.2532n
	19 13 51 13	60	8,9	-0 27.91	+5 45.2	16 54 27.28	-35 53 36.4	9.6513n	0.1045n
	19 14 18 38	59	8,8	-0 26.67	-5 18.7	16 54 27.52	-35 53 36.7	9.5999n	9.9590n
	20 13 50 38	59	8,8	-0 0.27	-7 26.3	16 54 53.96	-35 55 44.4	9.6466n	0.0889n
	20 14 0 55	60	8,8	-0 0.82	+3 32.2	16 54 54.41	-35 55 49.5	9.6089n	9.9815n
	31 12 58 7	61	8,8	-0 21.59	+7 0.4	16 58 19.00	-36 16 56.6	9.6689n	0.1354n
Abril	1 15 18 10	61	10,9	-0 10.66	+5 12.6	16 58 29.97	-36 18 44.5	9.1978n	8.9625
	3 15 2 51	61	8,8	+0 5.03	+2 6.1	16 58 45.73	-36 21 51.1	9.2484n	8.7716
	5 12 42 10	62	20,8t	-1 12.70	+3 43.3	16 58 55.47	-36 24 36.5	9.6649n	0.1160n
	19 12 1 22	63	8,8	+0 7.39	+7 4.2	16 57 17.11	-36 37 18.5	9.6394n	0.0241n
	19 12 26 16	64	8,8	+0 3.78	-2 5.9	16 57 16.61	-36 37 19.2	9.5893n	9.8656n
	23 12 37 54	65	8,8	+0 23.04	-2 56.7	16 55 52.80	-36 37 57.1	9.5159n	9.6111n
	27 12 27 23	66	16,8t	-5 52.99	+0 31.2	16 54 5.44	-36 36 56.4	9.4948n	9.5320n
Mayo	1 11 52 28	67	8,8	+0 6.61	+8 15.9	16 51 55.93	-36 34 7.4	9.5403n	9.7193n
	7 11 21 19	68	8,8	+0 18.55	+4 57.0	16 48 1.86	-36 26 11.8	9.5524n	9.7482n
	8 11 29 6	68	8,8	-0 25.12	+6 45.5	16 47 18.21	-36 24 23.3	9.5183n	9.6556n
	23 9 55 28	69	8,8	+0 8.17	-6 10.2	16 34 40.46	-35 40 24.5	9.5717n	9.8991n
	25 10 24 41	70	16,8t	-2 12.87	-0 32.7	16 32 47.09	-35 31 53.9	9.4608n	9.6134n
	26 10 14 16	71	16,8t	+2 14.26	+5 27.4	16 31 50.95	-35 27 28.2	9.4786n	9.6736n
	28 9 42 34	72	8,8	+0 12.00	+4 59.2	16 29 58.50	-35 18 21.9	9.5414n	9.8532n
	28 10 14 58	73	18,8t	+1 41.71	+3 42.4	16 29 57.23	-35 18 12.4	9.4424n	9.6017n



T.M. La Plata	*	Comp.	Cometa—Estrella		Pos. Aparente del Cometa		Log. p'Δ	
			Δ A.R.	Δ Decl.	A.R.	Decl.	en A.R.	en Decl.
			h m s	u s	l "	h m s	o l "	

(704) *Interamnia*

1914		*	Comp.	Cometa—Estrella		Pos. Aparente del Cometa		Log. p'Δ	
h	m s			Δ A.R.	Δ Decl.	A.R.	Decl.	en A.R.	en Decl.
Junio	10 13 51 58	74	8,8	+0 29.51	+0 38.1	16 17 41.45	-34 4 20.6	9.5925	0.0620n
	11 8 23 10	75	8,8	+0 6.00	+9 18.9	16 17 0.68	-33 59 25.9	9.5628n	0.0052n
	11 8 40 12	76	8,8	+0 15.32	+5 46.9	16 17 0.19	-33 59 21.1	9.5195n	9.9199n
	24 12 57 2	77	16,8t	+2 33.40	-3 31.1	16 6 39.89	-32 29 2.2	9.6067n	0.1714n
	25 7 33 5	78	8,8	+0 22.14	+1 44.9	16 6 9.47	-32 23 30.2	9.5151n	0.0248n
Julio	3 7 38 19	79	8,8	-0 15.91	-4 43.3	16 1 37.94	-31 26 18.6	9.3725n	9.9286n
	14 12 14 31	80	8,8	+0 4.47	-7 30.0	15 57 48.35	-30 9 15.5	9.6662	0.3650n
	15 7 42 56	80	4,8	-0 4.89	-2 10.9	15 57 38.98	-30 3 56.4	9.0145n	9.8905n

Cometa Mellish, 1917a

1917		*	Comp.	Cometa—Estrella		Pos. Aparente del Cometa		Log. p'Δ	
h	m s			Δ A.R.	Δ Decl.	A.R.	Decl.	en A.R.	en Decl.
Abril	21 17 38 12	81	8,8	+0 18.31	+0 19.6	0 46 56.83	- 3 26 9.7	9.6728n	0.6905n
	21 17 54 45	82	8,—t	-0 21.30	...	0 46 58.29	...	9.6645n	...
	21 18 0 42	82	—,5t	...	+8 45.2	...	- 3 26 49.4	...	0.6868n
	25 17 21 55	83	8,8	+0 0.32	-7 3.6	0 55 52.02	- 5 44 47.8	9.6778n	0.6860n
	26 17 29 55	84	8,9	-0 33.53	+4 13.0	0 57 59.28	- 6 12 16.2	9.6744n	0.6817n
Mayo	1 16 59 46	87	10,10	-0 31.97	+2 50.0	1 9 14.06	- 8 0 44.1	9.6834n	0.6839n
	1 17 26 0	88	9,8	+0 31.47	-3 31.0	1 9 16.50	- 8 1 3.5	9.6741n	0.6736n
	2 16 55 0	89	—,5	...	-2 27.5	...	- 8 18 26.4	...	0.6844n
	2 16 58 59	89	9,—	+0 19.31	...	1 11 25.11	...	9.6835n	...
	19 17 19 12	92	8,6t	+4 2.72	-2 13.9	1 44 23.24	-11 45 2.2	9.6618n	0.6406n
	20 16 48 15	93	10,10	+0 0.67	+1 56.2	1 46 1.81	-11 54 23.6	9.6791n	0.6570n
	20 17 15 53	94	—,4t	...	+0 21.2	...	-11 54 34.4	...	0.6403n
	22 16 55 45	95	10,10	-0 19.86	+3 28.6	1 49 17.72	-12 13 24.4	9.6733n	0.6480n
	22 17 48 31	96	12,8t	-0 56.30	+1 40.3	1 49 21.03	-12 13 46.0	9.6293n	0.6153n
	22 17 48 31	97	12,8t	+1 7.66	-1 33.8	1 49 21.12	-12 13 43.4	9.6293n	0.6153n

MEAN PLACES OF THE COMPARISON STARS

LUGARES MEDIOS DE LAS ESTRELLAS DE COMPARACIÓN

*	A. R. 1913.0	Red. a lug. ap.	Decl. 1913.0	Red. a lug. ap.	Autoridad
1....	23 <sup>h</sup> 47 <sup>m</sup> 53 <sup>s</sup> .19	+3 <sup>s</sup> .48	+ 0°58' 28".2	+22".1	(10.5) Conexiones con *2.
2....	23 47 49.33	+3.48	+ 1 0 49.8	+22.1	A. G. Nicolajew, 5901.
3....	19 6 17.50	+2.34	- 9 18 35.6	- 0.4	Conexión con *4 por Hussey.
4....	19 6 35.32	+2.34	- 9 15 39.7	- 0.4	A. G. Wien-Ottakring, 6607.
5....	19 11 13.14	+2.38	-10 16 24.4	- 0.3	(10.5) Conexión con *6 por Hussey.
6....	19 11 36.14	+2.38	-10 14 10.9	- 0.3	A. G. Cambridge, U. S., 6691.
7....	19 16 38.44	+2.41	-11 12 17.4	- 0.2	A. G. Cambridge, U. S., 6747.
8....	19 21 20.43	+2.45	-12 14 1.6	- 0.2	(SD. —12° 53'97") Conexión con *9 por Hussey.
9....	19 23 20.99	+2.46	-12 19 10.2	0.0	A. G. Cambridge, U. S., 6802.
10....	19 26 45.48	+2.48	-13 12 45.3	- 0.1	(10.5) Conexión con *11 por Hussey.
11....	19 26 2.55	+2.48	-13 9 50.8	- 0.1	A. G. Cambridge, U. S., 6830.
12....	19 32 35.33	+2.53	-14 11 33.7	+ 0.1	(SD. - 14° 54'77"). Conexión con *13 por Hussey.

*	A. R. 1913.0	Red. a lug. ap.	Decl. 1913.0	Red. a lug. ap.	Autoridad
13....	19 <sup>h</sup> 32 <sup>m</sup> 54 <sup>s</sup> 44	+2.53	-14° 9' 7" 0	+ 0.1	A. G. Washington, 7369.
14....	19 49 56.09	+2.66	-17 16 44.1	+ 0.2	A. G. Washington, 7484.
15....	19 55 44.45	+2.70	-18 11 39.7	+ 0.3	Bordeaux, 6023.
16....	20 2 9.88	+2.74	-19 12 39.4	+ 0.4	(11.5) Conexión con *17.
17....	20 4 30.99	+2.76	-19 9 18.1	+ 0.6	Bordeaux, 6061.
18....	20 8 20.62	+2.79	-20 11 35.6	+ 0.5	(10.5) Conexión con *19 por Hussey.
19....	20 8 20.18	+2.79	-20 8 58.7	+ 0.5	Cincinnati Zone Cat., 3359.
20....	21 1 40.76	+3.16	-28 0 43.8	+ 1.8	Catálogo General Argentino, 28937.
21....	21 3 43.19	+3.17	-28 0 27.5	+ 2.0	(C6D -28° 17134). Conexión con *20.
22....	21 10 55.69	+3.22	-28 43 9.1	+ 2.3	(11.0) Conexión con *23.
23....	21 11 12.34	+3.22	-28 37 58.7	+ 2.3	Córdoba, Zonas Est., XXI, 269.
24....	21 11 17.70	+3.22	-28 52 17.9	+ 2.2	Córdoba, Zonas Est., XXI, 272.
25....	21 18 12.98	+3.27	-29 34 5.9	+ 2.5	(C6D -29° 17743). Conexión con *26 por Hussey.
26....	21 16 39.37	+3.26	-29 32 7.6	+ 2.4	Catálogo General Argentino, 29281.
27....	21 25 24.27	+3.31	-30 26 30.0	+ 2.7	(C6D -30° 18655). Conexión con *28 por Hussey.
28....	21 24 54.82	+3.31	-30 30 1.0	+ 2.6	Córdoba, Zonas Est., XXI, 703.
29....	21 49 23.34	+3.45	-32 41 30.3	+ 3.5	Córdoba, (Comunicado).
30....	22 11 54.15	+3.56	-34 28 26.6	+ 4.3	Catálogo General Argentino, 30416.
31....	22 42 53.91	+3.67	-36 18 29.0	+ 5.8	(C6D -36° 15558). Conexión con *32.
32....	22 46 52.16	+3.69	-36 21 1.1	+ 6.0	Catálogo General Argentino, 31110.
33....	23 5 48.87	+3.74	-37 14 9.9	+ 6.8	Córdoba, Zonas Est., XXIII, 95.
34....	23 21 18.01	+3.78	-37 43 14.3	+ 7.4	Córdoba, Zonas Est., XXIII, 518.
35....	23 19 44.66	+3.77	-37 40 41.8	+ 7.3	Catálogo General Argentino, 31707.
36....	23 24 11.32	+3.75	-37 52 36.3	+ 7.4	Catálogo General Argentino, 31778.
37....	23 28 34.34	+3.79	-37 56 8.3	+ 7.6	(11.0) Conexión con 36*.
38....	0 34 32.94	+3.82	-38 2 58.3	+ 9.9	Conexión con *39.
39....	0 36 0.47	+3.82	-38 3 29.2	+ 9.9	Córdoba, Zonas Est., O, 911.
40....	1 3 41.74	+3.55	-37 8 27.3	+10.6	(C6D -37° 415) Conexión con *41.
41....	1 7 3.06	+3.59	-37 6 0.2	+10.7	Catálogo General Argentino, 1103.
	1914.0		1914.0		
42....	16 21 40.28	+1.82	- 7 43 29.2	-17.0	(10.0) Conexión con *43.
43....	16 21 56.59	+1.82	- 7 39 26.4	-17.0	A. G. Wien-Ottakring, 5702.
44....	16 25 1.63	+1.83	- 7 18 14.4	-17.1	(10.5) Conexión con *45.
45....	16 25 51.87	+1.83	- 7 19 40.1	-17.1	A. G. Wien-Ottakring, 5715.
46....	16 27 46.52	+1.85	- 6 43 18.6	-17.2	(11.0) Conexión con *47.
47....	16 28 36.01	+1.85	- 6 46 3.0	-17.2	A. G. Wien-Ottakring, 5728.
48....	8 48 33.03	+0.91	+ 3 43 33.3	- 2.0	(BD. + 3° 2083) Conexión con *49.
49....	8 51 36.52	+0.92	+ 3 37 36.9	- 2.2	A. G. Albany, 3599.
50....	8 52 5.47	+0.90	+ 2 43 22.5	- 2.4	A. G. Albany, 3604.
51....	8 51 54.76	+0.90	+ 2 27 47.7	- 2.5	A. G. Albany, 3602.
52....	8 58 9.05	+0.88	+ 0 11 57.2	- 3.3	(12.5) Conexión con *53.
53....	8 57 54.77	+0.88	+ 0 11 20.6	- 3.3	A. G. Nicolajew, 2778.
54....	16 41 5.13	+0.81	-34 59 44.7	- 5.9	Córdoba, Zonas Est., XVI, 2687.
55....	16 41 28.38	+0.80	-34 58 35.7	- 5.9	Córdoba, Zonas Est., XVI, 2715.
56....	16 22 0.37	+0.80	-35 0 43.2	- 5.9	Córdoba, Zonas Est., XVI, 2755.
57....	16 26 17.05	+0.84	-35 18 47.3	- 6.0	Córdoba, Zonas Est., XVI, 3065.
58....	16 27 44.57	+1.09	-35 18 54.2	- 6.1	Córdoba, Zonas Est., XVI, 3180.
59....	16 44 52.68	+1.13	-35 48 11.4	- 6.3	Catálogo General Argentino, 23002.
60....	16 44 53.68	+1.51	-35 59 15.0	- 6.6	Córdoba, Zonas Est., XVI, 3739.
61....	16 68 38.66	+1.55	-36 23 49.9	- 6.7	Córdoba, Zonas Est., XVI, 4001.
62....	17 0 6.06	+1.93	-36 28 12.3	- 7.1	Catálogo General Argentino, 23119.
63....	16 57 7.13	+2.04	-36 44 14.0	- 7.3	Córdoba, Zonas Est., XVI, 3888.
64....	16 57 10.25	+2.11	-36 35 4.6	- 7.5	(C6D. -36° 11169). Conexión con *66.
65....	16 55 27.06	+2.59	-36 34 51.3	- 8.7	(C6D. -36° 11150). Conexión con *66.
66....	16 59 55.62	+2.58	-36 37 18.6	- 8.7	Catálogo General Argentino, 23113.
67....	16 51 46.38	+2.70	-36 42 13.6	- 9.1	Córdoba, Zonas Est., XVI, 3499.
68....	16 27 40.21	+2.81	-36 30 57.9	- 9.0	Córdoba, Zonas Est., XVI, 3169.
		+2.94		- 9.7	
		+3.10		-10.9	
		+3.12		-10.9	

*	A. R. 1914.0		Rep. a lug. ap.	Decl. 1914.0		Rep. a lug. ap.	Autoridad
	h	m		h	m		
69....	16 <sup>h</sup> 24 <sup>m</sup> 28 <sup>s</sup> 88		+3 <sup>s</sup> 41	-35° 34' 0" 9		-13" 4	(Cód. -35° 11064). Conexión con * 70.
70....	16 34 56.52		+3.44	-35 31 7.7		-13.5	Catálogo General Argentino, 22546.
71....	16 29 33.24		+3.45	-35 32 41.6		-14.0	Catálogo General Argentino, 22430.
72....	16 29 43.02		+3.48	-35 23 6.8		-14.3	Córdoba, Zonas Est., XVI, 1867.
73....	16 28 12.04		+3.48	-35 21 40.4		-14.4	Catálogo General Argentino, 22407.
74....	16 17 8.38		+3.56	-34 4 42.2		-16.5	(Cód. -33° 11137). Conexión con *75 y *76.
75....	16 16 51.12		+3.56	-34 8 28.2		-16.6	Córdoba, Zonas Est., XVI, 1008.
76....	16 16 41.31		+3.56	-34 4 51.4		-16.6	Córdoba, Zonas Est., XVI, 996, rechazando la A. R. de zona 706.
77....	16 4 2.98		+3.51	-32 25 12.9		-18.2	Catálogo General Argentino, 21875.
78....	16 5 43.81		+3.52	-32 24 56.9		-18.2	(Cód. -32° 11476). Conexión con *77.
79....	16 1 50.39		+3.46	-31 21 16.7		-18.6	Córdoba, Zonas Est., XV, 4152.
80....	15 57 40.53		-3.35 -3.34	-30 1 26.4		-19.1 -19.1	Catálogo General Argentino, 21732.
	1917.0			1917.0			
81....	0 46 37.82		+0.70	- 3 26 35.4		+ 6.1	(SD -3° 110). Conexión con *82.
82....	0 47 18.89		+0.76	- 3 35 40.7		+ 6.1	A. G. Strassburg, 186. (= C. G. A. 771).
83....	0 55 50.97		+0.73	- 5 37 51.2		+ 7.0	A. G. Strassburg, 217. (= A. G. Wien Ott., 204).
84....	0 58 32.07		+0.74	- 6 16 36.4		+ 7.2	(SD. -6° 192). Conexión con *85 y *86.
85....	0 54 33.49		+0.75	- 6 19 42.8		+ 7.3	A. G. Wien-Ottakring, 198. (= C. G. A. 899).
86....	1 1 33.14		+0.73	- 6 18 2.3		+ 7.2	A. G. Wien-Ottakring, 222.
87....	1 9 45.26		+0.77	- 8 3 42.3		+ 8.2	A. G. Wien-Ottakring, 250. (= C. G. A. 1142).
88....	1 8 44.26		+0.77	- 7 57 40.7		+ 8.2	(SD. -8° 212). Conexión con *87.
89....	1 11 5.01		+0.79	- 8 16 7.2		+ 8.3	(SD. -8° 221). Conexión con *98 y en A. R. con *91.
90....	1 10 12.92		+0.79	- 8 22 13.5		+ 8.3	A. G. Wien-Ottakring, 252. (= C. G. A. 1149).
91....	1 10 11.30		+0.79	- 8 21 30.4		+ 8.3	A. G. Wien-Ottakring, 251. (= C. G. A. 1148).
92....	1 40 19.55		+0.97	-11 42 59.9		+11.6	A. G. Cambridge, U. S., 385.
93....	1 46 0.18		+0.96	-11 56 31.4		+11.6	(11.0) Conexión con *94.
94....	1 50 49.90		+0.94	-11 55 7.0		+11.4	A. G. Cambridge, U. S., 431.
95....	1 49 36.60		+0.98	-12 17 4.1		+11.1	(10.5) Conexión con *96 y *97.
96....	1 50 16.35		+0.98	-12 15 37.3		+11.0	A. G. Cambridge, U. S., 429.
97....	1 48 12.47		+0.99	-12 12 20.7		+11.1	A. G. Cambridge, U. S., 421.

DOUBLY CONNECTED AND UNUSED STARS

ESTRELLAS DOBLEMENTE OBSERVADAS O NO USADAS

1913	Estrella		Comp.	Aparentes*		Lugar Medio Deducido		Notas
	Observada	de Ref.		Δ A. R.	Δ Decl.	A. R. 1913.0	Decl. 1913.0	
Sept. 9	*1	*2	? ?	+0 <sup>m</sup> 3 <sup>s</sup> 91	-2' 21" 0	23 <sup>h</sup> 47 <sup>m</sup> 53 <sup>s</sup> 24	+ 0° 58' 28" 8	Hussey Dawson
9	*1	*2	10,10	+0 3.80	-2 22.2	23 47 53.13	+ 0 58 27.6	
Dic. 4	*34	*35	16,4t	+1 33.10	-2 31.4	23 21 17.75	-37 43 13.3	
	1914.0					1914.0	1914.0	
Abr. 5	*61	*62	20,8t	-1 27.49	+4 22.5	16 58 38.57	-36 23 49.7	
Jun. 10	*74	*75	4,4	+0 17.19	+3 45.7	16 17 8.31	-34 4 42.5	
10	*74	*76	4,4	+0 27.15	+0 9.6	16 17 8.46	-34 4 41.8	
	1917.0					1917.0	1917.0	
Oct. 5	*84	*85	12,6t	+3 58.56	+3 6.8	0 58 32.05	- 6 16 35.9	

1917	Estrella		Comp.	Aparentes		Lugar Medio Deducido		Notas
	Observada	de Ref.		$\Delta$ A. R.	$\Delta$ Decl.	A. R. 1917.0	Decl. 1917.0	
Oct. 5	*84	*86	12,6t	-3 1.05	+1 25.5	0 58 32.09	- 6 16 36.8	
7	- 8°212	*87	10,8	-0 27.04	+2 56.4	1 9 18.22	- 8 0 45.9	
7	*89	*90	20,10t	+0 52.10	+6 6.3	1 11 5.02	- 8 16 7.2	
7	*89	*91	20,—t	+0 53.70	...	1 11 5.00	...	
May. 20	-12°347	*94	4,3t	-2 17.15	+0 15.9	1 48 32.74	-11 55 1.1	
22	*95	*96	12,10t	-0 39.82	-1 27.3	1 49 36.53	-12 17 4.7	
22	*95	*97	12,3t	+1 24.19	-4 41.6:	1 49 36.67	-12 17 2.3:	

## PHENOMENA

## FENÓMENOS

### OCCULTATIONS BY THE MOON

### OCULTACIONES POR LA LUNA

Fecha	Fenómeno	Hora Sidérea	Hora Media
1913. Marzo, 26	Antares. Desapareció al borde obscuro. Apareció al borde brillante.	12 <sup>h</sup> 16 <sup>m</sup> 17. <sup>s</sup> 9 13 10 26.0	12 <sup>h</sup> 0 <sup>m</sup> 23. <sup>s</sup> 7 12 54 22.9
1917. Enero, 8	<sup>1</sup> Saturno. Borde exterior del anillo exterior, tocó. Borde exterior del anillo exterior, desapareció. Borde exterior del anillo interior, tocó. Borde interior del anillo interior, tocó. Borde interior del anillo interior, desapareció. Disco del planeta, tocó. Disco del planeta, desapareció.	8 1 4 8 7 22 8 1 38 8 2 4 8 6 32 8 2 36 8 5 45	12 48 28 12 54 45 12 49 2 12 49 28 12 53 55 12 50 0 12 53 8

### SATELLITES OF JUPITER

### SATÉLITES DE JÚPITER

Fecha	Fenómeno	Hora Sidérea	Hora Media
1914, Junio 10	I, Ec. Dis.	16 <sup>h</sup> 2 <sup>m</sup> 8. <sup>s</sup> 6	10 <sup>h</sup> 47 <sup>m</sup> 45. <sup>s</sup>
11	III, Ec. Dis.	18 45 10.8	13 26 25
24	I, Ec. Dis.	20 46 37.7	14 36 25
25	II, Ec. Dis.	21 3 3.5	14 48 49
Julio 13	II, Ec. Dis.	16 38 47.0	6 14 32

<sup>1</sup> Perhaps these times should all be increased one minute.

<sup>1</sup> Tal vez necesitan todas estas observaciones una corrección de + 1<sup>m</sup>.



UNIVERSIDAD NACIONAL DE LA PLATA  
PUBLICACIONES DEL OBSERVATORIO ASTRONÓMICO; TOMO IV (Parte IIª)

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RESULTADO  
DE LAS  
OBSERVACIONES CON LA ECUATORIAL  
DE 433 MILÍMETROS DE ABERTURA

EFFECTUADAS DE 1918.0 A 1921.5

POR

BERNHARD H. DAWSON



LA PLATA  
OBSERVATORIO ASTRONÓMICO

—  
1922





## ERRATAS

Since the publication of Part I and during the printing of Part II, the following errata have been noted. Many of the earlier ones can be attributed to my inexperience at the beginning of the work.

I am indebted to Mr. Innes for a large proportion of the corrections and also for the correction of many other points which might otherwise have remained erroneous in Part II.

Después de la publicación de Parte I y durante la impresión de Parte II, se han notado los siguientes errores. Muchos de ellos pueden imputarse a mi falta de práctica al principio del trabajo.

Estoy agradecido al señor Innes por buena proporción de las correcciones aquí enumeradas, como también de varias otras que han evitado posibles errores en la Parte II.

Página	Estrella	En	Dice	Debe leerse
17	<i>h</i> 3348	C.P.D.	—60°6;	—60°7;
24	<i>h</i> 3517	C.P.D.	—69°180;	—69°130;
27	<i>h</i> 3583	C.P.D.	—60°267;	—60°263;
27	<i>h</i> 3610	C.P.D.	—63°269; 10.1	—63°270; 9.1
29	<i>h</i> 3662AD	—	AD	BD
30	<i>h</i> 3679	C.P.D.	—62°372; 6.9	R Doradus; Var.
30	<i>h</i> 3684	C.P.D.	Anon.	—67°336; 9.4
30	<i>h</i> 3686	Nota	M	N
31	<i>h</i> 3685	Nota	M	N
33	<i>h</i> 3787	C.P.D.	—54°857 + 6;	—54°867 + 6;
35	<i>h</i> 3831	Nota	A	F
36	Δ 26	C.P.D.	—65°585 + 6;	—65°565 + 6;
37	<i>h</i> 3887	—	—	Ver nota 169.
37	I 181	Promedio	244°1	248°1
38	<i>h</i> 3920	C.P.D.	—45°1031	—48°1031
38	<i>h</i> 3920	Nota	M	F
38	<i>h</i> 3924	C.P.D.	—60°744 + 2;	—60°744 + 3;
40	Rü 6	—	—	También = Δ 44.
43	<i>h</i> 4023	Nota	N	M
43	Hargrave	C.P.D.	—48°1373; 4.3	V Puppis; Var.
44	<i>h</i> 4032	C.P.D.	—46°1984;	—46°1983 + 2;
44	<i>h</i> 4043	C.P.D.	—46°2059;	—46°2061 + 59;
45	<i>h</i> 4045	Decl.	—50°60'	—50°6'
46	Bris 2018	C.P.D.	—71°677 + 8;	z Volantis;
46	Bris 2018	AC	AC ... (5.8 ... 8.5)	BC ... (6.0 ... 8.5)
54	Có.	—	Có.;	Rus 132;
57	G 152	—	G 152 = Rus 153;	Bris 3133 = Rus 153;
59	<i>h</i> 4367	C.P.D.	—55°3807 <sup>2</sup> ;	—55°3810;
67	<i>h</i> 4547	C.P.D.	—60°4273;	c Crucis
68	δ 13	—	δ 13;	Có.;

Página	Estrella	En	Dice	Debe leerse
68	Có.	C.P.D.	-57°2852 + 1;	-57°5852 + 1;
71	Delavan 6	—	Delavan 6;	Có.;
71	h 4649	Mag.	8:2	9.2
72	h 4651	Nota	93	94
72	Pollock	—	Pollock;	Có. = Pollock 3;
77	h 4766	—	h 4766;	Δ 134 = h4766;
79	h 4805	Nota	N	R?
85	h 4936	C.P.D.	-46°5526;	-46°8526;
90	h 5048	Promedio	256°0	356°0
91	h 5058	C.P.D.	-50°10727;	-50°10827;
92	Hg (317)	Promedio	(7.7 ... 8.7)	(8.2 ... 8.7)
95	h 5143	C.P.D.	-46°5800;	-46°9800;
98	h 5217	—	—	Ver nota 223.
99	h 5258	Promedio	1913.30	1913.77
102	Δ 238	C.P.D.	75°1738;	-75°1748;
105	J 238	—	J 238 = β 751;	J 238;
107	h 5420	C.P.D.	-53°10523;	-53°10522;
120	—	línea 22	de comparación	observada
128	-60°952	Δ A.R.	-34°51	+34°51
133	-58°3108	* Ref.	-58°3108	-58°3116
134	-58°3198	Δ Decl.	+3'40"5	+0'22"0
135	-60°3147	Δ Decl.	+4 27.8	+4 39.4
139	(704)	Junio 24	log p.Δ en A.R.; 9.6067n	9.6067
140	61	A.R.	16°68'38"66	16°58'38"66
153	h 3494	20.987	Imágenes; 2	2½
154	h 3527	—	h 3527 =	h 3537 =
155	h 3581	Nota	168	150
164	Hargrave	C.P.D.	-75°386;	-75°376;
169	h 4047	Posición	7°24'2"2; -88°48'	7°21'34"2; -88°49'
169	h 3975	Nota	182	R?
173	h 4099	C.P.D.	-39°2448 + 9;	-39°2448 + 7;
176	h 5195	—	h 5195;	h 4195;
191	h 4539	—	h 4539;	* h 4539;
211	Δ 219 BC	—	BC = λ 219	BC = λ 344
231	Rigel	—	β 553	β 555
236	h 2421	Nota	236	236 a
169	Piazzi = Δ 49	Agréguese la medida	19.938 53°2 9"08	5.8 2½ 370
170	Δ 56	»	19.938 176.8 49.86	6.3 2 370

## INTRODUCTION

The present publication represents a continuation of the same lines of work as contained in Part I of this volume, with the slight variations here noted.

The chief program in double star observing continued to be the stars from Herschel's Cape list, south of declination  $-30^\circ$ , until that list was practically completed. In 1918 observations were begun, employing the nights of inferior definition, on a secondary program, made up of stars from Burnham's *General Catalogue* which had not been identified in the *Durchmusterungen* or other star catalogs. Additional known pairs were later included in the observing list, and in 1920 a systematic search for new pairs was begun. The work now completed, as published in the two parts of this volume, represents over 7500 measures, and embraces :

1. All Herschel stars south of  $-30^\circ$ , irrespective of previous measurement, except a few that could not be found or that appeared single.

2. All stars of Herschel's Cape list north of  $-30^\circ$  that have not been measured by other observers since the publication of  $\beta$ . G. C.

3. All stars of  $\beta$ . G. C. south of  $-21^\circ 40'$  remaining unidentified at the beginning of 1918.

## INTRODUCCIÓN

La publicación actual representa una continuación de los trabajos contenidos en la primera parte de este tomo, con las pequeñas modificaciones aquí enumeradas.

El programa principal en la observación de estrellas dobles continuó siendo el de las estrellas de Herschel al sur de la declinación  $-30^\circ$  hasta la casi terminación de esa lista. En 1918 se empezó, en noches de imágenes inferiores, la observación de un programa secundario formado de las estrellas del *General Catalogue* de Burnham, que no habían sido identificadas en las *Durchmusterungen* u otros catálogos. Después se amplió la lista con otras estrellas conocidas, y en 1920 se empezó la busca sistemática de pares nuevos. El trabajo ya realizado, contenido en las dos partes de este tomo, representa más de 7500 medidas y contiene :

- 1° Todas las estrellas de Herschel al sur de los  $-30^\circ$ , exceptuando unas pocas que era imposible encontrar o que aparecían sin compañera.

- 2° Todas las estrellas descubiertas por Herschel en el Cabo de Buena Esperanza, situadas al norte de  $-30^\circ$  y que no habían sido medidas por otro observador después de 1906.

- 3° Todas las estrellas del *General Catalogue* al sur de  $-21^\circ 40'$  que quedaban sin identificar a principios de 1918.

4. All Burnham's stars south of  $-30^\circ$ .

5. Many miscellaneous known pairs.

6. 111 new pairs, about half of them picked up accidentally, the others being the first results of the systematic search.

The differences which may be noted in the methods of observing between Parts I and II are: All the measures in the second part have been made with the Warner and Swasey micrometer and a larger proportion have been made within two hours of the meridian. The vast majority of the measures have five or six settings in angle and four double distances, a less number being considered sufficient only in case of close agreement *inter se* concurrent with excellent seeing. In the settings in distance, the line joining the eyes has been kept perpendicular to the micrometer wires whenever possible, and otherwise parallel to them, as before, but in the angle settings part of them have been made in one position and the rest in the other whenever conditions did not distinctly favor one of them.

In the arrangement of the results the same form has been employed. An asterisk before the name of the star indicates that it is also contained in Part I, but that the mean results here given do not include the previous measures. An asterisk before a mean result signifies that it is formed from the measures given in Part II combined with others in Part I, and that the mean given in Part I is to be struck out.

A few abbreviations for observers, not given in Part I, have been used, among them the letter  $\delta$  to designate my own stars. I trust the others will be understood without indexing them. The note « N » is not to be taken in too strict a sense, for I have not compared *all* previous lists of measures, and a few will probably have escaped my attention, as did several in Part I.

4° Todas las estrellas de Burnham al sur de los  $-30^\circ$ .

5° Un gran número de otros pares conocidos.

6° 111 pares nuevos, de los cuales cerca de la mitad fueron encontrados en el curso de los otros trabajos, y los demás representan los primeros resultados de la busca sistemática.

Pueden anotarse las siguientes diferencias de método de observación entre la primera parte y ésta. Todas las medidas de la publicación actual fueron efectuadas con el micrómetro Warner and Swasey, y esta vez, en mayor proporción que antes, se han efectuado dentro de dos horas del meridiano. La gran mayoría de las medidas han consistido en cinco o seis lecturas en ángulo y cuatro distancias dobles, aceptándose menor número como suficientes, únicamente en el caso de ser a la vez muy concordantes entre sí y hechas con excelentes imágenes. Las lecturas en distancias se han hecho como antes, pero las de ángulo han sido divididas entre las dos posiciones de los ojos cuando la posición no favorecía marcadamente una de ellas.

Se ha empleado la misma disposición de los resultados. Un asterisco delante del nombre de la estrella indica que también figura en la Parte I, pero que los nuevos promedios no incluyen aquellos resultados; si está delante del promedio, significa que éste incluye también las medidas de la primera parte y que el promedio anterior debe tacharse.

He empleado algunas abreviaciones que no figuran en la primera parte, entre ellas la letra  $\delta$  para designar las estrellas mías. Espero que las otras se entenderán sin explicaciones. La nota « N » no quiere decir estrictamente que no hay otras medidas sino que no he visto otras en las listas que he comparado, y algunas pueden haber pasado desapercibidas.

In the star connections the methods of observing remained the same except that the limit of five hours from the meridian was changed to three. In the reductions, the apparent differences of right ascension and declination were reduced to 1925.0 instead of to the beginning of the year of observation. The connections of 1917 were rereduced and the new results are given in a separate table.

The eclipses of Jupiter's satellites were observed at the request of Mr. Innes. All except the first few were observed with 370 magnification and with Jupiter occulted near the middle of the field of view.

Finally I wish to acknowledge my indebtedness to Mr. Innes and to the late Prof. Doolittle for checking the new pairs picked up and also to the latter for the observing lists north of  $-30^{\circ}$ . I also express my thanks to Mr. Numa Tapia for assistance in many parts of the work, especially as recorder in the dome, in the reduction of the star connections and in reading the proof, which has again been checked directly against the observing books.

En las conexiones de estrellas, los métodos de observación han sido los mismos, excepto en lo que se refiere al ángulo horario, el cual se ha limitado a tres horas en vez de cinco. En las reducciones, las diferencias aparentes de ascensión recta y de declinación se han reducido a 1925.0 en vez de al principio del año de observación. También se han reducido a 1925.0 las conexiones de 1917, poniendo los resultados en un cuadro aparte.

Los eclipses de satélites de Júpiter se observaron a pedido del señor Innes. Después de los primeros, todos se han observado con aumento de 370, ocultando el disco del planeta con un diafragma en el campo visual.

Por último, quiero expresar mi agradecimiento al señor Innes y al malogrado profesor Doolittle por su ayuda en verificar la novedad de los pares encontrados, y a éste por los programas de estrellas al norte de  $-30^{\circ}$ . También quiero expresar mi agradecimiento al señor Numa Tapia por su ayuda en muchas partes del trabajo, especialmente en apuntar las observaciones, en la reducción de las conexiones y en la lectura de las pruebas, las que nuevamente se han comparado directamente con los cuadernos de observación.



# MICROMETRIC MEASURES OF DOUBLE STARS

## MEDIDAS MICROMÉTRICAS DE ESTRELLAS DOBLES

*h* 5442 = Rus. 1;  $-78^{\circ} 1$ ; 8.6

A.R.  $0^h 1^m 17^s$ ; Decl.  $-78^{\circ} 11'$

18.767	63.9	24.78	1.9	$1\frac{1}{2}$	370
18.851	63.4	24.86	2.8	2	370
18.81	63.6	24.82	(8.6 ... 11.9)		F

*h* 3353;  $-75^{\circ} 15$ ; 8.9

A.R.  $0^h 7^m 56^s$ ; Decl.  $-75^{\circ} 23'$

17.852	295.9	22.95	0.2	2	370
17.945	296.8	23.19	3.3	$2\frac{1}{2}$	370
17.964	296.6	23.12	3.8	2	370
17.92	296.4	23.09	(8.8 ... 11.6)		N

*h* 3354;  $-36^{\circ} 20 + 19$ ;  $10.2 + 10.4$

A.R.  $0^h 8^m 23^s$ ; Decl.  $-36^{\circ} 46'$

19.755	334.9	17.46	2.7	$2\frac{1}{2}$	370
19.758	334.6	17.30	1.7	2	370
19.76	334.7	17.38	(10.1 ... 10.4)		A?

*h* 3355;  $-38^{\circ} 13$ ; 9.4

A.R.  $0^h 8^m 31^s$ ; Decl.  $-38^{\circ} 18'$

19.845	23.2	4.56	2.2	2	370
19.848	22.9	4.46	2.5	$2\frac{1}{2}$	370
19.883	22.6	4.53	1.4	$2\frac{1}{2}$	370
19.86	22.9	4.52	(9.7 ... 10.9)		N

*h* 3356; Cód  $-39^{\circ} 45$ ; Neb

A.R.  $0^h 8^m 45^s$ ;  $-39^{\circ} 35'$

19.883	136	11.9	1.7	$2\frac{1}{2}$	370
			(13 ... 13 $\frac{1}{2}$ )		159

*h* 3367;  $-32^{\circ} 47$ ; 8.6

A.R.  $0^h 21^m 25^s$ ; Decl.  $-32^{\circ} 39'$

18.835	179.5	5.38	2.0	$2\frac{1}{2}$	370
18.865	179.4	5.54	2.7	2	370
18.911	180.7	5.58	1.6	2	370
18.87	179.9	5.50	(9.8 ... 10.4)		

BC = I 438

18.835	213.4	2.12	2.1	2	475
18.865	208.9	—	2.9	$1\frac{1}{2}$	370
18.911	208.8	2.20	1.8	$1\frac{1}{2}$	370
18.87	210.4	2.16	(10.4 ... 11.8)		23

\* I 260;  $\beta_1$  Tucanae; 3.8

A.R.  $0^h 25^m 49^s$ ; Decl.  $-63^{\circ} 39'$

20.831	189.9	0.2+	2.3	3	650
20.861	96+	$< 0.25$	1.7	3	650
20.864	Ver la nota 160			$3\frac{1}{2}$	650

*h* 3374;  $-75^{\circ} 47 + 8$ ;  $9.2 + 10.0$

A.R.  $0^h 27^m 9^s$ ; Decl.  $-75^{\circ} 57'$

17.852	117.1	30.53	0.4	2	370
17.945	117.3	30.52	4.0	2	370
17.90	117.2	30.52	(9.3 ... 9.8)		F

*h* 3375;  $-35^{\circ} 60$ ; 7.0

A.R.  $0^h 27^m 36^s$ ; Decl.  $-35^{\circ} 40'$

19.755	167.3	5.90	2.9	3	370
19.758	166.2	5.88	1.8	2	370
19.788	167.0	5.96	2.9	$2\frac{1}{2}$	370
19.77	166.8	5.91	(6.8 ... 8.5)		D?

\* I 45;  $-56^{\circ} 103$ ; 7.2A.R.  $0^h 27^m 38^s$ ; Decl.  $-56^{\circ} 1'$ 

20.831	257.6	0.52	2.0	3	650
20.861	254.1	0.49	1.9	3 $\frac{1}{2}$	650
20.864	258.5	0.56	0.6	4	650
20.85	256.7	0.52	(8.3 ... 8.7)		P

h 3384;  $-33^{\circ} 71$ ; 9.4A.R.  $0^h 34^m 41^s$ ; Decl.  $-33^{\circ} 27'$ 

18.835	265.2	5.92	2.3	2	370
18.865	265.0	5.93	3.1	1 $\frac{1}{2}$	370
18.911	266.7	6.06	2.1	2	370
18.87	265.6	5.97	(9.7 ... 11.3)		N

## h 3393; Anon.

A.R.  $0^h 36^m 20^s$ ; Decl.  $-75^{\circ} 20'$ 

17.852	298.6	5.31	0.6	2	370
17.945	300.4	5.56	4.3	2	370
17.964	300.7	5.30	4.2	2 $\frac{1}{2}$	370
17.92	299.9	5.39	(11.5 ... 12.5)		N

HdA;  $\lambda_1$  Sculptoris; 6.4A.R.  $0^h 36^m 42^s$ ; Decl.  $-39^{\circ} 9'$ 

19.845	344.5	0.58	2.6	2	475
19.848	342.3	0.57	2.6	2	650
19.883	345.7	0.61	1.9	2 $\frac{1}{2}$	650
19.86	344.2	0.59	(6.7 ... 6.8)		P

## h 3392; Anon.

A.R.  $0^h 37^m 50^s$ ; Decl.  $-79^{\circ} 11'$ 

18.851	287.5	12.11	3.4	2	370
18.854	288.2	12.19	2.3	2	370
18.85	287.8	12.15	(10.8 ... 10.8)		N

h 3396;  $-33^{\circ} 80$ ; 9.4A.R.  $0^h 40^m 5^s$ ; Decl.  $-33^{\circ} 58'$ 

18.835	219.0	4.15	2.4	2 $\frac{1}{2}$	370
18.911	220.5	4.30	2.2	2 $\frac{1}{2}$	370
18.917	218.9	4.47	2.3	2	370
18.89	219.5	4.31	(9.7 ... 11.2)		N

h 3399;  $-39^{\circ} 56$ ; 8.7A.R.  $0^h 43^m 10^s$ ; Decl.  $-39^{\circ} 49'$ 

19.845	290.6	8.51	2.7	2	370
19.848	290.1	8.52	2.7	3	370
19.883	290.2	8.46	2.0	3	370
19.86	290.3	8.50	(9.3 ... 9.7)		N

h 3401;  $-35^{\circ} 81$ ; 9.2A.R.  $0^h 44^m 20^s$ ; Decl.  $-35^{\circ} 10'$ 

19.755	102.1	6.32	3.0	3	370
19.758	102.3	6.52	2.0	2	370
19.788	102.3	6.49	3.0	2 $\frac{1}{2}$	370
19.77	102.2	6.44	(9.8 ... 10.5)		N

h 3410; Cód  $-31^{\circ} 398$ ; 9.3A.R.  $0^h 54^m 40^s$ ; Decl.  $-31^{\circ} 52'$ 

18.835	252.9	22.25	3.1	3	370
18.911	252.8	22.61	2.4	2 $\frac{1}{2}$	370
18.87	252.9	22.43	(10.1 ... 10.5)		N

h 3411;  $-30^{\circ} 103$ ; 9.2A.R.  $0^h 56^m 0^s$ ; Decl.  $-30^{\circ} 40'$ 

18.835	3.6	27.17	3.3	3	370
18.911	4.2	27.06	2.5	2 $\frac{1}{2}$	370
18.87	3.9	27.12	(8.9 ... 11.2)		N

h 3415;  $-41^{\circ} 101$ ; 6.9A.R.  $0^h 58^m 10^s$ ; Decl.  $-41^{\circ} 19'$ 

19.845	148.9	1.09	2.9	2	475
19.848	149.4	1.18	2.9	2 $\frac{1}{2}$	650
19.875	147.8	1.15	4.0	2 $\frac{1}{2}$	370
19.86	148.7	1.14	(7.6 ... 8.2)		161

O. Stone =  $\beta$  735;  $-34^{\circ} 95$ ; 7.5A.R.  $0^h 58^m 39^s$ ; Decl.  $-34^{\circ} 12'$ 

19.941	219.2	8.70	3.0	2 $\frac{1}{2}$	370
19.955	218.5	8.81	3.4	2	370
19.95	218.8	8.75	(6.8 ... 11.5)		F

\* Sellors 1;  $\beta$  Phoenicis; 5.0A.R.  $1^h 0^m 30^s$ ; Decl.  $-47^{\circ} 23'$ 

20.831	5.6	1.52	2.4	3	650
20.861	3.9	1.65	2.1	3	650
20.874	8.9	1.84	2.7	3	370
20.877	4.3	1.90	0.3	3	370
20.86	5.7	1.73	(4.3 ... 4.4)		B

## \* AC = h 3417

20.861	51.5	57.35	2.3	2 $\frac{1}{2}$	370
20.874	51.8	57.19	2.8	2 $\frac{1}{2}$	370
20.877	51.6	57.54	0.4	3	370
20.87	51.6	57.36	(4.3 ... 11.4)		R

h 3420;  $-82^{\circ} 16$ ; 8.4A.R.  $1^h 6^m 1^s$ ; Decl.  $-82^{\circ} 19'$ 

18.905	32.6	22.62	2.0	1	370
18.908	32.3	22.63	1.4	2	370
18.91	32.4	22.63	(8.2 ... 11.9)		N



\* *h* 3423;  $\alpha$  Tucanae; 5.2

A.R. 1<sup>h</sup> 11<sup>m</sup> 31<sup>s</sup>; Decl. -69° 32'

20.823	346.8	5.47	2.8	2	370
20.831	346.0	5.45	2.6	2½	650
20.861	346.3	5.36	2.5	3	370
20.84	346.4	5.43	(4.9Y ... 8.2R) P		

\* *h* 3426; -67° 81; 6.2

A.R. 1<sup>h</sup> 12<sup>m</sup> 43<sup>s</sup>; Decl. -67° 4'

20.823	336.6	2.79	2.9	2	370
20.831	336.9	2.55	2.8	3	370
20.861	338.2	2.45	2.7	2½	370
20.874	337.6	2.80	3.0	2½	370
20.85	337.3	2.65	(7.3 ... 9.0) M		

$\beta$  1229; -35° 132; 7.6

A.R. 1<sup>h</sup> 13<sup>m</sup> 32<sup>s</sup>; Decl. -35° 9'

19.755	290.9	1.11	3.2	2½	370
19.848	290.2	1.22	3.5	2½	650
19.875	289.8	1.15	4.2	2½	370
19.83	290.3	1.16	(8.9 ... 9.1) F		

\* *h* 3430; -57° 292; 6.8

A.R. 1<sup>h</sup> 15<sup>m</sup> 30<sup>s</sup>; Decl. -57° 60'

20.831	233.2	2.67	3.0	3	650
20.861	233.5	2.47	2.9	2½	370
20.874	234.2	2.78	3.0	2½	370
20.85	233.6	2.64	(7.4Y ... 10.0b) M		

*h* 3432; -31° 168; 8.4

A.R. 1<sup>h</sup> 16<sup>m</sup> 57<sup>s</sup>; Decl. -31° 17'

18.835	220.8	8.37	3.5	3	370
18.911	221.2	8.35	2.7	2	370
18.917	221.8	8.46	2.5	2	370
18.89	221.3	8.39	(8.5 ... 11.3) F		

$\Delta$  3; *R* Sculptoris; Var.

A.R. 1<sup>h</sup> 21<sup>m</sup> 13<sup>s</sup>; Decl. -33° 12'

19.941	{	265.1	372.7	Mag.	10.8	150
		84.5	513.9	"	11.5	
		352	160	"	12.5	

*h* 3436; -30° 163; 7.4

A.R. 1<sup>h</sup> 21<sup>m</sup> 16<sup>s</sup>; Decl. -30° 53'

18.835	126.6	9.85	3.7	3	370
18.911	127.6	9.99	2.8	2	370
18.917	127.4	9.91	2.7	1½	370
18.89	127.2	9.92	(6.9Y ... 9.7b) F		

*h* 3441; Ver la nota 163

*h* 3443; -80° 24 + 3; 8.8 + 9.4

A.R. 1<sup>h</sup> 24<sup>m</sup> 37<sup>s</sup>; Decl. -80° 33'

18.854	284.2	39.67	2.4	2	370
18.903	284.3	39.41	1.6	2	370
18.88	284.2	39.54	(8.7 ... 9.5) N		

\* I 264; -54° 342; 7.8

A.R. 1<sup>h</sup> 26<sup>m</sup> 36<sup>s</sup>; Decl. -54° 1'

20.831	96.4	0.67	3.2	3½	650
20.877	97.9	0.62	0.6	3	650
20.880	93.6	0.67	23.6	2½	475
20.86	96.0	0.65	(8.8 ... 9.3) B		

*h* 3445; -41° 148 + 7; 8.9 + 9.4

A.R. 1<sup>h</sup> 27<sup>m</sup> 20<sup>s</sup>; Decl. -41° 54'

19.845	265.5	18.50	3.3	2	370
19.848	264.9	18.50	3.0	3	370
19.85	265.2	18.50	(8.9 ... 9.9) N		

$\epsilon$  31; -30° 181; 7.6

A.R. 1<sup>h</sup> 29<sup>m</sup> 14<sup>s</sup>; Decl. -30° 33'

20.831	274.5	0.23	3.6	3½	650
20.864	270.1	0.26	1.3	4	650
20.877	274.7	0.24	1.0	3½	650
20.86	273.1	0.24	(8.3 ... 8.6)		

AB,C =  $\approx$  1000

18.835	58.5	1.60	3.9	3	370
19.010	58.5	1.71	4.2	3	370
20.831	66.4	1.47	3.8	3	650
20.864	63.7	1.55	1.2	4	370
18.92	58.5	1.65			
20.85	65.0	1.51	((7.6) ... 12.4) R		

*h* 3447;  $\zeta$  Sculptoris; 6.4

A.R. 1<sup>h</sup> 30<sup>m</sup> 22<sup>s</sup>; Decl. -30° 33'

18.835	101.0	2.02	4.1	3	370
18.868	100.2	2.01	0.9	2	650
18.911	99.3	1.90	3.0	2	475
18.87	100.2	1.98	(6.7 ... 7.8) M		

*h* 3448; -37° 147 + 8; 9.0 + 8.8

A.R. 1<sup>h</sup> 30<sup>m</sup> 36<sup>s</sup>; Decl. -37° 56'

19.755	56.9	28.66	3.7	3	370
19.758	56.7	28.76	2.7	2	370
19.76	56.8	28.71	(9.0 ... 9.3) N		

*h* 3453;  $-79^{\circ} 40'$ ; 7.1A.R.  $1^{\text{h}} 32^{\text{m}} 49^{\text{s}}$ ; Decl.  $-79^{\circ} 8'$ 

18.854	304.3	50.05	2.7	$1\frac{1}{2}$	370
18.903	304.1	50.24	1.9	$1\frac{1}{2}$	370
18.88	304.2	50.14	(6.4 ... 13.5)		M?

Piazz = *h* 3452;  $-38^{\circ} 140'$ ; 7.3A.R.  $1^{\text{h}} 34^{\text{m}} 10^{\text{s}}$ ; Decl.  $-38^{\circ} 6'$ 

19.755	275.6	20.51	3.9	$2\frac{1}{2}$	370
19.758	276.2	20.52	2.9	2	370
19.845	275.5	20.53	3.4	2	370
19.848	275.8	20.40	3.2	$2\frac{1}{2}$	370
19.80	275.8	20.49	(7.3 ... 8.7)		22

\*  $\Delta 5$ ; *p* Eridani; 6.5A.R.  $1^{\text{h}} 35^{\text{m}} 4^{\text{s}}$ ; Decl.  $-56^{\circ} 50'$ 

18.950	214.2	8.86	4.5	2	370
18.958	213.5	8.90	3.0	2	370
18.969	213.2	9.00	4.9	2	370
19.747	213.2	9.15	23.5	$2\frac{1}{2}$	475
19.772	213.6	8.97	3.3	$2\frac{1}{2}$	370
20.861	212.7	8.93	3.0	$2\frac{1}{2}$	370
20.874	212.8	9.15	3.2	$2\frac{1}{2}$	370
20.880	212.7	8.98	23.8	$2\frac{1}{2}$	475
20.904	212.5	8.99	0.8	$3\frac{1}{2}$	370
18.96	213.6	8.92			
19.76	213.4	9.06			
20.88	212.7	9.01	(5.9 ... 5.9)		B

*h* 3454; Anon.A.R.  $1^{\text{h}} 36^{\text{m}} 0$ ; Decl.  $-77^{\circ} 40'$ 

17.852	285.8	14.68	1.5	2	370
18.027	287.1	14.80	4.9	$2\frac{1}{2}$	370
17.94	286.5	14.74	(9.9 ... 12.1)		N

*h* 3457;  $-74^{\circ} 116'$ ; 9.5A.R.  $1^{\text{h}} 36^{\text{m}} 58^{\text{s}}$ ; Decl.  $-74^{\circ} 21'$ 

17.852	230.8	23.86	1.2	2	370
17.964	231.3	24.27	4.5	$2\frac{1}{2}$	370
18.027	231.5	24.46	4.6	$2\frac{1}{2}$	370
17.95	231.2	24.20	(9.4 ... 11.7)		N

Rus 11;  $-76^{\circ} 123'$ ; 8.0A.R.  $1^{\text{h}} 37^{\text{m}} 41^{\text{s}}$ ; Decl.  $-76^{\circ} 39'$ 

17.964	127.7	1.49	5.0	2	370
18.027	126.2	1.46	5.1	$2\frac{1}{2}$	475
18.175	126.8	1.44	7.5	2	370
18.06	126.9	1.46	(8.6 ... 8.9)		D?

*h* 3458;  $-37^{\circ} 163'$ ; 9.7A.R.  $1^{\text{h}} 38^{\text{m}} 52^{\text{s}}$ ; Decl.  $-37^{\circ} 20'$ 

19.755	315.2	10.26	4.0	$2\frac{1}{2}$	370
19.758	314.1	10.01	3.1	$1\frac{1}{2}$	370
19.788	314.8	10.11	3.2	$2\frac{1}{2}$	370
19.77	314.7	10.13	(9.8 ... 11.2)		N

*h* 3464;  $-76^{\circ} 125'$ ; 7.9A.R.  $1^{\text{h}} 39^{\text{m}} 32^{\text{s}}$ ; Decl.  $-76^{\circ} 53'$ 

17.852	156.6	3.12	1.8	$1\frac{1}{2}$	370
18.027	156.3	2.85	5.4	2	475
18.175	156.4	2.96	7.7	2	370
18.02	156.4	2.98	(8.2 ... 10.8)		F?

*h* 3467;  $\tau_1$  Hydri; 7.0A.R.  $1^{\text{h}} 41^{\text{m}} 18^{\text{s}}$ ; Decl.  $-79^{\circ} 47'$ 

18.908	348.4	15.98	1.6	2	370
18.961	349.3	16.01	2.8	2	370
18.93	348.8	16.00	(6.6 ... 12.2)		N

*h* 3465;  $-40^{\circ} 155'$ ; 7.8A.R.  $1^{\text{h}} 41^{\text{m}} 18^{\text{s}}$ ; Decl.  $-40^{\circ} 34'$ 

19.845	272.8	8.89	3.7	$2\frac{1}{2}$	370
19.848	272.8	8.92	3.3	3	370
19.876	273.2	8.99	4.4	$2\frac{1}{2}$	370
19.86	272.9	8.93	(8.2 ... 10.6)		N

 $\delta 32$ ;  $-39^{\circ} 151'$ ; 8.0A.R.  $1^{\text{h}} 44^{\text{m}} 40^{\text{s}}$ ; Decl.  $-39^{\circ} 27'$ 

19.883	332.8	4.10	2.3	$2\frac{1}{2}$	370
19.895	334.6	4.16	4.4	2	370
19.905	333.5	4.10	3.2	3	370
19.89	333.6	4.12	(8.0 ... 13.3)		164

*h* 3474;  $\tau_2$  Hydri; 6.3A.R.  $1^{\text{h}} 48^{\text{m}} 59^{\text{s}}$ ; Decl.  $-80^{\circ} 48'$ 

18.908	28.7	39.39	1.8	$1\frac{1}{2}$	370
18.961	27.8	40.14	3.0	2	370
18.93	28.2	39.77	(6.2 ... 13.5)		N

\* *h* 3475 = Rus 12;  $-60^{\circ} 162'$ ; 6.7A.R.  $1^{\text{h}} 51^{\text{m}} 18^{\text{s}}$ ; Decl.  $-60^{\circ} 55'$ 

20.874	55.7	2.74	3.4	$2\frac{1}{2}$	370
20.880	55.0	2.46	0.0	$2\frac{1}{2}$	475
20.904	55.4	2.47	1.0	$3\frac{1}{2}$	370
20.89	55.4	2.56	(7.4 ... 7.5)		P

Hu 1558;  $-54^{\circ} 409$ ; 8.3

A.R.  $1^h 56^m 40^s$ ; Decl.  $-54^{\circ} 37'$

19.007	49.1	4.04	5.3	$2\frac{1}{2}$	370
19.747	49.0	4.17	0.2	2	475
19.955	49.1	3.95	4.3	$2\frac{1}{2}$	370
19.57	49.1	4.05	(8.8 ... 12.5)		142

$h 3478$ ;  $-30^{\circ} 238 + 9$ ; 8.6 + 9.0

A.R.  $1^h 57^m 9^s$ ; Decl.  $-30^{\circ} 56'$

18.835	143.7	41.73	4.2	$2\frac{1}{2}$	370
18.868	143.8	41.63	1.1	2	370
18.85	143.7	41.68	(8.1 ... 8.8)		A <sup>2</sup>

$h 3480$ ;  $-36^{\circ} 189$ ; 9.3

A.R.  $1^h 58^m 55^s$ ; Decl.  $-36^{\circ} 52'$

19.755	100.1	22.19	4.3	$2\frac{1}{2}$	370
19.788	99.7	21.95	3.4	$2\frac{1}{2}$	370
19.77	99.9	22.07	(9.2 ... 11.8)		A

$\varepsilon 33$ ;  $-34^{\circ} 204$ ; 8.6

A.R.  $2^h 0^m 42^s$ ; Decl.  $-34^{\circ} 30'$

20.905	332.4	3.22	3.0	4	370
20.918	333.4	3.28	3.5	3	370
20.91	332.9	3.25	(8.9 ... 13.0)		

Aguilar;  $-61^{\circ} 178$ ; 9.0

A.R.  $2^h 1^m 15^s$ ; Decl.  $-61^{\circ} 24'$

18.027	183.9	6.28	4.4	3	370
18.038	184.1	6.34	5.4	3	475
18.03	184.0	6.31	(9.6 ... 10.1)		7

$h 3484$ ;  $-60^{\circ} 182 + 3$ ; 7.4 + 10.0

A.R.  $2^h 3^m 31^s$ ; Decl.  $-60^{\circ} 16'$

19.007	61.1	52.59	4.9	2	370
19.136	61.0	52.73	6.5	$1\frac{1}{2}$	370
19.07	61.1	52.66	(7.9 ... 9.5)		165

$h 3492$ ;  $-33^{\circ} 227$ ; 9.8:

A.R.  $2^h 10^m 28^s$ ; Decl.  $-33^{\circ} 27'$

19.008	42.0	19.99	6.9	$2\frac{1}{2}$	370
19.010	41.4	20.05	4.6	$2\frac{1}{2}$	370
19.01	41.7	20.02	(9.6 ... 10.2)		N

Có 5;  $-33^{\circ} 228$ ; 8.4

A.R.  $2^h 11^m 32^s$ ; Decl.  $-33^{\circ} 34'$

19.010	270.6	2.10	4.8	$2\frac{1}{2}$	370
19.103	271.1	1.95	6.8	2	370
19.106	271.0	2.00	5.7	2	370
19.07	270.9	2.02	(9.1 ... 9.3)		23

$h 3494 = \lambda 18$ ;  $-36^{\circ} 221$ ; 8.2

A.R.  $2^h 14^m 32^s$ ; Decl.  $-36^{\circ} 1'$

19.755	5.7	0.90	4.5	$2\frac{1}{2}$	650
19.788	6.4	0.83	3.5	3	370
19.848	8.3	0.99	3.6	$2\frac{1}{2}$	650
19.876	5.5	0.80	4.7	$2\frac{1}{2}$	370
20.905	2.2	0.93	3.3	4	650
20.918	4.7	0.78	3.6	3	650
20.987	2.3	0.98	4.2	2	370
19.82	6.5	0.88			
20.94	3.1	0.90	(8.7 ... 9.0)		B

$\beta 738$ ;  $-30^{\circ} 287$ ; 7.4

A.R.  $2^h 17^m 47^s$ ; Decl.  $-30^{\circ} 26'$

20.091	51.6	0.43	6.0	$2\frac{1}{2}$	650
20.094	52.3	0.45	6.1	$2\frac{1}{2}$	475
20.097	54.0	0.47	5.1	$2\frac{1}{2}$	650
20.831	47.9	0.39	4.0	3	650
20.864	51.0	0.38	1.5	4	650
20.880	50.1	0.50	1.4	3	475
20.896	50.4	0.39	2.0	3	650
20.09	52.6	0.45			
20.87	49.9	0.41	(8.0 ... 8.2)		B

$\beta 739$ ;  $-30^{\circ} 290$ ; 7.8

A.R.  $2^h 19^m 21^s$ ; Decl.  $-30^{\circ} 26'$

20.091	265.3	1.80	6.1	$2\frac{1}{2}$	650
20.094	265.3	1.90	6.2	$2\frac{1}{2}$	475
20.097	265.3	1.92	5.2	$2\frac{1}{2}$	650
20.09	265.3	1.87	(8.1 ... 8.6)		D

\* $\varepsilon 1$ ;  $-58^{\circ} 214$ ; 7.5

A.R.  $2^h 24^m 15^s$ ; Decl.  $-58^{\circ} 42'$

20.880	226.0	0.82	1.2	3	475
20.896	225.4	1.01	2.2	3	650
20.904	225.9	0.86	1.1	$3\frac{1}{2}$	650
20.89	225.8	0.90	(7.9 ... 8.7)		F

$h 3504$ ;  $-30^{\circ} 303$ ; 7.8

A.R.  $2^h 24^m 57^s$ ; Decl.  $-30^{\circ} 55'$

18.835	269.0	6.75	4.6	$2\frac{1}{2}$	370
18.868	269.4	6.81	1.9	$2\frac{1}{2}$	370
18.911	269.9	6.91	3.2	2	475
18.87	269.4	6.82	(8.2 ... 9.0)		F

$h 3508$ ;  $-78^{\circ} 51$ ; 8.7

A.R.  $2^h 26^m 14^s$ ; Decl.  $-78^{\circ} 19'$

18.908	91.1	16.33	2.0	1	370
18.961	92.0	16.17	3.2	2	370
18.963	91.9	16.23	2.7	2	370
18.94	91.7	16.24	(9.0 ... 11.1)		N

$h$  3509;  $-32^\circ 27'$ ; 7.4A.R.  $2^h 28^m 51^s$ ; Decl.  $-32^\circ 4'$ 

18.835	59.1	23.61	4.8	2	370
18.868	59.3	23.48	2.1	$2\frac{1}{2}$	370
18.85	59.2	23.54	(8.1 ... 11.8)		166

 $h$  3519;  $-83^\circ 45'$ ; 8.2A.R.  $2^h 29^m 24^s$ ; Decl.  $-83^\circ 2'$ 

18.963	124.9	31.23	2.5	2	370
19.155	126.9	31.15	7.0	2	370
19.06	125.9	31.19	(8.5 ... 13.5)		R <sup>2</sup>

 $h$  3522;  $-76^\circ 21'$ ; 6.8A.R.  $2^h 33^m 50^s$ ; Decl.  $-76^\circ 26'$ 

18.027	290.1	34.27	5.7	2	370
18.175	290.2	34.34	7.9	2	370
18.10	290.2	34.30	(6.9 ... 10.7)		N

BC; C = 12.6

18.175	354.0	11.38	8.0	2	370
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 $h$  3523 Ver la nota 165 $h$  3527;  $-41^\circ 25'$ ; 7.0A.R.  $2^h 38^m 30^s$ ; Decl.  $-41^\circ 4'$ 

19.845	43.4	2.11	4.1	$2\frac{1}{2}$	475
19.848	42.7	2.14	4.3	$2\frac{1}{2}$	370
19.876	42.7	1.96	5.0	$2\frac{1}{2}$	370
19.86	42.9	2.07	(7.1 ... 7.4)		F

 $\geq 34$ ;  $-31^\circ 31'$ ; 9.0A.R.  $2^h 38^m 36^s$ ; Decl.  $-31^\circ 36'$ 

19.008	33.6	2.07	7.1	3	370
19.010	32.9	2.13	4.9	$2\frac{1}{2}$	650
19.103	27.8	2.10	6.9	2	370
19.106	31.0	2.11	5.9	2	370
19.06	31.3	2.10	(9.0 ... 10.6)		166

 $h$  3530;  $-81^\circ 53'$ ; 9.2A.R.  $2^h 38^m 53^s$ ; Decl.  $-81^\circ 18'$ 

18.961	216.7	15.03	3.4	2	370
18.963	214.8	14.80	2.9	$1\frac{1}{2}$	370
18.96	215.8	14.92	(9.0 ... 12.8)		N

AC

18.961	170.0	19.28	3.3	2	370
18.963	170.6	19.26	2.8	2	370
18.96	170.3	19.27	(9.0 ... 11.5)		N

 $h$  3529;  $-32^\circ 29'$ ; 10.2A.R.  $2^h 41^m 41^s$ ; Decl.  $-32^\circ 50'$ 

19.010	136.5	19.97	5.1	$2\frac{1}{2}$	370
19.125	130.9	20.05	6.2	2	370
19.07	133.7	20.01	(10.2 ... 14.9)		A

 $\geq 35$ ;  $-37^\circ 29'$ ; 7.4A.R.  $2^h 43^m 8^s$ ; Decl.  $-37^\circ 50'$ 

19.755	173.0	1.74	4.9	3	370
19.788	174.2	1.88	3.6	3	370
19.848	171.3	1.79	3.9	2	370
19.80	172.8	1.80	(7.5 ... 12.4)		

Piazzini =  $h$  3532;  $-37^\circ 29'$ ; 6.4A.R.  $2^h 43^m 39^s$ ; Decl.  $-37^\circ 56'$ 

19.755	145.9	5.57	4.7	3	370
19.788	146.3	5.64	3.8	3	370
19.848	146.4	5.60	4.1	2	370
19.80	146.2	5.60	(7.0 ... 8.2)		F

 $h$  3536;  $\gamma_2$  Fornacis; 6.6A.R.  $2^h 45^m 11^s$ ; Decl.  $-36^\circ 22'$ 

19.755	10.1	4.96	5.2	3	370
19.788	12.0	5.01	4.0	$2\frac{1}{2}$	370
19.848	11.6	5.12	3.8	$2\frac{1}{2}$	370
19.80	11.2	5.03	(6.1 ... 12.2)		F

 $h$  3527 =  $h$  3531; Cód  $-40^\circ 73'$ ; 9.9A.R.  $2^h 45^m 32^s$ ; Decl.  $-40^\circ 48'$ 

19.845	31.2	16.40	4.8	2	370
19.848	31.1	16.24	4.5	2	370
19.85	31.1	16.32	(10.8 ... 11.1)		167

 $h$  3539;  $-78^\circ 67'$ ; 8.6A.R.  $2^h 46^m 13^s$ ; Decl.  $-78^\circ 39'$ 

18.908	63.0	7.78	2.1	1	370
18.961	62.1	7.95	3.5	2	370
18.963	63.5	8.03	3.1	2	370
18.94	62.9	7.92	(9.1 ... 9.7)		N

Cód 7;  $-39^\circ 24'$ ; 8.1A.R.  $2^h 51^m 44^s$ ; Decl.  $-39^\circ 57'$ 

19.876	185.4	3.53	5.4	3	370
19.884	185.6	3.60	2.8	3	370
19.895	185.2	3.50	5.1	$2\frac{1}{2}$	370
19.88	185.4	3.54	(8.5 ... 8.9)		F

Piazzini =  $\Delta 9$ ; 0 Eridani; 4.1

A.R. 2<sup>h</sup> 53<sup>m</sup> 31<sup>s</sup>; Decl. -40° 48'

19.848	87.2	8.66	4.6	2½	370
19.876	86.8	8.34	5.2	2	370
19.884	87.0	8.48	2.9	2½	370
19.87	87.0	8.49	(3.4 ... 4.4)		

*h* 3549; -38° 258; 10.0

A.R. 2<sup>h</sup> 58<sup>m</sup> 13<sup>s</sup>; Decl. -38° 33'

19.848	275.9	6.28	4.7	2½	370
19.876	275.6	6.62	5.6	2½	370
19.884	274.9	6.25	3.0	3	370
19.895	276.3	6.40	5.2	2	370
19.88	275.7	6.39	(10.1 ... 11.9)		22

*h* 3560; Anon.

A.R. 3<sup>h</sup> 1<sup>m</sup> 5; Decl. -84° 42'

19.155	241.4	12.32	7.4	1½	370
19.158	241.6	12.71	7.2	2	370
19.177	242.8	12.45	7.1	2	370
19.16	241.9	12.49	(9.6 ... 12.7)		N

*h* 3553; -38° 270; 8.6

A.R. 3<sup>h</sup> 4<sup>m</sup> 40<sup>s</sup>; Decl. -38° 20'

19.876	226.5	12.54	5.8	2½	370
19.884	226.4	12.26	3.1	2½	370
19.895	226.5	12.28	5.4	2½	370
19.89	226.5	12.36	(8.8 ... 10.0)		F

\* I 55 = Sellors 25; -44° 338; 6.4

A.R. 3<sup>h</sup> 8<sup>m</sup> 2<sup>s</sup>; Decl. -44° 53'

20.891	159.1	0.65	2.2	4	650
20.896	157.0	0.72	2.3	3	650
20.918	160.5	0.71	3.8	3	650
20.90	158.9	0.69	(7.1 ... 7.5)		B

\* AB,C = *h* 3556

20.896	207.3	3.17	2.4	3	370
20.918	207.7	3.28	4.1	3	370
20.91	207.5	3.22	((6.5) ... 10.6)		P

$\delta$  36; -34° 327; 9.4

A.R. 3<sup>h</sup> 9<sup>m</sup> 14<sup>s</sup>; Decl. -34° 5'

20.905	45.3	0.69	4.1	3	650
21.050	44.3	0.54	5.8	2½	370
20.98	44.8	0.62	(9.3 ... 10.4)		

*h* 3568 -79° 91; 5.6

A.R. 3<sup>h</sup> 11<sup>m</sup> 50<sup>s</sup>; Decl. -79° 28'

18.961	224.7	15.39	3.8	2	370
18.963	224.3	15.38	3.2	2	370
18.96	224.5	15.38	(6.2 ... 8.4)		F

*h* 3577; -82° 57; 8.7

A.R. 3<sup>h</sup> 17<sup>m</sup> 14<sup>s</sup>; Decl. -82° 17'

19.155	246.9	24.94	7.6	1½	370
19.158	247.5	25.07	7.4	1½	370
19.16	247.2	25.00	(8.2 ... 13.5)		N

*h* 3578; -32° 368; 9.2

A.R. 3<sup>h</sup> 22<sup>m</sup> 41<sup>s</sup>; Decl. -32° 41'

18.950	38.8	26.72	2.7	2	370
18.969	37.3	26.64	6.3	2	370
18.96	38.0	26.68	(8.4 ... 12.6)		N

*h* 3582; -83° 64; 7.7

A.R. 3<sup>h</sup> 22<sup>m</sup> 46<sup>s</sup>; Decl. -83° 59'

19.155	298.2	19.57	7.7	1½	370
19.158	297.4	19.37	7.6	2	370
19.177	296.1	19.68	7.3	2	370
19.16	297.2	19.54	(7.6 ... 10.5)		N

*h* 3581; Anon.

A.R. 3<sup>h</sup> 24<sup>m</sup> 7; Decl. -80° 57'

18.963	326.1	10.42	3.3	2	370
19.155	327.6	10.84	8.1	2	370
19.158	326.8	10.44	7.0	2	370
19.09	326.8	10.57	(10.1 ... 11.0)		168

*h* 3585; Anon.

A.R. 3<sup>h</sup> 25<sup>m</sup> 5; Decl. -84° 52'

19.155	292.7	16.46	7.8	2	370
19.158	292.9	16.65	7.7	2	370
19.16	292.8	16.56	(10.0 ... 10.4)		N

$\Delta$  15; -40° 343; 6.6

A.R. 3<sup>h</sup> 35<sup>m</sup> 18<sup>s</sup>; Decl. -40° 45'

19.876	327.5	7.88	6.3	2½	370
19.884	326.8	7.97	3.3	2½	370
19.88	327.2	7.92	(7.2 ... 8.4)		F

*h* 3595; Anon.

A.R. 3<sup>h</sup> 37<sup>m</sup> 0<sup>s</sup>; Decl. -83° 1'

19.155	314.6	11.84	8.0	1½	370
19.158	313.7	11.90	7.8	2	370
19.16	314.1	11.87	(9.3 ... 10.9)		N

*h* 3589; -41° 382; 7.4

A.R. 3<sup>h</sup> 39<sup>m</sup> 40<sup>s</sup>; Decl. -41° 3'

19.884	347.6	5.29	3.4	3	370
19.895	348.9	5.34	5.5	2½	370
19.908	349.6	5.29	5.6	3	370
19.90	348.7	5.31	(6.9 ... 9.3)		C

\*  $\lambda$  30 Ver la nota 169

$h$  3593;  $-41^\circ 388$ ; 8.8  
A.R. 3<sup>h</sup> 42<sup>m</sup> 5<sup>s</sup>; Decl.  $-41^\circ 3'$

19.895	138.1	15.52	5.9	2½	370
19.908	138.1	15.72	5.7	2½	370
19.90	138.1	15.62	(9.2 ... 11.5)		N

$\lambda$  32;  $-36^\circ 411$ ; 5.9  
A.R. 3<sup>h</sup> 43<sup>m</sup> 8<sup>s</sup>; Decl.  $-36^\circ 30'$

19.755 Redonda y sin compañera; 3,370

$h$  3596;  $-32^\circ 424$ ; 7.6  
A.R. 3<sup>h</sup> 43<sup>m</sup> 35<sup>s</sup>; Decl.  $-32^\circ 10'$

18.950	136.7	9.26	3.7	2	370
18.969	137.2	9.32	6.7	2	370
19.008	136.6	9.43	7.4	3	370
18.98	136.8	9.34	(8.3 ... 8.6)		F

$\Delta$  16;  $f$  Eridani; 5.1  
A.R. 3<sup>h</sup> 44<sup>m</sup> 0<sup>s</sup>; Decl.  $-38^\circ 0'$

19.908	208.6	7.76	5.8	2½	370
19.927	208.8	7.76	4.3	2½	370
19.92	208.7	7.76	(3.8 ... 4.2)		P

$h$  3605;  $-80^\circ 89$ ; 9.2  
A.R. 3<sup>h</sup> 44<sup>m</sup> 50<sup>s</sup>; Decl.  $-80^\circ 43'$

19.248	175.6	18.58	8.7	2	370
19.278	175.2	18.37	9.2	2	370
19.26	175.4	18.48	(9.5 ... 11.8)		20

$h$  3607;  $-81^\circ 88 + 9$ ; 9.0 + 9.0  
A.R. 3<sup>h</sup> 45<sup>m</sup> 32<sup>s</sup>; Decl.  $-81^\circ 15'$

18.961	125.4	37.17	4.0	2	370
18.963	125.8	37.16	3.4	2	370
18.96	125.6	37.16	(8.4 ... 8.8)		F

$h$  3612;  $-80^\circ 93 + 4$ ; 8.5 + 9.2  
A.R. 3<sup>h</sup> 49<sup>m</sup> 30<sup>s</sup>; Decl.  $-80^\circ 24'$

18.961	162.2	19.31	4.2	2	370
18.963	161.9	19.43	3.6	2	370
18.96	162.0	19.37	(8.2 ... 9.2)		F

$h$  3611;  $-40^\circ 385$ ; 7.4  
A.R. 3<sup>h</sup> 52<sup>m</sup> 13<sup>s</sup>; Decl.  $-40^\circ 17'$

19.895	140.2	4.23	6.1	2½	370
19.908	140.5	4.26	5.9	3	370
19.944	140.6	4.17	2.7	2½	370
19.92	140.4	4.22	(7.9 ... 8.7)		D?

$h$  3614;  $-37^\circ 462$ ; 10.8  
A.R. 3<sup>h</sup> 56<sup>m</sup> 46<sup>s</sup>; Decl.  $-37^\circ 28'$

19.927	48.4	16.75	4.7	2	370
19.952	47.2	16.85	2.7	2½	370
19.963	48.4	16.85	2.3	2½	370
19.95	48.0	16.82	(10.2 ... 12.8)		N

$\beta$  1004;  $-34^\circ 424$ ; 7.0  
A.R. 3<sup>h</sup> 57<sup>m</sup> 16<sup>s</sup>; Decl.  $-34^\circ 50'$

19.755	130.7	1.84	5.7	3½	650
19.927	132.0	1.95	4.5	2½	475
19.944	131.3	1.82	2.8	2½	370
21.050	130.1	2.12	6.2	2½	370
21.063	130.3	1.98	6.0	2½	370
21.113	131.6	2.01	6.4	2½	370
19.91	131.3	1.87			
21.08	130.7	2.04	(7.3 ... 8.0)		B

AC

19.927	139.4	55.11	4.6	2	475
19.944	138.3	55.19	2.9	2½	370
19.94	138.9	55.15	(7.3 ... 11.1)		R

$h$  3621 =  $h$  3622;  $-36^\circ 470$ ; 7.5  
A.R. 4<sup>h</sup> 0<sup>m</sup> 15<sup>s</sup>; Decl.  $-36^\circ 11'$

19.755	112.1	10.44	5.5	3	370
19.927	111.8	10.31	4.8	2½	370
19.941	112.3	10.28	4.9	2½	370
19.87	112.1	10.34	(8.8 ... 9.1)		F

I 152;  $-35^\circ 426$ ; 7.5  
A.R. 4<sup>h</sup> 0<sup>m</sup> 16<sup>s</sup>; Decl.  $-35^\circ 47'$

21.063	250.9	—	6.2	2½	370
21.113	247.7	0.83	6.6	2½	370
21.09	249.3	0.83	(8.5 ... 8.5)		F

$h$  3624;  $-75^\circ 256$ ; 9.1  
A.R. 4<sup>h</sup> 1<sup>m</sup> 9<sup>s</sup>; Decl.  $-75^\circ 6'$

18.030	26.4	24.36	7.0	2	370
18.175	26.4	24.13	8.2	2½	370
18.10	26.4	24.24	(9.4 ... 10.4)		21

$h$  3623;  $-32^\circ 464$ ; 8.8  
A.R. 4<sup>h</sup> 1<sup>m</sup> 55<sup>s</sup>; Decl.  $-32^\circ 48'$

18.969	288.2	5.11	6.9	1½	370
19.008	288.4	5.05	7.5	3	370
19.010	288.5	5.07	5.3	3	370
19.00	288.4	5.08	(9.2 ... 9.7)		A?

*h* 3627;  $-34^{\circ} 45' + 49$ ; 9.4 + 10.8

A.R. 4<sup>h</sup> 7<sup>m</sup> 12<sup>s</sup>; Decl.  $-34^{\circ} 5'$

19.927	292.2	27.20	5.2	2½	370
19.944	292.3	27.01	3.1	2½	370
19.94	292.3	27.10	(9.0 ... 10.4)		R

*h* 3628;  $-36^{\circ} 49' + 2$ ; 7.3 + 7.6

A.R. 4<sup>h</sup> 7<sup>m</sup> 56<sup>s</sup>; Decl.  $-36^{\circ} 28'$

19.755	49.7	50.31	5.8	3	370
19.927	49.7	50.54	5.0	2½	370
19.84	49.7	50.42	(7.5 ... 8.5)		F

*h* 3632;  $-30^{\circ} 565$ ; 7.3

A.R. 4<sup>h</sup> 10<sup>m</sup> 9<sup>s</sup>; Decl.  $-30^{\circ} 23'$

18.950	162.9	11.06	3.9	1½	370
18.969	162.7	11.17	7.1	2	370
18.96	162.8	11.12	(7.8 ... 10.3)		F

*h* 3640;  $-76^{\circ} 263$ ; 8.9

A.R. 4<sup>h</sup> 11<sup>m</sup> 9<sup>s</sup>; Decl.  $-76^{\circ} 11'$

18.030	73.4	14.26	7.2	2	370
18.175	73.8	14.55	8.6	2	370
18.186	73.2	14.30	7.6	2	370
18.13	73.5	14.37	(9.0 ... 12.3)		N

*X* Eridani; 3.1

A.R. 4<sup>h</sup> 13<sup>m</sup> 10<sup>s</sup>; Decl.  $-34^{\circ} 6'$

AB = I 270 Ver la nota 170

AB, C = *h* 3636

19.927	12.9	49.07	5.4	2½	370
19.944	13.5	49.73	3.3	2½	370
19.952	13.7	48.89	2.9	3	370
19.94	13.4	49.23	(2.9 ... 11.8)		N

*h* 3642;  $-34^{\circ} 471$ ; 6.0

A.R. 4<sup>h</sup> 14<sup>m</sup> 20<sup>s</sup>; Decl.  $-34^{\circ} 12'$

19.927	158.3	6.21	5.5	2½	370
19.944	158.5	6.00	3.4	3	370
19.952	159.1	6.18	3.1	3	370
19.94	158.6	6.13	(7.0 ... 8.5)		F

*h* 3646;  $-41^{\circ} 473 + 5$ ; 7.8 + 9.6

A.R. 4<sup>h</sup> 17<sup>m</sup> 44<sup>s</sup>; Decl.  $-41^{\circ} 31'$

19.884	136.9	38.19	3.5	3	370
19.895	136.9	38.16	6.3	2½	370
19.89	136.9	38.18	(8.1 ... 9.7)		F

(Sigue Continued.)

BC = I 272

19.884	199.0	1.67	3.6	2	475
19.895	196.9	1.48	6.5	2	370
19.908	201.1	1.34	6.0	2½	370
19.89	199.0	1.50	(9.7 ... 12.3)		M

*h* 3650;  $-40^{\circ} 482$ ; 7.4

A.R. 4<sup>h</sup> 22<sup>m</sup> 25<sup>s</sup>; Decl.  $-40^{\circ} 49'$

19.884	183.4	3.31	3.7	2½	475
19.895	183.8	3.43	6.7	2	370
19.908	182.8	3.33	6.1	2½	370
19.90	183.3	3.36	(7.1 ... 8.5)		F

*h* 3652;  $-33^{\circ} 506$ ; 9.0

A.R. 4<sup>h</sup> 24<sup>m</sup> 43<sup>s</sup>; Decl.  $-33^{\circ} 51'$

18.969	116.4	10.11	7.4	1	370
19.008	116.2	9.95	7.7	2½	370
18.99	116.3	10.03	(9.3 ... 12.3)		N

*h* 3659;  $-35^{\circ} 499$ ; 6.4

A.R. 4<sup>h</sup> 26<sup>m</sup> 8<sup>s</sup>; Decl.  $-35^{\circ} 56'$

19.952	36.0	36.63	3.3	2½	370
19.974	36.8	36.68	2.8	2	370
19.96	36.4	36.65	(6.6 ... 14.2)		N

\* *β* 746;  $-36^{\circ} 546$ ; 7.6

A.R. 4<sup>h</sup> 27<sup>m</sup> 2<sup>s</sup>; Decl.  $-36^{\circ} 10'$

19.928	8.2	1.46	5.7	2	475
19.944	7.6	1.31	3.6	3	475
19.952	8.7	1.38	3.5	3	650
19.94	8.2	1.38	(8.3 ... 9.3)		M

Hu 1371;  $-31^{\circ} 560$ ; 8.9

A.R. 4<sup>h</sup> 28<sup>m</sup> 13<sup>s</sup>; Decl.  $-31^{\circ} 23'$

19.242	168.6	1.05	8.5	3½	650
19.251	172.3	1.04	8.1	2	650
19.25	170.4	1.05	(8.6 ... 11.0)		N

*β* 747;  $-38^{\circ} 461$ ; 7.6

A.R. 4<sup>h</sup> 28<sup>m</sup> 40<sup>s</sup>; Decl.  $-38^{\circ} 33'$

19.884	220.4	3.14	3.8	2½	475
19.908	221.8	3.16	6.2	2½	370
19.944	220.5	3.03	4.0	2½	370
19.91	220.9	3.11	(8.0 ... 9.7)		D?

*h* 3663;  $-35^{\circ} 507$ ; 8.9

A.R. 4<sup>h</sup> 29<sup>m</sup> 30<sup>s</sup>; Decl.  $-35^{\circ} 6'$

19.952	344.7	31.72	3.7	2½	370
19.974	344.6	31.79	3.0	2	370
19.96	344.7	31.75	(9.2 ... 12.1)		N

*h* 3673;  $-77^{\circ} 172$ ; 7.5A.R. 4<sup>h</sup> 30<sup>m</sup> 24<sup>s</sup>; Decl.  $-77^{\circ} 58'$ 

18.030	65.9	10.14	7.6	2	370
18.175	65.7	10.32	8.8	2	370
18.186	65.4	10.14	7.8	2 $\frac{1}{2}$	370
18.13	65.7	10.20	(7.7 ... 7.9)		F

*h* 3667;  $-38^{\circ} 468$ ; 9.5A.R. 4<sup>h</sup> 31<sup>m</sup> 0<sup>s</sup>; Decl.  $-38^{\circ} 17'$ 

19.884	296.4	18.59	3.9	2 $\frac{1}{2}$	370
19.908	296.4	18.88	6.3	2	370
19.944	297.2	18.59	4.1	2	370
19.91	296.7	18.69	(9.2 ... 12.3)		N

*h* 3672;  $-35^{\circ} 517$ ; 8.3A.R. 4<sup>h</sup> 34<sup>m</sup> 5<sup>s</sup>; Decl.  $-35^{\circ} 33'$ 

19.928	301.7	4.53	5.9	2	370
19.944	301.5	4.53	3.8	2 $\frac{1}{2}$	370
19.952	302.6	4.61	3.9	2 $\frac{1}{2}$	370
19.94	301.9	4.56	(9.0 ... 10.1)		A

*h* 3674;  $-37^{\circ} 555$ ; 8.6A.R. 4<sup>h</sup> 34<sup>m</sup> 31<sup>s</sup>; Decl.  $-37^{\circ} 35'$ 

19.952	207.6	39.94	4.0	2 $\frac{1}{2}$	370
19.974	208.0	39.53	3.2	2	370
19.979	207.8	39.89	2.7	2	370
19.97	207.8	39.79	(8.1 ... 12.5)		N

*h* 3692;  $-83^{\circ} 91$ ; 6.6A.R. 4<sup>h</sup> 37<sup>m</sup> 32<sup>s</sup>; Decl.  $-83^{\circ} 10'$ 

19.158	181.5	47.95	8.3	1 $\frac{1}{2}$	370
19.177	182.1	47.52	7.5	2	370
19.17	181.8	47.73	(7.0 ... 12.5)		N

\* *h* 3683;  $-59^{\circ} 370$ ; 7.1.A.R. 4<sup>h</sup> 38<sup>m</sup> 14<sup>s</sup>; Decl.  $-59^{\circ} 11'$ 

20.896	68.4	—	2.9	3	650
20.927	71.5	0.53	5.5	3	650
20.932	73.4	0.64	6.0	2 $\frac{1}{2}$	475
20.978	75.6	0.63	3.2	2 $\frac{1}{2}$	475
20.93	72.2	0.60	(7.8 ... 8.0)		P

*h* 3691;  $-77^{\circ} 175 + 6$ ; 9.1 + 9.5A.R. 4<sup>h</sup> 39<sup>m</sup> 45<sup>s</sup>; Decl.  $-77^{\circ} 6'$ 

18.030	43.5	37.56	7.9	2	370
18.175	43.5	37.46	9.0	2	370
18.10	43.5	37.51	(8.6 ... 9.1)		F

\* *h* 3686;  $-61^{\circ} 359$ ; 7.6A.R. 4<sup>h</sup> 40<sup>m</sup> 8<sup>s</sup>; Decl.  $-61^{\circ} 27'$ 

20.896	220.3	7.45	3.2	2	370
20.927	219.4	7.31	5.7	2 $\frac{1}{2}$	650
20.932	220.3	7.34	6.2	2 $\frac{1}{2}$	475
20.92	220.0	7.33	(8.6 ... 8.8)		F

*h* 3708?; Anon.A.R. 4<sup>h</sup> 41<sup>m</sup>; Decl.  $-88^{\circ} 22'$ 

19.174	8.4	17.70	8.7	2	370
19.177	9.9	17.44	8.4	1 $\frac{1}{2}$	370
19.18	9.1	17.57	(11.2 ... 11.4)		172

\* *h* 3696;  $-56^{\circ} 732$ ; 8.4A.R. 4<sup>h</sup> 45<sup>m</sup> 29<sup>s</sup>; Decl.  $-56^{\circ} 14'$ 

20.896	298.3	3.80	3.4	2	370
20.927	296.6	3.80	5.9	2 $\frac{1}{2}$	370
20.932	297.2	3.80	6.3	2 $\frac{1}{2}$	370
20.92	297.4	3.80	(8.8 ... 10.2)		M

AC; C = 14.0

20.932	116.3	14.41	6.4	2 $\frac{1}{2}$	370
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*h* 3695;  $-38^{\circ} 519$ ; 7.4A.R. 4<sup>h</sup> 46<sup>m</sup> 11<sup>s</sup>; Decl.  $-38^{\circ} 47'$ 

19.884	45.7	39.97	4.1	2 $\frac{1}{2}$	370
19.979	45.7	40.56	2.9	2	370
19.985	45.4	40.31	2.8	2	370
19.95	45.6	40.28	(7.2 ... 13.0)		N

*h* 3697;  $-41^{\circ} 581$ ; 6.9A.R. 4<sup>h</sup> 46<sup>m</sup> 12<sup>s</sup>; Decl.  $-41^{\circ} 32'$ 

19.884	274.1	14.43	4.2	2 $\frac{1}{2}$	370
19.979	273.9	14.54	3.0	2	370
19.93	274.0	14.49	(6.8 ... 10.8)		A

*h* 3698;  $-38^{\circ} 521$ ; 9.3A.R. 4<sup>h</sup> 46<sup>m</sup> 41<sup>s</sup>; Decl.  $-38^{\circ} 24'$ 

19.884	281.1	10.34	4.3	2 $\frac{1}{2}$	370
19.979	280.8	9.79	3.2	2	370
19.985	280.8	10.13	2.9	2	370
19.95	280.9	10.09	(9.7 ... 13.4)		N

*h* 3704;  $-41^{\circ} 591$ ; 10.0A.R. 4<sup>h</sup> 50<sup>m</sup> 12<sup>s</sup>; Decl.  $-41^{\circ} 34'$ 

19.979	206.7	16.82	3.7	2	370
19.985	207.9	16.74	3.1	2 $\frac{1}{2}$	370
19.98	207.3	16.78	(10.8 ... 12.0)		N



Hu 1382;  $-31^{\circ} 664$ ; 8.8

A.R.  $4^h 53^m 54^s$ ; Decl.  $-31^{\circ} 50'$

19.221	5.9	2.07	8.7	2	475
19.242	6.7	1.86	8.7	$3\frac{1}{2}$	650
19.251	6.9	1.96	8.3	2	650
19.24	6.5	1.96	(8.7 ... 10.2)		N

$h 3711$ ;  $-41^{\circ} 609$ ; 8.6

A.R.  $4^h 54^m 54^s$ ; Decl.  $-41^{\circ} 7'$

19.979	350.2	14.02	3.8	2	370
19.985	348.9	14.22	3.2	$2\frac{1}{2}$	370
19.990	347.9	14.30	3.1	2	370
19.98	349.0	14.18	(9.0 ... 13.1)		N

$h 3713$ ;  $-43^{\circ} 529$ ; 9.2

A.R.  $4^h 55^m 21^s$ ; Decl.  $-43^{\circ} 18'$

19.990	340.1	22.89	3.3	2	370
19.993	340.0	22.80	3.0	2	370
19.99	340.0	22.84	(9.5 ... 11.8)		F

BC =  $\delta 37$

19.990	13.9	2.62	3.5	2	370
19.993	17.7	2.37	3.2	2	370
19.998	15.5	2.56	3.2	2	370
19.99	15.7	2.52	(11.8 ... 12.3)		

$h 3721$ ;  $-80^{\circ} 131$ ; 7.7

A.R.  $4^h 55^m 22^s$ ; Decl.  $-80^{\circ} 51'$

18.961	225.3	3.55	4.6	$1\frac{1}{2}$	370
18.963	225.4	3.42	3.7	2	370
19.155	226.6	3.35	8.3	2	370
19.03	225.8	3.44	(8.4 ... 9.2)		M?

$h 3716$ ;  $-63^{\circ} 343$ ; 9.1

A.R.  $4^h 56^m 21^s$ ; Decl.  $-66^{\circ} 40'$

18.025	283.3	5.50	9.9	2	370
18.044	285.2	5.67	7.0	$2\frac{1}{2}$	370
18.189	282.1	5.69	8.5	2	370
18.191	281.4	6.14	7.0	2	370
18.11	283.0	5.75	(9.9 ... 11.7)		171

$h 3717$ ;  $-39^{\circ} 567$ ; 9.6

A.R.  $4^h 57^m 51^s$ ; Decl.  $-39^{\circ} 46'$

19.979	195.4	12.94	4.0	$2\frac{1}{2}$	370
19.985	195.8	13.09	3.4	2	370
19.98	195.6	13.01	(10.3 ... 11.5)		F?

$h 3718$ ;  $-33^{\circ} 676 + 5$ ;  $8.4 + 9.0$

A.R.  $4^h 58^m 6^s$ ; Decl.  $-33^{\circ} 20'$

19.952	168.7	31.79	4.2	$2\frac{1}{2}$	370
19.974	168.8	31.78	3.4	$2\frac{1}{2}$	370
19.96	168.7	31.78	(9.0 ... 9.4)		N

$h 3719$

Ver la nota

173

$h 3722$ ;  $-74^{\circ} 309$ ; 9.5

A.R.  $4^h 58^m 51^s$ ; Decl.  $-74^{\circ} 25'$

18.175	159.2	26.35	9.4	$2\frac{1}{2}$	370
18.186	159.4	26.38	8.0	2	370
18.18	159.3	26.36	(9.8 ... 10.0)		R?

J 47 =  $\beta 750$  = Rus 56;  $\gamma$  Caeli; 6.0

A.R.  $4^h 59^m 55^s$ ; Decl.  $-35^{\circ} 39'$

19.944	310.1	3.31	4.5	$2\frac{1}{2}$	370
19.974	309.8	3.20	3.6	3	370
19.979	310.1	3.32	4.1	$2\frac{1}{2}$	370
19.97	310.0	3.28	(4.5 ... 8.8)		F

$h 3725$ ;  $-39^{\circ} 583 + 2$ ;  $9.8 + 9.4$

A.R.  $5^h 2^m 52^s$ ; Decl.  $-39^{\circ} 49'$

19.990	323.5	24.44	3.7	$2\frac{1}{2}$	370
19.993	323.6	24.46	3.5	$2\frac{1}{2}$	370
19.99	323.6	24.45	(9.2 ... 9.6)		F?

$h 3726$ ;  $-45^{\circ} 564$ ; 9.8 :

A.R.  $5^h 3^m 0^s$ ; Decl.  $-45^{\circ} 50'$

20.004	62.9	18.36	3.4	$2\frac{1}{2}$	370
20.009	62.5	18.47	4.1	$2\frac{1}{2}$	370
20.01	62.7	18.41	(10.2 ... 10.8)		F?

$h 3733$ ;  $-79^{\circ} 162 + 3$ ;  $9.7 + 9.8$

A.R.  $5^h 3^m 18^s$ ; Decl.  $-79^{\circ} 34'$

18.961	113.0	19.92	4.8	$1\frac{1}{2}$	370
18.963	113.6	19.86	3.8	2	370
18.96	113.3	19.89	(9.4 ... 9.7)		N

Hg 2;  $-74^{\circ} 312$ ; 7.1

A.R.  $5^h 4^m 25^s$ ; Decl.  $-74^{\circ} 31'$

18.030	171.1	1.15	8.3	2	475
18.175	170.7	1.05	9.7	2	370
18.186	172.9	1.15	8.3	$2\frac{1}{2}$	475
18.13	171.6	1.12	(7.7 ... 8.2)		M?

$h 3728$ ;  $-41^{\circ} 638$ ; 7.4

A.R.  $5^h 4^m 30^s$ ; Decl.  $-41^{\circ} 23'$

19.990	259.8	10.02	3.8	$2\frac{1}{2}$	370
19.998	259.6	9.82	3.3	2	370
20.004	259.6	10.19	3.5	$2\frac{1}{2}$	370
20.00	259.7	10.01	(7.2 ... 10.4)		20

$h$  3730;  $-35^{\circ} 606$ ; 9.0A.R. 5<sup>h</sup> 5<sup>m</sup> 33<sup>s</sup>; Decl.  $-35^{\circ} 27'$ 

19.952	343.0	9.97	4.4	2	370
19.974	342.8	9.87	3.8	2½	370
19.979	341.6	10.03	4.2	1½	370
19.97	342.5	9.96	(9.0 ... 12.3)		N

 $h$  3741;  $-78^{\circ} 165$ ; 7.6A.R. 5<sup>h</sup> 6<sup>m</sup> 58<sup>s</sup>; Decl.  $-78^{\circ} 28'$ 

18.961	112.1	46.26	5.0	1	370
18.963	112.1	46.59	3.9	2	370
19.155	112.4	46.54	8.4	1½	370
19.03	112.2	46.46	(6.8 ... 10.2)		D?

 $h$  3735;  $-32^{\circ} 740$ ; 7.4A.R. 5<sup>h</sup> 8<sup>m</sup> 51<sup>s</sup>; Decl.  $-32^{\circ} 3'$ 

19.008	151.7	7.20	7.9	2½	370
19.013	152.6	7.29	4.0	3	370
19.103	151.6	7.31	7.2	2	370
19.04	152.0	7.27	(8.2 ... 8.4)		F

 $h$  3737;  $-36^{\circ} 671$ ; 9.8A.R. 5<sup>h</sup> 9<sup>m</sup> 2<sup>s</sup>; Decl.  $-36^{\circ} 12'$ 

19.974	311.1	19.02	3.9	2½	370
19.979	311.8	19.60	4.4	1½	370
19.982	311.3	19.79	4.2	2	370
19.98	311.4	19.47	(9.4 ... 12.4)		N

 $h$  3740;  $-36^{\circ} 679 + 8$ ; 7.4 + 9.1A.R. 5<sup>h</sup> 10<sup>m</sup> 46<sup>s</sup>; Decl.  $-36^{\circ} 48'$ 

19.928	286.9	23.93	6.2	2	370
19.974	286.6	23.83	4.1	2½	370
19.95	286.7	23.88	(7.2 ... 8.9)		F

Hu 1389;  $-31^{\circ} 740$ ; 8.4A.R. 5<sup>h</sup> 11<sup>m</sup> 28<sup>s</sup>; Decl.  $-31^{\circ} 6'$ 

19.221	117.1	1.01	8.9	2	650
19.243	112.4	1.07	8.9	3	650
19.251	115.6	0.93	8.5	2	650
19.24	115.0	1.00	(8.2 ... 9.0)		N

 $\delta$  38;  $-33^{\circ} 748$ ; 9.2A.R. 5<sup>h</sup> 11<sup>m</sup> 57<sup>s</sup>; Decl.  $-33^{\circ} 13'$ 

19.008	175.2	0.95	8.3	2½	370
19.013	174.6	0.95	4.2	2½	370
19.125	171.0	0.94	6.5	2	475
19.05	173.6	0.95	(9.6 ... 10.1)		

 $\delta$  39;  $-30^{\circ} 839$ ; 9.4A.R. 5<sup>h</sup> 13<sup>m</sup> 7<sup>s</sup>; Decl.  $-30^{\circ} 16'$ 

19.013	192.1	1.90	4.8	3	370
19.111	190.2	2.00	6.7	1½	475
19.125	189.6	1.99	6.7	2	475
19.08	190.6	1.96	(9.5 ... 10.5)		

 $h$  3744 = I 735;  $-38^{\circ} 601$ ; 8.6A.R. 5<sup>h</sup> 13<sup>m</sup> 22<sup>s</sup>; Decl.  $-38^{\circ} 6'$ 

19.990	286.2	4.21	4.1	2½	370
19.998	285.3	4.37	3.5	2½	370
20.004	286.3	4.08	3.7	2½	370
20.00	285.9	4.22	(9.8 ... 10.4)		F

 $h$  3745;  $-34^{\circ} 634$ ; 7.8A.R. 5<sup>h</sup> 13<sup>m</sup> 30<sup>s</sup>; Decl.  $-34^{\circ} 10'$ 

19.974	169.1	13.50	4.3	2½	370
19.982	169.0	13.86	4.4	2½	370
19.985	169.2	13.84	4.2	2½	370
19.98	169.1	13.73	(8.6 ... 10.6)		D?

 $h$  3749;  $-30^{\circ} 844 + 5$ ; 9.7 + 10.0A.R. 5<sup>h</sup> 14<sup>m</sup> 43<sup>s</sup>; Decl.  $-30^{\circ} 12'$ 

18.230	144.6	20.36	9.0	2	370
18.238	144.2	20.40	8.8	1½	370
19.013	144.7	20.44	4.6	3	370
18.49	144.5	20.40	(9.8 ... 10.0)		N

 $h$  3751;  $-33^{\circ} 766 + 5$ ; 9.2 + 10.4A.R. 5<sup>h</sup> 15<sup>m</sup> 47<sup>s</sup>; Decl.  $-33^{\circ} 31'$ 

19.008	321.6	20.49	8.7	2	370
19.013	321.9	20.35	4.4	3	370
19.01	321.8	20.42	(9.0 ... 10.3)		D?

 $h$  3753;  $-35^{\circ} 637$ ; 9.4A.R. 5<sup>h</sup> 16<sup>m</sup> 50<sup>s</sup>; Decl.  $-35^{\circ} 50'$ 

19.974	183.3	7.21	4.5	2½	370
19.982	183.9	7.24	4.5	2½	370
19.985	184.6	7.25	4.3	2½	370
19.990	183.4	7.16	4.2	2½	370
19.98	183.8	7.22	(9.4 ... 10.1)		R?

 $h$  3757;  $-31^{\circ} 780$ ; 7.6A.R. 5<sup>h</sup> 18<sup>m</sup> 31<sup>s</sup>; Decl.  $-31^{\circ} 52'$ 

19.013	306.2	15.61	5.0	2½	370
19.103	307.9	15.82	7.3	1½	370
19.111	307.3	15.75	6.9	1½	370
19.08	307.1	15.73	(7.5 ... 11.5)		R?

*h* 3809;  $-87^{\circ} 76$ ; 9.0  
 A.R. 5<sup>h</sup> 20<sup>m</sup> 25<sup>s</sup>; Decl.  $-87^{\circ} 20'$

19.174	225.8	18.80	9.2	2	370
19.177	226.0	18.88	8.6	2	370
19.18	225.9	18.84	(8.8 ... 11.6)		5

*h* 3760;  $-35^{\circ} 650$ ; 7.6  
 A.R. 5<sup>h</sup> 21<sup>m</sup> 26<sup>s</sup>; Decl.  $-35^{\circ} 28'$

19.944	221.9	7.58	4.7	2½	370
19.974	222.1	7.54	4.8	2	370
19.982	221.4	7.63	4.6	2½	370
19.97	221.8	7.58	(7.9 ... 8.8)		F

AC

19.944	281.0	25.70	4.9	2	370
19.974	281.2	25.72	4.7	2	370
19.96	281.1	25.71	(7.9 ... 10.4)		142

*h* 3762;  $-32^{\circ} 819$ ; 7.7  
 A.R. 5<sup>h</sup> 23<sup>m</sup> 12<sup>s</sup>; Decl.  $-32^{\circ} 31'$

19.103	211.7	25.76	7.5	1	370
19.125	212.2	25.46	6.8	2½	370
19.133	212.4	25.48	7.5	2	370
19.12	212.1	25.57	(7.1 ... 13.1)		N

*h* 3773;  $-82^{\circ} 116$ ; 8.8  
 A.R. 5<sup>h</sup> 24<sup>m</sup> 40<sup>s</sup>; Decl.  $-82^{\circ} 25'$

19.158	279.5	19.01	8.4	2	370
19.169	280.2	18.49	9.6	2	370
19.177	278.9	18.77	7.8	2	370
19.17	279.5	18.76	(9.1 ... 10.4)		F

*h* 3769;  $-40^{\circ} 741$ ; 8.8  
 A.R. 5<sup>h</sup> 27<sup>m</sup> 50<sup>s</sup>; Decl.  $-40^{\circ} 28'$

19.985	276.9	5.89	4.5	2½	370
19.990	275.8	5.74	4.4	2½	370
19.998	275.6	5.86	3.6	2½	370
19.99	276.1	5.83	(10.2 ... 11.5)		N

*h* 3771;  $-69^{\circ} 378$ ; Neb.  
 A.R. 5<sup>h</sup> 28<sup>m</sup> 31<sup>s</sup>; Decl.  $-69^{\circ} 14'$

18.191	76.4	5.55	7.8	2	370
18.194	77.8	5.85	7.6	2	370
18.202	74.5	5.57	7.1	1½	370
18.20	76.2	5.66	(11.4 ... 13.0)		174

*h* 3775;  $-69^{\circ} 383$ ; Neb.  
 A.R. 5<sup>h</sup> 29<sup>m</sup> 14<sup>s</sup>; Decl.  $-69^{\circ} 14'$

18.191	236.8	9.29	8.1	2	370
18.194	237.3	9.49	7.7	2	370
18.202	236.5	9.22	7.2	2	370
18.20	236.9	9.33	(11.3 ... 12.7)		175

*h* 3774;  $-56^{\circ} 872$ ; 10.0  
 A.R. 5<sup>h</sup> 30<sup>m</sup> 22<sup>s</sup>; Decl.  $-56^{\circ} 5'$

17.118	30.7	9.87	8.3	2	370
19.136	28.5	9.60	7.1	1½	370
19.201	27.7	10.61	8.2	1½	370
18.48	29.0	10.03	(10.4 ... 13.5)		120

*h* 3779;  $-66^{\circ} 424$ ; Neb.  
 A.R. 5<sup>h</sup> 30<sup>m</sup> 26<sup>s</sup>; Decl.  $-66^{\circ} 58'$

18.025	350.9	4.47	10.3	2	370
18.044	353.0	4.69	7.2	2	370
18.194	352.5	4.98	7.5	2	370
18.09	352.1	4.71	(10.8 ... 12.3)		176

AC; C = 13.0

18.191	305.6	7.68	7.3	2	370
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Aa; a = 12.5

18.191	256:	2.4:	7.2	2	370
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*h* 3772;  $-31^{\circ} 847$ ; 8.9  
 A.R. 5<sup>h</sup> 31<sup>m</sup> 0<sup>s</sup>; Decl.  $-31^{\circ} 32'$

19.103	51.7	11.61	7.7	1½	370
19.125	51.3	11.26	7.0	2½	370
19.136	51.2	11.22	7.8	2½	370
19.12	51.4	11.36	(9.7 ... 9.9)		N

*h* 3782;  $-41^{\circ} 768$ ; 9.1  
 A.R. 5<sup>h</sup> 34<sup>m</sup> 21<sup>s</sup>; Decl.  $-41^{\circ} 17'$

19.824	64.3	20.65	2.5	2	370
19.985	64.3	20.77	4.6	2½	370
19.90	64.3	20.71	(9.5 ... 11.4)		N

*h* 3781;  $-41^{\circ} 770$ ; 7.6  
 A.R. 5<sup>h</sup> 34<sup>m</sup> 39<sup>s</sup>; Decl.  $-41^{\circ} 22'$

19.824	134.8	15.98	2.6	2	370
19.985	135.0	15.99	4.8	2½	370
19.90	134.9	15.99	(8.1 ... 9.6)		88

\* *h* 3784;  $-46^{\circ} 609$ ; 8.0  
 A.R. 5<sup>h</sup> 34<sup>m</sup> 40<sup>s</sup>; Decl.  $-46^{\circ} 10'$

20.927	63.8	5.31	6.1	2½	370
20.932	64.3	5.25	6.5	3	370
20.979	65.0	5.25	5.5	3½	370
20.95	64.4	5.27	(7.2 Y ... 9.2 O)		M

*h* 3795;  $\gamma$  Mensae; 7.1  
 A.R. 5<sup>h</sup> 36<sup>m</sup> 51<sup>s</sup>; Decl.  $-76^{\circ} 26'$

18.175	106.7	38.08	10.1	1½	370
18.186	107.0	38.29	9.0	2	370
18.219	107.0	38.34	8.8	2	370
18.19	106.9	38.24	(5.5 ... 11.1)		R?

## I 740; —35° 713; 8.0

A.R. 5<sup>h</sup> 36<sup>m</sup> 55<sup>s</sup>; Decl. —35° 19'

20.154	193.4	0.57	7.1	2	475
20.157	194.2	0.50	8.0	2½	650
20.16	193.8	0.53	(9.3 ... 9.6)		P

## I 347; —75° 321; 8.0

A.R. 5<sup>h</sup> 37<sup>m</sup> 8<sup>s</sup>; Decl. —75° 19'

18.175	126.0	8.91	9.9	2	370
18.186	127.8	8.73	8.6	2	370
18.205	126.6	9.01	8.4	1½	370
18.19	126.8	8.88	(8.1 ... 12.7)		

## h 3794 —34° 719; 7.7

A.R. 5<sup>h</sup> 38<sup>m</sup> 22<sup>s</sup>; Decl. —34° 1'

19.103	277.9	23.41	7.8	1	370
19.125	278.5	23.54	7.4	2½	370
19.11	278.2	23.48	(7.0 ... 12.0)		51

## h 3796; —69° 456; Neb.

A.R. 5<sup>h</sup> 39<sup>m</sup> 36<sup>s</sup>; Decl. —69° 10'

17.031	186.1	11.47	5.6	2	370
18.191	181.9	11.95	8.4	2	370
18.194	186.0	11.36	7.9	2	370
17.81	184.7	11.59	(9.3 ... 13.3)		

## AC

18.194	299.1	11.19	8.0	2	370
18.219	295.1	11.02	8.6	2	370
18.21	297.1	11.10	(9.3 ... 12.9)		

## Ac

18.191	295.6	11.75	8.5	2	370
18.210	286.0	11.40	7.7	2	370
18.20	290.8	11.58	(9.3 ... 12.8)		

## AD

18.191	51.8	12.17	8.7	2	370
18.194	52.1	12.30	8.2	2	370
18.19	52.0	12.24	(9.3 ... 13.6)		

## AE

18.191	3.8	20.31	8.9	2	370
18.194	4.3	20.36	8.4	1½	370
18.19	4.0	20.33	(9.3 ... 11.7)		

## AF

18.202	47.0	22.18	8.4	2	370
18.205	47.8	22.24	7.7	1½	370
18.20	47.4	22.21	(9.3 ... 12.3)		

## AG

18.202	135.7	25.92	8.5	2	370
18.205	136.6	26.31	7.9	1½	370
18.20	136.1	26.11	(9.3 ... 12.3)		

(Sigue Continued.)

## Aa

18.202	345.6	7.25	8.8	2	370
18.219	347.2	7.64	8.5	2½	370
18.21	346.4	7.45	(9.3 ... 13.7)		

## Cape; —89° 17; 9.9

A.R. 5<sup>h</sup> 40<sup>m</sup> 36<sup>s</sup>; Decl. —89° 32'

19.177	96.9	6.71	8.2	2	370
19.182	97.9	6.82	7.6	2	370
19.18	97.4	6.76	(10.6 ... 11.2)		

## h 3817; —80° 160; 8.9

A.R. 5<sup>h</sup> 45<sup>m</sup> 59<sup>s</sup>; Decl. —80° 25'

18.963	243.6	17.38	4.2	1½	370
19.155	243.9	17.43	8.6	2	370
19.06	243.8	17.41	(9.1 ... 10.7)		R

## h 3814; —74° 349; 8.7

A.R. 5<sup>h</sup> 46<sup>m</sup> 32<sup>s</sup>; Decl. —74° 55'

19.955	175.3	4.23	4.9	2½	370
19.971	175.5	4.32	4.9	2½	370
20.092	175.7	4.65	7.6	2	370
20.097	174.5	4.51	8.7	2½	370
20.03	175.2	4.43	(9.3 ... 9.3)		F?

## h 3806; Cód —39° 2221; 10

A.R. 5<sup>h</sup> 46<sup>m</sup> 35<sup>s</sup>; Decl. —39° 29'

19.985	115.2	14.47	5.0	3	370
19.990	114.9	14.43	4.5	2½	370
19.998	114.7	14.48	3.8	2½	370
19.99	114.9	14.46	(11.1 ... 11.5)		D?

## h 3807; —41° 831; 8.2

A.R. 5<sup>h</sup> 47<sup>m</sup> 42<sup>s</sup>; Decl. —41° 43'

19.985	272.0	5.18	4.9	2½	370
19.998	270.9	5.18	3.9	2	370
20.004	271.8	5.10	3.8	2½	370
20.00	271.6	5.15	(8.3 ... 11.2)		C

## Hu 1396; —30° 1071; 8.5

A.R. 5<sup>h</sup> 49<sup>m</sup> 0<sup>s</sup>; Decl. —30° 42'

19.221	139.1	1.87	9.3	2	475
19.243	142.7	1.78	9.1	3	650
19.251	139.1	2.12	8.8	2	650
19.253	138.2	1.58	7.7	2	650
19.24	139.8	1.84	(8.8 ... 10.6)		

*h* 3819;  $\gamma$  Columbae; 3.6

A.R. 5<sup>h</sup> 53<sup>m</sup> 6<sup>s</sup>; Decl. -35° 18'

19.982	110.0	34.09	4.8	2½	370
19.985	109.2	33.75	5.1	3	370
19.998	109.4	33.77	4.3	2	370
19.99	109.5	33.87	(4.6 ... 12.7)		N

*h* 3823; -31° 976; 8.6

A.R. 5<sup>h</sup> 55<sup>m</sup> 40<sup>s</sup>; Decl. -31° 3'

19.013	277.9	1.88	5.3	3	370
19.125	276.6	2.05	7.5	2½	370
19.136	277.2	2.03	7.9	2½	370
19.221	276.2	2.08	9.5	2	475
19.12	277.0	2.01	(8.3 ... 8.6)		

BC = Hu 1399

19.013	319.9	0.75	5.5	2½	370
19.125	315.6	0.81	7.6	2½	475
19.136	306.6	0.85	8.0	2½	370
19.221	306.8	0.86	9.6	2	475
19.12	312.2	0.82	(8.6 ... 9.5)		

*h* 3826; -41° 867; 9.3

A.R. 5<sup>h</sup> 57<sup>m</sup> 3<sup>s</sup>; Decl. -41° 28'

19.985	156.2	15.68	5.3	3	370
19.998	156.0	16.05	4.1	2	370
20.004	156.2	15.70	4.1	2½	370
20.00	156.1	15.81	(10.2 ... 11.8)		N

*h* 3827; -41° 873 + 2; 8.7 + 8.7

A.R. 5<sup>h</sup> 57<sup>m</sup> 48<sup>s</sup>; Decl. -41° 10'

19.985	243.9	23.22	5.4	3	370
19.998	244.0	23.43	4.2	2	370
19.99	244.0	23.32	(9.1 ... 9.4)		F

*h* 3832; -33° 1005; 9.0:

A.R. 6<sup>h</sup> 0<sup>m</sup> 58<sup>s</sup>; Decl. -33° 16'

19.125	150.1	13.14	7.7	2½	370
19.136	149.4	13.02	8.2	2½	370
19.13	149.8	13.08	(9.7 ... 9.9)		N

\* *h* 3834; -45° 755; 7.2

A.R. 6<sup>h</sup> 1<sup>m</sup> 4<sup>s</sup>; Decl. -45° 5'

20.927	223.5	4.47	4.7	2½	370
20.932	224.1	4.35	6.6	3	370
20.973	223.8	4.36	5.8	2½	370
20.94	223.8	4.39	(6.5 ... 9.0 R)		D

$\Delta$  23; -48° 777; 7.4

A.R. 6<sup>h</sup> 1<sup>m</sup> 32<sup>s</sup>; Decl. -48° 27'

20.927	64.5	1.85	4.8	2½	370
20.932	64.7	1.85	6.7	3	370
20.973	65.7	2.06	5.9	2½	370
20.979	65.1	1.83	5.6	4	370
20.95	65.0	1.90	(7.4 Y ... 7.7 Y)		P

*h* 3844; -69° 575; 9.0

A.R. 6<sup>h</sup> 8<sup>m</sup> 57<sup>s</sup>; Decl. -69° 40'

18.191	91.4	13.13	9.2	2	370
18.197	91.1	13.16	8.9	2	370
18.19	91.2	13.14	(9.0 ... 12.4)		N

AC; C = 11.0

18.191	135.2	34.76	9.4	2	370
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*h* 3840; -30° 1175; 9.5

A.R. 6<sup>h</sup> 9<sup>m</sup> 7<sup>s</sup>; Decl. -30° 28'

18.252	230.9	12.01	10.3	1½	370
18.273	231.0	12.04	9.9	2	370
19.125	231.9	11.88	7.9	2	370
18.55	231.3	11.98	(10.2 ... 10.6)		

\* *h* 3846 = Cape 23; -49° 895; 8.6

A.R. 6<sup>h</sup> 11<sup>m</sup> 10<sup>s</sup>; Decl. -49° 4'

20.927	61.5	4.61	5.0	2½	370
20.932	61.6	4.76	6.8	3	370
20.93	61.6	4.69	(9.0 ... 10.0)		D?

*h* 3855; -74° 376; 8.9

A.R. 6<sup>h</sup> 15<sup>m</sup> 38<sup>s</sup>; Decl. -74° 28'

18.186	79.8	8.69	9.5	2	370
18.219	79.8	8.59	9.0	2½	370
18.317	80.3	8.57	8.9	2½	370
18.24	80.0	8.62	(9.4 ... 9.8)		F

AC

18.219	2.0	25.99	9.1	2	370
18.317	1.2	25.56	9.0	2	370
18.27	1.6	25.78	(9.4 ... 12.1)		

*h* 3849; -39° 904 + 6; 7.8 + 8.5

A.R. 6<sup>h</sup> 15<sup>m</sup> 41<sup>s</sup>; Decl. -39° 26'

20.009	52.9	39.83	4.3	2½	370
20.094	52.7	39.86	7.9	2	370
20.05	52.8	39.84	(7.4 ... 8.7)		F

$h$  3857;  $-36^{\circ} 9'45''$ ; 7.2A.R.  $6^h 19^m 41^s$ ; Decl.  $-36^{\circ} 39'$ 

19.944	255.9	13.23	5.1	2	370
19.974	254.8	13.23	5.1	2	370
19.96	255.4	13.23	(6.5 ... 10.8)		F

AC =  $\Delta$  28; C =  $-36^{\circ} 9'47''$ ; 7.7

19.944	69.9	66.27	5.3	2	370
19.974	70.2	66.30	5.2	$1\frac{1}{2}$	370
19.96	70.0	66.28	(6.5 ... 7.2)		R <sup>2</sup>

 $h$  3858;  $-34^{\circ} 9'26''$ ; 7.4A.R.  $6^h 21^m 10^s$ ; Decl.  $-34^{\circ} 58'$ 

19.944	313.4	3.90	5.5	3	370
19.982	313.0	3.86	5.3	3	370
19.985	313.6	3.83	5.5	3	475
19.97	313.3	3.86	(7.7 ... 8.6)		5

 $h$  3862;  $-67^{\circ} 5'78''$ ; 8.8A.R.  $6^h 21^m 33^s$ ; Decl.  $-67^{\circ} 31'$ 

18.191	288.1	7.69	9.6	2	370
18.197	288.1	7.66	9.1	2	370
18.205	289.4	7.69	8.0	$1\frac{1}{2}$	370
18.20	288.5	7.68	(8.9 ... 11.9)		N

\*  $h$  3861;  $-58^{\circ} 6'90''$ ; 8.6A.R.  $6^h 21^m 38^s$ ; Decl.  $-58^{\circ} 7'$ 

20.927	72.0	2.14	5.2	$2\frac{1}{2}$	370
20.951	73.4	2.26	6.3	$2\frac{1}{2}$	370
20.973	73.7	2.17	6.1	$2\frac{1}{2}$	370
20.95	73.0	2.19	(9.0 ... 9.3)		M

 $h$  3860;  $-40^{\circ} 10'11''$ ; 7.5A.R.  $6^h 21^m 47^s$ ; Decl.  $-40^{\circ} 54'$ 

20.004	227.4	8.54	4.2	2	370
20.094	220.8	8.75	8.0	2	370
20.097	227.2	8.64	7.3	3	370
20.07	227.1	8.64	(7.4 ... 9.2)		F

 $h$  3868;  $-75^{\circ} 3'74''$ ; 8.9A.R.  $6^h 23^m 12^s$ ; Decl.  $-75^{\circ} 10'$ 

18.219	146.6	26.15	9.4	2	370
18.325	145.2	26.05	9.5	$1\frac{1}{2}$	370
18.808	147.4	25.75	5.2	2	370
18.45	146.4	25.98	(8.4 ... 13.8)		N

AC

18.219	57.9	40.42	9.7	$1\frac{1}{2}$	370
18.325	58.0	40.01	9.3	$1\frac{1}{2}$	370
18.808	56.7	40.54	5.4	2	370
18.45	57.5	40.32	(8.4 ... 13.3)		N

 $\beta$  753;  $-32^{\circ} 11'76''$ ; 5.7A.R.  $6^h 24^m 1^s$ ; Decl.  $-32^{\circ} 17'$ 

20.075	51.1	1.52	8.3	2	370
20.081	46.3	1.40	8.3	3	650
20.094	43.4	1.54	7.6	$2\frac{1}{2}$	475
20.097	44.7	1.54	7.1	3	650
20.09	46.4	1.50	(6.7 ... 9.1)		177

 $h$  3872; Anon.A.R.  $6^h 24^m 53^s$ ; Decl.  $-79^{\circ} 55'$ 

19.158	24.0	22.16	8.6	2	370
19.169	23.7	22.07	10.2	2	370
19.16	23.8	22.12	(9.9 ... 10.1)		N

 $\Delta$  29;  $-40^{\circ} 10'31'' + 2''$ ;  $8.4 + 8.6$ A.R.  $6^h 25^m 4^s$ ; Decl.  $-40^{\circ} 17'$ 

20.004	113.8	67.73	4.3	$2\frac{1}{2}$	370
20.094	113.8	67.70	8.1	$2\frac{1}{2}$	370
20.05	113.8	67.72	(7.8 ... 8.1)		

Hargrave;  $-75^{\circ} 3'86''$ ; 7.9A.R.  $6^h 25^m 20^s$ ; Decl.  $-75^{\circ} 3'$ 

18.219	58.9	2.76	10.0	$1\frac{1}{2}$	370
18.317	55.9	2.77	9.2	2	370
18.808	55.0	—	5.6	$2\frac{1}{2}$	370
18.958	55.7	3.06	7.2	2	370
18.58	56.4	2.86	(8.3 ... 11.7)		F

AC =  $h$  3870

18.219	7.0	26.35	9.8	2	370
18.317	8.2	26.14	9.3	2	370
18.958	6.9	26.26	7.3	2	370
18.50	7.4	26.25	(8.3 ... 12.3)		142

I 4;  $-40^{\circ} 10'43''$ ; 7.2A.R.  $6^h 26^m 38^s$ ; Decl.  $-40^{\circ} 22'$ 

20.094	301.6	1.09	8.3	$2\frac{1}{2}$	475
20.097	301.0	1.08	7.4	3	650
20.113	301.5	0.83	5.7	$2\frac{1}{2}$	370
20.10	301.4	1.00	(7.2 ... 7.4)		20

 $h$  3869;  $-31^{\circ} 12'18''$ ; 5.4A.R.  $6^h 27^m 59^s$ ; Decl.  $-31^{\circ} 56'$ 

19.125	258.0	24.88	8.1	2	370
19.136	257.8	24.95	8.3	2	370
19.13	257.9	24.92	(6.6 ... 9.1)		R <sup>2</sup>

\*  $h$  3874;  $\mu$  Pictoris; 5.4A.R.  $6^h 30^m 6^s$ ; Decl.  $-58^{\circ} 40'$ 

20.927	231.9	2.72	5.3	$2\frac{1}{2}$	370
20.973	234.6	2.80	6.2	2	370
21.061	233.1	2.70	8.2	3	370
20.99	233.2	2.74	(6.2 ... 10.6)		20

$\beta$  754;  $-33^{\circ}$  1235; 7.1

A.R. 6<sup>h</sup> 30<sup>m</sup> 11<sup>s</sup>; Decl.  $-33^{\circ}$  55'

20.081	41.8	0.89	8.5	3½	650
20.094	39.4	0.90	7.7	2½	475
20.097	40.4	1.07	7.2	3	650
20.09	40.5	0.95	(7.5 ... 7.7)		C

$\beta$  755;  $-36^{\circ}$  1001; 6.0

A.R. 6<sup>h</sup> 31<sup>m</sup> 4<sup>s</sup>; Decl.  $-36^{\circ}$  41'

19.944	258.2	1.38	5.9	2½	370
19.982	257.2	1.33	5.6	3	475
19.985	258.9	1.28	5.6	2½	475
19.97	258.1	1.33	(6.7 ... 7.6)		F

AC = h 3875

19.982	299.9	21.50	5.7	3	475
19.985	300.4	21.51	5.7	2½	475
19.98	300.1	21.50	(6.7 ... 11.6)		F

$\delta$  40;  $-36^{\circ}$  1009; 7.8

A.R. 6<sup>h</sup> 31<sup>m</sup> 52<sup>s</sup>; Decl.  $-36^{\circ}$  33'

19.982	146.5	5.22	5.8	2½	475
19.985	149.8	5.20	5.8	2	475
20.056	146.9	5.35	7.3	2	370
20.01	147.7	5.26	(8.7 ... 13.8)		

$\delta$  41;  $-35^{\circ}$  979; 9.4

A.R. 6<sup>h</sup> 31<sup>m</sup> 53<sup>s</sup>; Decl.  $-35^{\circ}$  56'

19.982	100.6	2.25	5.9	2½	370
20.056	99.1	2.20	7.4	2	370
20.081	98.8	2.33	8.0	3	370
20.04	99.5	2.26	(9.8 ... 12.3)		

h 3880;  $-66^{\circ}$  567; 9.4

A.R. 6<sup>h</sup> 32<sup>m</sup> 33<sup>s</sup>; Decl.  $-66^{\circ}$  10'

18.191	81.5	5.02	9.8	2½	370
* 17.41	81.6	5.01	(10.4 ... 10.5)		4 n

h 3878;  $-35^{\circ}$  985; 10.0

A.R. 6<sup>h</sup> 33<sup>m</sup> 7<sup>s</sup>; Decl.  $-35^{\circ}$  50'

19.982	13.5	11.74	6.2	3	370
20.056	11.9	11.94	7.5	2	370
20.081	12.8	11.76	8.1	3	370
20.04	12.7	11.81	(11.1 ... 12.4)		178

h 3881;  $-40^{\circ}$  1100; 8.1

A.R. 6<sup>h</sup> 34<sup>m</sup> 52<sup>s</sup>; Decl.  $-40^{\circ}$  28'

20.004	160.0	28.49	4.5	2½	370
20.094	160.6	28.31	8.4	2	370
20.097	160.5	28.46	7.5	3	370
20.07	160.4	28.42	(7.9 ... 11.5)		N

h 3888;  $-78^{\circ}$  232 + 3; 7.9 + 9.5

A.R. 6<sup>h</sup> 36<sup>m</sup> 15<sup>s</sup>; Decl.  $-78^{\circ}$  49'

19.158	116.4	35.59	8.8	2	370
19.169	116.0	35.78	10.5	2	370
19.183	116.0	35.80	9.3	2	370
19.17	116.1	35.72	(7.3 ... 9.8)		F

h 3885;  $-69^{\circ}$  638; 8.0

A.R. 6<sup>h</sup> 36<sup>m</sup> 55<sup>s</sup>; Decl.  $-69^{\circ}$  59'

18.197	172.9	4.50	9.3	2½	370
18.202	173.1	4.64	9.0	2½	370
18.205	174.7	4.42	8.2	1½	370
18.20	173.6	4.52	(8.8 ... 11.6)		N

h 5443;  $-40^{\circ}$  1111; 6.5

A.R. 6<sup>h</sup> 37<sup>m</sup> 10<sup>s</sup>; Decl.  $-40^{\circ}$  14'

20.154	107.6	15.38	7.2	2½	370
20.176	106.9	15.74	7.2	2½	370
20.209	107.5	15.63	8.8	2	370
20.18	107.3	15.58	(6.8 ... 10.6)		F

h 3892;  $-80^{\circ}$  184; 9.4

A.R. 6<sup>h</sup> 37<sup>m</sup> 38<sup>s</sup>; Decl.  $-80^{\circ}$  59'

19.158	219.3	27.29	8.9	2	370
19.182	218.6	27.26	9.0	2	370
19.17	218.9	27.27	(9.7 ... 9.8)		F

$\Delta$  32;  $-38^{\circ}$  982; 7.0

A.R. 6<sup>h</sup> 38<sup>m</sup> 1<sup>s</sup>; Decl.  $-38^{\circ}$  17'

20.004	277.0	8.16	4.9	2	370
20.081	276.6	8.25	8.7	3	370
20.04	276.8	8.21	(6.9 ... 7.9)		F

h 3887;  $-43^{\circ}$  989; 9.6

A.R. 6<sup>h</sup> 39<sup>m</sup> 19<sup>s</sup>; Decl.  $-43^{\circ}$  25'

20.004	251.7	7.03	4.7	2½	370
20.094	252.2	7.05	8.5	2½	370
20.097	251.8	7.07	7.6	3	370
20.07	251.9	7.05	(10.6 ... 11.1)		179

h 3891;  $-30^{\circ}$  1408; 6.3

A.R. 6<sup>h</sup> 40<sup>m</sup> 46<sup>s</sup>; Decl.  $-30^{\circ}$  49'

19.125	222.0	5.20	8.4	2½	370
19.136	223.1	5.03	8.4	2½	370
19.221	222.1	5.18	9.8	2	475
19.16	222.4	5.14	(6.4 ... 8.9)		F

*h* 3903;  $-85^{\circ} 86$ ; 10.1A.R. 6<sup>h</sup> 41<sup>m</sup> 3<sup>s</sup>; Decl.  $-85^{\circ} 1'$ 

19.158	252.7	21.24	9.4	1½	370
19.182	251.7	21.45	8.6	2	370
19.199	252.5	21.14	10.4	1½	370
19.18	252.3	21.28	(9.3 ... 12.6)		N

*h* 3893;  $-37^{\circ} 1046 + 5$ ; 6.0 + 9.8A.R. 6<sup>h</sup> 43<sup>m</sup> 5<sup>s</sup>; Decl.  $-37^{\circ} 48'$ 

19.985	298.8	65.36	6.0	2	370
20.081	299.1	65.37	8.9	3	370
20.097	298.9	65.58	7.8	2½	370
20.05	298.9	65.44	(5.3 ... 11.1)		N

*h* 3895;  $-47^{\circ} 948$ ; 7.7A.R. 6<sup>h</sup> 43<sup>m</sup> 21<sup>s</sup>; Decl.  $-47^{\circ} 40'$ 

20.209	64.2	26.08	8.7	2	370
20.215	63.9	25.98	8.4	2½	370
20.21	64.0	26.03	(7.4 ... 12.0)		142

*h* 3899; Anon.A.R. 6<sup>h</sup> 44<sup>m</sup> 32<sup>s</sup>; Decl.  $-80^{\circ} 32'$ 

20.149	312.7	11.03	6.3	2	370
20.157	312.2	11.48	6.6	2½	370
20.176	311.5	11.24	7.3	2	370
20.16	312.1	11.25	(10.6 ... 12.4)		N

IIIh 251 =  $\Delta$  36;  $-31^{\circ} 1334 + 6$ ; 6.3 + 7.8A.R. 6<sup>h</sup> 45<sup>m</sup> 40<sup>s</sup>; Decl.  $-31^{\circ} 34'$ 

19.125	65.8	43.27	8.5	2	370
19.136	65.3	42.80	8.5	2	370
19.221	65.2	42.92	10.5	2	370
19.16	65.4	43.00	(6.2 ... 8.1)		F

\* I 181;  $-44^{\circ} 1113$ ; 8.2A.R. 6<sup>h</sup> 46<sup>m</sup> 11<sup>s</sup>; Decl.  $-44^{\circ} 54'$ 

20.927	253.5	0.89	6.5	3	650
21.039	252.0	0.87	5.6	3	370
21.061	252.1	0.77	8.4	3	370
21.01	252.5	0.84	(8.9 ... 9.5)		20

\* I 159;  $-45^{\circ} 1069$ ; 7.8A.R. 6<sup>h</sup> 46<sup>m</sup> 19<sup>s</sup>; Decl.  $-45^{\circ} 18'$ 

20.927	323.5	6.49	6.6	2½	370
21.039	323.9	6.75	5.7	3	370
20.98	323.7	6.62	(6.40 ... 12.2)		F?

\* *h* 3904;  $-74^{\circ} 412$ ; 9.4A.R. 6<sup>h</sup> 49<sup>m</sup> 9<sup>s</sup>; Decl.  $-74^{\circ} 6'$ 

18.317	104.7	8.67	11.1	2	370
18.320	104.8	8.53	10.6	2½	370
18.32	104.8	8.60	(9.7 ... 11.8)		142

*h* 3900;  $-34^{\circ} 1066$ ; 7.2A.R. 6<sup>h</sup> 49<sup>m</sup> 41<sup>s</sup>; Decl.  $-34^{\circ} 4'$ 

19.125	282.9	2.79	8.7	2	370
19.136	283.0	2.53	8.6	2½	370
19.221	282.0	2.63	10.7	2	475
19.16	282.6	2.65	(7.6 ... 9.2)		F

*h* 3901;  $-37^{\circ} 1080 + 79$ ; 7.8 + 9.9A.R. 6<sup>h</sup> 50<sup>m</sup> 45<sup>s</sup>; Decl.  $-37^{\circ} 20'$ 

19.985	218.1	22.25	6.3	2	370
20.056	219.0	22.26	7.7	2½	370
20.02	218.5	22.26	(8.1 ... 11.4)		N

*h* 3911;  $-76^{\circ} 422 + 3$ ; 8.5 + 9.3A.R. 6<sup>h</sup> 52<sup>m</sup> 39<sup>s</sup>; Decl.  $-76^{\circ} 42'$ 

18.317	46.3	21.97	11.4	2	370
18.320	46.9	21.99	10.9	2	370
18.32	46.6	21.98	(7.4 ... 10.4)		180

I 65;  $-35^{\circ} 1065$ ; 6.8A.R. 6<sup>h</sup> 52<sup>m</sup> 49<sup>s</sup>; Decl.  $-35^{\circ} 20'$ 

20.081	225.1	0.29	9.1	3	650
20.097	229.2	0.35	8.0	2½	650
20.09	227.2	0.32	(7.2 ... 7.4)		P

I 66;  $-35^{\circ} 1068$ ; 7.5A.R. 6<sup>h</sup> 53<sup>m</sup> 48<sup>s</sup>; Decl.  $-35^{\circ} 15'$ 

20.056	254.9	2.17	8.0	2½	475
20.081	254.6	2.03	9.2	3	650
20.097	254.4	2.08	8.1	2½	650
20.08	254.6	2.09	(8.2 ... 10.2)		F

AC = *h* 3905

20.056	269.6	14.98	7.9	2½	475
20.081	269.1	14.89	9.3	3	650
20.07	269.3	14.93	(8.2 ... 9.6)		F

*h* 3907;  $-37^{\circ} 1093$ ; 8.0A.R. 6<sup>h</sup> 54<sup>m</sup> 36<sup>s</sup>; Decl.  $-37^{\circ} 35'$ 

19.985	233.1	24.19	6.4	2	370
20.056	232.8	24.48	7.8	2½	370
20.081	232.8	24.23	9.5	3	370
20.04	232.9	24.30	(8.8 ... 12.0)		N



$h$  3918;  $-68^{\circ} 581$ ; 10.1

A.R.  $6^h 56^m 47^s$ ; Decl.  $-68^{\circ} 19'$

18.191	325.4	11.66	10.0	$2\frac{1}{2}$	370
18.197	326.2	11.62	9.5	2	370
18.202	325.7	11.72	9.1	$2\frac{1}{2}$	370
18.20	325.8	11.67	(10.5 ... 11.8)		N

$h$  3926;  $-76^{\circ} 427 + 6$ ;  $9.0 + 9.3$

A.R.  $6^h 57^m 1^s$ ; Decl.  $-76^{\circ} 58'$

18.317	296.5	24.65	11.6	$1\frac{1}{2}$	370
18.320	296.5	24.73	11.0	2	370
18.32	296.5	24.69	(9.4 ... 10.2)		F

$h$  3916;  $-30^{\circ} 1505$ ; 9.0

A.R.  $6^h 57^m 4^s$ ; Decl.  $-30^{\circ} 56'$

19.125	286.0	10.70	8.9	2	370
19.136	285.9	10.76	8.8	$2\frac{1}{2}$	370
19.13	285.9	10.73	(10.0 ... 10.1)		N

$h$  3917;  $-30^{\circ} 1507$ ; 9.1

A.R.  $6^h 57^m 6^s$ ; Decl.  $-30^{\circ} 36'$

19.125	99.4	6.20	9.1	2	370
19.136	99.6	6.36	8.9	2	370
19.221	98.9	6.31	10.9	2	475
19.16	99.3	6.29	(9.5 ... 9.9)		N

\*  $h$  3927;  $-74^{\circ} 422 + 3$ ;  $9.5 + 9.6$

A.R.  $6^h 57^m 58^s$ ; Decl.  $-74^{\circ} 7'$

18.317	16.8	15.01	11.3	$2\frac{1}{2}$	370
18.320	17.0	14.92	10.7	$2\frac{1}{4}$	370
18.32	16.9	14.96	(9.5 ... 9.8)		F

\*  $h$  3920;  $-48^{\circ} 1031$ ; 8.0

A.R.  $6^h 58^m 51^s$ ; Decl.  $-48^{\circ} 49'$

20.927	108.5	5.15	6.7	3	370
21.039	108.9	5.14	6.0	3	370
20.98	108.7	5.14	(9.0 ... 9.3)		F

$h$  3919;  $-35^{\circ} 1095$ ; 8.6

A.R.  $6^h 58^m 55^s$ ; Decl.  $-35^{\circ} 8'$

20.056	258.3	10.31	8.2	$2\frac{1}{2}$	370
20.081	259.0	10.26	9.6	3	370
20.07	258.7	10.28	(9.0 ... 9.6)		F

$h$  3932;  $-77^{\circ} 288$ ; 7.4

A.R.  $7^h 0^m 2^s$ ; Decl.  $-77^{\circ} 37'$

18.317	283.9	8.28	11.8	2	370
18.958	283.5	8.37	7.5	$2\frac{1}{2}$	370
19.089	283.2	8.34	6.8	$2\frac{1}{2}$	370
19.158	284.1	8.26	10.8	2	370
18.88	283.7	8.31	(7.8 ... 10.0)		F

$h$  3928;  $-34^{\circ} 1137$ ; 7.3

A.R.  $7^h 1^m 0^s$ ; Decl.  $-34^{\circ} 35'$

20.056	154.2	3.89	8.3	2	370
20.078	153.3	3.86	7.7	$1\frac{1}{2}$	370
20.081	153.6	3.89	9.7	3	475
20.07	153.7	3.88	(6.8 ... 8.2)		D?

AC; C =  $-34^{\circ} 1135$ ; 9.2

20.056	288.4	37.41	8.3	2	370
20.078	288.4	37.54	7.8	$1\frac{1}{2}$	370
20.07	288.4	37.47	(6.8 ... 9.8)		21

AD

20.056	125.1	38.85	8.4	$1\frac{1}{2}$	370
20.078	125.4	38.59	7.8	$1\frac{1}{2}$	370
20.07	125.2	38.72	(6.8 ... 10.5)		181

$h$  3931;  $-42^{\circ} 1216 + 17$ ;  $7.6 + 8.5$

A.R.  $7^h 2^m 0^s$ ; Decl.  $-42^{\circ} 8'$

20.004	40.5	72.31	5.1	2	370
20.094	40.4	72.40	8.7	2	370
20.05	40.4	72.36	(7.9 ... 9.2)		F

AC; C = 10.5

20.004	212.6	57.33	5.2	$1\frac{1}{2}$	370
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$\beta$  757;  $-36^{\circ} 1169$ ; 6.1

A.R.  $7^h 8^m 0^s$ ; Decl.  $-36^{\circ} 20'$

19.985	68.7	2.91	6.5	2	370
20.056	65.8	2.74	8.5	2	370
20.081	65.0	2.70	10.0	3	475
20.04	66.5	2.78	(6.5 ... 9.3)		F

$h$  3940;  $-30^{\circ} 1573$ ; 7.6

A.R.  $7^h 8^m 24^s$ ; Decl.  $-30^{\circ} 45'$

19.125	99.3	6.95	9.2	2	370
19.133	100.3	6.84	10.3	2	370
19.136	99.7	6.94	9.0	$2\frac{1}{2}$	370
19.13	99.8	6.91	(8.6 ... 10.9)		N

$h$  3942;  $-33^\circ$  1399; 8.7A.R.  $7^h$   $9^m$   $5^s$ ; Decl.  $-33^\circ$   $27'$ 

19.125	38.0	5.41	9.4	$2\frac{1}{2}$	370
19.133	38.1	5.27	10.5	2	370
19.136	38.9	5.51	9.1	$2\frac{1}{2}$	370
19.13	38.3	5.40	(10.1 ... 10.5)		88

Bris 1523;  $-30^\circ$  1600 + 1599; 7.6 + 8.2A.R.  $7^h$   $12^m$   $7^s$ ; Decl.  $-30^\circ$   $40'$ 

19.125	182.2	37.95	9.8	2	370
19.136	182.2	38.04	9.3	2	370
19.13	182.2	38.00	(7.1 ... 8.8)		F

 $h$  3946;  $-33^\circ$  1416; 9.6A.R.  $7^h$   $12^m$   $22^s$ ; Decl.  $-33^\circ$   $2'$ 

19.125	287.6	5.80	9.6	$2\frac{1}{2}$	370
19.136	288.1	6.10	9.2	2	370
19.221	289.5	5.79	11.2	2	370
19.16	288.4	5.90	(10.9 ... 11.8)		N

 $\Delta$  43;  $\pi$  Argus; 6.3A.R.  $7^h$   $12^m$   $45^s$ ; Decl.  $-36^\circ$   $52'$ 

19.985	212.5	69.24	6.6	2	370
20.056	212.7	69.14	8.6	2	370
20.02	212.6	69.19	(2.8 ... 8.6)		21

\*  $h$  3951;  $-50^\circ$  1203; 10.2A.R.  $7^h$   $13^m$   $30^s$ ; Decl.  $-50^\circ$   $46'$ 

20.927	77.9	8.89	6.9	3	370
21.039	77.5	9.02	6.3	$3\frac{1}{2}$	370
21.061	77.6	9.04	7.0	$2\frac{1}{2}$	370
21.01	77.7	8.98	(10.00 ... 11.4b)		R

 $h$  3949;  $-30^\circ$  1612; 7.7A.R.  $7^h$   $13^m$   $43^s$ ; Decl.  $-30^\circ$   $34'$ 

19.125	77.3	2.99	10.0	2	370
19.136	77.5	3.20	9.5	2	370
19.221	77.3	3.15	11.1	2	475
19.16	77.4	3.11	(7.7 ... 8.1)		F

J 80;  $-36^\circ$  1227; 7.8A.R.  $7^h$   $14^m$   $6^s$ ; Decl.  $-36^\circ$   $32'$ 

19.982	210.7	3.05	6.4	3	370
19.985	211.6	3.05	6.8	$2\frac{1}{2}$	370
20.056	211.1	3.05	8.7	$2\frac{1}{2}$	370
20.01	211.1	3.05	(9.5 ... 9.9)		F

 $h$  3959;  $-74^\circ$  430; 9.5A.R.  $7^h$   $15^m$   $11^s$ ; Decl.  $-74^\circ$   $24'$ 

18.317	204.9	15.78	12.0	2	370
18.958	204.3	16.60	7.6	2	370
19.158	203.9	16.16	11.0	2	370
18.81	204.4	16.18	(9.0R ... 12.5)		N

 $h$  3954;  $-32^\circ$  1438; 9.5A.R.  $7^h$   $16^m$   $52^s$ ; Decl.  $-32^\circ$   $46'$ 

19.136	92.1	6.92	9.6	2	370
19.221	92.4	6.97	11.4	2	370
19.234	91.2	6.81	9.4	$2\frac{1}{2}$	370
19.20	91.9	6.90	(9.8 ... 11.9)		N

 $h$  3957;  $-35^\circ$  1214; 7.4A.R.  $7^h$   $17^m$   $46^s$ ; Decl.  $-35^\circ$   $41'$ 

19.944	194.2	7.80	6.1	$2\frac{1}{2}$	370
19.982	194.5	7.88	6.5	3	370
20.056	193.6	7.98	8.8	$2\frac{1}{2}$	370
19.99	194.1	7.89	(8.0 ... 8.8)		D?

 $h$  3965;  $-35^\circ$  1223; 6.8A.R.  $7^h$   $19^m$   $27^s$ ; Decl.  $-35^\circ$   $36'$ 

19.982	305.8	25.42	6.6	$2\frac{1}{2}$	370
20.056	305.8	25.37	8.9	$2\frac{1}{2}$	370
20.02	305.8	25.40	(6.9 ... 12.5)		N

 $h$  3966;  $-37^\circ$  1248; 7.0A.R.  $7^h$   $20^m$   $21^s$ ; Decl.  $-37^\circ$   $3'$ 

19.944	321.9	7.18	6.2	$2\frac{1}{2}$	370
19.982	321.4	7.14	6.8	$2\frac{1}{2}$	370
20.056	321.6	7.35	9.0	2	370
19.99	321.6	7.22	(7.3 ... 7.3)		F

 $h$  3968;  $-41^\circ$  1411; 8.2A.R.  $7^h$   $21^m$   $56^s$ ; Decl.  $-41^\circ$   $52'$ 

20.094	141.1	26.01	8.8	2	370
20.097	141.0	25.88	8.3	$2\frac{1}{2}$	370
20.10	141.0	25.94	(7.5 ... 12.0)		R?

 $h$  3969;  $-34^\circ$  1311; 7.5A.R.  $7^h$   $22^m$   $23^s$ ; Decl.  $-34^\circ$   $4'$ 

19.982	226.7	17.34	6.9	$2\frac{1}{2}$	370
19.985	226.9	17.38	6.9	2	370
19.98	226.8	17.36	(7.8 ... 8.7)		F

*h* 4047; —88° 65; 8.2

A.R. 7<sup>h</sup> 24<sup>m</sup> 2<sup>s</sup>; Decl. —88° 48'

19.174	166.4	19.52	9.6	2	370
19.182	167.0	19.05	8.0	2	370
19.199	165.8	19.38	9.0	1½	370
19.18	166.4	19.32	(8.7 ... 12.8)		182

AC

19.174	340.4	34.80	9.8	2	370
19.182	342.3	34.92	8.2	2	370
19.199	341.2	34.50	8.9	1½	370
19.18	341.3	34.74	(8.7...13.0)		182

Piazzini = Δ 49; —31° 1586; 6.2

A.R. 7<sup>h</sup> 24<sup>m</sup> 3<sup>s</sup>; Decl. —31° 35'

19.985	52.5	9.05	7.0	2½	370
20.056	53.2	9.15	9.1	2	370
20.02	52.8	9.10	(7.1 ... 7.8)		F

*h* 3975; —81° 219; 8.9:

A.R. 7<sup>h</sup> 25<sup>m</sup> 1<sup>s</sup>; Decl. —81° 22'

19.158	338.6	10.91	10.2	2	370
19.175	338.0	10.83	11.0	2	370
19.17	338.3	10.87	(9.4 ... 10.0)		182

*h* 3976; —68° 640; 8.4

A.R. 7<sup>h</sup> 26<sup>m</sup> 28<sup>s</sup>; Decl. —68° 39'

18.192	135.3	7.23	10.3	2	370
18.197	135.4	7.40	9.9	2	370
18.202	135.7	7.42	9.4	2½	370
18.20	135.5	7.35	(9.1 ... 11.3)		N

AC

18.192	332.3	9.33	10.2	2	370
18.197	331.8	9.32	9.7	2	370
18.202	332.7	9.37	9.3	2	370
18.20	332.3	9.34	(9.1 ... 11.7)		N

*h* 3987; —78° 261; 8.6

A.R. 7<sup>h</sup> 28<sup>m</sup> 39<sup>s</sup>; Decl. —78° 55'

19.158	236.3	47.29	10.5	2	370
19.175	236.2	47.04	11.2	2	370
19.17	236.2	47.16	(7.7 ... 12.7)		N

*h* 3980; —57° 1247; 9.0

A.R. 7<sup>h</sup> 28<sup>m</sup> 41<sup>s</sup>; Decl. —57° 19'

20.149	131.8	23.10	6.7	2	370
20.215	129.6	23.58	8.7	2½	370
20.18	129.6	23.34	(9.2 ... 14.1)		76

(Sigue Continued.)

BC

20.149	258.2	7.46	6.9	2	370
20.215	265.2	7.39	8.9	2½	370
20.18	263.9	7.10	(14.1 ... 14.8)		76

AC

20.215	142.6	18.88	8.6	2½	370
20.18	145.1	19.07	(9.2 ... 14.8)		76

*h* 3979; —36° 1371; 8.4

A.R. 7<sup>h</sup> 29<sup>m</sup> 10<sup>s</sup>; Decl. —36° 10'

19.985	249.1	9.03	7.1	3	370
20.056	249.8	9.09	9.2	2½	370
20.081	249.1	9.01	10.1	3	475
20.04	249.3	9.04	(9.9 ... 10.0)		D?

λ 82; —36° 1374; 9.4

A.R. 7<sup>h</sup> 29<sup>m</sup> 21<sup>s</sup>; Decl. —36° 6'

19.985	352.5	7.83	7.2	3	370
20.056	353.6	7.75	9.3	2	370
20.02	353.0	7.79	(10.5 ... 11.8)		F

*h* 3985; —67° 763; 8.5

A.R. 7<sup>h</sup> 29<sup>m</sup> 32<sup>s</sup>; Decl. —67° 53'

18.192	86.9	3.14	10.5	2	370
18.202	88.9	3.05	9.5	2½	370
18.290	87.3	2.99	11.2	2½	370
18.23	87.7	3.06	(9.0 ... 9.6)		F

*h* 4010; —87° 106; 8.8

A.R. 7<sup>h</sup> 29<sup>m</sup> 44<sup>s</sup>; Decl. —87° 9'

19.158	241.8	15.28	9.8	1½	370
19.174	240.9	15.18	10.3	2	370
19.17	241.3	15.23	(9.2 ... 12.7)		182

*h* 3996; —84° 132; 7.2

A.R. 7<sup>h</sup> 31<sup>m</sup> 38<sup>s</sup>; Decl. —84° 14'

19.158	255.9	16.63	10.0	1½	370
19.174	254.8	16.62	10.6	2	370
19.17	255.3	16.62	(7.5 ... 11.6)		182

*h* 3991; —74° 445 + 4; 9.8 + 9.8

A.R. 7<sup>h</sup> 32<sup>m</sup> 31<sup>s</sup>; Decl. —74° 46'

18.317	225.7	14.72	12.1	2	370
18.958	225.0	14.94	7.8	2	370
19.158	226.6	14.98	11.2	2	370
18.81	225.8	14.88	(9.5 ... 10.9)		R?

\*  $h$  3997;  $-73^\circ 457$ ; 6.2A.R.  $7^h 37^m 54^s$ ; Decl.  $-73^\circ 60'$ 

20.927	114.2	2.02	7.1	3	370
21.061	116.0	2.07	7.2	$2\frac{1}{2}$	370
21.110	115.8	2.14	8.3	$2\frac{1}{2}$	370
21.03	115.3	2.08	(7.3 ... 7.4)		P

 $h$  4001;  $-67^\circ 792$ ; 8.9R.A.  $7^h 38^m 36^s$ ; Decl.  $-67^\circ 10'$ 

18.192	312.3	6.10	10.6	$2\frac{1}{2}$	370
18.202	312.4	6.27	9.8	2	370
18.290	312.2	6.11	11.4	$2\frac{1}{2}$	370
18.23	312.3	6.16	(9.0 ... 11.7)		51

I 392;  $-30^\circ 1990$ ; 8.6A.R.  $7^h 40^m 22^s$ ; Decl.  $-30^\circ 15'$ 

19.221	361.0	0.91	11.6	2	370
19.234	359.7	0.97	9.6	$2\frac{1}{2}$	650
19.243	361.4	1.00	9.3	3	650
19.23	360.7	0.96	(9.6 ... 10.0)		F <sup>3</sup>

 $\Delta$  54<sup>3</sup>;  $-37^\circ 1567$ ; 10.5A.R.  $7^h 40^m 59^s$ ; Decl.  $-37^\circ 56'$ 

20.056	126.2	4.77	9.5	$2\frac{1}{2}$	370
20.081	125.3	4.93	10.3	3	475
20.097	125.3	4.66	8.5	$2\frac{1}{2}$	370
20.08	125.6	4.79	(10.5 ... 11.0)		183

 $\Delta$  56;  $-41^\circ 1685 + 4$ ; 7.6 + 8.8A.R.  $7^h 42^m 55^s$ ; Decl.  $-41^\circ 12'$ 

20.094	176.8	49.72	8.9	2	370
20.097	177.0	49.68	8.4	$2\frac{1}{2}$	370
20.10	176.9	49.70	(7.4 ... 7.6)		184

 $h$  4009;  $-31^\circ 1946$ ; 8.6A.R.  $7^h 45^m 31^s$ ; Decl.  $-31^\circ 51'$ 

19.221	318.0	9.47	11.7	2	370
19.234	318.5	9.37	10.5	3	370
19.240	318.6	9.38	10.2	2	370
19.23	318.4	9.41	(8.7 ... 9.1)		R

 $h$  4011;  $-66^\circ 749 + 8$ ; 9.7 + 9.4A.R.  $7^h 46^m 27^s$ ; Decl.  $-66^\circ 46'$ 

18.192	301.4	17.50	10.8	$2\frac{1}{2}$	370
18.202	302.0	17.41	10.0	2	370
18.20	301.7	17.46	(9.5 ... 10.1)		F

(Sigue Continued.)

BC =  $\delta$  42

18.192	319.4	3.59	11.0	2	370
18.202	320.3	3.68	10.2	2	370
18.290	316.1	3.39	11.5	$2\frac{1}{2}$	370
18.23	318.6	3.55	(10.1 ... 12.8)		

 $h$  4020;  $-75^\circ 464$ ; 9.5A.R.  $7^h 49^m 26^s$ ; Decl.  $-75^\circ 26'$ 

18.317	315.1	20.44	12.3	2	370
18.958	315.1	20.56	8.0	2	370
18.64	315.1	20.50	(9.3 ... 12.9)		N

 $h$  4019;  $-41^\circ 1854$ ; 8.1A.R.  $7^h 51^m 6^s$ ; Decl.  $-41^\circ 30'$ 

20.094	155.3	5.51	9.1	2	370
20.121	155.3	5.58	6.5	2	370
20.132	154.9	5.51	6.8	$2\frac{1}{2}$	370
20.12	155.2	5.53	(7.8 ... 9.9)		F

I 26;  $-47^\circ 1708$ ; 6.9A.R.  $7^h 53^m 38^s$ ; Decl.  $-47^\circ 33'$ 

20.927	35.6	0.83	7.5	3	370
20.965	37.4	0.88	5.9	3	650
21.061	36.0	0.73	7.5	3	475
20.98	36.3	0.81	(7.1 ... 7.7)		P

\*  $h$  4031;  $-60^\circ 988$ ; 6.7A.R.  $7^h 56^m 18^s$ ; Decl.  $-60^\circ 31'$ 

20.927	357.5	5.48	7.3	$2\frac{1}{2}$	370
21.061	357.9	5.42	7.4	$2\frac{1}{2}$	370
21.110	357.0	5.58	8.7	2	370
21.03	357.5	5.49	(7.4 ... 8.3)		20

Piazzini =  $h$  4035;  $-32^\circ 1937 + 9$ ; 7.9 + 9.4A.R.  $7^h 58^m 12^s$ ; Decl.  $-32^\circ 7'$ 

19.221	133.9	34.78	11.9	2	370
19.235	134.1	34.83	10.6	$2\frac{1}{2}$	370
19.240	133.8	34.77	10.4	2	370
19.23	133.9	34.79	(6.7 ... 9.3)		F

\* I 8;  $-44^\circ 2138$ ; 7.3A.R.  $7^h 58^m 25^s$ ; Decl.  $-44^\circ 19'$ 

20.927	307.1	2.45	7.6	3	370
21.061	307.2	2.50	7.7	3	475
21.110	306.8	2.37	9.0	2	370
21.383	306.8	2.48	11.2	$2\frac{1}{2}$	370
21.12	307.0	2.45	(7.0 ... 10.6)		

*h* 4038 = *h* 4030;  $-40^{\circ} 2039$ ; 5.7

A.R.  $7^{\text{h}} 58^{\text{m}} 27^{\text{s}}$ ; Decl.  $-40^{\circ} 58'$

20.094	345.9	27.09	9.3	2	370
20.121	346.0	26.96	6.6	2	370
20.11	346.0	27.02	(6.2 ... 9.0R) D?		

*h* 4039;  $-37^{\circ} 1830$ ; 8.5

A.R.  $7^{\text{h}} 58^{\text{m}} 40^{\text{s}}$ ; Decl.  $-37^{\circ} 51'$

20.081	55.1	8.59	10.5	3	370
20.097	55.6	8.72	8.8	3	370
20.113	54.9	8.74	6.0	$2\frac{1}{2}$	370
20.10	55.2	8.68	(9.6 ... 9.9) N		

*h* 4040;  $-36^{\circ} 1862 + 3$ ;  $9.4 + 9.6$

A.R.  $7^{\text{h}} 58^{\text{m}} 43^{\text{s}}$ ; Decl.  $-36^{\circ} 5'$

20.081	133.2	20.65	10.6	3	370
20.097	132.9	20.60	8.9	3	370
20.09	133.1	20.63	(9.6 ... 10.5) F		

*h* 4046;  $-33^{\circ} 1949 + 50$ ;  $8.2 + 8.3$

A.R.  $8^{\text{h}} 0^{\text{m}} 56^{\text{s}}$ ; Decl.  $-33^{\circ} 13'$

19.221	88.5	22.10	12.0	$1\frac{1}{2}$	370
19.235	88.1	22.00	10.8	$2\frac{1}{2}$	370
19.240	88.4	21.80	10.6	$1\frac{1}{2}$	370
19.23	88.3	21.97	(6.8 ... 9.1) F		

AC = I 189

19.235	58.1	27.79	10.9	2	370
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BC

19.240	5.8	14.12	10.7	1	370
19.251	5.3	14.04	9.2	2	370
19.25	5.6	14.08	(9.1 ... 11.8) F?		

*h* 4048;  $-41^{\circ} 2170$ ; 8.3

A.R.  $8^{\text{h}} 4^{\text{m}} 26^{\text{s}}$ ; Decl.  $-41^{\circ} 50'$

20.094	210.0	8.02	9.5	$2\frac{1}{2}$	370
20.121	210.5	7.90	6.7	2	370
20.132	210.1	7.78	7.0	$2\frac{1}{2}$	370
20.12	210.2	7.90	(9.5 ... 9.8) F?		

*h* 4049;  $-37^{\circ} 1937$ ; 9.3

A.R.  $8^{\text{h}} 5^{\text{m}} 19^{\text{s}}$ ; Decl.  $-37^{\circ} 60'$

20.113	319.7	8.64	6.1	$2\frac{1}{2}$	370
20.135	319.7	8.71	9.3	$2\frac{1}{2}$	370
20.138	319.0	8.58	9.4	2	370
20.13	319.5	8.64	(9.7 ... 11.0) 185		

*h* 4055;  $-69^{\circ} 838$ ; 8.6

A.R.  $8^{\text{h}} 5^{\text{m}} 31^{\text{s}}$ ; Decl.  $-69^{\circ} 30'$

18.175	190.3	5.92	11.0	$2\frac{1}{2}$	370
18.192	189.7	5.99	12.0	2	370
18.194	190.8	5.78	10.6	2	370
18.19	190.3	5.90	(8.4 ... 8.6) D		

*h* 4056;  $-67^{\circ} 876$ ; 9.7

A.R.  $8^{\text{h}} 6^{\text{m}} 1^{\text{s}}$ ; Decl.  $-67^{\circ} 9'$

18.175	2.2	10.64	11.2	3	370
18.192	2.1	10.69	11.8	2	370
18.18	2.2	10.66	(10.7 ... 10.8) N		

*h* 4051;  $-36^{\circ} 2035$ ; 6.9

A.R.  $8^{\text{h}} 6^{\text{m}} 24^{\text{s}}$ ; Decl.  $-36^{\circ} 55'$

20.113	265.3	17.75	6.3	$2\frac{1}{2}$	370
20.135	264.8	18.09	9.5	2	370
20.138	265.8	18.02	9.5	2	370
20.13	265.3	17.95	(6.7 ... 13.3) F		

AC =  $\geq$  43

20.113	205.3	16.84	6.4	2	370
20.135	205.7	16.70	9.4	2	370
20.138	206.3	16.74	9.6	2	370
20.13	205.8	16.76	(6.7 ... 13.5)		

*h* 4052;  $-35^{\circ} 1998$ ; 8.5

A.R.  $8^{\text{h}} 6^{\text{m}} 29^{\text{s}}$ ; Decl.  $-35^{\circ} 26'$

20.113	124.7	16.21	6.2	$2\frac{1}{2}$	370
20.135	124.6	16.22	9.6	2	370
20.12	124.7	16.21	(9.4 ... 11.2) N		

*h* 4068; Anon.

A.R.  $8^{\text{h}} 7^{\text{m}} 20^{\text{s}}$ ; Decl.  $-77^{\circ} 6'$

18.317	307.3	13.94	12.6	2	370
18.958	307.4	14.10	8.1	$1\frac{1}{2}$	370
18.64	307.3	14.02	(10.6 ... 12.2) 186		

$\Delta$  66 = R $\ddot{u}$  7;  $\epsilon$  Volantis; 5.0

A.R.  $8^{\text{h}} 7^{\text{m}} 33^{\text{s}}$ ; Decl.  $-68^{\circ} 15'$

18.175	23.3	6.14	11.6	3	370
18.192	22.7	6.17	12.1	2	370
18.194	25.5	5.99	10.7	2	370
18.19	23.8	6.10	(4.5 ... 8.1) D?		

*h* 4061;  $-66^{\circ} 801$ ; 9.5

A.R.  $8^{\text{h}} 7^{\text{m}} 50^{\text{s}}$ ; Decl.  $-66^{\circ} 48'$

18.175	20.8	8.27	11.4	3	370
18.192	20.9	8.64	12.2	2	370
18.194	21.1	8.56	10.8	2	370
18.19	20.9	8.49	(10.8 ... 11.4) N		

$h$  4086;  $-85^{\circ} 137 + 8$ ;  $8.0 + 9.8$   
 A.R.  $8^h 7^m 58^s$ ; Decl.  $-85^{\circ} 35'$

19.175	85.2	54.07	11.5	2	370
19.183	85.4	54.10	9.9	2	370
19.18	85.3	54.08	(8.4 ... 9.4)		F?

$h$  4067;  $-83^{\circ} 203$ ;  $7.9$   
 A.R.  $8^h 8^m 23^s$ ; Decl.  $-83^{\circ} 22'$

19.175	72.1	—	11.9	2	370
19.183	72.5	31.45	10.3	2	370
19.305	72.8	31.37	9.2	2	370
19.22	72.5	31.41	(7.9 ... 11.7)		N

AC

19.183	103.0	40.24	10.6	2	370
19.305	101.6	40.41	9.3	1½	370
19.24	102.3	40.32	(7.9 ... 13.0)		N

$h$  4064;  $-69^{\circ} 850$ ;  $9.5$   
 A.R.  $8^h 8^m 36^s$ ; Decl.  $-69^{\circ} 2'$

18.175	278.8	14.51	11.9	2½	370
18.192	278.1	14.53	12.3	2	370
18.18	278.5	14.52	(9.3 ... 11.8)		N

I 192;  $-68^{\circ} 743$ ;  $7.4$   
 A.R.  $8^h 8^m 37^s$ ; Decl.  $-68^{\circ} 37'$

18.175	171.8	1.90	11.8	3½	370
18.194	173.6	2.06	10.9	2	370
18.202	172.8	2.05	10.5	2	370
18.19	172.7	2.00	(7.4 ... 10.7)		F

$h$  4058 Ver la nota 162

$h$  4060;  $-36^{\circ} 2102 + 3$ ;  $8.4 + 9.1$   
 A.R.  $8^h 8^m 51^s$ ; Decl.  $-36^{\circ} 2'$

20.113	178.6	22.28	6.5	2½	370
20.135	178.8	22.21	9.7	2	370
20.12	178.7	22.25	(8.9 ... 10.5)		F

$h$  4059;  $-31^{\circ} 2207$ ;  $7.1$   
 A.R.  $8^h 9^m 14^s$ ; Decl.  $-31^{\circ} 46'$

19.235	330.0	29.50	11.2	2½	370
19.251	330.6	29.68	9.3	2½	370
19.24	330.3	29.59	(6.6 ... 13.1)		N

$h$  4062;  $h_2$  Puppis;  $7.0 + 9.2$   
 A.R.  $8^h 9^m 37^s$ ; Decl.  $-39^{\circ} 58^s$

20.094	340.5	51.04	9.6	1½	370
20.122	340.7	51.10	6.9	2	370
20.11	340.6	51.07	(5.0 ... 9.9)		N

$\lambda$  98 = I—;  $-35^{\circ} 2098$ ;  $7.7$   
 A.R.  $8^h 10^m 12^s$ ; Decl.  $-35^{\circ} 18'$

20.113	67.1	5.88	6.7	3	370
20.135	66.7	5.64	9.9	2	370
20.138	66.5	5.74	9.8	2	370
20.13	66.8	5.75	(7.50 ... 12.7)		R

$h$  4063;  $-36^{\circ} 2155$ ;  $7.0$   
 A.R.  $8^h 10^m 50^s$ ; Decl.  $-36^{\circ} 60'$

20.113	350.2	17.67	6.8	3	370
20.135	350.6	17.66	9.8	2½	370
20.12	350.4	17.66	(8.1 ... 9.5R)		R?

$\beta$  454 = Cape 8;  $-30^{\circ} 2357$ ;  $7.5$   
 A.R.  $8^h 10^m 53^s$ ; Decl.  $-30^{\circ} 33'$

19.235	14.8	2.33	11.3	2½	475
19.251	13.6	2.48	9.4	2½	475
19.253	15.0	2.37	9.0	2	650
19.25	14.5	2.39	(7.1 ... 8.9)		F

$h$  4076; Anon.  
 A.R.  $8^h 13^m 19^s$ ; Decl.  $-67^{\circ} 26'$

18.175	82.8	3.13	12.3	2½	370
18.194	80.9	3.87	11.1	2	370
18.202	78.9	3.65	10.6	2	370
18.19	80.9	3.55	(11.9 ... 12.7)		A

$h$  4073;  $-36^{\circ} 2228$ ;  $6.9$   
 A.R.  $8^h 13^m 34^s$ ; Decl.  $-36^{\circ} 59'$

20.056	177.9	2.19	9.7	2	370
20.081	178.0	2.08	10.7	3	650
20.097	178.1	2.13	9.0	2½	650
20.08	178.0	2.13	(7.5 ... 8.2)		21

$\delta$  44;  $-40^{\circ} 2357$ ;  $8.1$   
 A.R.  $8^h 15^m 4^s$ ; Decl.  $-40^{\circ} 3'$

20.095	133.1	0.68	9.8	2	475
20.133	136.8	0.68	7.3	2½	650
20.138	136.4	0.67	10.0	2½	475
20.12	135.4	0.68	(9.3 ... 9.6)		

$h$  4081;  $-47^{\circ} 2079 + 8$ ;  $7.6 + 10.0$   
 A.R.  $8^h 15^m 15^s$ ; Decl.  $-47^{\circ} 48'$

20.217	185.4	42.47	8.3	3	370
20.220	185.4	42.55	8.3	1½	370
20.22	185.4	42.51	(6.9 ... 11.1)		120

*h* 4083; —35° 2252; 10.2

A.R. 8<sup>h</sup> 16<sup>m</sup> 9<sup>s</sup>; Decl. —35° 49'

20.056	115.7	26.4	9.8	2	150
			(9.5 ... Neb)		187

*h* 4085; —36° 2321; 5.3

A.R. 8<sup>h</sup> 16<sup>m</sup> 39<sup>s</sup>; Decl. —36° 5'

20.056	273.0	7.66	9.9	2	370
20.081	273.6	7.15	10.9	3	370
20.097	273.7	7.33	9.2	3	370
20.113	273.9	7.00	6.9	3	370
20.09	273.6	7.28	(5.8 ... 12.3)		R?

*h* 4087; —40° 2395; 7.7

A.R. 8<sup>h</sup> 17<sup>m</sup> 42<sup>s</sup>; Decl. —40° 35'

20.095	288.9	1.97	9.9	2	475
20.122	290.4	1.61	7.1	2	370
20.133	291.5	1.55	7.4	3	650
20.138	290.9	1.66	10.1	2½	475
20.12	290.4	1.70	(7.8 ... 8.3)		M

AC

20.122	337.8	13.72	7.4	2	370
20.133	340.1	13.65	7.5	3	370
20.138	340.0	13.73	10.2	2½	475
20.13	339.3	13.70	(7.8 ... 13.3)		N

AD

20.122	305.1	30.50	7.5	2	370
20.133	305.3	30.46	7.6	2½	370
20.13	305.2	30.48	(7.8 ... 13.9)		N

*h* 2446; —30° 2469 + 8; 9.6 + 9.4

A.R. 8<sup>h</sup> 19<sup>m</sup> 27<sup>s</sup>; Decl. —30° 15'

19.235	286.2	28.63	11.5	2½	370
19.251	286.2	28.54	9.5	2½	370
19.24	286.2	28.58	(9.5 ... 9.7)		F

I 798; —34° 2398; 9.0

A.R. 8<sup>h</sup> 19<sup>m</sup> 40<sup>s</sup>; Decl. —34° 35'

20.081	269.6	2.17	11.2	3	475
20.097	269.4	2.23	9.3	2½	475
20.113	269.0	2.07	7.0	3	370
20.10	269.3	2.16	(9.5 ... 10.9)		D?

δ 45; —35° 2354; 9.4

A.R. 8<sup>h</sup> 19<sup>m</sup> 50<sup>s</sup>; Decl. —35° 13'

20.081	184.2	1.11	11.1	3	475
20.097	180.6	1.08	9.4	2½	475
20.113	186.0	1.09	7.1	2½	370
20.10	183.6	1.09	(10.1 ... 11.2)		

*h* 4092; —39° 2390; 9.0

A.R. 8<sup>h</sup> 21<sup>m</sup> 21<sup>s</sup>; Decl. —39° 9'

20.095	209.9	8.96	10.1	2	475
20.122	209.1	8.71	7.7	2	370
20.133	208.8	8.55	7.8	2½	370
20.12	209.3	8.74	(10.0 ... 11.1)		N

*h* 4093; —38° 2296; 6.6

A.R. 8<sup>h</sup> 21<sup>m</sup> 43<sup>s</sup>; Decl. —38° 39'

20.095	122.7	8.29	10.2	2	370
20.122	122.6	8.20	7.8	2	370
20.138	123.6	8.13	10.4	2	475
20.12	123.0	8.21	(6.8 ... 7.6)		F

*h* 4094; —35° 2423 + 2; 9.2 + 9.4

A.R. 8<sup>h</sup> 21<sup>m</sup> 54<sup>s</sup>; Decl. —35° 6'

20.056	218.2	17.17	10.0	2	370
20.081	218.1	17.34	11.3	3	370
20.097	217.9	17.39	9.4	3	370
20.08	218.1	17.30	(9.3 ... 10.3)		F

*h* 4105; —78° 321; 10.3

A.R. 8<sup>h</sup> 22<sup>m</sup> 2<sup>s</sup>; Decl. —78° 50'

19.158	72.3	12.34	11.5	2	370
19.183	72.7	12.46	9.6	2	370
19.17	72.5	12.40	(10.5 ... 10.9)		N

*h* 4098; —39° 2435; 8.6

A.R. 8<sup>h</sup> 23<sup>m</sup> 32<sup>s</sup>; Decl. —39° 41'

20.095	276.1	14.58	10.3	1½	370
20.138	276.2	14.73	10.7	2	370
20.12	276.2	14.66	(9.1 ... 12.2)		N

*h* 4099; —39° 2448 + 9; 9.0 + 10.2

A.R. 8<sup>h</sup> 24<sup>m</sup> 14<sup>s</sup>; Decl. —39° 38'

20.095	217.6	28.27	10.4	1½	370
20.138	217.8	28.48	10.9	2	370
20.12	217.8	28.38	(9.3 ... 11.9)		9

I 394; —38° 2364; 8.2

A.R. 8<sup>h</sup> 24<sup>m</sup> 56<sup>s</sup>; Decl. —38° 11'

20.155	192.7	0.91	9.8	2½	475
20.160	192.8	0.89	7.9	2½	475
20.16	192.8	0.90	(8.6 ... 9.2)		M?

*h* 4109; —76° 514 + 15; 7.4 + 8.6

A.R. 8<sup>h</sup> 25<sup>m</sup> 35<sup>s</sup>; Decl. —76° 2'

18.317	128.0	26.12	12.9	1½	370
19.158	128.2	26.05	11.7	2	370
18.74	128.1	26.08	(7.7 ... 8.5)		F

$\Delta 71; -40^\circ 2570 + 3; 7.8 + 8.8$ A.R. 8<sup>h</sup> 26<sup>m</sup> 2<sup>s</sup>; Decl.  $-40^\circ 6'$ 

20.138	49.6	63.83	11.1	1½	370
20.176	49.5	63.84	8.2	1½	370
20.16	49.6	63.84	(7.0 ... 7.3R)		

 $h 4106; -36^\circ 2624; 8.2$ A.R. 8<sup>h</sup> 26<sup>m</sup> 40<sup>s</sup>; Decl.  $-36^\circ 16'$ 

20.056	147.8	4.41	10.2	2½	370
20.081	147.5	4.53	11.5	3	370
20.097	147.8	4.41	9.5	2½	370
20.08	147.7	4.44	(8.0 ... 9.8)		R

 $h 4107; -38^\circ 2399; 6.8$ A.R. 8<sup>h</sup> 26<sup>m</sup> 47<sup>s</sup>; Decl.  $-38^\circ 39'$ 

20.122	328.5	4.57	8.0	2	370
20.133	329.6	4.49	8.0	2½	370
20.155	329.2	4.39	9.7	2½	370
20.14	329.1	4.48	(6.7 ... 8.8)		F

AC; C =  $-38^\circ 2400; 9.4$ 

20.122	99.8	30.71	8.1	2	370
20.155	100.5	30.84	9.7	2½	370
20.14	100.2	30.78	(6.7 ... 9.2)		F

 $h 4110; -66^\circ 861; 7.5$ A.R. 8<sup>h</sup> 28<sup>m</sup> 31<sup>s</sup>; Decl.  $-66^\circ 43'$ 

18.175	215.2	25.04	12.5	2	370
18.192	215.6	24.85	12.5	2	370
18.18	215.4	24.94	(7.5 ... 12.0)		N

 $h 4113; -38^\circ 2489; 8.7:$ A.R. 8<sup>h</sup> 31<sup>m</sup> 46<sup>s</sup>; Decl.  $-38^\circ 20'$ 

20.133	202.9	11.54	8.1	3	370
20.155	202.7	11.38	9.9	2½	370
20.14	202.8	11.46	(9.7 ... 10.0)		N

 $h 4114; -40^\circ 2680; 9.2$ A.R. 8<sup>h</sup> 31<sup>m</sup> 52<sup>s</sup>; Decl.  $-40^\circ 34'$ 

20.155	224.8	4.25	10.0	2	370
20.160	224.9	4.08	8.1	2	370
20.176	224.5	4.04	8.3	2	370
20.16	224.7	4.12	(10.2 ... 10.5)		N

 $h 4115; -33^\circ 2314; 7.1$ A.R. 8<sup>h</sup> 32<sup>m</sup> 33<sup>s</sup>; Decl.  $-33^\circ 18'$ 

19.235	158.1	22.43	11.7	2½	370
19.251	157.8	22.43	9.8	2	370
19.24	158.0	22.43	(6.9 ... 11.8)		N

(Sigue Continued.)

AC

19.235	20.2	44.99	11.8	2	370
19.251	20.0	45.04	9.9	1½	370
19.24	20.1	45.01	(6.9 ... 12.5)		N

AD

19.235	197.4	29.73	12.0	1½	370
19.251	196.9	29.98	10.0	1½	370
19.24	197.2	29.86	(6.9 ... 13.1)		

 $h 4132; -82^\circ 250; 10.6$ A.R. 8<sup>h</sup> 32<sup>m</sup> 51<sup>s</sup>; Decl.  $-82^\circ 53'$ 

19.183	326.3	11.45	12.0	2	370
19.305	326.4	11.24	10.0	2	370
19.24	326.4	11.34	(10.8 ... 11.1)		N

 $h 4121 = \text{Hg } 17; -63^\circ 1007; 9.2$ A.R. 8<sup>h</sup> 33<sup>m</sup> 53<sup>s</sup>; Decl.  $-63^\circ 11'$ 

18.295	6.4	5.58	9.6	3½	370
18.298	6.1	5.48	9.2	3	370
18.301	6.6	5.31	9.3	2½	370
18.30	6.4	5.46	(9.8 ... 10.5)		R

 $h 4125; -62^\circ 1058; 7.2$ A.R. 8<sup>h</sup> 35<sup>m</sup> 5<sup>s</sup>; Decl.  $-62^\circ 25'$ 

18.295	236.7	7.67	9.8	3½	370
18.298	237.3	7.62	9.3	3	370
18.301	236.2	7.53	9.5	2	370
18.30	236.7	7.61	(5.6 ... 11.2)		A?

I 810

Ver la nota

162

 $h 4129; -36^\circ 2883; 8.4$ A.R. 8<sup>h</sup> 37<sup>m</sup> 59<sup>s</sup>; Decl.  $-36^\circ 4'$ 

20.056	349.3	8.21	10.4	2½	370
20.113	349.3	8.16	7.4	2½	370
20.136	348.3	8.09	10.1	2½	370
20.10	349.0	8.15	(8.9 ... 12.9)		N

 $h 4134; \theta \text{ Volantis}; 5.5$ A.R. 8<sup>h</sup> 38<sup>m</sup> 37<sup>s</sup>; Decl.  $-69^\circ 56'$ 

18.175	107.6	44.95	12.7	2	370
* 17.37	107.8	44.98	(5.7 ... 9.8)		

 $h 4137 = \text{I } 812; -74^\circ 532; 8.8$ A.R. 8<sup>h</sup> 39<sup>m</sup> 36<sup>s</sup>; Decl.  $-74^\circ 28'$ 

19.158	198.8	5.52	12.0	2	370
19.265	199.5	5.26	11.2	2½	370
19.289	199.9	5.23	9.0	2	370
19.24	199.4	5.34	(8.8 ... 11.2)		A?



HdA; —36° 2915 Ver la nota 162

I 815; —40° 2824; 7.9

A.R. 8<sup>h</sup> 40<sup>m</sup> 7<sup>s</sup>; Decl. —40° 50'

20.155	0.4	4.30	10.2	2	370
20.160	0.4	4.46	8.2	2½	370
20.16	0.4	4.38	(7.2 ... 11.5)		

\* I 10; δ Argus; 3.5

A.R. 8<sup>h</sup> 41<sup>m</sup> 17<sup>s</sup>; Decl. —54° 15'

20.157	163.5	2.96	11.0	2½	475
20.217	164.7	3.03	8.5	2½	370
20.220	164.2	3.18	8.6	2	370
20.223	164.4	3.07	9.6	3	475
20.19	164.2	3.06	(2.0 ... 8.2)		B

h 4138; —39° 2860; 7.6

A.R. 8<sup>h</sup> 42<sup>m</sup> 9<sup>s</sup>; Decl. —39° 2'

20.155	324.0	8.49	10.4	2	370
20.160	324.1	8.50	8.4	2½	370
20.171	323.4	8.43	10.3	2	370
20.16	323.8	8.47	(8.3 ... 11.8)		N

h 4144; —35° 2947; 7.6

A.R. 8<sup>h</sup> 45<sup>m</sup> 29<sup>s</sup>; Decl. —35° 28'

20.056	314.9	2.72	10.5	3	475
20.097	315.3	2.70	9.9	2½	475
20.113	315.8	2.47	7.5	3	650
20.136	313.2	2.63	10.2	2½	370
20.10	314.8	2.63	(7.4 ... 10.0)		D?

h 4158; —84° 191 + 2; 9.2 + 10.5

A.R. 8<sup>h</sup> 47<sup>m</sup> 2<sup>s</sup>; Decl. —84° 14'

19.183	61.4	20.85	12.3	2	370
19.305	61.4	21.08	10.2	2	370
19.24	61.4	20.96	(8.9 ... 11.8)		N

h 4149; —37° 2914; 8.6

A.R. 8<sup>h</sup> 48<sup>m</sup> 3<sup>s</sup>; Decl. —37° 44'

20.056	205.4	8.05	10.7	3	370
20.113	204.7	8.14	7.6	2½	370
20.136	205.7	7.87	10.3	2½	370
20.10	205.3	8.02	(9.2 ... 11.7)		188

h 4150; —41° 3112; 7.7

A.R. 8<sup>h</sup> 49<sup>m</sup> 20<sup>s</sup>; Decl. —41° 21'

20.155	265.8	17.40	11.2	2	370
20.160	264.9	17.59	8.5	2	370
20.171	264.5	17.69	10.1	2	370
20.16	265.1	17.56	(7.4 ... 9.9)		N

h 4152; —63° 1054; 8.8

A.R. 8<sup>h</sup> 49<sup>m</sup> 36<sup>s</sup>; Decl. —63° 13'

18.295	341.5	7.58	10.0	3½	370
18.298	341.4	7.51	9.4	3	370
18.301	340.9	7.72	10.7	2	370
18.30	341.3	7.60	(9.1 ... 10.8)		N

h 4154; —31° 2609; 8.6;

A.R. 8<sup>h</sup> 51<sup>m</sup> 38<sup>s</sup>; Decl. —31° 36'

19.251	244.6	12.46	10.1	2	370
19.336	242.4	12.33	11.0	2½	370
19.982	244.8	12.26	7.2	2½	370
19.52	243.9	12.35	(9.0 ... 9.1)		N

h 4163; —76° 546; 8.9

A.R. 8<sup>h</sup> 53<sup>m</sup> 3<sup>s</sup>; Decl. —76° 49'

19.265	322.5	19.31	11.3	2	370
19.289	322.7	19.50	9.2	2	370
19.28	322.6	19.40	(8.8 ... 12.4)		N

h 4157; —35° 3075; 8.5

A.R. 8<sup>h</sup> 53<sup>m</sup> 54<sup>s</sup>; Decl. —35° 8'

20.056	281.7	16.42	10.8	3	370
20.113	282.5	16.10	7.8	2½	370
20.136	282.6	16.08	10.4	2	370
20.10	282.3	16.20	(8.5 ... 12.0)		N

ε 46; —62° 1137; 9.3

A.R. 8<sup>h</sup> 54<sup>m</sup> 2<sup>s</sup>; Decl. —62° 56'

18.295	183.7	1.71	10.2	3½	370
18.298	185.7	1.83	9.5	3	370
18.301	185.0	1.81	10.9	2	370
18.30	184.8	1.78	(9.6 ... 10.6)		

h 4164; —65° 1056; 8.0

A.R. 8<sup>h</sup> 55<sup>m</sup> 27<sup>s</sup>; Decl. —65° 43'

18.295	143.8	10.74	10.4	2½	370
18.298	145.1	10.98	10.4	2½	370
18.301	143.9	10.83	11.0	2	370
18.30	144.3	10.85	(7.9 ... 10.0)		F?

\* h 4165; —51° 1821; 5.5

A.R. 8<sup>h</sup> 57<sup>m</sup> 52<sup>s</sup>; Decl. —51° 42'

20.247	105.7	1.16	8.4	3	370
20.327	105.5	1.09	10.8	3	650
20.439	105.0	1.23	11.7	2½	475
20.34	105.4	1.16	(6.8 ... 7.9)		P

*h* 4166;  $-33^{\circ} 2486$ ; 7.4A.R. 8<sup>h</sup> 58<sup>m</sup> 10<sup>s</sup>; Decl.  $-33^{\circ} 6'$ 

19.251	153.0	13.24	10.2	1½	370
19.982	152.6	13.88	7.3	2½	370
19.985	152.4	13.99	7.4	2½	370
19.996	153.2	—	8.0	1½	370
19.999	152.8	13.85	8.6	2½	370
19.84	152.8	13.74	(7.9 ... 8.8)		N

*h* 4167;  $-65^{\circ} 1060$ ; 8.0A.R. 8<sup>h</sup> 58<sup>m</sup> 25<sup>s</sup>; Decl.  $-65^{\circ} 52'$ 

18.295	26.5	4.35	10.5	2	370
18.298	28.0	4.20	10.5	2	370
18.301	24.5	4.59	11.2	1½	370
18.315	25.6	4.36	12.8	2½	370
18.30	26.2	4.37	(8.8 ... 12.7)		41

*h* 4169;  $-37^{\circ} 3085$ ; 8.6A.R. 8<sup>h</sup> 58<sup>m</sup> 50<sup>s</sup>; Decl.  $-37^{\circ} 41'$ 

20.056	288.6	10.37	11.0	2½	370
20.113	288.6	10.14	7.9	2½	370
20.08	288.6	10.25	(8.4 ... 11.4)		189

*h* 4171;  $-69^{\circ} 996$ ; 9.9 :A.R. 8<sup>h</sup> 59<sup>m</sup> 0<sup>s</sup>; Decl.  $-69^{\circ} 14'$ 

18.192	236.3	14.72	12.7	2	370
18.194	237.2	14.48	11.3	2	370
18.202	236.6	14.75	10.8	2½	370
18.20	236.7	14.65	(9.8 ... 11.0)		N

*h* 4173; Cód  $-31^{\circ} 6917$ ; 9.5A.R. 9<sup>h</sup> 1<sup>m</sup> 14<sup>s</sup>; Decl.  $-31^{\circ} 43'$ 

19.982	298.8	12.48	8.2	2	370
19.985	299.7	12.27	7.6	2	370
20.095	300.6	12.74	10.9	2	370
20.02	299.7	12.50	(11.1 ... 12.2)		N

AC

19.982	239.9	14.36	8.1	2½	370
19.985	239.4	14.47	7.5	2	370
20.095	240.0	14.02	10.9	2	370
20.02	239.8	14.28	(11.1 ... 11.5)		N

*h* 4176;  $-41^{\circ} 3331 + 29$ ; 9.6  $+ 9.6$ A.R. 9<sup>h</sup> 1<sup>m</sup> 19<sup>s</sup>; Decl.  $-41^{\circ} 36'$ 

20.133	292.4	20.78	8.4	3	370
20.155	292.1	20.89	11.3	2	370
20.14	292.3	20.83	(10.0 ... 10.1)		N

*h* 4179;  $-34^{\circ} 3217$ ; 10.0A.R. 9<sup>h</sup> 1<sup>m</sup> 25<sup>s</sup>; Decl.  $-34^{\circ} 13'$ 

20.097	289.7	11.62	10.1	2½	370
20.113	290.1	11.50	7.9	2½	370
20.10	289.9	11.56	(10.6 ... 10.8)		N

*h* 4184;  $-75^{\circ} 557$ ; 9.5A.R. 9<sup>h</sup> 3<sup>m</sup> 18<sup>s</sup>; Decl.  $-75^{\circ} 49'$ 

19.265	224.2	25.94	11.5	2	370
19.289	223.9	25.95	9.3	2	370
19.28	224.0	25.94	(9.0R ... 13.4)		N

*h* 4185;  $-63^{\circ} 1098 + 7$ ; 9.1  $+ 9.1$ A.R. 9<sup>h</sup> 5<sup>m</sup> 28<sup>s</sup>; Decl.  $-63^{\circ} 32'$ 

18.295	243.7	10.55	10.8	2½	370
18.315	244.7	10.44	12.9	2½	370
18.30	244.2	10.50	(8.9 ... 9.0)		F?

*h* 4194;  $-83^{\circ} 267$ ; 9.7 :A.R. 9<sup>h</sup> 6<sup>m</sup> 43<sup>s</sup>; Decl.  $-83^{\circ} 11'$ 

19.183	61.8	16.15	12.5	2	370
19.306	62.6	16.29	10.4	2	370
19.24	62.2	16.22	(10.5 ... 11.0)		R

*h* 4187;  $\lambda$  Argus; Ver la nota 190*h* 5195; Anon.A.R. 9<sup>h</sup> 10<sup>m</sup> 55<sup>s</sup>; Decl.  $-64^{\circ} 25'$ 

18.295	65.3	16.28	11.1	2½	370
18.315	65.1	16.46	13.1	2½	370
18.30	65.2	16.37	(9.2 ... 9.8)		191

*h* 4198;  $-40^{\circ} 3392$ ; 9.9A.R. 9<sup>h</sup> 14<sup>m</sup> 15<sup>s</sup>; Decl.  $-40^{\circ} 0'$ 

20.133	4.2	11.63	8.7	2½	370
20.155	2.4	11.32	12.3	2	370
20.160	3.3	11.50	8.9	2	370
20.15	3.3	11.48	(10.4 ... 10.2)		

AC; C =  $-40^{\circ} 3393$ ; 10.0

20.133	175.5	12.22	8.6	2½	370
20.155	176.3	12.28	12.1	2	370
20.160	175.4	12.02	8.7	2	370
20.15	175.7	12.17	(10.4 ... 10.1)		

*h* 4211;  $\zeta$  Octantis; Ver la nota 162

*h* 4204; —80° 328; 10.3

A.R. 9<sup>h</sup> 14<sup>m</sup> 34<sup>s</sup>; Decl. —80° 39'

19.278	3.2	9.96	9.6	2	370
19.308	2.2	10.02	9.4	1½	370
19.314	3.6	9.14	9.0	1½	370
19.30	3.0	9.71	(11.7 ... 12.8)		N

ε 47; Cód —31° 7158; 9.0

A.R. 9<sup>h</sup> 15<sup>m</sup> 10<sup>s</sup>; Decl. —31° 12'

19.985	218.7	4.92	7.8	2	370
19.999	216.4	4.58	8.8	2½	370
20.095	215.1	5.29	11.0	2	370
20.03	216.7	4.93	(11.1 ... 11.5)		

*h* 4205; Anon.

A.R. 9<sup>h</sup> 15<sup>m</sup> 25<sup>s</sup>; Decl. —80° 37'

19.278	223.3	10.13	9.7	1½	370
19.308	222.3	9.95	9.6	1½	370
19.314	222.8	9.10	9.2	1½	370
19.30	222.8	9.73	(10.7 ... 13.2)		N

*h* 4200; —31° 2712; 7.5

A.R. 9<sup>h</sup> 15<sup>m</sup> 27<sup>s</sup>; Decl. —31° 14'

19.254	72.3	3.21	9.4	3	650
19.336	72.8	3.16	11.3	2½	370
19.982	72.6	3.31	8.4	2	370
19.985	73.4	3.33	7.7	2½	370
19.64	72.8	3.25	7.9 ... 8.6)		F

Rü 10; —69° 1036; 7.3

A.R. 9<sup>h</sup> 16<sup>m</sup> 23<sup>s</sup>; Decl. —69° 17'

18.175	17.7	10.48	12.9	2½	370
18.192	18.8	10.34	12.8	2	370
18.194	18.4	10.40	11.4	2	370
18.19	18.3	10.41	(8.2 ... 8.5)		F

*h* 4203; —32° 2587 + 6; 9.8 + 9.6

A.R. 9<sup>h</sup> 17<sup>m</sup> 14<sup>s</sup>; Decl. —32° 13'

19.336	240.4	14.94	11.4	2½	370
19.982	239.9	14.95	8.5	2	370
19.985	240.2	14.98	7.9	2	370
19.77	240.2	14.96	(9.8 ... 9.9)		22

*h* 4206; —74° 579; 5.5

A.R. 9<sup>h</sup> 17<sup>m</sup> 38<sup>s</sup>; Decl. —74° 22'

AB = I 12. Ver la nota 168  
(Sigue Continued.)

AB,C

19.265	341.6	7.09	11.7	2½	370
19.314	343.1	7.01	9.3	2	370
19.338	342.4	6.96	10.6	2	370
19.31	342.4	7.02	(5.8 ... 10.2)		N

AB,D

19.265	352.1	48.10	11.9	3	370
19.314	353.1	48.27	9.5	2	370
19.29	352.6	48.18	(5.8 ... 10.3)		N

*h* 4208; —36° 3598; 9.0

A.R. 9<sup>h</sup> 20<sup>m</sup> 32<sup>s</sup>; Decl. —36° 44'

20.097	129.2	15.99	10.2	2	370
20.113	129.3	16.18	8.1	2½	370
20.10	129.3	16.09	(8.8 ... 9.6)		F

*h* 4214; —77° 503; 8.0

A.R. 9<sup>h</sup> 21<sup>m</sup> 3<sup>s</sup>; Decl. —77° 7'

19.265	193.4	9.24	12.3	2½	370
19.289	193.4	9.33	9.5	2	370
19.338	193.0	9.18	10.8	2½	370
19.30	193.3	9.25	(8.5 ... 9.6)		F

*h* 4210 = Rus 118; —66° 1013; 9.0

A.R. 9<sup>h</sup> 21<sup>m</sup> 24<sup>s</sup>; Decl. —66° 57'

18.192	240.1	4.17	13.0	2	370
18.194	239.8	3.96	11.8	2	370
18.290	239.0	4.23	11.8	2½	370
18.23	239.6	4.12	(9.0 ... 9.6)		F

*h* 4216; —69° 1062 + 1; 9.4 + 9.6

A.R. 9<sup>h</sup> 24<sup>m</sup> 5<sup>s</sup>; Decl. —69° 25'

18.194	332.4	15.47	11.6	2	370
18.290	333.7	15.50	12.0	3	370
18.451	333.2	15.52	12.2	2	370
18.31	333.1	15.50	(10.7 ... 11.2)		21

*h* 4217; —77° 507; Ver la nota 84

Piazzi = Δ 78; ζ<sub>1</sub> Antliae; 6.2

A.R. 9<sup>h</sup> 25<sup>m</sup> 26<sup>s</sup>; Decl. —31° 20'

19.336	211.2	8.23	11.7	2	370
19.985	211.1	8.26	8.1	2½	370
19.66	211.1	8.25	(6.3 ... 7.3)		F

\* Copeland 1;  $\psi$  Argus; 4.7A.R. 9<sup>h</sup> 25<sup>m</sup> 47<sup>s</sup>; Decl. -39° 55'

20.056	145.2	1.10	11.2	3	650
20.133	145.4	0.99	8.9	3	650
20.157	144.5	1.04	10.7	2½	475
20.160	145.1	1.11	9.1	2½	475
21.110	148.2	1.14	7.9	2½	370
21.383	151.9	0.93	11.5	2½	370
21.389	148.9	0.79	12.2	3	370
20.13	145.1	1.06			
21.29	149.7	0.95	(4.0 ... 4.8)		B

*h* 4218; -35° 3616; 7.8A.R. 9<sup>h</sup> 28<sup>m</sup> 0<sup>s</sup>; Decl. -35° 51'

20.012	28.5	6.12	8.2	2	370
20.114	28.5	5.93	8.7	2½	370
20.136	29.2	5.92	10.6	2	370
20.09	28.7	5.99	(7.9 ... 10.6)		F

*h* 4226; -77° 519 + 20; 9.3 + 9.3A.R. 9<sup>h</sup> 29<sup>m</sup> 51<sup>s</sup>; Decl. -77° 42'

19.289	123.6	22.89	9.8	2	370
19.338	123.4	22.72	11.0	2½	370
19.31	123.5	22.80	(9.0 ... 9.2R)		20

*h* 4223; -38° 3475; 9.8A.R. 9<sup>h</sup> 30<sup>m</sup> 22<sup>s</sup>; Decl. -38° 59'

20.171	352.0	20.04	10.6	2	370
20.176	353.2	19.96	8.4	2	370
20.17	352.6	20.00	(9.5 ... 11.2)		N

## AC

20.171	193.6	24.57	10.7	2	370
20.176	193.6	23.96	8.5	2	370
20.17	193.6	24.26	(9.5 ... 11.2)		N

## AD; D = -38° 3474; 10.5

20.171	262.3	28.97	10.8	2	370
20.176	262.4	28.91	8.6	2	370
20.17	262.4	28.94	(9.5 ... 10.6)		N

## AE

20.171	317.0	37.01	10.9	2	370
20.176	318.0	37.55	8.7	1½	370
20.17	317.5	37.28	(9.5 ... 11.6)		N

## AF; F = -38° 3477; 10.5

20.171	126.0	46.15	11.0	2	370
20.176	125.8	46.30	8.8	2	370
20.17	125.9	46.22	(9.5 ... 10.8)		N

*h* 4224; -30° 2898; 7.5 :A.R. 9<sup>h</sup> 30<sup>m</sup> 40<sup>s</sup>; Decl. -30° 40'

19.254	117.7	7.50	9.6	2½	370
19.999	117.4	7.41	9.0	2½	370
20.113	116.8	7.46	8.3	2½	370
19.79	117.3	7.46	(8.1Y ... 8.7b)		F

## \* Aguilar 8; -59° 1420; 8.9

A.R. 9<sup>h</sup> 31<sup>m</sup> 2<sup>s</sup>; Decl. -59° 50'

19.248	277.6	2.74	9.4	2½	370
19.338	275.7	2.70	11.6	2½	370
19.29	276.6	2.72	(9.2 ... 11.3)		142

 $\delta$  48; -38° 3513; 9.0A.R. 9<sup>h</sup> 32<sup>m</sup> 31<sup>s</sup>; Decl. -38° 38'

20.133	76.3	0.58	9.2	3½	475
20.171	72.7	0.52	11.2	2	475
20.190	72.5	0.60	7.8	2½	475
20.16	73.8	0.57	(9.5 ... 10.0)		

*h* 4230; -77° 526; 9.7A.R. 9<sup>h</sup> 32<sup>m</sup> 33<sup>s</sup>; Decl. -77° 29'

19.289	335.2	10.39	10.1	2	370
19.338	335.4	10.16	11.3	2½	370
19.382	335.1	10.35	10.3	2	370
19.34	335.2	10.30	(9.8 ... 11.3)		N

## AC

19.338	133.0	18.96	11.5	2	370
19.382	134.2	19.01	10.4	2	370
19.36	133.6	18.98	(9.8 ... 14.1)		N

*h* 4228; -31° 2806; 8.4A.R. 9<sup>h</sup> 33<sup>m</sup> 27<sup>s</sup>; Decl. -31° 47'

19.254	160.5	2.32	9.8	2½	370
19.999	160.6	2.54	9.1	2½	370
20.114	160.6	2.44	8.4	2½	370
19.79	160.6	2.43	(9.0 ... 9.5)		R?

## AC

20.114	238.6	21.33	8.5	2½	370
20.136	238.8	21.16	10.9	2	370
20.13	238.7	21.24	(9.0 ... 11.7)		R?

## AD; D = 13.3

20.136	292.9	17.54	11.1	2	370
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*h* 4229; -38° 3539; 9.6A.R. 9<sup>h</sup> 34<sup>m</sup> 27<sup>s</sup>; Decl. -38° 22'

20.012	331.9	8.61	8.3	2½	370
20.176	331.8	8.79	9.0	2	370
20.179	332.6	8.95	11.6	2	370
20.12	332.1	8.78	(11.2 ... 11.6)		D?

*h* 4231; —41° 3920; 8.1

A.R. 9<sup>h</sup> 34<sup>m</sup> 43<sup>s</sup>; Decl. —41° 6'

20.155	211.6	7.76	12.5	1½	370
20.171	211.2	7.80	11.3	2	475
20.179	211.2	7.78	11.7	2	370
20.17	211.3	7.78	(8.9 ... 9.7)		N

*h* 4236; Cód —30° 7837; 9.7

A.R. 9<sup>h</sup> 38<sup>m</sup> 13<sup>s</sup>; Decl. —30° 11'

18.287	302.3	12.85	13.0	2	370
19.264	301.9	12.79	8.9	2½	370
19.999	303.6	13.09	9.2	2½	370
19.18	302.6	12.91	(11.2 ... 11.2)		192

*h* 4237; Cód —30° 7838; 9.3

A.R. 9<sup>h</sup> 38<sup>m</sup> 15<sup>s</sup>; Decl. —30° 9'

18.287	29.4	15.06	13.2	1½	370
19.264	31.5	15.34	9.1	2½	370
19.999	31.5	15.71	9.3	2½	370
19.18	30.8	15.37	(10.6 ... 11.9)		192

*h* 4241; —66° 1042 + 39; 7.2 + 9.4

A.R. 9<sup>h</sup> 39<sup>m</sup> 29<sup>s</sup>; Decl. —66° 21'

18.194	304.3	34.14	12.0	2	370
18.290	304.7	34.18	12.2	2½	370
18.24	304.5	34.16	(7.0 ... 10.5)		N

*h* 4239; —38° 3603; 8.3

A.R. 9<sup>h</sup> 39<sup>m</sup> 55<sup>s</sup>; Decl. —38° 1'

20.012	195.2	9.99	8.7	2	370
20.114	194.7	9.95	9.1	2	370
20.122	195.4	9.93	8.3	2	370
20.08	195.1	9.96	(8.8 ... 10.8)		N

*h* 4243 Ver la nota 193

*h* 4242; —41° 3996; 7.6

A.R. 9<sup>h</sup> 40<sup>m</sup> 43<sup>s</sup>; Decl. —41° 5'

20.122	358.1	8.00	8.5	2	370
20.155	358.1	7.83	12.7	1½	370
20.171	357.7	7.86	11.4	2½	475
20.15	358.0	7.90	(8.0 ... 9.9)		F

*h* 4244; —31° 2867 + 8; 10.2 + 9.7

A.R. 9<sup>h</sup> 41<sup>m</sup> 33<sup>s</sup>; Decl. —31° 53'

19.264	30.4	13.26	9.2	3	370
19.999	30.4	13.22	9.4	2½	370
19.63	30.4	13.24	(9.4 ... 9.4)		5

*h* 4248; —69° 1108; 8.0

A.R. 9<sup>h</sup> 41<sup>m</sup> 59<sup>s</sup>; Decl. —69° 13'

18.194	320.0	10.63	12.3	2	370
18.290	320.0	10.66	12.4	3	370
18.24	320.0	10.65	(8.3 ... 9.1)		F

*h* 4246; —37° 3755; 7.8

A.R. 9<sup>h</sup> 42<sup>m</sup> 23<sup>s</sup>; Decl. —37° 36'

20.136	142.2	32.51	11.7	2	370
20.176	141.7	32.36	9.3	2	370
20.179	143.1	32.39	12.1	2	370
20.16	142.3	32.42	(6.8 ... 13.8)		N

AC

20.136	24.3	35.34	11.5	2½	370
20.176	24.3	34.79	9.2	2	370
20.179	24.5	34.78	11.9	2	370
20.16	24.4	34.97	(6.8 ... 13.9)		N

*h* 4249; —34° 3758; 7.7

A.R. 9<sup>h</sup> 43<sup>m</sup> 26<sup>s</sup>; Decl. —34° 26'

20.114	303.5	4.48	9.2	2	370
20.136	303.0	4.36	11.4	2½	370
20.146	303.5	4.30	9.3	3	370
20.13	303.3	4.38	(8.2 ... 8.3)		20

Rü 11; Argus; 4.6

A.R. 9<sup>h</sup> 43<sup>m</sup> 59<sup>s</sup>; Decl. —64° 30'

18.295	128.6	5.12	11.2	2½	370
19.315	126.7	5.09	13.2	2	370
18.432	127.8	5.12	12.3	2½	370
18.462	128.0	5.18	12.4	2	370
18.38	127.8	5.13	(3.2 ... 6.0)		F

*h* 4250; —36° 3913; 9.2

A.R. 9<sup>h</sup> 44<sup>m</sup> 29<sup>s</sup>; Decl. —36° 24'

20.114	68.9	8.96	9.3	2	370
20.136	69.1	8.92	11.9	2	370
20.176	68.6	8.90	9.4	2½	370
20.14	68.9	8.93	(10.0 ... 10.3)		F

*h* 4258; —75° 615; 8.6

A.R. 9<sup>h</sup> 44<sup>m</sup> 29<sup>s</sup>; Decl. —75° 19'

19.289	162.4	8.87	10.4	1½	370
19.379	161.9	8.78	13.6	2½	370
19.382	161.9	8.81	10.6	2	370
19.35	162.1	8.82	(8.8 ... 9.9)		F

$h$  4252;  $-64^{\circ}$  1088 + 7; 8.9 + 9.2A.R.  $9^h$  44<sup>m</sup> 43<sup>s</sup>; Decl.  $-64^{\circ}$  32'

18.295	302.9	12.47	11.4	3	370
18.315	302.5	12.46	13.3	2½	370
18.30	302.7	12.47	(9.0 ... 9.2)		F

 $h$  4253;  $-32^{\circ}$  2742; 9.7 :A.R.  $9^h$  44<sup>m</sup> 59<sup>s</sup>; Decl.  $-32^{\circ}$  45'

20.095	35.4	12.12	11.2	2	370
20.100	35.9	12.05	8.7	2½	370
20.10	35.7	12.08	(9.8 ... 10.3)		N

 $h$  4259;  $-41^{\circ}$  4079; 8.9A.R.  $9^h$  46<sup>m</sup> 36<sup>s</sup>; Decl.  $-41^{\circ}$  56'

20.122	162.4	5.64	8.6	2½	370
20.160	163.6	5.84	9.4	2½	475
20.171	163.1	5.62	11.6	2½	475
20.15	163.0	5.70	(9.5 ... 11.0)		N

 $h$  4265;  $-79^{\circ}$  450; 8.8 :A.R.  $9^h$  47<sup>m</sup> 25<sup>s</sup>; Decl.  $-79^{\circ}$  56'

19.385	228.1	16.66	11.6	2½	370
19.407	228.6	16.55	12.9	2	370
19.40	228.3	16.61	(9.0 ... 9.9)		R

 $\Delta$  82 =  $h$  4272 = Rus 134;  $-85^{\circ}$  210; 6.7A.R.  $9^h$  48<sup>m</sup> 8<sup>s</sup>; Decl.  $-85^{\circ}$  26'

19.183	271.1	15.69	12.8	2	370
19.306	271.3	15.77	10.5	2	370
19.24	271.2	15.73	(7.6 ... 8.2)		F

 $h$  4270;  $-75^{\circ}$  326; 9.0A.R.  $9^h$  51<sup>m</sup> 38<sup>s</sup>; Decl.  $-75^{\circ}$  60'

19.289	306.0	13.10	10.5	1½	370
19.382	303.6	13.30	10.7	2	370
19.385	306.5	13.16	11.0	2½	370
19.32	305.4	13.19	(9.2 ... 11.1)		N

 $h$  4267;  $-41^{\circ}$  4166; 8.6A.R.  $9^h$  52<sup>m</sup> 18<sup>s</sup>; Decl.  $-41^{\circ}$  50'

20.122	153.5	9.69	8.8	2½	370
20.160	152.9	9.88	9.5	2	370
20.171	153.8	9.89	11.7	2	475
20.15	153.4	9.82	(9.4 ... 11.7)		F

 $h$  4268;  $-33^{\circ}$  2770; 10.0A.R.  $9^h$  52<sup>m</sup> 27<sup>s</sup>; Decl.  $-33^{\circ}$  42'

20.095	248.1	14.54	11.3	2½	370
20.100	247.6	14.70	8.8	2	370
20.10	247.9	14.62	(10.0 ... 10.9)		N

Rü 12;  $-68^{\circ}$  1002; 7.0A.R.  $9^h$  52<sup>m</sup> 29<sup>s</sup>; Decl.  $-68^{\circ}$  36'

18.194	212.7	9.31	12.5	2	370
18.290	213.1	9.45	12.5	3	370
18.24	212.9	9.38	(7.1 ... 9.5)		F

 $h$  4276;  $-78^{\circ}$  480; 9.7A.R.  $9^h$  53<sup>m</sup> 14<sup>s</sup>; Decl.  $-78^{\circ}$  9'

19.385	297.5	12.47	11.3	2	370
19.407	298.6	13.03	13.2	1	370
19.423	298.7	12.71	13.7	1½	370
19.40	298.3	12.74	(9.9 ... 12.0)		N

 $h$  4271;  $\gamma$  Antliae; 7.0A.R.  $9^h$  53<sup>m</sup> 31<sup>s</sup>; Decl.  $-35^{\circ}$  18'

20.176	318.2	31.02	9.5	2	370
20.179	317.9	30.93	12.3	2½	370
20.18	318.0	30.98	(5.5 ... 11.2)		120

 $h$  4275;  $-34^{\circ}$  3861; 9.2A.R.  $9^h$  55<sup>m</sup> 11<sup>s</sup>; Decl.  $-34^{\circ}$  5'

20.176	68.2	3.96	9.6	2½	370
20.180	68.0	3.91	12.6	3	370
20.193	68.6	4.32	9.5	3	370
20.204	68.5	4.00	9.0	3	370
20.19	68.3	4.05	(9.7 ... 10.5)		N

 $h$  4281;  $-79^{\circ}$  464; 9.1A.R.  $9^h$  56<sup>m</sup> 20<sup>s</sup>; Decl.  $-79^{\circ}$  50'

19.385	284.0	9.54	11.8	2½	370
19.423	284.5	9.62	13.9	1½	370
19.429	285.5	9.72	13.5	2	370
19.41	284.7	9.63	(9.3 ... 10.0)		N

 $h$  4280;  $-33^{\circ}$  2805; 9.0A.R.  $9^h$  57<sup>m</sup> 55<sup>s</sup>; Decl.  $-33^{\circ}$  5'

20.095	319.5	7.06	11.4	2½	370
20.100	317.9	7.08	8.9	2½	370
20.116	319.1	7.00	8.8	2	370
20.10	318.8	7.05	(9.1 ... 13.4)		N

$h$  4286 $\beta$ ;  $-66^\circ$  1172; 8.5

A.R.  $10^h$   $1^m$  58 $s$ ; Decl.  $-66^\circ$  39'

20.215	200.0	28.77	11.1	$2\frac{1}{2}$	370
20.217	200.0	28.91	8.7	$2\frac{1}{2}$	370
20.22	200.0	28.84	(8.9 ... 10.8)		194

$h$  4288;  $-75^\circ$  636 + 4; 9.0 + 9.0

A.R.  $10^h$   $3^m$  4 $s$ ; Decl.  $-75^\circ$  28'

19.289	289.2	35.39	10.6	2	370
19.382	289.0	35.35	10.9	2	370
19.35	289.1	35.37	(9.0 ... 9.1)		R $\beta$

$\hat{z}$  49;  $-34^\circ$  3944; 8.2

A.R.  $10^h$   $3^m$  28 $s$ ; Decl.  $-34^\circ$  19'

20.176	246.3	3.60	9.7	$2\frac{1}{2}$	370
20.179	247.6	3.83	9.5	$2\frac{1}{2}$	370
20.204	248.2	3.62	9.2	$2\frac{1}{2}$	370
20.19	247.4	3.68	(8.9 ... 12.7)		

$h$  4287;  $-34^\circ$  3946; 9.6

A.R.  $10^h$   $3^m$  39 $s$ ; Decl.  $-34^\circ$  11'

20.119	111.5	11.23	9.4	$2\frac{1}{2}$	370
20.176	110.9	11.25	9.8	$2\frac{1}{2}$	370
20.15	111.2	11.24	(9.8 ... 10.7)		195

$h$  4289;  $-63^\circ$  1296; 9.2

A.R.  $10^h$   $4^m$  6 $s$ ; Decl.  $-63^\circ$  59'

18.295	240.3	11.95	12.0	3	370
18.315	240.2	12.14	13.5	2	370
18.30	240.3	12.04	(10.0 ... 10.2)		196

$h$  4292;  $-65^\circ$  1248 + 50; 7.2 + 9.6

A.R.  $10^h$   $5^m$  13 $s$ ; Decl.  $-65^\circ$  12'

18.295	123.2	60.13	12.2	$2\frac{1}{2}$	370
18.315	123.0	60.17	13.7	$1\frac{1}{2}$	370
18.30	123.1	60.15	(6.0 ... 9.6)		N

I 13;  $-68^\circ$  1034; 6.0

A.R.  $10^h$   $6^m$  24 $s$ ; Decl.  $-68^\circ$  4'

18.194	141.4	1.07	13.0	2	475
18.290	141.5	0.76	13.1	$2\frac{1}{2}$	650
18.451	141.6	0.94	13.5	2	475
18.31	141.5	0.92	(6.5 ... 6.5)		

AB,C =  $h$  4295

18.194	39.5	26.04	12.8	2	370
18.290	39.6	26.14	12.9	$2\frac{1}{2}$	370
18.24	39.6	26.09	((5.7) ... 11.1)		F

$h$  4298;  $-69^\circ$  1158; 9.8

A.R.  $10^h$   $7^m$  19 $s$ ; Decl.  $-69^\circ$  48'

18.194	297.7	7.66	13.3	2	370
18.290	299.2	7.84	13.3	$2\frac{1}{2}$	370
18.451	296.1	7.84	12.4	2	370
18.31	297.7	7.78	(11.4 ... 11.6)		N

$\hat{z}$  50;  $-66^\circ$  1198; 9.5

A.R.  $10^h$   $7^m$  56 $s$ ; Decl.  $-66^\circ$  41'

20.215	152.4	3.47	11.3	$2\frac{1}{2}$	370
20.217	153.0	3.41	8.9	$2\frac{1}{2}$	370
20.223	154.8	3.11	10.1	$2\frac{1}{2}$	370
20.228	154.2	3.16	8.6	2	370
20.22	153.6	3.29	(10.4 ... 11.0)		

$h$  4300;  $-32^\circ$  2851; 8.6

A.R.  $10^h$   $10^m$  6 $s$ ; Decl.  $-32^\circ$  40'

19.254	108.7	8.96	10.0	3	370
20.057	108.2	9.12	11.5	$2\frac{1}{2}$	370
20.095	107.6	9.08	11.5	$2\frac{1}{2}$	370
19.80	108.2	9.05	(9.1 ... 9.8)		N

$h$  4301;  $-65^\circ$  1276; 7.7

A.R.  $10^h$   $10^m$  10 $s$ ; Decl.  $-65^\circ$  5'

18.295	25.5	6.92	12.4	$2\frac{1}{2}$	370
18.315	24.7	6.87	13.8	2	370
18.462	25.6	6.93	12.6	2	370
18.36	25.3	6.91	(8.5 ... 8.8)		A $\beta$

$h$  4310;  $-83^\circ$  336; 7.4

A.R.  $10^h$   $11^m$  20 $s$ ; Decl.  $-83^\circ$  28'

19.183	262.8	4.01	13.2	2	370
19.289	270.2	4.12	11.1	2	370
19.306	269.7	3.92	10.6	2	370
19.26	269.6	4.02	(8.1 ... 8.9)		A $\beta$

$h$  4304;  $-32^\circ$  2871; 7.7

A.R.  $10^h$   $14^m$  36 $s$ ; Decl.  $-32^\circ$  30'

20.057	286.2	9.66	11.6	2	370
20.095	285.9	9.65	11.6	$2\frac{1}{2}$	370
20.100	286.2	9.50	9.1	$2\frac{1}{2}$	370
20.08	286.1	9.60	(7.8 ... 10.1)		N

$h$  4306;  $-64^\circ$  1248; 6.0

A.R.  $10^h$   $15^m$  12 $s$ ; Decl.  $-64^\circ$  3'

18.295	314.0	2.40	12.6	$2\frac{1}{2}$	370
18.315	313.9	2.38	14.0	2	370
18.462	315.8	2.21	12.7	$2\frac{1}{2}$	370
18.36	314.6	2.33	(6.9 ... 7.0)		20

$h$  4314;  $-66^\circ 1231 + 2$ ;  $8.6 + 8.7$

A.R.  $10^h 17^m 15^s$ ; Decl.  $-66^\circ 54'$

18.195	12.3	19.02	13.4	2	370
18.290	12.6	19.05	13.5	2	370
18.24	12.5	19.04	(8.2 ... 8.5)		F

Aguilar 9;  $-57^\circ 3143$ ; 9.0

A.R.  $10^h 19^m 51^s$ ; Decl.  $-57^\circ 52'$

18.345	39.3	2.22	11.4	3	370
18.347	40.0	2.13	10.0	$2\frac{1}{2}$	370
* 17.90	39.7	2.22	(9.2 ... 10.8)		

$h$  4318; Cód  $-33^\circ 6953$ ; 9.3

A.R.  $10^h 20^m 8^s$ ; Decl.  $-33^\circ 34'$

20.057	19.2	12.00	11.7	2	370
20.095	18.8	11.80	11.7	$2\frac{1}{2}$	370
20.100	18.8	11.69	9.2	3	370
20.08	18.9	11.83	(10.6 ... 10.9)		197

$\Delta$  86;  $-41^\circ 4648 + 5$ ;  $7.6 + 7.9$

A.R.  $10^h 25^m 48^s$ ; Decl.  $-41^\circ 35'$

20.155	291.2	83.24	13.0	$1\frac{1}{2}$	370
20.160	291.2	83.46	9.6	2	370
20.16	291.2	83.35	(7.4 ... 7.9)		F

BC; C =  $-41^\circ 4646$ ; 10.2

20.155	75.3	41.88	13.2	$1\frac{1}{2}$	370
20.160	74.9	42.06	9.7	2	370
20.16	75.1	41.97	(7.9 ... 10.0)		

$h$  4325;  $-30^\circ 3129$ ; 9.6

A.R.  $10^h 25^m 58^s$ ; Decl.  $-30^\circ 42'$

19.999	162.9	11.91	9.7	$2\frac{1}{2}$	370
20.057	162.9	11.98	12.0	2	370
20.03	162.9	11.94	(9.40 ... 10.2b)		N

$h$  4326;  $-39^\circ 4480 + 1$ ;  $10.0 + 10.0$

A.R.  $10^h 26^m 9^s$ ; Decl.  $-39^\circ 17'$

20.122	149.1	38.93	9.5	$2\frac{1}{2}$	370
20.160	149.3	39.06	9.9	2	370
20.14	149.2	39.00	(9.4 ... 10.2)		N

$\Delta$  87;  $-60^\circ 1945 + 4$ ;  $8.6 + 7.4$

A.R.  $10^h 26^m 13^s$ ; Decl.  $-60^\circ 43'$

19.445	331.4	82.61	13.2	2	370
19.459	331.5	82.63	13.1	$2\frac{1}{2}$	370
19.45	331.5	82.62	(6.7 ... 8.0)		F

$h$  4331;  $-30^\circ 3137$ ; 9.7

A.R.  $10^h 28^m 18^s$ ; Decl.  $-30^\circ 29'$

19.999	256.0	5.34	9.9	3	370
20.095	257.0	5.20	11.8	$2\frac{1}{2}$	370
20.100	256.1	5.11	9.3	3	370
20.06	256.4	5.22	(10.7 ... 11.1)		N

\* WO 106;  $-54^\circ 3797$ ; 7.9

A.R.  $10^h 28^m 23^s$ ; Decl.  $-54^\circ 44'$

20.247	249.8	1.54	8.6	$2\frac{1}{2}$	370
20.327	249.9	1.56	11.0	3	650
20.439	250.4	1.67	11.9	$2\frac{1}{2}$	475
20.34	250.0	1.59	(8.6 ... 9.3)		D?

$h$  4335;  $-69^\circ 1288$ ; 8.2

A.R.  $10^h 28^m 33^s$ ; Decl.  $-69^\circ 26'$

18.195	220.0	7.95	13.6	2	370
18.290	219.6	8.15	13.8	$2\frac{1}{2}$	370
18.451	220.9	7.96	13.7	$1\frac{1}{2}$	370
18.31	220.2	8.02	(8.9 ... 9.3)		A?

$h$  4334;  $-34^\circ 4189$ ; 9.2

A.R.  $10^h 29^m 2^s$ ; Decl.  $-34^\circ 46'$

20.119	265.8	9.10	9.8	$2\frac{1}{2}$	370
20.171	265.1	9.33	11.9	2	475
20.177	265.0	9.25	10.0	$2\frac{1}{2}$	370
20.16	265.3	9.23	(9.9 ... 10.6)		D?

$\Delta$  93;  $-63^\circ 1501 + 3$ ;  $8.1 + 8.4$

A.R.  $10^h 30^m 40^s$ ; Decl.  $-63^\circ 29'$

18.295	39.0	25.30	12.8	$2\frac{1}{2}$	370
18.462	39.1	25.77	13.4	2	370
18.465	38.9	25.00	13.5	$2\frac{1}{2}$	370
18.41	39.0	25.36	(8.0 ... 8.7)		F

BC = I 74

18.295	231.5	2.93	12.9	$2\frac{1}{2}$	370
18.462	232.0	3.17	13.7	$1\frac{1}{2}$	370
18.465	231.7	3.08	14.3	$2\frac{1}{2}$	370
18.41	231.7	3.06	(8.7 ... 11.0)		F

$\delta$  51;  $-57^\circ 3504$ ; 9.0

A.R.  $10^h 31^m 0^s$ ; Decl.  $-57^\circ 33'$

17.428	184.6	2.57	15.4	2	370
18.339	183.0	2.26	12.2	2	370
18.347	180.1	2.21	10.3	2	370
18.361	182.8	2.26	10.5	2	475
18.12	182.6	2.32	(9.1 ... 12.0)		



C.P.D.;  $-57^{\circ} 3506$ ; 8.1:

A.R.  $10^h 31^m 1^s$ ; Decl.  $-57^{\circ} 35'$

18.339	109.1	14.14	12.4	2	370
18.361	108.9	14.16	10.3	2	475
18.35	109.0	14.15	(8.2 ... 9.3)		

BC =  $\delta 52$

18.339	34.5	2.26	12.5	2	370
18.347	33.5	2.36	10.2	2	370
18.361	35.6	2.34	10.4	2	475
18.35	34.6	2.32	(9.3 ... 12.5)		

C.P.D.;  $-57^{\circ} 3524$ ; 8.5:

A.R.  $10^h 31^m 12^s$ ; Decl.  $-57^{\circ} 34'$

17.428	328.9	12.89	15.5	2	370
18.339	329.5	12.68	12.7	2½	370
18.345	329.7	12.70	11.6	3	370
18.04	329.4	12.76	(8.9 ... 9.3)		

C.P.D.;  $-57^{\circ} 3526$ ; 8.2:

A.R.  $10^h 31^m 13^s$ ; Decl.  $-57^{\circ} 36'$

17.428	344.6	12.02	15.4	2	370
18.339	344.5	11.67	12.8	2½	370
18.345	344.1	11.82	11.8	2½	370
18.04	344.4	11.84	(8.7 ... 9.1)		

*h* 5444;  $-81^{\circ} 449 + 8$ ; 7.1 + 9.0

A.R.  $10^h 32^m 33^s$ ; Decl.  $-81^{\circ} 17'$

19.423	235.3	41.76	14.1	1½	370
19.429	234.9	42.00	13.7	1½	370
19.43	235.1	41.88	(7.4 ... 9.8) N		

\*  $\delta 5$ ;  $-57^{\circ} 3589$ ; 10.1

A.R.  $10^h 32^m 47^s$ ; Decl.  $-57^{\circ} 60'$

Identificada en 1918

$\delta 53$ ;  $-58^{\circ} 2441$ ; 9.0

A.R.  $10^h 33^m 29^s$ ; Decl.  $-58^{\circ} 29'$

20.228	126.4	7.34	9.2	2½	370
20.242	128.3	7.34	8.6	3	370
20.247	128.0	7.54	8.7	2½	370
20.24	127.6	7.41	(9.5 ... 10.0)		

$\Delta 94$ ;  $t_2$  Carinae; 7.3

A.R.  $10^h 34^m 0^s$ ; Decl.  $-58^{\circ} 32'$

17.589	20.6	14.65	15.5	2	370
* 17.39	20.2	14.58	(5.20 ... 8.5b)		

\* G 152 = Rus 153;  $-58^{\circ} 2474 + 5$ ; 8.4 + 8.6

A.R.  $10^h 34^m 14^s$ ; Decl.  $-58^{\circ} 10'$

20.218	74.2	21.21	12.6	2½	370
20.228	74.9	21.01	9.4	2½	370
20.22	74.6	21.11	(6.40 ... 8.7) R?		

I 1091;  $-57^{\circ} 3635$ ; 9.4

A.R.  $10^h 34^m 22^s$ ; Decl.  $-57^{\circ} 58'$

18.345	3.4	1.98	12.4	2½	370
18.347	1.8	2.19	10.5	2	370
18.369	2.5	2.29	12.0	2	370
18.36	2.6	2.15	(9.9 ... 10.3) 23		

*h* 4340; Cód  $-33^{\circ} 7148$ ; 9.5

A.R.  $10^h 34^m 22^s$ ; Decl.  $-33^{\circ} 47'$

20.215	128.1	6.53	12.7	2½	370
20.223	127.4	6.61	9.9	2½	370
20.228	126.9	6.79	9.9	3	370
20.22	127.5	6.64	(10.2R ... 12.5) N		

*h* 4343 = I 75;  $-64^{\circ} 1394$ ; 8.9

A.R.  $10^h 35^m 12^s$ ; Decl.  $-64^{\circ} 26'$

18.295	92.2	5.92	13.2	2½	370
18.315	98.7	5.86	14.4	1½	370
18.462	99.0	5.93	13.9	1½	370
18.36	99.0	5.90	(9.4 ... 10.2) N		

*h* 4342;  $-30^{\circ} 3159$ ; 8.2:

A.R.  $10^h 35^m 54^s$ ; Decl.  $-30^{\circ} 6'$

19.235	54.7	25.44	14.0	2½	370
19.251	54.6	25.23	13.0	2	370
19.999	54.6	25.16	10.1	2½	370
19.49	54.6	25.28	(8.2 ... 11.2) 198		

\* *h* 4345 = I 859;  $-53^{\circ} 4060$ ; 8.3

A.R.  $10^h 36^m 22^s$ ; Decl.  $-53^{\circ} 27'$

20.247	3.5	5.36	8.8	2½	370
20.327	2.1	5.29	11.0	3	650
20.439	2.2	5.33	12.0	2½	475
20.34	2.6	5.33	(8.5 ... 11.3) R		

*h* 4346;  $-60^{\circ} 2162$ ; 8.8

A.R.  $10^h 36^m 47^s$ ; Decl.  $-60^{\circ} 23'$

20.171	83.2	27.77	12.6	2½	370
20.215	83.6	27.60	11.8	2½	370
20.217	83.0	27.82	9.6	2½	370
20.20	83.3	27.73	(8.8 ... 10.30) F		

(Sigue Continued.)

## AC

20.215	247.0	10.32	12.0	2½	370
20.217	246.4	10.32	9.7	2½	370
20.22	246.7	10.32	(8.8 ... 12.9)		N

$\Delta$  97;  $-60^\circ 2203$ ; 6.4

A.R.  $10^h 38^m 27^s$ ; Decl.  $-60^\circ 31'$

18.304	174.1	12.52	10.4	2	370
18.470	173.9	12.26	13.3	2	475
18.479	173.7	12.44	13.0	2	370
18.42	173.9	12.41	(7.3 ... 8.8)		F

$h$  4349;  $-39^\circ 4617$ ; 8.6

A.R.  $10^h 38^m 30^s$ ; Decl.  $-39^\circ 26'$

20.122	246.7	4.53	9.7	2½	370
20.133	246.7	4.50	9.5	3½	475
20.160	246.6	4.61	10.0	2½	370
20.14	246.7	4.55	(9.2 ... 9.8)		N

$h$  4352;  $-48^\circ 3487$ ; 8.0

A.R.  $10^h 38^m 47^s$ ; Decl.  $-48^\circ 14'$

20.206	207.4	19.97	9.3	3	370
20.215	207.3	20.09	12.2	2½	370
20.21	207.3	20.03	(6.9 ... 11.6)		195

## AC

20.206	230.1	47.24	9.5	3	370
20.215	229.9	47.65	12.3	2½	370
20.21	230.0	47.44	(6.9 ... 13.4)		N

$\hat{c}$  54;  $-39^\circ 4632$ ; 8.4 :

A.R.  $10^h 39^m 31^s$ ; Decl.  $-39^\circ 36'$

20.133	14.2	0.52	9.6	3	475
20.177	15.6	0.55	10.1	2½	475
20.180	16.4	0.52	13.0	3	650
20.16	15.4	0.53	(9.8 ... 10.0)		

## AB,C

20.177	65.0	17.77	10.2	2½	370
20.180	65.3	17.85	12.8	3	370
20.18	65.2	17.81	((9.1) ... 10.2)		

$h$  4373;  $-40^\circ 4750$ ; 8.8 :

A.R.  $10^h 43^m 15^s$ ; Decl.  $-40^\circ 47'$

20.122	352.3	9.28	9.9	2½	370
20.133	352.8	9.36	9.9	3	475
20.160	351.7	9.41	10.2	2½	475
20.14	352.3	9.35	(9.7 ... 10.5)		R

$h$  4376;  $-69^\circ 1386 + 7$ ; 9.4 + 9.8

A.R.  $10^h 43^m 54^s$ ; Decl.  $-69^\circ 52'$

18.290	137.3	15.72	14.2	2½	370
18.479	137.8	15.54	14.2	2	370
18.38	137.5	15.63	(9.4R ... 11.2)		R?

$h$  4375;  $-38^\circ 4399$ ; 10.3

A.R.  $10^h 44^m 26^s$ ; Decl.  $-38^\circ 55'$

20.133	296.7	7.24	10.2	3	370
20.160	295.9	7.25	10.4	2	370
20.15	296.3	7.24	(12.7 ... 12.9)		N

\* Rus 161;  $-58^\circ 2755$ ; 5.9

A.R.  $10^h 44^m 27^s$ ; Decl.  $-58^\circ 40'$

20.247	271.3	1.08	8.9	2½	370
20.327	273.8	1.06	11.2	3½	650
20.439	274.9	1.19	12.2	2½	475
20.34	273.3	1.11	(7.3 ... 8.7)		P

$h$  4351 = Rus 160;  $-68^\circ 1323$ ; 8.8

A.R.  $10^h 45^m 8^s$ ; Decl.  $-68^\circ 5'$

20.206	232.5	8.02	9.0	3	370
20.215	232.5	8.07	11.6	2½	370
20.217	232.5	8.05	9.1	3	370
20.21	232.5	8.05	(9.7 ... 9.8R)		199

$h$  4378;  $-59^\circ 2784 + 3$ ; 7.2 + 9.2

A.R.  $10^h 46^m 2^s$ ; Decl.  $-59^\circ 18'$

18.304	345.7	31.23	10.6	2	370
18.470	[341.3]	30.88	14.1	2	370
18.479	345.6	30.93	13.2	2	370
18.481	345.4	30.86	12.2	3	370
18.43	345.6	30.97	(7.3 ... 10.4)		F

$h$  4380;  $-69^\circ 1418$ ; 8.8

A.R.  $10^h 48^m 7^s$ ; Decl.  $-69^\circ 14'$

18.290	110.6	15.34	14.4	2	370
18.479	109.8	15.22	14.4	2	370
18.38	110.2	15.28	(9.0 ... 12.0)		N

$h$  4381;  $-38^\circ 4450 + 2$ ; 7.7 + 8.8

A.R.  $10^h 48^m 51^s$ ; Decl.  $-38^\circ 5'$

20.122	42.2	25.91	10.3	2	370
20.133	42.1	25.97	10.4	2½	370
20.13	42.2	25.94	(7.1 ... 8.8)		F?

*h* 4382;  $-63^{\circ} 17'43'' + 4$ ; 8.9 + 9.7

A.R.  $10^h 49^m 42^s$ ; Decl.  $-63^{\circ} 18'$

18.296	16.2	14.08	13.5	2	370
18.462	16.0	14.05	14.0	2	370
18.38	16.1	14.06	(9.2 ... 10.5)	N	

BC; C = 13.2

18.462	321.5	8.93	14.2	1 1/2	370
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*h* 4390;  $-82^{\circ} 433$ ; 9.2

A.R.  $10^h 50^m 40^s$ ; Decl.  $-82^{\circ} 33'$

20.223	329.4	14.31	10.4	2	370
20.228	328.4	14.37	8.8	2	370
20.23	328.9	14.34	(9.2 ... 12.0)	N	

*h* 4385;  $-41^{\circ} 50'11''$ ; 8.0

A.R.  $10^h 50^m 59^s$ ; Decl.  $-41^{\circ} 22'$

20.160	240.8	21.47	10.6	2	370
20.206	241.8	21.59	9.6	2 1/2	370
20.18	241.3	21.53	(8.2 ... 13.6)	N	

AC

20.160	262.3	23.74	10.7	2	370
20.206	261.9	23.60	9.7	2 1/2	370
20.18	262.1	23.67	(8.2 ... 13.9)	N	

*h* 4389;  $-30^{\circ} 32'50''$ ; 7.9

A.R.  $10^h 52^m 19^s$ ; Decl.  $-30^{\circ} 54'$

19.999	336.3	10.26	10.2	2 1/2	370
20.057	336.2	10.40	12.1	2	370
20.03	336.3	10.33	(8.4 ... 9.6)	N	

*h* 4393;  $-68^{\circ} 13'77''$ ; 6.7

A.R.  $10^h 52^m 57^s$ ; Decl.  $-68^{\circ} 22'$

18.290	130.8	8.75	14.7	1 1/2	370
18.479	130.4	8.72	14.5	2	370
18.481	129.9	8.79	13.9	2 1/2	370
18.42	130.4	8.75	(6.9 ... 9.7)	F	

*h* 4391;  $-34^{\circ} 44'19''$ ; 7.6

A.R.  $10^h 53^m 12^s$ ; Decl.  $-34^{\circ} 12'$

18.999	58.9	26.75	10.4	2 1/2	370
20.057	59.1	26.71	12.2	2	370
20.03	59.0	26.73	(8.0 ... 11.4)	N	

Tapia;  $-62^{\circ} 18'37''$ ; 9.4

A.R.  $10^h 53^m 20^s$ ; Decl.  $-62^{\circ} 12'$

BC

20.204	254.4	3.64	10.9	2 1/2	370
20.242	253.5	4.05	8.9	3	370
20.247	252.2	3.71	9.1	2 1/2	370
20.23	253.4	3.80	(9.50 ... 14.2)	200	

*h* 4396;  $-36^{\circ} 47'55''$ ; 8.9

A.R.  $10^h 55^m 38^s$ ; Decl.  $-36^{\circ} 21'$

20.119	256.7	16.80	10.0	2 1/2	370
20.171	256.2	16.71	12.1	2 1/2	370
20.207	256.8	16.82	11.4	3	370
20.17	256.6	16.78	(9.0 ... 11.0)	N	

$\geq 55$ ;  $-61^{\circ} 20'37''$ ; 8.8

A.R.  $10^h 57^m 2^s$ ; Decl.  $-61^{\circ} 29'$

18.388	200.4	5.66	11.9	2	370
18.470	202.0	5.73	14.2	2	370
18.43	201.2	5.70	(8.8 ... 12.0)		

*h* 4400;  $-60^{\circ} 24'9''$ ; 9.8

A.R.  $10^h 58^m 54^s$ ; Decl.  $-60^{\circ} 42'$

18.470	200.1	7.71	14.4	2	370
18.481	201.2	7.85	12.4	3	370
18.487	202.7	7.78	13.0	1 1/2	370
18.48	201.3	7.78	(9.7 ... 12.8)	N	

*h* 4406;  $-83^{\circ} 383$ ; 9.5

A.R.  $10^h 59^m 7^s$ ; Decl.  $-83^{\circ} 15'$

19.183	5.8	8.30	13.5	2	370
19.289	5.8	8.08	11.2	1 1/2	370
19.306	5.7	8.23	10.8	2	370
19.26	5.8	8.20	(9.8 ... 10.1)	F	

$\geq 56$ ;  $-60^{\circ} 25'10''$ ; 8.8

A.R.  $11^h 0^m 16^s$ ; Decl.  $-60^{\circ} 14'$

18.470	150.0	5.86	14.5	2	370
18.481	150.4	5.78	12.5	3	370
18.45	150.2	5.82	(9.2 ... 9.6)		

*h* 4402;  $-37^{\circ} 45'71''$ ; 9.6

A.R.  $11^h 0^m 18^s$ ; Decl.  $-37^{\circ} 47'$

20.119	119.5	9.52	10.2	2 1/2	370
20.231	120.5	9.56	11.0	2 1/2	370
20.242	120.8	9.70	9.1	2 1/2	370
20.20	120.3	9.59	(10.1 ... 11.1)	N	

AC

20.231	76.8	13.72	11.1	2 1/2	370
20.242	79.5	13.70	9.2	2 1/2	370
20.24	78.2	13.71	(10.1 ... 14.2)	N	

I 869;  $-40^{\circ} 49'64''$ ; 8.0

A.R.  $11^h 1^m 23^s$ ; Decl.  $-40^{\circ} 47'$

20.177	331.4	1.70	10.5	2 1/2	370
20.180	330.4	—	13.3	3	650
20.207	332.4	1.74	10.2	2 1/2	475
20.19	331.4	1.72	(8.3 ... 9.9)	D?	

(Sigue Continued.)

AC = *h* 4408 AB

20.177	345.3	20.42	10.6	2½	370
20.207	345.4	20.60	9.9	2½	370
20.19	345.3	20.51	(8.3 ... 11.5)		N

AD = *h* 4408 AC

20.177	110.0	22.29	10.7	2	370
20.207	109.2	22.51	10.1	2½	370
20.19	109.6	22.40	(8.3 ... 13.5)		R?

*h* 4409; —41° 5118; 5.6A.R. 11<sup>h</sup> 1<sup>m</sup> 29<sup>s</sup>; Decl. —41° 58'

20.160	267.8	2.05	10.9	2½	370
20.177	267.9	2.09	10.8	2½	370
20.180	269.6	1.92	13.1	3	650
20.17	268.4	2.02	(5.6 ... 8.2)		20

*h* 4413; Cód —33° 7541; 9.9A.R. 11<sup>h</sup> 4<sup>m</sup> 27<sup>s</sup>; Decl. —33° 55'

19.999	325.1	11.24	10.5	2½	370
20.100	324.5	—	9.5	2½	370
20.114	326.2	11.52	10.1	1½	370
20.119	325.8	11.53	10.3	2	370
20.08	325.4	11.43	(10.9 ... 12.4)		N

*h* 4415; —63° 1860; 5.7A.R. 11<sup>h</sup> 7<sup>m</sup> 33<sup>s</sup>; Decl. —63° 29'

18.296	124.4	18.97	13.7	2	370
18.462	124.7	19.20	14.4	1½	370
18.38	124.5	19.08	(5.7 ... 12.0)		142

*h* 4419; —34° 4566; 10.2A.R. 11<sup>h</sup> 9<sup>m</sup> 19<sup>s</sup>; Decl. —34° 23'

20.119	114.5	13.82	10.4	2	370
20.136	113.5	13.62	12.9	2	370
20.13	114.0	13.72	(10.9 ... 12.5)		N

*h* 4424; —76° 658; 9.1A.R. 11<sup>h</sup> 13<sup>m</sup> 2<sup>s</sup>; Decl. —76° 12'

19.286	352.2	7.75	11.3	2½	370
19.289	353.3	7.72	10.8	2	370
19.328	352.3	7.83	11.4	2½	370
19.30	352.6	7.77	(9.2 ... 9.4)		N

## BC

19.289	267.4	6.79	10.9	2	370
19.328	265.8	7.15	11.5	2	370
19.31	266.6	6.97	(9.4 ... 13.3)		

## Hu 1483; —56° 4430; 9.0

A.R. 11<sup>h</sup> 16<sup>m</sup> 2<sup>s</sup>; Decl. —56° 43'

18.402	42.2	2.16	14.1	2½	370
18.481	42.7	1.92	12.7	2½	370
21.389	44.4	2.10	13.4	3	370
19.42	43.1	2.06	(9.1 ... 12.3)		M?

*h* 4428; —30° 3320; 8.2A.R. 11<sup>h</sup> 16<sup>m</sup> 26<sup>s</sup>; Decl. —30° 13'

19.552	156.8	20.29	14.4	2½	370
19.563	156.6	20.64	14.5	2½	370
19.576	158.2	20.36	15.2	2	370
19.56	157.2	20.43	(8.1 ... 12.8)		N

*h* 4430; —30° 3322; 8.6A.R. 11<sup>h</sup> 16<sup>m</sup> 54<sup>s</sup>; Decl. —30° 12'

19.552	275.3	18.79	14.5	2½	370
19.563	275.1	18.69	14.3	2½	370
19.56	275.2	18.74	(8.4 ... 11.5)		N

*h* 4432; —64° 1657; 5.5A.R. 11<sup>h</sup> 17<sup>m</sup> 57<sup>s</sup>; Decl. —64° 16'

18.296	299.9	2.43	13.9	2	370
18.462	299.4	2.78	14.5	2	370
18.465	299.4	2.35	14.4	2½	475
18.479	299.5	2.62	14.7	2	370
18.43	299.5	2.54	(5.6 ... 6.7)		A

*h* 4427; —83° 412; 9.9A.R. 11<sup>h</sup> 19<sup>m</sup> 3<sup>s</sup>; Decl. —83° 5'

20.223	132.3	6.54	10.8	2	370
20.228	133.1	6.97	8.9	2	370
20.242	132.5	6.84	9.4	2½	370
20.23	132.6	6.78	(11.0 ... 11.2)		9

## \* Bris. 3574; —60° 2911; 8.7

A.R. 11<sup>h</sup> 19<sup>m</sup> 15<sup>s</sup>; Decl. —60° 58'

20.207	91.9	2.07	13.0	2½	475
20.228	95.5	1.97	9.6	2½	370
20.242	95.1	1.90	9.6	3	370
20.439	95.4	1.89	12.3	2½	475
21.386	100.4	1.95	12.3	2½	370
21.389	98.7	1.72	13.2	3	370
20.28	94.5	1.96			
21.39	99.5	1.84	(8.2 ... 9.4)		B

*h* 4438; —39° 5090; 7.2A.R. 11<sup>h</sup> 21<sup>m</sup> 27<sup>s</sup>; Decl. —39° 11'

20.133	196.5	23.12	10.5	3	370
20.160	196.3	23.17	11.1	2	370
20.14	196.4	23.14	(7.2 ... 11.2)		N

*h* 4439;  $-30^{\circ} 3333 + 4$ ;  $8.2 + 9.0$

A.R.  $11^{\text{h}} 22^{\text{m}} 2^{\text{s}}$ ; Decl.  $-30^{\circ} 33'$

19.552	109.5	18.57	14.6	$2\frac{1}{2}$	370
19.563	109.1	18.42	14.6	$2\frac{1}{2}$	370
19.56	109.3	18.50	(8.6 ... 9.4)		N

*h* 4440;  $-77^{\circ} 675$ ;  $8.3$

A.R.  $11^{\text{h}} 22^{\text{m}} 56^{\text{s}}$ ; Decl.  $-77^{\circ} 50'$

19.286	161.4	22.57	11.4	$2\frac{1}{2}$	370
19.289	162.5	22.40	11.0	$1\frac{1}{2}$	370
19.328	162.2	22.14	11.7	2	370
19.30	162.0	22.37	(7.8 ... 12.5)		N

*h* 4443; Anon.

A.R.  $11^{\text{h}} 24^{\text{m}} 45^{\text{s}}$ ; Decl.  $-68^{\circ} 56'$

18.479	111.6	8.87	15.1	2	370
18.481	111.0	8.50	14.0	$2\frac{1}{2}$	370
18.503	110.8	8.66	15.3	$2\frac{1}{2}$	370
18.49	111.1	8.68	(13.1 ... 13.2)		N

$\varepsilon$  57;  $-68^{\circ} 1516$ ;  $9.6$

A.R.  $11^{\text{h}} 25^{\text{m}} 4^{\text{s}}$ ; Decl.  $-68^{\circ} 33'$

18.479	297.7	3.82	15.3	2	370
18.481	297.0	3.97	14.1	$2\frac{1}{2}$	370
18.503	296.5	4.28	15.5	$2\frac{1}{2}$	370
18.49	297.1	4.02	(12.1 ... 12.7)		

*h* 4447;  $-63^{\circ} 1913 + 14$ ;  $9.5 + 9.4$

A.R.  $11^{\text{h}} 26^{\text{m}} 31^{\text{s}}$ ; Decl.  $-63^{\circ} 15'$

18.296	169.3	20.41	14.1	2	370
18.318	169.1	20.26	15.0	$2\frac{1}{2}$	370
18.31	169.2	20.33	(10.4 ... 10.5)		F

*h* 4449;  $\xi$  Hydrae;  $5.5$

A.R.  $11^{\text{h}} 26^{\text{m}} 52^{\text{s}}$ ; Decl.  $-31^{\circ} 10'$

19.552	150.4	67.79	14.7	$2\frac{1}{2}$	370
19.563	150.6	67.90	14.7	$2\frac{1}{2}$	370
19.56	150.5	67.84	(3.6 ... 10.6)		N

*h* 4452;  $-63^{\circ} 1919 + 18$ ;  $8.8 + 9.5$

A.R.  $11^{\text{h}} 27^{\text{m}} 52^{\text{s}}$ ; Decl.  $-63^{\circ} 12'$

18.318	323.3	16.54	15.1	$2\frac{1}{2}$	370
18.427	323.5	16.49	14.0	$2\frac{1}{2}$	370
18.37	323.4	16.51	(9.2 ... 10.4)		F

*h* 4454;  $-34^{\circ} 4737 + 8$ ;  $9.0 + 10.0$

A.R.  $11^{\text{h}} 28^{\text{m}} 24^{\text{s}}$ ; Decl.  $-34^{\circ} 29'$

20.119	33.3	18.92	10.6	$2\frac{1}{2}$	370
20.136	33.1	19.10	13.1	2	370
20.13	33.2	19.01	(8.6 ... 10.9)		9

*h* 4455 = *h* 4463;  $-32^{\circ} 3125$ ;  $7.0$

A.R.  $11^{\text{h}} 30^{\text{m}} 24^{\text{s}}$ ; Decl.  $-32^{\circ} 53'$

19.552	243.4	3.52	14.8	$2\frac{1}{2}$	370
19.563	243.2	3.57	14.8	$2\frac{1}{2}$	475
19.576	244.1	3.52	15.4	2	370
19.56	243.6	3.54	(6.2Y ... 8.4)		C

*h* 4457; Anon.

A.R.  $11^{\text{h}} 30^{\text{m}} 45^{\text{s}}$ ; Decl.  $-59^{\circ} 23'$

17.608	295.0	6.96	16.5	3	370
18.470	295.2	7.17	14.7	2	370
18.481	292.3	6.90	12.9	$2\frac{1}{2}$	370
18.19	294.2	7.01	(12.2 ... 12.7)		N

BC; C = 14.1

17.608 289.3 4.01 16.6 3 370

$\Delta$  113;  $-38^{\circ} 4784 + 5$ ;  $7.3 + 8.2$

A.R.  $11^{\text{h}} 30^{\text{m}} 50^{\text{s}}$ ; Decl.  $-38^{\circ} 16'$

20.122	150.9	145.47	10.7	$1\frac{1}{2}$	370
20.160	151.0	145.70	11.2	2	370
20.14	151.0	145.59	(7.1 ... 7.60)		N

*h* 4462 = Rus 174;  $-82^{\circ} 467$ ;  $8.6$

A.R.  $11^{\text{h}} 33^{\text{m}} 13^{\text{s}}$ ; Decl.  $-82^{\circ} 23'$

19.183	259.7	5.14	13.8	2	370
19.289	262.3	4.84	11.4	$1\frac{1}{2}$	370
19.328	262.5	5.04	11.9	$2\frac{1}{2}$	370
19.27	261.5	5.01	(9.2 ... 10.9)		F

*h* 4461;  $-65^{\circ} 1698$ ;  $9.4$

A.R.  $11^{\text{h}} 33^{\text{m}} 21^{\text{s}}$ ; Decl.  $-65^{\circ} 19'$

18.318	112.6	10.12	15.6	$2\frac{1}{2}$	370
18.427	114.2	10.11	14.4	2	370
18.462	113.2	10.54	15.1	$1\frac{1}{2}$	370
18.40	113.3	10.26	(9.8 ... 12.7)		N

AC

18.318	38.6	—	15.4	2	370
18.427	39.7	16.66	14.3	2	370
18.462	39.7	16.51	14.9	2	370
18.40	39.3	16.59	(9.8 ... 13.4)		N

Wash.Z = C6;  $-37^{\circ} 4849$ ;  $7.2$

A.R.  $11^{\text{h}} 33^{\text{m}} 48^{\text{s}}$ ; Decl.  $-37^{\circ} 25'$

17.540	95.0	17.11	14.6	3	370
18.487	95.3	17.11	12.5	$2\frac{1}{2}$	370
18.01	95.1	17.11	(6.8 ... 8.2)		11

$\Delta 114 = \Delta 115; -37^\circ 4849; 7.2$ A.R.  $11^h 33^m 49^s$ ; Decl.  $-37^\circ 25'$ 

21.386	94.9	17.12	12.9	2½	370
21.389	95.1	17.07	13.8	3	370
21.39	95.0	17.09	(7.2 ... 9.0)		N

Bris 3706;  $-62^\circ 2206 + 5; 7.8 + 8.3$ A.R.  $11^h 34^m 0^s$ ; Decl.  $-62^\circ 47'$ 

18.318	276.8	27.81	14.7	2	370
18.427	276.9	27.77	14.1	2	370
18.462	276.8	28.00	14.7	2	370
18.40	276.8	27.86	(7.7 ... 8.5)		F?

 $h 4465; -31^\circ 3315 + 16; 7.0 + 8.0$ A.R.  $11^h 35^m 30^s$ ; Decl.  $-31^\circ 48'$ 

19.503	345.9	27.40	15.4	1½	370
19.516	344.9	27.23	15.4	2½	370
19.51	345.4	27.31	(5.7 ... 12.8)		R?

AC

19.503	44.4	67.01	15.3	1½	370
19.516	44.4	67.08	15.3	2½	370
19.51	44.4	67.04	(5.7 ... 8.5)		N

 $h 4466; -58^\circ 3798; 9.7$ A.R.  $11^h 36^m 13^s$ ; Decl.  $-58^\circ 16'$ 

17.608	316.3	8.11	16.8	3	370
17.633	315.6	7.48	17.5	2	370
18.481	315.2	7.69	13.1	2½	370
17.91	315.7	7.76	(10.8 ... 11.3)		N

 $h 4468; -82^\circ 469; 8.0$ A.R.  $11^h 36^m 40^s$ ; Decl.  $-82^\circ 24'$ 

19.183	146.6	22.22	14.0	1½	370
19.289	147.7	22.23	11.5	1½	370
19.328	147.3	22.38	12.1	2	370
19.27	147.2	22.28	(7.3 ... 11.4)		R

 $\delta 58; -37^\circ 4889; 8.2$ A.R.  $11^h 38^m 50^s$ ; Decl.  $-37^\circ 39'$ 

21.386	277.7	3.39	13.3	3	370
21.389	278.3	3.33	14.0	2½	370
21.39	278.0	3.36	(8.5 ... 13.2)		

 $h 4471; \lambda Muscae; 4.6$ A.R.  $11^h 39^m 43^s$ ; Decl.  $-66^\circ 2'$ 

18.479	275.9	40.54	15.6	1½	370
18.481	274.7	40.61	14.3	2½	370
18.503	275.2	40.59	15.7	2	370
18.49	275.3	40.58	(3.9 ... 12.8)		N

 $h 4475; -60^\circ 3373; 9.2$ A.R.  $11^h 42^m 55^s$ ; Decl.  $-60^\circ 45'$ 

18.405	124.7	4.04	15.4	2	370
18.427	127.6	4.58	13.8	2½	370
* 17.97	126.3	4.44	(10.5 ... 11.4)		22

 $h 4478; \beta Hydrae; 5.2$ A.R.  $11^h 46^m 36^s$ ; Decl.  $-33^\circ 13'$ 

19.503	356.9	1.40	15.6	2	650
19.516	355.0	1.53	15.7	3	475
19.552	355.4	1.40	15.2	3	650
19.52	355.8	1.43	(4.6 ... 5.7)		P

 $\Delta 116; -31^\circ 3352 + 1; 7.8 + 7.9$ A.R.  $11^h 50^m 24^s$ ; Decl.  $-31^\circ 34'$ 

19.503	263.1	19.57	15.7	2	370
19.505	262.8	19.67	15.7	1½	370
19.516	263.0	19.46	15.8	3	370
19.51	263.0	19.57	(7.8 ... 7.9)		F

BC

19.503	1.0	24.81	15.8	2	370
19.505	1.4	24.92	15.8	1½	370
19.50	1.2	24.86	(7.9 ... 12.1)		N

 $h 4484 = \lambda 141; -40^\circ 5469; 7.9$ A.R.  $11^h 52^m 1^s$ ; Decl.  $-40^\circ 15'$ 

20.133	309.9	3.30	10.9	3	370
20.160	309.3	3.62	11.4	2	370
20.177	308.5	3.45	11.0	3	370
20.185	309.2	3.55	11.0	2	370
20.16	309.2	3.48	(7.2 ... 10.1)		M

 $h 4485; -41^\circ 5660 + 59; 9.6 + 9.5$ A.R.  $11^h 53^m 1^s$ ; Decl.  $-41^\circ 38'$ 

20.133	350.7	15.73	11.1	3	370
20.160	350.4	15.75	11.6	2½	370
20.15	350.6	15.74	(10.1 ... 10.2)		N

 $h 4486; \varepsilon Chamaeleontis; 5.1$ A.R.  $11^h 53^m 26^s$ ; Decl.  $-77^\circ 32'$ 

20.158	183.9	1.15	11.5	2	475
20.223	186.7	1.45	11.2	2½	475
20.242	187.5	1.33	12.5	2½	370
20.21	186.0	1.31	(6.1 ... 6.5)		C

 $h 4487; -36^\circ 5292; 8.2$ A.R.  $11^h 53^m 53^s$ ; Decl.  $-36^\circ 3'$ 

20.100	125.1	5.75	9.9	3	370
20.114	125.5	5.71	10.3	1½	370
20.136	124.8	5.76	13.2	2½	370
20.12	125.1	5.74	(8.9 ... 9.4)		F

*h* 4488; —60° 35'22; 8.4

A.R. 11<sup>h</sup> 53<sup>m</sup> 58<sup>s</sup>; Decl. —60° 40'

17.603	138.3	7.24	16.2	2	370
18.402	138.5	7.27	15.4	2½	370
18.405	138.5	7.02	15.6	2	370
18.14	138.4	7.18	(8.9 ... 11.2)	N	

δ 59; —65° 17'71; 8.9

A.R. 11<sup>h</sup> 55<sup>m</sup> 26<sup>s</sup>; Decl. —65° 34'

18.320	218.1	1.12	15.6	2	370
18.427	214.8	1.07	14.6	2½	370
18.465	221.1	1.00	14.6	2½	475
18.481	216.0	1.12	14.4	2½	650
18.42	217.5	1.08	(9.4 ... 10.9)		

*h* 4490; —84° 37'1 + 2; 8.4 + 9.1

A.R. 11<sup>h</sup> 56<sup>m</sup> 8<sup>s</sup>; Decl. —84° 56'

19.289	144.9	24.99	11.7	2	370
19.328	144.7	25.11	12.3	2	370
19.31	144.8	25.05	(2.7Y ... 10.2b)	C?	

ε 60; —65° 17'79; 8.5

A.R. 11<sup>h</sup> 56<sup>m</sup> 47<sup>s</sup>; Decl. —65° 8'

18.320	131.6	3.18	15.8	2½	370
18.413	132.4	3.11	14.9	2	370
18.427	132.5	3.13	14.7	2½	370
18.39	132.2	3.14	(8.7 ... 11.3)		

*h* 4499; —36° 53'13; 8.6

A.R. 11<sup>h</sup> 57<sup>m</sup> 9<sup>s</sup>; Decl. —36° 13'

20.100	43.8	7.81	10.3	2½	370
20.114	45.0	7.99	10.4	1½	370
20.136	43.8	7.91	13.4	2½	370
20.12	44.2	7.90	(9.8 ... 10.1)	201	

λ 143; —38° 49'72; 7.4

A.R. 11<sup>h</sup> 57<sup>m</sup> 16<sup>s</sup>; Decl. —38° 19'

20.177	213.2	0.51	11.2	3	475
20.185	213.0	0.49	11.2	2½	475
20.223	205.5	0.58	11.4	2½	475
20.19	210.6	0.53	(7.6 ... 7.7)	M	

Δ 117; —61° 29'33 + 5; 8.2 + 8.8

A.R. 11<sup>h</sup> 58<sup>m</sup> 21<sup>s</sup>; Decl. —61° 18'

17.603	148.8	23.08	16.4	2	370
18.402	149.0	22.87	15.6	2½	370
18.405	149.4	22.90	15.8	2	370
18.12	149.1	22.95	(8.2 ... 8.3)	F	

(Sigue Continued.)

AC; C = —61° 29'34; 9.3

17.603	18.4	25.29	16.5	2	370
18.405	18.3	24.80	15.7	2	370
18.00	18.4	25.04	(8.2 ... 10.6)	F	

*h* 4495; —32° 31'97; 7.0

A.R. 11<sup>h</sup> 59<sup>m</sup> 41<sup>s</sup>; Decl. —32° 15'

19.503	316.5	6.74	15.9	2	370
19.505	317.3	6.65	16.0	1½	370
19.516	316.5	6.69	15.9	3	370
19.51	316.8	6.69	(7.1 ... 9.1)	F	

*h* 4498; —65° 17'88; 7.1

A.R. 11<sup>h</sup> 59<sup>m</sup> 55<sup>s</sup>; Decl. —65° 1'

18.318	61.3	8.77	16.0	3	370
18.320	61.0	8.65	15.9	2	370
18.413	60.2	8.71	15.0	2	370
18.35	60.8	8.71	(6.6 ... 8.4)	F	

*h* 4500 = Δ 118; —37° 50'41 + 3; 7.3 + 8.8

A.R. 12<sup>h</sup> 0<sup>m</sup> 12<sup>s</sup>; Decl. —37° 10'

20.136	30.5	50.19	13.6	2	370
20.185	30.8	50.49	11.4	2	370
20.223	30.5	50.21	11.6	2½	370
20.18	30.6	50.30	(7.2 ... 9.0)	202	

*h* 4501; γ Crucis; 5.3

A.R. 12<sup>h</sup> 0<sup>m</sup> 22<sup>s</sup>; Decl. —63° 55'

18.318	298.9	44.16	16.1	2	370
18.413	298.7	43.81	15.1	1½	370
18.37	298.8	43.99	(4.8 ... 11.8)	N	

*h* 4502; —75° 7'84; 8.8:

A.R. 12<sup>h</sup> 2<sup>m</sup> 8<sup>s</sup>; Decl. —75° 47'

18.640	359.7	14.25	16.5	2	370
18.654	360.3	14.43	17.3	2	370
19.286	359.5	14.20	11.6	2½	370
18.86	359.8	14.29	(9.1 ... 9.7)	F?	

J 148 = Howe 18 = Melb.; —34° 50'22; 6.6

A.R. 12<sup>h</sup> 3<sup>m</sup> 35<sup>s</sup>; Decl. —34° 1'

20.177	20.7	3.48	11.3	3	475
20.185	22.4	3.62	11.6	2	370
20.223	21.1	3.51	11.7	2½	370
20.19	21.4	3.54	(6.7 ... 8.5)	120	

λ 145; —37° 50'78; 6.6

A.R. 12<sup>h</sup> 4<sup>m</sup> 6<sup>s</sup>; Decl. —37° 10'

20.177	Sin compañera	3	475		
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$h$  4504;  $-82^\circ 50'$ ; 9.0A.R.  $12^h 5^m 5^s$ ; Decl.  $-82^\circ 40'$ 

20.242	222.2	43.89	12.7	$2\frac{1}{2}$	370
20.247	221.8	43.59	10.1	2	370
20.24	222.0	43.74	(8.2R ... 14.0)		120

Aguilar;  $-61^\circ 30'49''$ ; 8.6A.R.  $12^h 8^m 48^s$ ; Decl.  $-61^\circ 51'$ 

18.402	256.3	3.59	15.7	$2\frac{1}{2}$	370
18.413	253.6	3.48	15.4	$1\frac{1}{2}$	370
18.427	254.9	3.59	14.8	$2\frac{1}{2}$	370
18.41	254.9	3.55	(8.7 ... 11.1)		7

 $h$  4512;  $\zeta$  Crucis; 4.4A.R.  $12^h 11^m 41^s$ ; Decl.  $-63^\circ 18'$ 

18.413	340.2	33.56	15.6	$1\frac{1}{2}$	370
18.465	338.7	33.91	14.7	$2\frac{1}{2}$	370
18.471	338.9	33.80	15.2	2	370
18.45	339.3	33.76	(4.2 ... 13.3)		N

 $h$  4513;  $-32^\circ 32'26''$ ; 8; 7.9 + 9.6A.R.  $12^h 12^m 28^s$ ; Decl.  $-32^\circ 36'$ 

19.503	99.3	46.96	16.0	$1\frac{1}{2}$	370
19.516	99.3	46.97	16.0	$2\frac{1}{2}$	370
19.51	99.3	46.97	(7.9 ... 9.5)		N

 $h$  4515;  $-69^\circ 16'54''$ ; 8.2A.R.  $12^h 13^m 20^s$ ; Decl.  $-69^\circ 5'$ 

18.471	54.8	12.77	15.5	$1\frac{1}{2}$	370
18.479	54.6	12.68	16.0	2	370
18.48	54.7	12.72	(8.8 ... 10.9)		F?

 $h$  4516;  $-63^\circ 22'61''$ ; 7.8A.R.  $12^h 16^m 56^s$ ; Decl.  $-63^\circ 18'$ 

18.318	95.9	17.46	16.3	3	370
18.465	95.9	17.44	14.9	3	370
18.39	95.9	17.45	(8.5 ... 9.6)		R?

 $\delta$  61;  $-31^\circ 34'29''$ ; 9.2A.R.  $12^h 17^m 32^s$ ; Decl.  $-31^\circ 42'$ 

19.516	129.6	1.11	16.3	$2\frac{1}{2}$	475
19.552	133.0	1.16	15.3	$2\frac{1}{2}$	650
19.563	127.8	1.11	15.2	2	475
19.54	130.1	1.13	(10.2 ... 10.2)		

AB, C =  $h$  4519

19.503	272.1	9.15	16.2	2	370
19.516	271.6	9.08	16.2	$2\frac{1}{2}$	370
19.552	272.1	9.12	15.4	3	370
19.52	271.9	9.12	((9.7) ... 10.0)		N

 $h$  4521;  $-32^\circ 32'39''$ ; 9.1A.R.  $12^h 17^m 51^s$ ; Decl.  $-32^\circ 13'$ 

19.503	285.5	12.19	16.1	2	370
19.563	283.6	12.33	15.3	$1\frac{1}{2}$	370
19.576	283.8	12.43	15.5	2	370
19.55	284.3	12.32	(9.3 ... 11.3)		N

 $h$  4518;  $-40^\circ 56'88''$ ; 7.5A.R.  $12^h 18^m 8^s$ ; Decl.  $-40^\circ 41'$ 

20.133	208.1	10.08	11.2	$2\frac{1}{2}$	370
20.160	207.7	10.17	11.8	$2\frac{1}{2}$	370
20.15	207.9	10.12	(6.90 ... 9.6B)		F

 $h$  4522;  $-68^\circ 16'50''$ ; 7.4A.R.  $12^h 18^m 24^s$ ; Decl.  $-68^\circ 47'$ 

18.465	66.7	12.77	15.0	3	370
18.471	67.0	12.79	15.6	2	370
18.479	67.0	12.70	15.8	2	370
18.47	66.9	12.75	(8.2 ... 9.2)		9;42

 $\delta$  62;  $-32^\circ 32'43''$ ; 8.2A.R.  $12^h 18^m 37^s$ ; Decl.  $-32^\circ 24'$ 

19.516	102.7	1.00	16.5	3	475
19.552	101.6	1.05	15.5	3	650
19.563	102.3	0.93	15.0	$2\frac{1}{2}$	475
19.54	102.2	0.99	(8.7 ... 9.4)		

 $h$  4510;  $-36^\circ 54'97''$ ; 9; 9.4 + 9.6A.R.  $12^h 20^m 18^s$ ; Decl.  $-36^\circ 47'$ 

20.136	40.7	18.54	13.8	$2\frac{1}{2}$	370
20.177	40.6	18.24	11.5	3	370
20.223	40.4	18.47	11.9	$2\frac{1}{2}$	370
20.18	40.6	18.42	(9.7 ... 10.3)		22

BC; C =  $-36^\circ 54'98''$ ; 9.7

20.136	12.7	12.63	14.0	$2\frac{1}{2}$	370
20.177	12.9	12.62	11.6	3	370
20.223	12.7	12.69	11.9	3	370
20.18	12.8	12.65	(10.3 ... 10.2)		203

\*  $\Delta$  124;  $\gamma$  Crucis; 4.8 + 7.3A.R.  $12^h 24^m 14^s$ ; Decl.  $-56^\circ 25'$ 

19.278	31.2	110.59	11.8	2	370
19.287	31.1	110.63	12.2	$2\frac{1}{2}$	370
19.333	31.2	110.56	12.6	$2\frac{1}{2}$	370
19.30	31.2	110.59	(2.2 ... 8.5)		204

 $h$  4528;  $-31^\circ 34'59''$ ; 7.5A.R.  $12^h 27^m 35^s$ ; Decl.  $-31^\circ 24'$ 

19.576	151.1	24.83	15.6	2	370
19.587	151.4	24.74	15.1	$2\frac{1}{2}$	370
19.58	151.3	24.78	(7.4 ... 11.6)		R?



*h* 4529; —78° 765; 9.3

A.R. 12<sup>h</sup> 27<sup>m</sup> 57<sup>s</sup>; Decl. —78° 18'

19.287	315.6	7.91	11.9	2	370
19.328	314.8	8.05	12.5	2	370
19.423	313.5	7.99	14.5	14	370
19.35	314.6	7.98	(9.3 ... 13.1)		N

*h* 4530; —46° 5892; 9.3

A.R. 12<sup>h</sup> 28<sup>m</sup> 10<sup>s</sup>; Decl. —46° 36'

20.247	92.4	25.15	10.6	1½	370
20.256	92.7	24.59	11.7	2	370
20.338	92.4	25.03	11.6	2	370
20.28	92.5	24.92	(9.2 ... 11.0)		84

*h* 4533; —39° 5622; 6.4

A.R. 12<sup>h</sup> 29<sup>m</sup> 19<sup>s</sup>; Decl. —39° 11'

20.256	73.9	39.90	11.9	2	370
20.338	74.0	39.69	11.8	2	370
20.30	74.0	39.80	(6.2 ... 12.6)		N

*h* 4532; —32° 3272; 8.8

A.R. 12<sup>h</sup> 29<sup>m</sup> 21<sup>s</sup>; Decl. —32° 25'

19.576	266.6	4.99	15.7	2	370
19.587	268.2	4.75	15.2	2	370
19.590	266.9	5.02	15.4	2	370
19.58	267.2	4.92	(9.1 ... 9.8)		N

*h* 4535; —66° 1861; 6.7

A.R. 12<sup>h</sup> 31<sup>m</sup> 28<sup>s</sup>; Decl. —66° 30'

18.465	338.6	17.40	15.2	2½	370
18.471	338.1	17.08	15.8	2	370
18.479	338.9	17.24	16.1	2	370
18.47	338.5	17.24	(7.2 ... 11.8)		N

*h* 4537; —30° 3525; 9.0

A.R. 12<sup>h</sup> 32<sup>m</sup> 41<sup>s</sup>; Decl. —30° 6'

19.587	353.3	11.24	15.3	1½	370
19.590	352.8	10.99	15.5	2	370
19.598	352.9	11.01	16.0	2	370
19.59	353.0	11.08	(9.0 ... 10.0)		N

ε 63; —36° 5591; 8.9

A.R. 12<sup>h</sup> 32<sup>m</sup> 57<sup>s</sup>; Decl. —36° 35'

20.234	311.7	0.42	12.2	3½	650
20.636	287.7	0.3±	16.5	2½	650
21.053	312.1	0.42	11.6	4½	475
20.64	311.9	0.42	(9.2 ... 9.6)		

*h* 4539; γ Centauri; 3.6

A.R. 12<sup>h</sup> 34<sup>m</sup> 38<sup>s</sup>; Decl. —48° 16'

18.301	164.4	1.05	13.8	2½	475
18.432	343.4	0.85	12.8	2½	650
18.481	165.6	0.96	13.7	3	650
19.268	341.8	0.69	12.3	3	1125
19.325	341.0	0.84	12.1	4	1125
19.333	162.7	0.75	12.4	2½	475
20.081	340.8	0.79	11.8	3	650
20.147	342.3	0.87	12.5	3	650
20.149	341.1	0.86	11.7	3	650
20.158	341.6	0.87	11.8	2½	475
20.188	340.9	0.90	12.4	3½	475
21.053	158.5	0.79	11.3	4	475
21.387	160.1	0.80	14.5	3	370
21.389	159.0	0.79	13.6	3	370
18.40	344.5	0.95			
19.31	341.8	0.76			
20.14	341.3	0.86			
21.28	339.2	0.79	(3.1 ... 3.2)		B

*h* 4538; —82° 536; 8.5

A.R. 12<sup>h</sup> 35<sup>m</sup> 2<sup>s</sup>; Decl. —82° 58'

19.289	279.0	4.46	11.9	2	370
19.328	279.5	4.53	13.0	1½	370
19.429	279.0	4.30	14.3	2½	370
19.35	279.2	4.43	(9.5 ... 10.3)		F

*h* 4541; —62° 2892; 9.0

A.R. 12<sup>h</sup> 35<sup>m</sup> 6<sup>s</sup>; Decl. —62° 17'

18.427	142.0	11.24	15.3	2	370
18.462	142.8	11.33	15.4	1½	370
18.44	142.4	11.28	(8.5 ... 12.8)		N

*h* 4540; —72° 1292; 8.2

A.R. 12<sup>h</sup> 35<sup>m</sup> 15<sup>s</sup>; Decl. —72° 6'

18.482	168.0	11.78	16.0	2	370
18.503	167.6	11.45	16.1	2	370
18.509	169.4	11.75	13.5	1½	370
18.50	168.3	11.66	(9.0 ... 9.3)		F

*h* 4544; —78° 774; 8.7

A.R. 12<sup>h</sup> 36<sup>m</sup> 55<sup>s</sup>; Decl. —78° 47'

19.287	300.8	3.04	12.5	2	370
19.328	299.2	3.44	12.8	1½	370
19.429	298.2	3.22	14.0	2	370
19.35	299.4	3.23	(8.8 ... 13.4)		N

*h* 4545; —74° 969; 7.7

A.R. 12<sup>h</sup> 37<sup>m</sup> 39<sup>s</sup>; Decl. —74° 30'

18.635	191.3	9.16	17.2	2	370
18.640	192.3	9.08	16.7	2	370
18.654	192.4	9.16	17.4	2	370
18.64	192.0	9.13	(8.8 ... 9.0)		F

\* Rus 207;  $\beta$  Muscae; 4.1A.R. 12<sup>h</sup> 38<sup>m</sup> 38<sup>s</sup>; Decl. -67° 25'

19.268	352.3	1.29	12.4	2½	650
20.081	355.1	1.27	12.1	3	650
20.147	355.4	1.40	12.7	3	650
20.158	351.8	1.46	11.2	2½	475
19.91	353.7	1.36	(4.0 ... 4.7)		P

*h* 4550; -66° 1944; 8.1 :A.R. 12<sup>h</sup> 40<sup>m</sup> 39<sup>s</sup>; Decl. -66° 27'

18.462	98.2	13.63	15.6	1½	370
18.465	97.9	13.50	15.3	2½	370
18.46	98.0	13.56	(8.5 ... 9.1)		A

I 909; -41° 6109; 8.2

A.R. 12<sup>h</sup> 43<sup>m</sup> 37<sup>s</sup>; Decl. -41° 14'

20.133	271.1	0.35	11.6	3	650
20.177	269.0	0.47	11.8	3	475
20.223	271.7	0.47	12.1	3	475
20.18	270.6	0.43	(9.2 ... 9.6)		P

*h* 4554; -30° 3554; 8.3A.R. 12<sup>h</sup> 45<sup>m</sup> 0<sup>s</sup>; Decl. -30° 24'

19.503	25.1	31.69	16.3	2	370
19.587	25.3	31.88	15.5	1½	370
19.54	25.2	31.78	(7.5R ... 11.8)		N

Cogshall; -38° 5335; 7.6

A.R. 12<sup>h</sup> 46<sup>m</sup> 20<sup>s</sup>; Decl. -38° 43'

20.133	162.0	3.49	11.8	3	370
20.149	163.7	3.34	12.2	3½	370
20.177	168.1	3.46	12.0	2½	370
20.223	166.0	3.66	12.3	2½	370
20.17	165.0	3.49	(7.5 ... 13.5)		23

AC =  $\lambda$  165

20.149	234.8	20.65	12.3	3	370
20.223	231.7	20.62	12.4	2½	370
20.19	233.3	20.64	(7.5 ... 14.0)		

*h* 4559; -36° 5733; 9.2A.R. 12<sup>h</sup> 49<sup>m</sup> 31<sup>s</sup>; Decl. -36° 42'

20.136	154.2	15.44	14.2	2	370
20.160	153.6	14.87	12.3	2	370
20.177	153.6	15.40	12.1	2½	370
20.16	153.8	15.24	(9.7 ... 11.9)		N

*h* 4561; -77° 885; 10.0A.R. 12<sup>h</sup> 50<sup>m</sup> 54<sup>s</sup>; Decl. -77° 12'

18.635	51.0	27.60	17.4	2	370
18.640	51.3	27.71	16.8	2	370
18.64	51.2	27.66	(11.3 ... 11.3)		9

*h* 4560; -38° 5366; 7.3A.R. 12<sup>h</sup> 51<sup>m</sup> 6<sup>s</sup>; Decl. -38° 14'

20.133	251.7	29.77	11.9	2½	370
20.160	252.1	29.88	12.1	1½	370
20.15	251.9	29.82	(7.0 ... 12.3)		N

*h* 4563 = Rus 210; -32° 3342; 7.1A.R. 12<sup>h</sup> 54<sup>m</sup> 12<sup>s</sup>; Decl. -32° 57'

19.503	237.0	6.56	16.4	2	370
19.587	236.9	6.63	15.6	1½	370
19.590	236.8	6.57	15.7	2	370
19.56	236.9	6.59	(7.0Y ... 8.5c)		F

 $\delta$  64; -58° 4660; 8.5A.R. 12<sup>h</sup> 55<sup>m</sup> 45<sup>s</sup>; Decl. -58° 56'

21.023	176.8	3.90	10.4	2	370
21.031	175.8	4.06	10.7	2	370
21.03	176.3	3.98	(9.2 ... 9.3)		

 $\lambda$  168; -38° 5399; 7.7A.R. 12<sup>h</sup> 56<sup>m</sup> 39<sup>s</sup>; Decl. -38° 18'

20.133 Redonda; &lt;0"2 3 650

*h* 4565; -82° 561; 8.6A.R. 12<sup>h</sup> 56<sup>m</sup> 36<sup>s</sup>; Decl. -82° 3'

19.289	73.2	35.35	12.2	2	370
19.429	72.7	35.26	14.4	2	370
19.36	73.0	35.30	(8.4 ... 10.5)		N

*h* 4566; -77° 887; 6.9A.R. 12<sup>h</sup> 58<sup>m</sup> 20<sup>s</sup>; Decl. -77° 47'

18.635	229.3	30.38	17.6	2	370
18.640	229.0	—	17.0	1½	370
18.654	229.5	30.76	17.6	1½	370
18.64	229.3	30.57	(6.6 ... 14.3)		N

 $\Delta$  129 = Rü 16;  $\theta$  Muscae; 6.1A.R. 13<sup>h</sup> 0<sup>m</sup> 5<sup>s</sup>; Decl. -64° 38'

18.318	186.4	5.38	16.6	2½	370
18.320	186.4	5.39	16.2	2½	370
18.32	186.4	5.38	(6.0 ... 8.0)		F

*h* 4570; -36° 5807 + 6; 9.6 + 10.0A.R. 13<sup>h</sup> 0<sup>m</sup> 46<sup>s</sup>; Decl. -36° 30'

20.223	233.3	18.58	12.6	2½	370
20.231	233.4	18.43	11.4	2½	370
20.23	233.4	18.50	(9.7 ... 9.9)		F?

$\lambda$  170;  $-59^\circ 4815$ ; 5.1

A.R.  $13^h 4^m 30^s$ ; Decl.  $-59^\circ 15'$

20.149	Redonda:	$<0''.25$	3	650
20.188	Redonda:	$<0.15$	$3\frac{1}{2}$	650

AB,C = I 424

20.149	349.9	1.85	11.3	3	475
20.188	349.3	1.83	11.3	$3\frac{1}{2}$	650
20.242	349.2	1.67	12.9	$2\frac{1}{2}$	370
20.19	349.5	1.78	(6.7 ... 9.3)		

$h$  4571;  $-34^\circ 5553 + 2$ ;  $7.8 + 9.8$

A.R.  $13^h 4^m 32^s$ ; Decl.  $-34^\circ 28'$

20.223	267.2	23.47	12.7	3	370
20.231	267.0	23.63	11.6	$2\frac{1}{2}$	370
20.23	267.1	23.55	(7.1 ... 9.2)		F

$h$  4572;  $-31^\circ 3552 + 1$ ;  $9.0 + 9.4$

A.R.  $13^h 4^m 46^s$ ; Decl.  $-31^\circ 36'$

19.503	303.7	26.33	16.5	2	370
19.516	303.3	26.30	16.8	3	370
19.51	303.5	26.31	(9.3 ... 9.9)		N

$h$  4574;  $-31^\circ 3560$ ; 8.4

A.R.  $13^h 7^m 10^s$ ; Decl.  $-31^\circ 35'$

19.503	161.3	22.59	16.6	2	370
19.516	161.0	22.67	16.9	$2\frac{1}{2}$	370
19.51	161.1	22.63	(8.7 ... 12.8)		N

$h$  4577;  $-59^\circ 4873$ ; 8.8:

A.R.  $13^h 8^m 49^s$ ; Decl.  $-59^\circ 10'$

17.584	46.1	7.83	17.3	2	370
17.633	46.1	7.43	18.0	$1\frac{1}{2}$	370
18.340	46.9	7.71	15.7	$2\frac{1}{2}$	370
18.342	46.8	7.80	14.9	$2\frac{1}{2}$	370
17.97	46.5	7.71	(9.4 ... 10.2)		F?

AC

17.584	233.1	12.50	17.2	2	370
17.633	231.7	12.54	17.9	$1\frac{1}{2}$	370
18.340	233.5	12.33	15.6	2	370
18.342	232.2	12.34	14.8	$2\frac{1}{2}$	370
17.97	232.6	12.43	(9.4 ... 9.8)		F?

Có —;  $-60^\circ 4569$ ; 8.5

A.R.  $13^h 9^m 27^s$ ; Decl.  $-60^\circ 25'$

18.383	257.3	5.09	16.0	$1\frac{1}{2}$	370
18.402	256.2	5.36	15.9	$2\frac{1}{2}$	370
18.39	256.7	5.23	(8.9 ... 10.1)		7

$h$  4578;  $-36^\circ 5861$ ; 7.8

A.R.  $13^h 10^m 35^s$ ; Decl.  $-36^\circ 21'$

20.223	150.9	8.37	12.9	3	370
20.231	150.6	8.43	11.7	$2\frac{1}{2}$	370
20.234	151.0	8.42	12.4	3	370
20.23	150.8	8.41	(7.6 ... 10.6)		R?

$h$  4579;  $-63^\circ 2711$ ; 8.2

A.R.  $13^h 13^m 12^s$ ; Decl.  $-63^\circ 23'$

18.318	99.0	4.57	16.7	$2\frac{1}{2}$	370
18.320	99.5	4.42	16.3	$2\frac{1}{2}$	370
18.342	98.9	4.68	15.5	$2\frac{1}{2}$	370
18.402	98.5	4.67	16.1	$2\frac{1}{2}$	370
18.35	99.0	4.59	(8.6 ... 9.4)		F

$h$  4583;  $-63^\circ 2743$ ; 6.1

A.R.  $13^h 16^m 53^s$ ; Decl.  $-63^\circ 50'$

18.318	208.4	27.04	16.9	$2\frac{1}{2}$	370
18.320	209.3	27.18	16.4	2	370
18.402	208.5	27.07	16.3	$2\frac{1}{2}$	370
18.35	208.7	27.10	(6.0 ... 11.7)		R?

$h$  4582;  $-73^\circ 1143$ ; 7.6

A.R.  $13^h 17^m 1^s$ ; Decl.  $-73^\circ 32'$

18.482	25.4	—	16.2	2	370
18.503	25.7	14.18	16.3	2	370
18.509	24.9	13.95	13.7	$1\frac{1}{2}$	370
18.50	25.3	14.07	(8.4 ... 10.4)		N

$h$  4581;  $-79^\circ 731$ ; 9.4

A.R.  $13^h 17^m 7^s$ ; Decl.  $-79^\circ 7'$

19.287	279.3	10.73	12.8	2	370
19.289	279.6	10.73	13.2	$1\frac{1}{2}$	370
19.29	279.4	10.73	(10.4 ... 11.6)		N

$h$  4586;  $-67^\circ 2286$ ; 7.4

A.R.  $13^h 19^m 36^s$ ; Decl.  $-67^\circ 13'$

18.462	145.5	3.17	15.9	2	370
18.465	145.0	3.06	15.4	3	370
18.471	146.5	3.11	16.0	2	370
18.47	145.7	3.11	(8.2 ... 9.8)		M?

$h$  4584; Anon.

A.R.  $13^h 19^m 7^s$ ; Decl.  $-83^\circ 44'$

19.429	271.3	16.08	14.6	2	370
19.462	271.0	16.18	14.2	$2\frac{1}{2}$	370
19.45	271.1	16.13	(10.8 ... 11.0)		N

$h$  4588;  $-39^{\circ} 59' 84''$ ; 7.3A.R.  $13^h 20^m 1^s$ ; Decl.  $-39^{\circ} 31'$ 

20.223	137.8	45.51	13.1	$2\frac{1}{2}$	370
20.231	137.7	45.35	11.9	2	370
20.23	137.8	45.43	(7.1 ... 12.0)		N

 $h$  4585;  $-83^{\circ} 53' 0'' + 1$ ;  $9.4 + 9.4$ A.R.  $13^h 20^m 38^s$ ; Decl.  $-83^{\circ} 48'$ 

19.429	120.1	15.20	15.0	2	370
19.462	119.5	15.50	14.5	2	370
19.467	119.6	15.29	15.3	2	370
19.45	119.7	15.33	(9.8 ... 10.0)		N

 $h$  4590;  $-76^{\circ} 7' 67'' + 9$ ;  $7.2 + 9.1$ A.R.  $13^h 22^m 27^s$ ; Decl.  $-76^{\circ} 55'$ 

18.635	134.0	22.57	17.9	2	370
18.640	133.5	22.68	17.9	2	370
18.64	133.7	22.62	(6.6 ... 10.2)		F

 $h$  4592;  $-60^{\circ} 47' 34''$ ; 8.1A.R.  $13^h 22^m 56^s$ ; Decl.  $-60^{\circ} 5'$ 

17.512	225.9	17.40	16.7	2	370
18.340	224.9	16.98	15.9	2	370
18.427	224.5	17.22	15.6	2	370
18.09	225.1	17.20	(8.1 ... 13.4)		N

 $h$  4591;  $-60^{\circ} 47' 35''$ ; 9.0A.R.  $13^h 23^m 0^s$ ; Decl.  $-60^{\circ} 17'$ 

17.515	230.5	7.45	16.5	2	370
18.340	230.8	7.31	16.0	2	370
18.342	231.4	6.94	15.2	2	370
18.348	229.6	7.51	14.4	$1\frac{1}{2}$	370
18.14	230.6	7.30	(9.8 ... 9.8)		N

 $\Delta$  137 = Rü 17;  $-62^{\circ} 33' 26''$ ; 7.7A.R.  $13^h 23^m 39^s$ ; Decl.  $-62^{\circ} 24'$ 

18.340	357.4	15.97	16.2	2	370
18.342	358.1	16.12	15.3	$2\frac{1}{2}$	370
18.403	357.7	16.12	16.4	$2\frac{1}{2}$	370
18.36	357.7	16.07	(7.9 ... 9.1)		F

 $\lambda$  179;  $d$  Centauri; 6.2A.R.  $13^h 23^m 49^s$ ; Decl.  $-38^{\circ} 46'$ 

20.133	264.7	$0.15\pm$	12.4	3	650
20.234	260.2	$0.15\pm$	12.5	3	650
20.18	262.4	$0.15\pm$	(5.6 ... 5.7)		

 $h$  4595;  $-35^{\circ} 58' 42''$ ; 8.2A.R.  $13^h 28^m 4^s$ ; Decl.  $-35^{\circ} 0'$ 

20.136	99.7	8.92	14.4	$2\frac{1}{2}$	370
20.158	98.7	9.00	12.0	2	370
20.160	99.6	8.94	12.5	$2\frac{1}{2}$	370
20.15	99.3	8.95	(8.8 ... 9.0)		N

 $h$  4596 = Rus 222;  $-64^{\circ} 24' 87''$ ; 7.6A.R.  $13^h 28^m 42^s$ ; Decl.  $-64^{\circ} 18'$ 

18.318	283.6	1.54	17.1	3	370
18.320	281.6	1.66	16.5	$2\frac{1}{2}$	370
18.403	282.0	1.49	16.5	$2\frac{1}{2}$	370
18.35	282.4	1.56	(8.8 ... 9.2)		72

 $h$  4594;  $-79^{\circ} 7' 40''$ ; 9.0A.R.  $13^h 28^m 44^s$ ; Decl.  $-79^{\circ} 56'$ 

19.287	99.8	5.68	13.0	$2\frac{1}{2}$	370
19.289	99.2	5.61	13.4	$1\frac{1}{2}$	370
19.462	98.6	5.73	14.7	3	370
19.35	99.2	5.67	(9.9 ... 10.0)		F

I 365;  $-61^{\circ} 38' 41''$ ; 7.1A.R.  $13^h 28^m 45^s$ ; Decl.  $-61^{\circ} 3'$ 

19.325	134.4	0.35	13.6	3	1125
20.149	132.6	0.35	12.0	$3\frac{1}{2}$	650
20.188	128.5	0.35	11.7	$3\frac{1}{2}$	650
19.89	131.8	0.35	(7.3 ... 7.6)		B

 $h$  4597;  $-29^{\circ} 37' 88''$ ; 10.4A.R.  $13^h 28^m 53^s$ ; Decl.  $-29^{\circ} 59'$ 

19.503	197.0	6.69	16.7	2	370
19.517	197.9	6.96	17.1	$2\frac{1}{2}$	370
19.547	198.8	6.97	16.9	2	370
19.52	197.9	6.87	(9.8 ... 13.0)		N

 $h$  4598;  $-74^{\circ} 10' 81''$ ; 7.4A.R.  $13^h 31^m 5^s$ ; Decl.  $-74^{\circ} 28'$ 

18.635	45.5	13.03	18.2	2	370
18.640	45.2	13.27	18.0	2	370
18.654	45.9	13.06	17.7	$1\frac{1}{2}$	370
18.64	45.5	13.12	(7.0 ... 11.7)		F

 $h$  4601;  $-39^{\circ} 60' 32''$ ; 9.2A.R.  $13^h 31^m 50^s$ ; Decl.  $-39^{\circ} 2'$ 

20.133	284.4	11.41	12.5	$3\frac{1}{2}$	370
20.147	284.5	11.36	13.0	3	370
20.14	284.4	11.39	(9.9 ... 10.1)		F?

*h* 4608;  $-33^{\circ} 3465$ ; 6.8  
 A.R.  $13^{\text{h}} 35^{\text{m}} 10^{\text{s}}$ ; Decl.  $-33^{\circ} 21'$

19.503	179.8	4.50	16.8	2	370
19.517	179.6	4.40	17.3	3	370
19.547	179.9	4.48	17.0	$2\frac{1}{2}$	370
19.52	179.8	4.46	(7.7 ... 7.8)		M <sup>2</sup>

$\Delta$  140 = *h* 4607;  $-71^{\circ} 1507$ ; 8.7:  
 A.R.  $13^{\text{h}} 35^{\text{m}} 50^{\text{s}}$ ; Decl.  $-71^{\circ} 21'$

18.503	74.9	10.95	16.8	$2\frac{1}{2}$	370
18.509	75.9	10.99	14.0	2	370
18.51	75.4	10.97	(9.0 ... 10.0)		F

$\lambda$  187;  $-36^{\circ} 6101$ ; 9.0  
 A.R.  $13^{\text{h}} 36^{\text{m}} 0^{\text{s}}$ ; Decl.  $-36^{\circ} 47'$   
 La identificación de See es errónea.

*h* 4609;  $-37^{\circ} 5778$ ; 8.7  
 A.R.  $13^{\text{h}} 36^{\text{m}} 13^{\text{s}}$ ; Decl.  $-37^{\circ} 2'$

20.136	150.2	5.79	14.5	$2\frac{1}{2}$	370
20.160	149.7	5.92	12.7	$2\frac{1}{2}$	370
20.177	150.2	5.79	12.3	$2\frac{1}{2}$	370
20.16	150.0	5.83	(9.4 ... 10.5)		F

$\eta$  4611;  $-38^{\circ} 5587$ ; 10.2  
 A.R.  $13^{\text{h}} 38^{\text{m}} 29^{\text{s}}$ ; Decl.  $-38^{\circ} 47'$

20.240	294.0	10.34	13.3	$2\frac{1}{2}$	370
20.242	293.6	10.11	13.2	$2\frac{1}{2}$	370
20.24	293.8	10.22	(10.9 ... 11.2)		N

*h* 4612;  $\alpha$  Centauri; 6.2  
 A.R.  $13^{\text{h}} 39^{\text{m}} 39^{\text{s}}$ ; Decl.  $-35^{\circ} 38'$

20.160	341.7	26.47	12.9	2	370
20.177	342.2	26.28	12.5	$2\frac{1}{2}$	370
20.231	342.1	26.42	12.7	2	370
20.19	342.0	26.39	(5.7 ... 13.2)		120

*h* 4610;  $-79^{\circ} 744$ ; 7.7  
 A.R.  $13^{\text{h}} 40^{\text{m}} 3^{\text{s}}$ ; Decl.  $-79^{\circ} 39'$

19.287	309.2	16.24	13.2	2	370
19.289	311.5	16.68	13.6	$1\frac{1}{2}$	370
19.462	308.7	16.66	14.8	$2\frac{1}{2}$	370
19.35	309.8	16.53	(7.8 ... 13.2)		N

I 1110;  $-57^{\circ} 6313$ ; 9.2  
 A.R.  $13^{\text{h}} 41^{\text{m}} 30^{\text{s}}$ ; Decl.  $-57^{\circ} 26'$

20.242	338.2	6.42	13.6	$2\frac{1}{2}$	370
20.245	337.0	6.54	13.1	3	370
20.24	337.6	6.48	(9.1R ... 13.9)		142

(Sigue Continued.)

AC = *h* 4615; C =  $-57^{\circ} 6314$ ; 9.8

20.242	149.0	15.00	13.5	$2\frac{1}{2}$	370
20.245	148.8	15.01	13.0	3	370
20.24	148.9	15.01	(9.1R ... 9.9Y)		142

$\Delta$  146;  $-39^{\circ} 6085 + 6$ ; 7.3 + 8.2  
 A.R.  $13^{\text{h}} 41^{\text{m}} 51^{\text{s}}$ ; Decl.  $-39^{\circ} 54'$

20.147	86.2	60.09	13.2	$2\frac{1}{2}$	370
20.223	86.2	59.92	13.2	2	370
20.18	86.2	60.01	(7.0 ... 7.3R)		D

*h* 4616;  $-70^{\circ} 1685$ ; 9.0  
 A.R.  $13^{\text{h}} 42^{\text{m}} 37^{\text{s}}$ ; Decl.  $-70^{\circ} 33'$

18.550	348.7	4.57	14.3	$2\frac{1}{2}$	370
18.618	350.2	4.42	16.4	2	370
18.624	349.3	4.46	16.2	$2\frac{1}{2}$	370
18.60	349.4	4.48	(9.6 ... 11.3)		N

*h* 4618;  $-38^{\circ} 5613$ ; 9.6  
 A.R.  $13^{\text{h}} 43^{\text{m}} 53^{\text{s}}$ ; Decl.  $-38^{\circ} 51'$

20.133	25.1	17.66	13.0	$2\frac{1}{2}$	370
20.147	26.0	17.53	13.3	$2\frac{1}{2}$	370
20.223	25.2	17.60	13.4	2	370
20.17	25.4	17.60	(9.2 ... 12.1)		R

Hh 426 =  $\Delta$  148;  $\kappa$  Centauri; 4.1  
 A.R.  $13^{\text{h}} 44^{\text{m}} 37^{\text{s}}$ ; Decl.  $-32^{\circ} 22'$

19.503	109.0	7.95	16.9	2	370
19.517	109.1	8.10	17.4	3	370
19.547	109.1	7.86	17.1	2	370
19.52	109.1	7.97	(4.7 ... 6.3)		C

$\beta$  343;  $-30^{\circ} 3752$ ; 6.8  
 A.R.  $13^{\text{h}} 44^{\text{m}} 51^{\text{s}}$ ; Decl.  $-30^{\circ} 60'$

20.658	105.4	1.13	17.1	$2\frac{1}{2}$	370
21.381	101.2	1.26	15.7	$2\frac{1}{2}$	370
21.384	102.9	1.23	15.5	3	370
21.14	103.2	1.21	(6.7 ... 7.9)		P

$\Delta$  145;  $-66^{\circ} 2370 + 1$ ; 8.4 + 8.8  
 A.R.  $13^{\text{h}} 45^{\text{m}} 16^{\text{s}}$ ; Decl.  $-66^{\circ} 17'$

18.318	49.4	24.10	17.6	$2\frac{1}{2}$	370
18.403	49.5	24.05	16.8	$2\frac{1}{2}$	370
18.36	49.4	24.08	(8.6 ... 9.3)		F

Hh 428 = Piazz;  $\eta$  Centauri; 4.5  
 A.R.  $13^{\text{h}} 46^{\text{m}} 2^{\text{s}}$ ; Decl.  $-31^{\circ} 18'$

19.503	185.9	15.19	17.0	2	370
19.517	186.1	14.95	17.5	3	370
19.547	186.1	15.10	17.2	2	370
19.52	186.0	15.08	(5.2 ... 8.7)		C

$h\ 4623; -38^\circ\ 56'32; 8.4$ A.R.  $13^h\ 46^m\ 2^s$ ; Decl.  $-38^\circ\ 45'$ 

20.231	321.0	15.19	12.1	2	370
20.234	319.4	15.17	12.7	$2\frac{1}{2}$	370
20.23	320.2	15.18	(9.0 ... 14.4)		N

 $h\ 4622; -65^\circ\ 25'22; 9.1$ A.R.  $13^h\ 46^m\ 4^s$ ; Decl.  $-65^\circ\ 32'$ 

18.318	261.7	5.07	17.7	$2\frac{1}{2}$	370
18.320	261.0	5.07	16.7	$2\frac{1}{2}$	370
18.403	261.5	5.17	16.9	$2\frac{1}{2}$	370
18.35	261.4	5.10	(9.7 ... 10.8)		N

 $h\ 4621; -73^\circ\ 12'20 + 17; 9.0 + 9.6$ A.R.  $13^h\ 46^m\ 9^s$ ; Decl.  $-73^\circ\ 12'$ 

18.550	310.9	16.47	14.6	$2\frac{1}{2}$	370
18.618	311.3	17.58	16.7	2	370
18.58	311.1	16.52	(9.5 ... 9.9)		N

Howe 25;  $\gamma$  Centauri; 6.6A.R.  $13^h\ 46^m\ 15^s$ ; Decl.  $-35^\circ\ 3'$ 

20.158	98.4	1.00	12.2	$2\frac{1}{2}$	475
20.160	100.3	1.05	13.1	$2\frac{1}{2}$	370
20.177	99.3	1.02	12.6	$2\frac{1}{2}$	370
20.17	99.3	1.02	(7.0 ... 7.2)		M

AC =  $\beta$  1108

20.177	161.6	27.68	12.8	$2\frac{1}{2}$	370
20.234	161.3	27.56	12.8	$2\frac{1}{2}$	370
20.21	161.4	27.62	(7.0 ... 13.1)		F

I 401;  $-41^\circ\ 65'24; 7.8$ A.R.  $13^h\ 47^m\ 28^s$ ; Decl.  $-41^\circ\ 58'$ 

20.231	36.4	0.31	12.5	$2\frac{1}{2}$	650
20.234	31.0	0.25	13.1	3	650
20.23	33.7	0.28	(9.5 ... 9.7)		P

AB, C =  $h\ 4625$ 

20.133	7.6	13.70	12.8	3	370
20.231	7.5	13.71	12.3	$2\frac{1}{2}$	370
20.18	7.6	13.70	((9.0) ... 9.4)		F

 $h\ 4626; -69^\circ\ 19'62; 8.4$ A.R.  $13^h\ 47^m\ 47^s$ ; Decl.  $-69^\circ\ 42'$ 

18.463	58.5	4.24	17.2	2	370
18.465	58.0	4.34	15.6	3	370
18.479	59.1	4.38	16.3	2	370
18.47	58.5	4.32	(9.6 ... 9.8)		F?

 $h\ 4627; -71^\circ\ 15'38; 9.3$ A.R.  $13^h\ 47^m\ 58^s$ ; Decl.  $-71^\circ\ 22'$ 

18.550	275.7	10.92	14.4	$2\frac{1}{2}$	370
18.618	276.0	10.63	16.5	2	370
18.624	275.6	10.79	16.3	$2\frac{1}{2}$	370
18.60	275.8	10.78	(9.5 ... 11.8)		N

\*  $\Delta\ 151 = h\ 4634; -55^\circ\ 57'93 + 4; 8.2 + 8.8$ A.R.  $13^h\ 49^m\ 0^s$ ; Decl.  $-55^\circ\ 26'$ 

20.442	37.5	18.25	15.6	2	370
20.644	37.7	18.21	17.0	$2\frac{1}{2}$	370
20.647	37.8	18.33	16.8	$2\frac{1}{2}$	370
20.58	37.7	18.26	(8.1 ... 9.2)		205

 $h\ 4630; -65^\circ\ 25'51; 8.1$ A.R.  $13^h\ 49^m\ 2^s$ ; Decl.  $-65^\circ\ 2'$ 

18.318	311.1	4.23	17.9	$2\frac{1}{2}$	370
18.320	312.4	4.23	16.9	$2\frac{1}{2}$	370
18.403	311.9	4.34	17.1	$2\frac{1}{2}$	370
18.35	311.8	4.27	(8.8 ... 9.0)		F

 $h\ 4632; -65^\circ\ 25'53; 8.0$ A.R.  $13^h\ 49^m\ 14^s$ ; Decl.  $-65^\circ\ 11'$ 

18.318	12.0	6.57	18.0	2	370
18.320	12.9	6.26	17.0	$2\frac{1}{2}$	370
18.403	13.8	6.44	17.2	2	370
18.427	14.8	6.44	15.7	$2\frac{1}{2}$	370
18.37	13.4	6.43	(7.2 ... 11.2)		F?

 $h\ 4631; -69^\circ\ 19'70; 9.3$ A.R.  $13^h\ 49^m\ 25^s$ ; Decl.  $-69^\circ\ 47'$ 

18.463	266.5	11.86	17.3	2	370
18.465	265.9	11.72	15.7	$2\frac{1}{2}$	370
18.46	266.2	11.79	(10.8 ... 11.0)		F?

 $h\ 4629; -77^\circ\ 9'27; 8.3$ A.R.  $13^h\ 49^m\ 57^s$ ; Decl.  $-77^\circ\ 48'$ 

18.635	357.5	4.94	18.4	2	270
18.637	357.3	4.94	18.4	2	370
18.640	357.8	4.95	18.1	2	370
18.64	357.5	4.94	(9.6 ... 9.9)		F

 $h\ 4636; -39^\circ\ 61'31; 9.0$ A.R.  $13^h\ 50^m\ 14^s$ ; Decl.  $-39^\circ\ 22'$ 

20.133	34.1	3.96	13.1	$2\frac{1}{2}$	370
20.231	32.6	4.09	13.4	$2\frac{1}{2}$	370
20.240	33.9	3.70	13.5	$2\frac{1}{2}$	370
20.20	33.5	3.92	(9.7 ... 10.3)		206

$h$  4635;  $-78^{\circ} 838$ ; 9.3

A.R.  $13^h 50^m 55^s$ ; Decl.  $-78^{\circ} 4'$

18.635	248.3	11.83	18.6	2	370
18.637	248.6	12.00	18.5	2	370
19.287	248.2	11.79	13.7	2	370
19.290	248.2	11.64	13.7	$1\frac{1}{2}$	370
18.96	248.3	11.82	(9.8 ... 11.0)		F

Aguilar;  $-60^{\circ} 5147$ ; 8.8

A.R.  $13^h 52^m 56^s$ ; Decl.  $-60^{\circ} 42'$

18.481	267.0	3.50	14.8	2	370
18.503	267.7	3.69	15.9	2	370
18.509	265.2	3.60	14.2	2	370
18.50	266.6	3.60	(9.2 ... 11.7)		7

$\beta$  1197;  $-31^{\circ} 3731$ ; 7.4

A.R.  $13^h 55^m 47^s$ ; Decl.  $-31^{\circ} 5'$

20.658	205.5	1.88	17.3	$2\frac{1}{2}$	370
21.381	205.5	1.99	15.9	3	370
21.384	205.4	1.98	15.7	3	370
21.14	205.5	1.95	(6.9 ... 8.5)		P

$h$  4643;  $-36^{\circ} 6258$ ; 7.6

A.R.  $13^h 56^m 40^s$ ; Decl.  $-36^{\circ} 40'$

20.160	134.0	22.42	13.4	2	370
20.177	133.6	22.19	13.1	2	370
20.231	133.9	22.04	13.0	$2\frac{1}{2}$	370
20.19	133.8	22.22	(7.3 ... 12.4)		42

$h$  4641;  $-67^{\circ} 2493$ ; 8.8

A.R.  $13^h 57^m 49^s$ ; Decl.  $-67^{\circ} 49'$

18.463	64.6	9.95	17.5	2	370
18.465	64.5	9.91	15.8	$2\frac{1}{2}$	370
18.46	64.5	9.93	(9.8 ... 10.4)		N

$h$  4642;  $-62^{\circ} 3920$ ; 8.0

A.R.  $13^h 57^m 52^s$ ; Decl.  $-62^{\circ} 51'$

18.427	12.1	9.17	15.8	2	370
18.465	12.9	9.08	16.4	2	370
18.481	12.0	9.14	14.6	2	370
18.46	12.3	9.13	(7.6 ... 12.4)		N

AC; C =  $-62^{\circ} 3919$ ; 9.4

18.427	334.5	26.28	16.0	2	370
18.465	334.6	26.54	16.5	2	370
18.45	334.6	26.41	(7.6 ... 10.0)		N

AD

18.427	104.0	21.01	15.9	2	370
18.481	103.5	20.66	14.7	2	370
18.46	103.8	20.84	(7.6 ... 13.3)		

$\Delta$  154;  $-35^{\circ} 6098 + 9$ ; 8.2 + 9.5

A.R.  $13^h 58^m 4^s$ ; Decl.  $-35^{\circ} 57'$

20.231	129.9	20.66	13.2	$2\frac{1}{2}$	370
20.234	130.1	20.69	13.3	3	370
20.23	130.0	20.68	(8.6 ... 9.9)		F

\* Sellors 19;  $-49^{\circ} 6679$ ; 7.3

A.R.  $13^h 59^m 37^s$ ; Decl.  $-49^{\circ} 16'$

20.644	267.0	1.20	17.1	3	370
20.647	267.9	1.16	17.0	$2\frac{1}{2}$	370
20.65	267.4	1.18	(7.4 ... 7.8)		B

$h$  4654;  $-66^{\circ} 2463$ ; 8.2

A.R.  $14^h 0^m 50^s$ ; Decl.  $-66^{\circ} 0'$

18.465	12.7	8.22	16.0	3	370
18.471	12.3	8.08	16.2	$1\frac{1}{2}$	370
18.479	12.6	8.12	16.5	2	370
18.47	12.5	8.14	(8.7 ... 10.6)		F?

$h$  4648;  $-76^{\circ} 808$ ; 9.4

A.R.  $14^h 1^m 21^s$ ; Decl.  $-76^{\circ} 45'$

18.635	205.9	10.72	18.8	2	370
18.637	205.6	11.06	18.1	$1\frac{1}{2}$	370
18.640	207.0	11.07	18.2	2	370
18.64	206.2	10.95	(10.6 ... 11.4)		F?

$h$  4644;  $-82^{\circ} 596$ ; 10.0

A.R.  $14^h 1^m 39^s$ ; Decl.  $-82^{\circ} 56'$

19.290	68.1	10.31	14.1	$1\frac{1}{2}$	370
19.429	67.1	10.44	15.3	2	370
19.36	67.6	10.38	(11.0 ... 11.5)		N

$h$  4652 =  $h$  4657;  $-75^{\circ} 941$ ; 7.9

A.R.  $14^h 2^m 25^s$ ; Decl.  $-75^{\circ} 10'$

18.635	67.8	21.10	19.0	2	370
18.637	67.3	21.06	18.8	$1\frac{1}{2}$	370
18.64	67.6	21.08	(7.6 ... 12.1)		N

$h$  4655;  $-36^{\circ} 6313$ ; 8.2

A.R.  $14^h 2^m 34^s$ ; Decl.  $-36^{\circ} 24'$

20.160	268.4	5.80	13.5	2	370
20.177	269.1	5.69	13.3	2	370
20.204	268.5	5.73	13.7	$2\frac{1}{2}$	370
20.18	268.7	5.74	(8.4 ... 10.1)		F

*h* 4658; Anon.A.R. 14<sup>h</sup> 4<sup>m</sup> 44<sup>s</sup>; Decl. -69° 9'

18.465	257.8	6.37	16.1	2½	370
18.479	257.7	6.17	16.7	2	370
18.481	257.0	6.77	15.0	2	370
18.618	256.9	5.80	16.8	2	370
18.51	257.4	6.28	(12.4 ... 12.9)		N

*h* 4662; -32° 3584; 9.4A.R. 14<sup>h</sup> 5<sup>m</sup> 3<sup>s</sup>; Decl. -32° 20'

19.503	93.2	11.79	17.1	2	370
19.517	92.8	11.62	17.6	3	370
19.51	93.0	11.70	(9.8 ... 10.4)		N

*h* 4660; Anon.A.R. 14<sup>h</sup> 6<sup>m</sup> 5<sup>s</sup>; Decl. -72° 50'

18.550	288.1	5.67	14.8	2½	370
18.618	287.8	5.49	18.2	1½	370
18.624	287.2	5.80	16.4	2½	370
18.60	287.7	5.65	(11.4 ... 11.5)		228

*h* 4663; -38° 5760; 10.2A.R. 14<sup>h</sup> 6<sup>m</sup> 54<sup>s</sup>; Decl. -38° 35'

20.133	116.6	20.63	13.3	2½	370
20.188	166.6	20.58	13.3	3	370
20.204	116.5	20.72	13.8	2½	370
20.231	116.4	20.78	13.6	2½	370
20.19	116.5	20.68	(10.5 ... 10.9)		N

*h* 4668; -33° 3600; 9.2A.R. 14<sup>h</sup> 10<sup>m</sup> 34<sup>s</sup>; Decl. -33° 16'

19.503	280.0	8.99	17.3	2	370
19.517	279.3	8.73	17.8	3	370
19.547	279.5	8.65	17.4	2	370
19.52	279.6	8.79	(9.4 ... 10.9)		N

*h* 4667; -72° 1519; 7.5A.R. 14<sup>h</sup> 11<sup>m</sup> 3<sup>s</sup>; Decl. -72° 59'

18.482	140.6	2.14	16.4	2	370
18.550	140.2	2.49	15.0	2½	370
18.618	141.3	2.32	18.3	2	370
18.624	140.3	2.30	16.5	3	475
18.57	140.6	2.31	(8.3 ... 8.9)		M?

## β 1110; -36° 6384; 8.1

A.R. 14<sup>h</sup> 12<sup>m</sup> 11<sup>s</sup>; Decl. -36° 17'

20.204	130.4	4.04	13.9	2½	370
20.234	133.8	4.10	13.8	3	370
20.240	131.5	4.21	13.6	2½	370
20.23	131.9	4.12	(7.20 ... 11.7)		F

*h* 4671 = Rus 243; -79° 760; 7.7A.R. 14<sup>h</sup> 14<sup>m</sup> 7<sup>s</sup>; Decl. -79° 32'

19.268	127.6	5.06	13.0	2½	370
19.287	126.8	5.12	13.9	2	370
19.290	127.9	5.01	13.9	2	370
19.28	127.4	5.06	(8.3 ... 9.2)		20

*h* 4680; -75° 971; 8.9A.R. 14<sup>h</sup> 21<sup>m</sup> 54<sup>s</sup>; Decl. -75° 4'

18.635	11.4	8.05	19.3	2½	370
18.637	11.0	8.32	18.9	1½	370
18.640	12.1	8.31	18.4	1½	370
18.64	11.5	8.23	(9.4 ... 11.3)		N

*h* 4682; -41° 6797; 8.0A.R. 14<sup>h</sup> 21<sup>m</sup> 59<sup>s</sup>; Decl. -41° 57'

20.232	348.1	9.14	13.9	2½	370
20.234	346.8	9.32	13.9	3	370
20.240	347.0	8.77	13.8	3	370
20.24	347.3	9.08	(8.1 ... 12.4)		N

*h* 4683; -62° 4186; 8.5 :A.R. 14<sup>h</sup> 24<sup>m</sup> 49<sup>s</sup>; Decl. -62° 43'

18.427	62.6	13.34	16.2	2½	370
18.463	63.4	13.29	18.0	2	370
18.44	63.0	13.32	(8.8 ... 8.9)		20

*h* 4684; -64° 2923; 8.9A.R. 14<sup>h</sup> 25<sup>m</sup> 21<sup>s</sup>; Decl. -64° 20'

18.427	267.0	12.27	16.3	2	370
18.465	267.8	12.59	16.7	2	370
18.479	267.8	12.15	17.0	2	370
18.46	267.5	12.34	(8.6 ... 13.2)		N

## β 1112; -30° 3860; 7.6

A.R. 14<sup>h</sup> 25<sup>m</sup> 46<sup>s</sup>; Decl. -30° 10'

21.381	8.3	2.65	16.1	2½	370
21.384	8.7	2.67	15.8	3	370
21.387	7.0	2.62	15.4	3	370
21.38	8.0	2.65	(6.10 ... 11.6)		F

*h* 4686; -36° 6470; 9.1A.R. 14<sup>h</sup> 26<sup>m</sup> 39<sup>s</sup>; Decl. -36° 28'

20.150	86.2	13.46	13.8	3	370
20.160	86.3	13.18	13.8	2	370
20.204	86.2	13.44	14.0	2½	370
20.17	86.2	13.36	(10.2 ... 10.9)		9



*h* 4687;  $-36^{\circ} 6477$ ; 8.2

A.R.  $14^{\text{h}} 27^{\text{m}} 59^{\text{s}}$ ; Decl.  $-36^{\circ} 0'$

20.150	95.0	1.70	13.8	3	475
20.160	95.3	1.64	13.9	2	370
20.204	94.6	1.80	14.1	$2\frac{1}{2}$	650
20.17	95.0	1.71	(8.8 ... 9.0)		M

*h* 2731;  $-32^{\circ} 3676$ ; 9.0

A.R.  $14^{\text{h}} 28^{\text{m}} 10^{\text{s}}$ ; Decl.  $-32^{\circ} 34'$

19.517	108.6	12.29	18.0	$2\frac{1}{2}$	370
19.547	108.5	12.71	17.5	2	370
19.549	109.3	12.06	17.8	$1\frac{1}{2}$	370
19.54	108.8	12.35	(9.0 ... 12.6)		N

*h* 4688;  $-63^{\circ} 3343$ ; 8.9

A.R.  $14^{\text{h}} 29^{\text{m}} 11^{\text{s}}$ ; Decl.  $-63^{\circ} 44'$

18.427	67.2	4.50	16.4	2	370
18.463	67.7	4.62	18.2	2	370
18.465	68.1	4.53	16.8	2	370
18.45	67.7	4.55	(9.8 ... 10.6)		N

\*  $\alpha$  Centauri

A.R.  $14^{\text{h}} 30^{\text{m}} 59^{\text{s}}$ ; Decl.  $-60^{\circ} 19'$

18.301	221.2	15.48	14.3	$2\frac{1}{2}$	370
18.482	221.8	15.49	16.7	2	475
19.268	221.9	14.59	12.6	$2\frac{1}{2}$	650
19.484	222.0	14.65	16.2	$2\frac{1}{2}$	650
20.147	222.8	14.16	12.3	$2\frac{1}{2}$	370
20.150	223.0	14.22	15.5	$2\frac{1}{2}$	370
20.204	223.1	14.46	13.3	2	370
20.278	223.2	14.26	14.0	$2\frac{1}{2}$	370
21.384	225.1	13.26	16.6	$2\frac{1}{2}$	370
21.387	224.2	13.35	15.0	3	370
18.391	221.5	15.48			
19.376	222.0	14.62			
20.195	223.0	14.27			
21.386	224.6	13.31	(0.4 ... 1.3)		B

*h* 4689;  $-78^{\circ} 888 + 9$ ; 9.1 + 9.6

A.R.  $14^{\text{h}} 31^{\text{m}} 19^{\text{s}}$ ; Decl.  $-78^{\circ} 15'$

19.462	49.8	20.62	15.0	$2\frac{1}{2}$	370
19.467	49.3	20.35	15.4	2	370
19.484	50.1	20.76	16.4	$2\frac{1}{2}$	370
19.47	49.7	20.58	(9.3 ... 10.3)		N

$\Delta$  166;  $\alpha$  Circini; 3.7

A.R.  $14^{\text{h}} 32^{\text{m}} 26^{\text{s}}$ ; Decl.  $-64^{\circ} 26'$

18.427	235.0	15.94	16.6	$2\frac{1}{2}$	370
18.463	235.7	15.84	17.8	2	370
18.44	235.3	15.89	(3.8 ... 7.5)		A

*h* 2736;  $-31^{\circ} 3854 + 5$ ; 8.6 + 9.3

A.R.  $14^{\text{h}} 33^{\text{m}} 22^{\text{s}}$ ; Decl.  $-31^{\circ} 47'$

19.517	79.8	19.12	18.1	$2\frac{1}{2}$	370
19.547	79.7	19.22	17.6	$1\frac{1}{2}$	370
19.53	79.8	19.17	(8.1 ... 9.4)		N

$\beta$  414;  $-30^{\circ} 3883$ ; 7.0

A.R.  $14^{\text{h}} 34^{\text{m}} 24^{\text{s}}$ ; Decl.  $-30^{\circ} 24'$

21.381	346.6	1.05	16.3	3	370
21.384	346.1	1.05	16.0	3	370
21.387	347.4	1.01	15.6	$2\frac{1}{2}$	370
21.38	346.7	1.04	(7.1 ... 7.9)		F

*h* 4693;  $-72^{\circ} 1572 + 1$ ; 9.8 + 9.3

A.R.  $14^{\text{h}} 34^{\text{m}} 49^{\text{s}}$ ; Decl.  $-72^{\circ} 57'$

18.550	232.6	15.62	15.3	$2\frac{1}{2}$	370
18.618	232.6	15.39	18.4	2	370
18.56	232.6	15.51	(10.2 ... 10.6)		R?

*h* 2742;  $-31^{\circ} 3868$ ; 9.0

A.R.  $14^{\text{h}} 38^{\text{m}} 15^{\text{s}}$ ; Decl.  $-31^{\circ} 17'$

19.547	211.2	17.80	17.7	2	370
19.549	211.0	18.12	17.9	$1\frac{1}{2}$	370
19.55	211.1	17.96	(9.0 ... 11.0)		N

*h* 4695;  $-74^{\circ} 1246$ ; 6.8

A.R.  $14^{\text{h}} 38^{\text{m}} 24^{\text{s}}$ ; Decl.  $-74^{\circ} 25'$

18.635	290.5	—	19.5	2	370
18.637	289.4	17.89	19.0	$1\frac{1}{2}$	370
18.640	290.1	—	18.5	$1\frac{1}{2}$	370
18.654	291.0	17.82	18.2	$1\frac{1}{2}$	370
18.64	290.3	17.86	(6.7 ... 12.5)		N

*h* 4697;  $-70^{\circ} 1823 + 4$ ; 8.7 8.9

A.R.  $14^{\text{h}} 39^{\text{m}} 2^{\text{s}}$ ; Decl.  $-70^{\circ} 1'$

18.550	140.7	15.43	15.5	$2\frac{1}{2}$	370
18.618	140.8	15.43	18.5	2	370
18.58	140.7	15.43	(8.6 ... 9.6)		F?

G 210;  $-72^{\circ} 1594$ ; 9.2

A.R.  $14^{\text{h}} 39^{\text{m}} 15^{\text{s}}$ ; Decl.  $-72^{\circ} 56'$

21.315	96.2	9.47	13.8	$1\frac{1}{2}$	370
21.384	96.1	9.51	17.0	$2\frac{1}{2}$	370
21.35	96.1	9.49	(9.8 ... 10.6)		N

*h* 2744;  $-32^{\circ} 3720$ ; 9.4

A.R.  $14^{\text{h}} 40^{\text{m}} 18^{\text{s}}$ ; Decl.  $-32^{\circ} 53'$

19.547	60.5	13.03	17.9	2	370
19.549	60.6	12.93	18.0	$1\frac{1}{2}$	370
19.55	60.5	12.98	(9.2 ... 9.3)		N

$h 4701; -36^\circ 6561; 9.6$ A.R.  $14^h 40^m 26^s$ ; Decl.  $-36^\circ 16'$ 

20.150	82.9	10.73	13.9	3	370
20.204	83.5	10.80	14.3	3	370
20.18	83.2	10.76	(9.8 ... 10.5)		D?

 $h 4702; -35^\circ 6371; 7.7$ A.R.  $14^h 40^m 50^s$ ; Decl.  $-35^\circ 19'$ 

20.150	214.2	9.81	14.0	$3\frac{1}{2}$	370
20.204	214.8	9.74	14.4	3	370
20.232	215.3	9.80	14.4	$2\frac{1}{2}$	370
20.20	214.8	9.78	(7.2Y ... 9.7)		F

 $h 4704; -62^\circ 4315; 8.6$ A.R.  $14^h 42^m 26^s$ ; Decl.  $-62^\circ 11'$ 

18.427	283.7	5.31	16.7	2	370
18.465	283.6	5.44	17.0	$2\frac{1}{2}$	370
18.471	285.2	5.24	16.5	$1\frac{1}{2}$	370
18.45	284.2	5.33	(9.3 ... 10.5)		N

 $I 951; -39^\circ 6452; 8.8$ A.R.  $14^h 42^m 37^s$ ; Decl.  $-39^\circ 52'$ 

20.234	267.7	1.41	14.2	3	650
20.240	265.7	1.42	14.1	$3\frac{1}{2}$	370
20.242	266.9	1.37	13.9	3	730
20.24	266.8	1.40	(8.8 ... 9.6)		D?

 $h 4707; -65^\circ 2914; 7.9$ A.R.  $14^h 43^m 38^s$ ; Decl.  $-65^\circ 54'$ 

18.427	81.4	0.89	16.9	2	475
18.465	80.5	--	17.3	2	475
18.482	78.8	0.80	15.3	$2\frac{1}{2}$	475
18.624	79.5	0.76	17.8	3	475
18.50	80.0	0.82	(8.7 ... 8.9)		P

 $h 4703; -78^\circ 934; 8.7$ A.R.  $14^h 44^m 7^s$ ; Decl.  $-78^\circ 0'$ 

18.638	239.8	16.55	19.2	$1\frac{1}{2}$	370
18.654	239.7	16.89	18.4	2	370
18.714	239.6	16.88	18.7	1	370
18.67	239.7	16.77	(8.6 ... 12.5)		N

 $Hh 454 = h 2748; -30^\circ 3914 + 13; 8.2 + 9.0$ A.R.  $14^h 44^m 11^s$ ; Decl.  $-30^\circ 22'$ 

19.503	179.8	24.23	17.6	2	370
19.547	179.7	24.36	18.0	2	370
19.52	179.8	24.29	(8.5 ... 9.3)		D?

 $h 4711; -34^\circ 6229; 9.4$ A.R.  $14^h 44^m 30^s$ ; Decl.  $-34^\circ 30'$ 

20.232	331.9	13.57	14.6	$2\frac{1}{2}$	370
20.234	331.7	13.71	14.3	3	370
20.23	331.8	13.64	(9.2 ... 11.9)		N

 $h 4710; -41^\circ 6944; 9.0$ A.R.  $14^h 44^m 34^s$ ; Decl.  $-41^\circ 34'$ 

20.232	259.1	16.37	14.2	$2\frac{1}{2}$	370
20.234	258.9	16.45	14.1	3	370
20.23	259.0	16.41	(8.8 ... 9.5)		207

 $\Delta 173; -37^\circ 6282; 5.1$ A.R.  $14^h 45^m 0^s$ ; Decl.  $-37^\circ 17'$ 

20.150	Redonda	3	650
20.240	No es doble	$3\frac{1}{2}$	650

 $\beta 347; -32^\circ 3747; 7.7$ A.R.  $14^h 47^m 0^s$ ; Decl.  $-32^\circ 47'$ 

20.658	319.2	13.57	17.5	2	370
21.381	318.7	13.36	16.5	$2\frac{1}{2}$	370
21.384	318.9	13.47	16.1	$2\frac{1}{2}$	370
21.14	318.9	13.47	(6.40 ... 11.5)		F

 $h 4714; -63^\circ 3459 + 60; 8.0 + 8.4$ A.R.  $14^h 47^m 51^s$ ; Decl.  $-63^\circ 3'$ 

18.427	145.6	22.69	17.1	$2\frac{1}{2}$	370
18.465	145.3	22.75	17.2	3	370
18.45	145.4	22.72	(8.1 ... 8.7)		F

 $I 227 = \lambda 215; -34^\circ 6261; 7.5$ A.R.  $14^h 48^m 50^s$ ; Decl.  $-34^\circ 7'$ 

20.150	115.8	0.20	14.2	$3\frac{1}{2}$	650
20.204	104.9	0.25	14.5	3	650
20.234	119.8	0.30	14.4	3	650
20.20	113.5	0.25	(8.1 ... 8.2)		P

 $h 4717; -38^\circ 5998; 9.9$ A.R.  $14^h 49^m 26^s$ ; Decl.  $-38^\circ 48'$ 

20.240	218.5	18.25	14.6	$3\frac{1}{2}$	370
20.243	218.3	18.22	14.1	3	370
20.24	218.4	18.24	(9.5 ... 10.6)		N

 $h 4718; -34^\circ 6273; 8.2$ A.R.  $14^h 49^m 49^s$ ; Decl.  $-34^\circ 53'$ 

20.150	63.1	2.03	14.3	$3\frac{1}{2}$	650
20.204	62.6	2.07	14.6	$3\frac{1}{4}$	650
20.234	63.6	1.97	14.5	3	650
20.20	63.1	2.02	(7.50 ... 9.0c)		F

*h* 4721; —35° 6444; 9.6

A.R. 14<sup>h</sup> 51<sup>m</sup> 46<sup>s</sup>; Decl. —35° 51'

20.150	253.4	4.64	14.4	3½	370
20.232	250.2	4.93	14.7	2½	370
20.234	252.5	4.78	14.6	3	370
20.21	252.0	4.78	(10.4 ... 10.9)		N

*h* 4722; —30° 3939; 7.1

A.R. 14<sup>h</sup> 51<sup>m</sup> 57<sup>s</sup>; Decl. —30° 12'

19.503	339.2	8.61	17.7	2	370
19.547	339.0	8.60	18.1	2	370
19.549	338.9	8.62	18.2	2	370
19.53	339.0	8.61	(7.5 ... 9.6)		F

*h* 4724; —36° 6691; 7.9

A.R. 14<sup>h</sup> 53<sup>m</sup> 58<sup>s</sup>; Decl. —36° 26'

20.150	226.6	15.51	14.6	2½	370
20.234	226.2	15.39	14.7	3	370
20.19	226.4	15.45	(8.0 ... 10.5)		N

*λ* 218; —35° 6479; 7.4

A.R. 14<sup>h</sup> 55<sup>m</sup> 46<sup>s</sup>; Decl. —35° 27'

20.150	Redonda			3½	650
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\* *h* 4728;  $\pi$  Lupi; 4.7

A.R. 14<sup>h</sup> 56<sup>m</sup> 37<sup>s</sup>; Decl. —46° 34'

20.644	81.7	1.50	17.2	3	370
20.655	82.9	1.73	18.6	2	370
20.65	82.3	1.61	(4.4 ... 4.5)		B

*h* 4730; —36° 6717; 9.4

A.R. 14<sup>h</sup> 57<sup>m</sup> 16<sup>s</sup>; Decl. —36° 45'

20.232	321.1	21.24	14.8	2½	370
20.234	320.8	21.50	14.9	3	370
20.240	321.3	21.47	14.8	3½	370
20.24	321.1	21.40	(8.8 ... 13.3)		N

*h* 4729; —69° 2246; 8.8

A.R. 14<sup>h</sup> 57<sup>m</sup> 52<sup>s</sup>; Decl. —69° 41'

18.479	326.9	8.24	17.2	2	370
18.482	326.9	8.38	15.5	2½	370
18.624	326.8	8.30	18.0	2½	370
18.53	326.9	8.31	(9.8 ... 10.0)		N

*h* 4733; —39° 6569; 9.3

A.R. 15<sup>h</sup> 0<sup>m</sup> 30<sup>s</sup>; Decl. —39° 18'

20.243	318.1	22.28	14.2	2½	370
20.245	318.2	21.99	14.1	3	370
20.24	318.2	22.13	(9.30 ... 13.1)		N

*h* 4731; —77° 1076; 8.6

A.R. 15<sup>h</sup> 2<sup>m</sup> 14<sup>s</sup>; Decl. —77° 24'

20.245	249.4	3.28	13.5	3	370
20.707	251.1	3.06	19.3	2	370
20.825	251.9	3.31	21.5	2½	370
20.59	250.8	3.22	(9.6 ... 10.6)		142

*h* 4738; —36° 6735; 9.6

A.R. 15<sup>h</sup> 2<sup>m</sup> 24<sup>s</sup>; Decl. —36° 16'

19.601	158.7	16.63	18.1	2	370
19.604	156.1	16.48	16.6	2	370
19.609	157.1	16.49	16.0	2	370
19.60	157.3	16.53	(9.7 ... 11.4)		N

AC

19.601	29.3	15.98	18.2	1½	370
19.604	30.5	15.95	16.7	2½	370
19.609	29.6	16.22	15.9	2	370
19.60	29.8	16.05	(9.7 ... 11.3)		N

*h* 4745<sup>?</sup>; —35° 6512; 8.6

A.R. 15<sup>h</sup> 3<sup>m</sup> 35<sup>s</sup>; Decl. —35° 46'

19.604	19.9	24.76	16.8	2½	370
19.609	20.1	24.98	16.2	2	370
19.61	20.0	24.87	(8.9 ... 10.0)		208

BC

19.604	95.2	15.49	16.9	2½	370
19.609	94.8	15.36	16.3	2	370
19.61	95.0	15.43	(10.0 ... 11.0)		N

*h* 4741; —41° 7070; 10.1

A.R. 15<sup>h</sup> 3<sup>m</sup> 41<sup>s</sup>; Decl. —41° 51'

20.243	128.1	10.57	14.4	2½	370
21.381	128.1	10.73	16.7	3	370
21.384	127.3	10.77	16.3	2½	370
21.00	127.8	10.69	(9.7 ... 13.0)		N

*h* 2765; —31° 3968 + 7; 9.2 + 9.4

A.R. 15<sup>h</sup> 3<sup>m</sup> 53<sup>s</sup>; Decl. —31° 39'

19.547	348.1	29.72	18.3	2	370
19.549	348.2	30.03	18.4	2	370
19.582	348.0	29.99	18.3	2	370
19.56	348.1	29.91	(9.10 ... 9.7)		N

*h* 4743; —32° 3827; 7.6

A.R. 15<sup>h</sup> 4<sup>m</sup> 15<sup>s</sup>; Decl. —32° 21'

19.503	196.4	11.16	17.8	2	370
19.517	196.9	11.23	18.2	2½	370
19.51	196.7	11.20	(8.8 ... 9.1)		F

$\varepsilon$  65;  $-40^\circ 6851$ ; 9.5A.R.  $15^h 4^m 35^s$ ; Decl.  $-40^\circ 37'$ 

20.245	270.6	0.54	14.4	3	650
21.381	275.4	0.46	16.9	3	370
20.81	273.0	0.50	(10.2 ... 10.5)		

 $h$  4737;  $-75^\circ 1134$ ; 8.9A.R.  $15^h 5^m 40^s$ ; Decl.  $-75^\circ 40'$ 

18.638	88.9	8.37	19.4	2	370
18.654	88.0	8.19	18.6	2	370
18.733	89.1	8.33	19.9	2	370
18.68	88.7	8.30	(9.6 ... 10.5)		N

AC;  $C = 11.1$ 

18.733	141.4	33.92	20.0	2	370
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 $h$  4748;  $-40^\circ 6871 + 70$ ; 8.6 + 8.7A.R.  $15^h 5^m 50^s$ ; Decl.  $-40^\circ 59'$ 

20.243	7.5	16.95	14.6	3	370
20.245	7.2	16.92	14.6	3	370
20.24	7.4	16.94	(9.1 ... 9.2)		C

 $h$  4742;  $-75^\circ 1135$ ; 8.0A.R.  $15^h 6^m 0^s$ ; Decl.  $-75^\circ 6'$ 

18.638	199.2	32.23	19.5	2	370
18.733	199.4	31.88	20.2	2	370
18.736	198.9	31.99	19.6	2	370
18.70	199.2	32.03	(7.5 ... 13.5)		N

 $h$  4744;  $-79^\circ 831$ ; 9.4A.R.  $15^h 7^m 56^s$ ; Decl.  $-79^\circ 46'$ 

19.462	54.8	13.12	15.3	2½	370
19.467	53.9	13.24	15.5	2	370
19.46	54.4	13.18	(9.4 ... 10.9)		N

 $h$  4752;  $-34^\circ 6347$ ; 7.9A.R.  $15^h 9^m 21^s$ ; Decl.  $-34^\circ 7'$ 

19.609	6.0	18.19	16.5	1½	370
19.612	5.8	18.19	17.9	2½	370
19.61	5.9	18.19	(7.3 ... 10.4)		N

 $h$  4751;  $-74^\circ 1379$ ; 8.0A.R.  $15^h 9^m 45^s$ ; Decl.  $-74^\circ 45'$ 

18.638	120.7	5.08	19.7	2	370
18.733	120.4	4.94	20.4	1½	370
18.736	120.8	5.01	19.8	2½	370
18.70	120.6	5.01	(8.9 ... 9.2)		F

\*  $h$  4753;  $\mu_1$  Lupi; 5.1A.R.  $15^h 9^m 51^s$ ; Decl.  $-47^\circ 25'$ 

20.644	151.1	1.61	18.4	3	370
20.655	151.3	1.77	18.8	2	370
20.65	151.2	1.69	(5.8 ... 5.9)		P

 $h$  4755;  $-36^\circ 6773$ ; 8.0A.R.  $15^h 11^m 24^s$ ; Decl.  $-36^\circ 14'$ 

19.601	202.2	4.41	18.4	1½	370
19.609	202.8	4.53	16.6	1½	370
19.612	202.2	4.48	18.0	2½	370
19.61	202.4	4.47	(8.2 ... 9.4)		F

 $\Delta$  181;  $-37^\circ 6456 + 5$ ; 8.7 + 9.8A.R.  $15^h 12^m 11^s$ ; Decl.  $-37^\circ 55'$ 

19.612	349.6	29.53	18.2	2	370
19.620	349.4	29.54	18.4	2	370
19.62	349.5	29.54	(8.8 ... 9.3)		N

BC

19.612	328.4	21.48	18.4	2	370
19.620	328.7	21.60	18.5	2	370
19.62	328.6	21.54	(9.3 ... 10.0)		N

CD

19.612	92.2	8.23	18.6	2	370
19.620	91.0	8.52	18.6	2	370
19.62	91.6	8.38	(10.0 ... 11.7)		N

\* Sellors 20 = I 38;  $-47^\circ 7081$ ; 7.8A.R.  $15^h 13^m 58^s$ ; Decl.  $-47^\circ 28'$ 

20.644	199.0	0.86	17.5	3	370
20.653	199.0	0.94	18.3	2½	370
20.655	204.8	0.94	18.9	2	370
20.65	200.9	0.91	(8.8 ... 9.1)		P

\* Copeland 2 = Gale 3;  $\varepsilon$  Lupi; 4.2A.R.  $15^h 14^m 12^s$ ; Decl.  $-44^\circ 14'$ 

20.653	278.4	1.11	18.5	2½	370
20.655	274.7	1.23	19.1	2	370
20.65	276.6	1.17	(4.2 ... 5.7)		P

 $h$  4761;  $-64^\circ 3173 + 4$ ; 8.8 + 8.9A.R.  $15^h 15^m 10^s$ ; Decl.  $-64^\circ 54'$ 

18.318	0.7	12.25	18.2	2	370
18.427	1.8	12.16	17.5	2	370
18.37	1.3	12.20	(8.9 ... 9.0)		F

*h* 4765;  $-32^{\circ} 3888$ ; 9.6

A.R.  $15^{\text{h}} 16^{\text{m}} 22^{\text{s}}$ ; Decl.  $-32^{\circ} 36'$

19.503	98.0	10.22	17.9	2	370
19.582	97.8	10.16	18.7	2	370
19.585	97.7	9.93	17.2	2	370
19.56	97.8	10.10	(9.7R ... 10.4)		209

*h* 4760;  $-77^{\circ} 1123 + 4$ ; 8.5 + 8.9

A.R.  $15^{\text{h}} 16^{\text{m}} 28^{\text{s}}$ ; Decl.  $-77^{\circ} 5'$

18.638	15.3	19.06	19.8	2	370
18.733	15.8	19.11	20.5	$1\frac{1}{2}$	370
18.69	15.5	19.08	(8.6 ... 9.0)		F

*h* 4759 = *h* 4762;  $-79^{\circ} 844 + 5$ ; 8.7 + 9.5

A.R.  $15^{\text{h}} 16^{\text{m}} 58^{\text{s}}$ ; Decl.  $-79^{\circ} 46'$

19.462	61.8	21.43	15.8	$2\frac{1}{2}$	370
19.467	61.6	21.33	15.6	2	370
19.46	61.7	21.38	(8.6 ... 10.2)		A <sup>2</sup>

*h* 4764;  $\alpha_1$  Apodis; 6.0

A.R.  $15^{\text{h}} 17^{\text{m}} 56^{\text{s}}$ ; Decl.  $-72^{\circ} 57'$

18.550	254.6	27.02	15.8	$2\frac{1}{2}$	370
18.618	255.2	27.01	18.7	$1\frac{1}{2}$	370
18.624	254.9	26.90	16.7	3	370
18.60	254.9	26.98	(6.0 ... 12.6)		N

*h* 2778;  $-33^{\circ} 3855$ ; 8.9

A.R.  $15^{\text{h}} 18^{\text{m}} 14^{\text{s}}$ ; Decl.  $-33^{\circ} 18'$

19.585	216.9	27.44	17.4	$1\frac{1}{2}$	370
19.590	216.9	27.54	17.0	$1\frac{1}{2}$	370
19.59	216.9	27.49	(8.6 ... 11.2)		N

$\delta$  66;  $-40^{\circ} 6989$ ; 8.7

A.R.  $15^{\text{h}} 19^{\text{m}} 8^{\text{s}}$ ; Decl.  $-40^{\circ} 50'$

20.240	32.1	1.64	15.0	$3\frac{1}{2}$	370
20.243	33.1	1.55	14.8	3	370
20.245	32.5	1.71	14.7	$3\frac{1}{2}$	370
20.24	32.6	1.63	(8.1 ... 12.7)		

*h* 4770;  $-74^{\circ} 1427$ ; 8.5

A.R.  $15^{\text{h}} 21^{\text{m}} 8^{\text{s}}$ ; Decl.  $-74^{\circ} 28'$

18.550	216.5	8.03	16.1	2	370
18.618	216.7	8.04	18.8	2	370
18.624	215.6	9.06	16.8	$2\frac{1}{2}$	370
18.60	216.3	8.01	(10.2 ... 10.4)		F <sup>2</sup>

*h* 4776;  $-41^{\circ} 7233$ ; 6.7

A.R.  $15^{\text{h}} 22^{\text{m}} 1^{\text{s}}$ ; Decl.  $-41^{\circ} 29'$

20.232	228.7	5.89	15.0	3	370
20.240	228.2	5.88	15.2	4	370
20.243	228.6	5.93	14.9	3	370
20.24	228.5	5.90	(6.8 ... 8.8)		F

*h* 4773;  $-73^{\circ} 1607$ ; 8.4

A.R.  $15^{\text{h}} 22^{\text{m}} 25^{\text{s}}$ ; Decl.  $-73^{\circ} 56'$

18.550	234.0	6.50	16.2	2	370
18.618	233.0	6.35	18.9	2	370
18.624	233.7	6.48	16.9	3	370
18.60	233.6	6.44	(9.1 ... 9.2)		M

*h* 4782;  $-41^{\circ} 7243$ ; 9.3

A.R.  $15^{\text{h}} 24^{\text{m}} 2^{\text{s}}$ ; Decl.  $-41^{\circ} 28'$

20.232	264.2	8.05	15.1	$2\frac{1}{2}$	370
20.240	264.1	8.09	15.3	4	370
20.243	262.9	8.19	15.0	3	370
20.24	263.7	8.11	(10.9 ... 11.1)		N

$\Delta$  188;  $\epsilon$  Trianguli Aus.; 6.2 + 8.9

A.R.  $15^{\text{h}} 25^{\text{m}} 18^{\text{s}}$ ; Decl.  $-65^{\circ} 54'$

18.318	217.9	83.26	18.3	$1\frac{1}{2}$	370
18.427	217.9	83.10	17.7	2	370
18.37	217.9	83.18	(5.0 ... 9.7)		N

\* *h* 4786;  $\gamma$  Lupi; 4.2

A.R.  $15^{\text{h}} 26^{\text{m}} 50^{\text{s}}$ ; Decl.  $40^{\circ} 45'$

19.268	86.0	$0.10 \pm$	13.4	$2\frac{1}{2}$	1125
19.325	78.4	$\leq 0.10$	12.4	4	1125
19.30	82.2	0.08	(3.4 ... 3.6)		B

*h* 4780 = Rus 262;  $-80^{\circ} 779$ ; 9.0

A.R.  $15^{\text{h}} 26^{\text{m}} 53^{\text{s}}$ ; Decl.  $-80^{\circ} 8'$

19.462	270.6	5.17	16.0	2	370
19.467	270.3	5.19	15.8	2	370
19.484	270.7	5.27	16.6	$2\frac{1}{2}$	370
19.48	270.5	5.21	(9.8 ... 10.0)		210

*h* 2787;  $-30^{\circ} 4146$ ; 9.7

A.R.  $15^{\text{h}} 30^{\text{m}} 30^{\text{s}}$ ; Decl.  $-30^{\circ} 34'$

19.585	135.3	14.53	17.9	2	370
19.590	134.3	15.03	17.2	$1\frac{1}{2}$	370
19.593	135.2	14.88	18.9	3	370
19.59	134.9	14.81	(10.0 ... 10.5)		N

$h$  4787;  $-79^\circ 865$ ; 8.4:

A.R.  $15^h 30^m 44^s$ ; Decl.  $-79^\circ 13'$

19.462	303.4	10.14	16.2	$2\frac{1}{2}$	370
19.467	303.5	10.00	15.9	$2\frac{1}{2}$	370
19.46	303.5	10.07	(8.8 ... 9.7)		20

$I$  89;  $-39^\circ 6796$ ; 7.0

A.R.  $15^h 32^m 50^s$ ; Decl.  $-39^\circ 34'$

17.272	152.1	1.23	14.8	3	650
19.547	151.3	1.13	16.6	$2\frac{1}{2}$	650
19.582	156.0	1.46	18.1	2	475
18.80	153.1	1.27	(6.4 ... 7.8)		F

$h$  4792;  $-72^\circ 1668$ ; 8.3

A.R.  $15^h 33^m 36^s$ ; Decl.  $-72^\circ 3'$

18.618	107.6	7.51	19.1	2	370
18.624	106.7	7.73	17.5	3	370
18.626	107.7	7.73	16.9	$1\frac{1}{2}$	370
18.62	107.3	7.66	(8.9 ... 11.0)		F

$h$  2789;  $-30^\circ 4165 + 4$ ; 9.1 + 9.6

A.R.  $15^h 34^m 15^s$ ; Decl.  $-30^\circ 19'$

19.593	309.0	28.77	19.0	$1\frac{1}{2}$	370
19.598	309.1	28.63	16.5	$1\frac{1}{2}$	370
19.60	309.1	28.70	(8.7 ... 10.2)		F

BC

19.598	91.7	8.02	16.6	$1\frac{1}{2}$	370
19.604	92.5	7.89	18.7	$2\frac{1}{2}$	370
19.60	92.1	7.95	(10.2 ... 12.9)		N

$h$  4790;  $-78^\circ 1053$ ; 7.9

A.R.  $15^h 34^m 15^s$ ; Decl.  $-78^\circ 19'$

19.462	348.1	12.61	16.3	2	370
19.467	348.0	12.27	16.1	$2\frac{1}{2}$	370
19.484	348.4	12.60	18.6	$2\frac{1}{2}$	370
19.47	348.2	12.49	(8.5 ... 10.7)		N

Rü 20 = Rus 267;  $-65^\circ 3139$ ; 6.3

A.R.  $15^h 36^m 31^s$ ; Decl.  $-65^\circ 3'$

18.318	151.0	2.11	18.5	$2\frac{1}{2}$	370
18.427	149.6	2.10	17.8	$2\frac{1}{2}$	475
18.471	152.8	2.17	16.7	2	370
18.41	151.1	2.13	(6.9 ... 6.9)		20

$h$  4799;  $-68^\circ 2560$ ; 8.8:

A.R.  $15^h 36^m 36^s$ ; Decl.  $-68^\circ 36'$

18.479	79.6	11.47	17.5	2	370
18.482	80.0	11.53	15.6	$2\frac{1}{2}$	370
18.48	79.8	11.50	(9.0 ... 10.4)		N

$\Delta$  192;  $-35^\circ 6610 + 11$ ; 7.2 + 7.6

A.R.  $15^h 39^m 3^s$ ; Decl.  $-35^\circ 7'$

17.542	143.9	34.84	16.2	$2\frac{1}{2}$	370
19.222	143.4	34.82	17.7	2	370
19.601	143.8	35.03	18.7	$1\frac{1}{2}$	370
19.609	143.6	34.77	16.9	$1\frac{1}{2}$	370
19.612	143.6	34.66	18.9	2	370
19.12	143.7	34.82	(7.0 ... 7.2)		11

$h$  4801;  $-76^\circ 1121$ ; 9.0

A.R.  $15^h 40^m 7^s$ ; Decl.  $-76^\circ 51'$

18.638	160.1	13.11	20.0	2	370
18.711	160.4	13.04	20.5	2	370
18.67	160.2	13.08	(9.2 ... 12.5)		N

$\delta$  67;  $-41^\circ 7350$ ; 9.2

A.R.  $15^h 41^m 4^s$ ; Decl.  $-41^\circ 23'$

20.240	167.2	2.21	15.6	4	370
20.243	165.6	2.04	15.4	$2\frac{1}{2}$	370
20.245	167.0	2.15	15.1	$3\frac{1}{2}$	370
20.24	166.6	2.13	(9.3 ... 12.4)		

$h$  4798;  $-83^\circ 593$ ; 8.2

A.R.  $15^h 41^m 23^s$ ; Decl.  $-83^\circ 52'$

19.462	134.3	20.88	16.6	2	370
19.467	134.1	20.66	16.3	2	370
19.46	134.2	20.77	(8.1 ... 11.2)		182

$h$  4812;  $-37^\circ 6585$ ; 8.8

A.R.  $15^h 43^m 36^s$ ; Decl.  $-37^\circ 44'$

19.609	61.9	10.97	17.9	$2\frac{1}{2}$	370
19.621	62.1	10.88	18.9	2	370
19.61	62.0	10.93	(9.2 ... 9.9)		R

$\delta$  68;  $-40^\circ 7120$ ; 8.6

A.R.  $15^h 43^m 56^s$ ; Decl.  $-40^\circ 13'$

20.204	112.3	0.20±	15.5	3	650
20.234	132.4	0.20±	15.3	3	650
20.240	126.3	0.20±	15.4	4	650
20.23	123.7	0.20	(9.8 ... 10.0)		

$h$  4814;  $-36^\circ 6888$ ; 8.4

A.R.  $15^h 44^m 21^s$ ; Decl.  $-36^\circ 20'$

19.609	326.0	11.65	18.1	$2\frac{1}{2}$	370
19.621	327.1	11.57	19.0	2	370
19.61	326.5	11.61	(8.9 ... 10.5)		N

*h* 4815; —34° 6410; 9.2

A.R. 15<sup>h</sup> 45<sup>m</sup> 12<sup>s</sup>; Decl. —34° 30'

19.609	130.0	14.81	18.2	2	370
19.621	129.5	14.87	19.2	2	370
19.62	129.8	14.84	(8.9 ... 10.9)	22	

*h* 4819; —66° 2859; 8.9

A.R. 15<sup>h</sup> 47<sup>m</sup> 50<sup>s</sup>; Decl. —66° 19'

18.654	345.2	11.95	20.1	2	370
18.689	344.1	12.26	19.4	1½	370
18.711	344.6	11.84	20.3	2	370
18.68	344.6	12.02	(9.0 ... 11.0)	N	

Piazzini = Δ 196; ζ Lupi; 5.8

A.R. 15<sup>h</sup> 48<sup>m</sup> 54<sup>s</sup>; Decl. —33° 36'

19.517	48.2	10.68	18.4	2	370
19.563	48.5	10.36	18.9	2½	370
19.590	48.9	10.63	17.5	1½	370
19.593	49.5	10.55	19.2	2	370
19.55	48.8	10.55	(5.6 ... 6.2)	F	

δ 69; —38° 6305; 8.6

A.R. 15<sup>h</sup> 49<sup>m</sup> 19<sup>s</sup>; Decl. —38° 53'

20.234	40.1	5.91	15.5	3½	370
20.243	39.5	5.87	15.5	3	370
20.245	39.9	5.92	15.3	3	370
20.24	39.8	5.90	(8.7 ... 9.7)		

*h* 4821 = *h* 4820; —31° 4274 + 5; 8.3 + 8.3

A.R. 15<sup>h</sup> 50<sup>m</sup> 1<sup>s</sup>; Decl. —31° 36'

19.517	144.5	19.26	18.7	2	370
19.563	144.5	19.39	19.1	2½	370
19.590	144.8	19.24	17.4	2	370
19.56	144.6	19.30	(8.9 ... 9.0)	211	

*h* 4822; —38° 6311; 9.6

A.R. 15<sup>h</sup> 50<sup>m</sup> 20<sup>s</sup>; Decl. —38° 48'

20.150	92.2	10.15	14.8	2½	370
20.232	92.1	9.77	15.5	2½	370
20.234	90.4	9.93	15.8	3	370
20.21	91.6	9.95	(10.5 ... 10.6)	D?	

Δ 197 = Rü 21; η Lupi; 4.3

A.R. 15<sup>h</sup> 51<sup>m</sup> 51<sup>s</sup>; Decl. —38° 2'

19.609	20.6	15.36	18.4	2	370
19.612	20.7	15.10	19.0	2	370
19.623	20.8	15.12	16.4	2½	370
19.61	20.7	15.19	(3.6 ... 7.4)	F	

*h* 4816; —83° 599; 8.2

A.R. 15<sup>h</sup> 52<sup>m</sup> 9<sup>s</sup>; Decl. —83° 46'

19.462	336.6	22.97	16.8	1½	370
19.467	337.4	23.50	16.4	1½	370
19.484	336.0	23.05	18.9	2½	370
19.47	336.7	23.17	(8.2 ... 10.7)	N	

λ 256 = λ 253; —35° 6642; 8.3

A.R. 15<sup>h</sup> 52<sup>m</sup> 48<sup>s</sup>; Decl. —35° 38'

19.609	128.8	12.14	18.5	2	370
19.623	128.4	12.44	16.5	2½	370
19.62	128.6	12.29	(7.6 ... 11.0)	212	

*h* 4831; —36° 6938; 6.8

A.R. 15<sup>h</sup> 59<sup>m</sup> 3<sup>s</sup>; Decl. —36° 25'

19.610	357.7	40.91	18.7	2	370
19.623	358.1	40.86	16.6	2	370
19.62	357.9	40.88	(5.9 ... 11.8)	N	

δ 70; —53° 7155; 9.3

A.R. 15<sup>h</sup> 59<sup>m</sup> 11<sup>s</sup>; Decl. —53° 35'

19.306	234.5	4.19	13.0	1½	370
19.325	232.4	4.17	14.0	2	475
19.467	233.5	3.92	17.1	1½	370
19.37	233.5	4.09	(9.8 ... 11.1)		

*h* 4832; —33° 3977; 8.0

A.R. 15<sup>h</sup> 59<sup>m</sup> 17<sup>s</sup>; Decl. —33° 22'

19.598	353.6	37.65	17.9	1½	370
19.604	353.8	37.75	18.9	2½	370
19.60	353.7	37.70	(8.0 ... 10.1)	N	

BC

19.598	19.2	23.68	18.0	1½	370
19.604	19.7	23.64	19.0	2	370
19.60	19.5	23.66	(10.1 ... 10.8)	N	

λ 265; —38° 6374; 7.5

A.R. 16<sup>h</sup> 0<sup>m</sup> 12<sup>s</sup>; Decl. —38° 45'

20.245	297.8	16.32	15.6	3	370 F
			(7.0 ... 13.2)		

AC = Δ 199; C = —38° 6373; 7.7

20.150	184.6	44.33	15.0	2	370
20.245	184.6	44.32	15.5	3	370
20.20	184.6	44.32	(7.0 ... 7.2R)	F	

I 557;  $-30^{\circ} 4292$ ; 7.5A.R.  $16^h 1^m 36^s$ ; Decl.  $-30^{\circ} 43'$ 

19.639	208.5	0.64	17.4	$2\frac{1}{2}$	475
19.648	213.5	0.64	18.5	$2\frac{1}{2}$	475
19.705	216.3	0.57	19.3	3	650
19.66	212.8	0.62	(8.0 ... 8.2)		

Bris 5584 + 6;  $\delta$  Apodis; 7.0 + 7.3A.R.  $16^h 1^m 45^s$ ; Decl.  $-78^{\circ} 22'$ 

18.736	12.3	102.88	20.0	2	370
18.747	11.9	102.85	21.5	2	370
18.752	11.7	102.87	21.0	$1\frac{1}{2}$	370
18.74	12.0	102.87	(5.1 ... 5.9)		182

AC; C = 12.5

18.747	73.7	90.49	21.6	$1\frac{1}{2}$	370
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Hd 141 $\beta$ ;  $-31^{\circ} 4328$ ; 8.2A.R.  $16^h 1^m 58^s$ ; Decl.  $-31^{\circ} 16'$ 

19.637	0.1	7.55	17.0	2	370
19.639	0.7	7.66	17.5	2	370
19.64	0.4	7.60	(9.0 ... 9.6)		

 $h$  4830;  $-42^{\circ} 7308$  + 7; 10.0 + 9.8A.R.  $16^h 2^m 10^s$ ; Decl.  $-42^{\circ} 38'$ 

20.234	226.1	25.91	16.0	3	370
20.245	226.2	25.96	15.8	3	370
20.24	226.1	25.94	(9.4 ... 9.5)		F $\beta$

 $h$  4840 =  $h$  4836 = Ho 401;  $-34^{\circ} 6481$ ; 8.0A.R.  $16^h 9^m 19^s$ ; Decl.  $-34^{\circ} 30'$ 

19.610	297.7	4.97	18.8	$2\frac{1}{2}$	370
19.612	297.9	5.14	19.1	$2\frac{1}{2}$	370
19.621	297.6	5.01	19.4	2	370
19.61	297.7	5.04	(8.4 ... 9.1)		F

 $h$  4843 = I 92;  $-33^{\circ} 4024$ ; 7.8A.R.  $16^h 13^m 24^s$ ; Decl.  $-33^{\circ} 0'$ 

19.593	268.1	12.31	19.4	2	370
19.599	268.0	12.52	18.2	$1\frac{1}{2}$	370
19.60	268.1	12.41	(7.5 ... 11.7)		F

 $h$  4847;  $-30^{\circ} 4351$  + 50; 9.1 + 9.7A.R.  $16^h 15^m 1^s$ ; Decl.  $-30^{\circ} 47'$ 

19.593	223.1	15.71	19.7	2	370
19.599	223.2	15.67	18.4	$1\frac{1}{2}$	370
19.60	223.1	15.69	(9.4 ... 9.5)		N

 $h$  4845;  $-40^{\circ} 7267$ ; 7.6A.R.  $16^h 15^m 9^s$ ; Decl.  $-40^{\circ} 57'$ 

20.150	133.6	1.92	15.2	$2\frac{1}{2}$	370
20.240	132.3	1.97	16.2	$3\frac{1}{2}$	370
20.243	132.9	1.97	15.7	3	370
20.21	132.9	1.95	(8.1 ... 8.6)		D $\beta$

 $h$  4848;  $-32^{\circ} 4139$ ; 7.0A.R.  $16^h 15^m 54^s$ ; Decl.  $-32^{\circ} 54'$ 

19.593	153.7	6.41	19.5	2	370
19.599	153.5	6.24	18.3	$1\frac{1}{2}$	370
19.604	154.4	6.29	19.1	$2\frac{1}{2}$	370
19.60	153.9	6.31	(7.1 ... 7.5)		F

\* C6 45;  $-48^{\circ} 8449$ ; 7.6A.R.  $16^h 16^m 1^s$ ; Decl.  $-48^{\circ} 51'$ 

20.644	177.0	1.66	18.7	$2\frac{1}{2}$	370
20.653	176.3	1.64	18.7	$2\frac{1}{2}$	370
20.655	177.6	1.48	19.2	$2\frac{1}{2}$	370
20.65	177.0	1.59	(8.3R ... 8.5R)		B

AC; C = 12.0

20.653	102.1	12.13	18.8	$2\frac{1}{2}$	370 R
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 $\Delta$  201 = Rus 278;  $\delta$  Trianguli Aus.; 6.0A.R.  $16^h 16^m 22^s$ ; Decl.  $-63^{\circ} 46'$ 

18.318	15.9	19.55	18.8	2	370
18.427	15.7	19.74	17.9	2	370
18.471	15.8	19.68	16.9	2	370
18.41	15.8	19.66	(6.0 ... 10.1)		R

 $h$  4852;  $-37^{\circ} 6666$ ; 8.8A.R.  $16^h 16^m 34^s$ ; Decl.  $-37^{\circ} 37'$ 

19.610	142.3	13.51	19.1	3	370
19.612	142.5	13.34	19.2	2	370
19.626	141.8	13.61	18.7	2	370
19.62	142.2	13.49	(9.1 ... 10.5)		213

 $h$  4849;  $-65^{\circ} 3311$ ; 8.0A.R.  $16^h 18^m 2^s$ ; Decl.  $-65^{\circ} 46'$ 

18.318	145.8	15.62	19.0	$2\frac{1}{2}$	370
18.427	145.4	15.64	18.1	2	370
18.37	145.6	15.63	(8.5 ... 10.3)		R $\beta$

 $h$  4855;  $-67^{\circ} 3149$ ; 8.8A.R.  $16^h 22^m 9^s$ ; Decl.  $-67^{\circ} 53'$ 

18.479	298.0	7.12	17.8	2	370
18.624	297.9	7.08	18.4	$2\frac{1}{2}$	370
18.626	298.5	7.07	17.4	$1\frac{1}{2}$	370
18.58	298.1	7.09	(9.5 ... 10.6)		F



*h* 4860;  $-79^{\circ} 903$ ; 8.6

A.R.  $16^{\text{h}} 27^{\text{m}} 39^{\text{s}}$ ; Decl.  $-79^{\circ} 25'$

18.747	235.9	14.65	21.8	2	370
18.752	234.9	14.80	21.2	2	370
18.755	235.6	14.64	21.5	1½	370
18.75	235.5	14.70	(8.9 ... 12.7)		N

Hd 142;  $-31^{\circ} 4426$ ; 8.6 :

A.R.  $16^{\text{h}} 28^{\text{m}} 0^{\text{s}}$ ; Decl.  $-31^{\circ} 20'$

19.640	209.0	14.66	18.9	2	370
19.708	208.7	15.05	19.9	1½	370
19.752	208.7	14.42	19.8	2½	370
19.70	208.8	14.71	(8.9 ... 11.7)		

*h* 4869;  $-30^{\circ} 4418$ ; 9.2

A.R.  $16^{\text{h}} 29^{\text{m}} 42^{\text{s}}$ ; Decl.  $-30^{\circ} 42'$

19.593	219.9	9.15	19.9	2	370
19.604	219.8	9.13	19.3	2½	370
19.610	219.7	9.24	19.9	2	370
19.60	219.8	9.17	(9.6 ... 9.8)		A

*h* 4868 Ver la nota 214

*h* 4870;  $-36^{\circ} 7010$ ; 6.4

A.R.  $16^{\text{h}} 30^{\text{m}} 43^{\text{s}}$ ; Decl.  $-36^{\circ} 58'$

19.612	10.2	31.02	19.4	2	370
19.626	10.1	30.86	18.9	1½	370
19.62	10.2	30.94	(6.2 ... 11.0)		142

Rus 283 = I 98 =  $\lambda$  284;  $-36^{\circ} 7024$ ; 7.3

A.R.  $16^{\text{h}} 34^{\text{m}} 8^{\text{s}}$ ; Decl.  $-36^{\circ} 50'$

19.610	73.0	0.82	19.4	3	1125
19.648	73.0	0.91	18.6	2½	475
19.705	73.6	0.86	19.5	3	650
19.65	73.2	0.86	(7.2 ... 7.9)		20

*h* 4865;  $-83^{\circ} 611$ ; 8.9

A.R.  $16^{\text{h}} 34^{\text{m}} 48^{\text{s}}$ ; Decl.  $-83^{\circ} 47'$

19.467	310.3	4.24	16.6	1½	370
19.484	310.3	4.29	19.1	3	370
19.503	310.7	4.30	18.1	2	370
19.48	310.4	4.28	(9.3 ... 10.0)		N

$\hat{c}$  71;  $-38^{\circ} 6521$ ; 9.3

A.R.  $16^{\text{h}} 36^{\text{m}} 21^{\text{s}}$ ; Decl.  $-38^{\circ} 58'$

20.204	126.4	1.33	15.8	3	370
20.234	126.4	1.22	16.2	3	370
20.243	126.1	1.48	16.0	3	370
20.23	126.3	1.34	(10.3 ... 10.5)		

$\Delta$  209;  $-36^{\circ} 7043 + 4$ ; 7.6 + 8.3

A.R.  $16^{\text{h}} 39^{\text{m}} 50^{\text{s}}$ ; Decl.  $-36^{\circ} 39'$

19.612	143.0	23.24	19.6	2	370
19.642	142.7	23.22	18.5	1½	370
19.63	142.9	23.23	(7.5 ... 8.7)		A?

*h* 4884;  $-82^{\circ} 700 + 1$ ; 7.1 + 8.7

A.R.  $16^{\text{h}} 43^{\text{m}} 51^{\text{s}}$ ; Decl.  $-82^{\circ} 8'$

19.467	8.5	34.93	16.7	1½	370
19.484	8.0	35.05	19.2	2	370
19.503	7.8	35.07	18.2	1½	370
19.48	8.1	35.02	(7.8 ... 9.2)		215

*h* 4892;  $-41^{\circ} 7718$ ; 7.3

A.R.  $16^{\text{h}} 45^{\text{m}} 18^{\text{s}}$ ; Decl.  $-41^{\circ} 35'$

20.234	299.6	8.79	16.4	3	370
20.245	299.7	8.82	16.5	3	370
20.707	300.1	8.81	20.4	1½	370
20.40	299.8	8.81	(7.6 ... 10.1)		F

$Aa = \lambda$  294;  $a = 12.5$

20.245 46.7 6.83 16.6 2½ 370

*h* 4893 =  $\lambda$  301;  $-41^{\circ} 7744$ ; 7.6

A.R.  $16^{\text{h}} 45^{\text{m}} 40^{\text{s}}$ ; Decl.  $-41^{\circ} 37'$

20.245	52.6	7.20	16.7	3	370
20.707	52.4	7.36	20.3	1½	370
20.48	52.5	7.28	(8.0 ... 10.2)		F

*h* 4894; Anon.

A.R.  $16^{\text{h}} 47^{\text{m}} 20^{\text{s}}$ ; Decl.  $-63^{\circ} 0'$

18.427	303.7	6.71	18.5	2	370
18.624	303.2	6.56	18.5	2½	370
18.629	304.1	6.62	17.4	1½	370
18.56	303.7	6.63	(12.4 ... 12.9)		A?

$\lambda =$  Olivier 16;  $-30^{\circ} 4533$ ; 8.2

A.R.  $16^{\text{h}} 50^{\text{m}} 10^{\text{s}}$ ; Decl.  $-30^{\circ} 1'$

19.593	193.3	1.36	20.2	2	370
19.604	192.7	1.45	19.4	2½	475
19.610	192.6	1.33	20.0	2	370
19.60	192.9	1.38	(8.9 ... 9.2)		F

AC = *h* 4903

19.604	91.7	18.47	19.5	2	475
19.610	91.5	18.61	20.1	2	370
19.61	91.6	18.54	(8.9 ... 10.1)		20

$\geq 72; -41^\circ 7818; 8.2$ A.R.  $16^h 53^m 11^s$ ; Decl.  $-41^\circ 1'$ 

20.240	357.2	3.31	16.5	3 $\frac{1}{2}$	370
20.243	357.2	3.31	16.4	3	370
20.24	357.2	3.31	(8.3 ... 11.4)		

 $h 4908; \text{C6D} -39^\circ 11013; 9.0$ A.R.  $16^h 53^m 21^s$ ; Decl.  $-39^\circ 32'$ 

20.240	178.3	4.98	16.6	4	370
20.243	178.4	5.03	16.2	3	370
20.806	179.6	5.08	21.2	2	370
20.814	178.5	5.48	21.7	2 $\frac{1}{2}$	370
20.53	178.7	5.14	(10.0 ... 10.2)		216

 $h 4904; -75^\circ 1348; 8.1$ A.R.  $16^h 53^m 37^s$ ; Decl.  $-75^\circ 12'$ 

18.638	188.3	6.87	20.4	2	370
18.634	188.1	6.91	20.3	2	370
18.711	187.9	6.85	20.6	2	370
18.67	188.1	6.88	(8.2 ... 9.9)		F

 $h 4910; -35^\circ 6833; 9.2$ A.R.  $16^h 54^m 6^s$ ; Decl.  $-35^\circ 52'$ 

19.612	261.3	8.45	19.9	2	370
19.689	261.4	8.64	19.9	2	370
19.691	62.1	8.39	18.8	2 $\frac{1}{2}$	370
19.66	261.6	8.49	(10.0 ... 10.1)		217

 $h 4915; -37^\circ 6909; 8.2$ A.R.  $16^h 56^m 18^s$ ; Decl.  $-37^\circ 42'$ 

19.612	337.5	11.27	19.7	2	370
19.689	337.1	11.45	20.0	2	370
19.65	337.3	11.36	(8.30 ... 11.3)		N

 $h 4914; -72^\circ 2041; 8.4$ A.R.  $16^h 58^m 15^s$ ; Decl.  $-72^\circ 33'$ 

18.618	77.8	3.58	19.3	2 $\frac{1}{2}$	370
18.632	76.6	3.31	21.3	2	370
18.635	75.9	3.46	21.1	3	370
18.63	76.8	3.45	(9.3 ... 9.5)		F

 $\Delta 214; -67^\circ 3397 + 6; 7.8 + 8.7$ A.R.  $17^h 0^m 31^s$ ; Decl.  $-67^\circ 2'$ 

18.624	355.7	30.05	19.2	2	370
18.626	356.1	30.10	17.7	1 $\frac{1}{2}$	370
18.62	355.9	30.07	(6.8 ... 9.2)		R

 $h 4912; -82^\circ 707; 6.2$ A.R.  $17^h 0^m 58^s$ ; Decl.  $-82^\circ 39'$ 

19.467	122.1	25.11	16.8	1 $\frac{1}{2}$	370
19.484	122.1	25.11	19.4	2	370
19.48	122.1	25.11	(6.6 ... 11.4)		N

 $h 4921; -31^\circ 4585; 8.4$ A.R.  $17^h 1^m 20^s$ ; Decl.  $-31^\circ 31'$ 

19.585	145.9	8.72	20.2	2	370
19.604	146.3	8.72	19.9	3	370
19.610	146.8	8.89	20.2	2	370
19.60	146.3	8.78	(8.7 ... 9.2)		218

 $h 4924; -69^\circ 2709; 8.8$ A.R.  $17^h 5^m 10^s$ ; Decl.  $-69^\circ 4'$ 

18.624	92.5	12.65	19.4	2	370
18.629	93.3	12.95	17.1	1 $\frac{1}{2}$	370
18.632	92.0	12.49	21.1	2	370
18.63	92.6	12.70	(9.2 ... 11.4)		N

 $h 4925; \text{Anon.}$ A.R.  $17^h 5^m 10^s$ ; Decl.  $-62^\circ 41'$ 

18.427	311.0	22.84	18.8	2	370
18.624	312.0	23.45	18.8	2 $\frac{1}{2}$	370
18.53	311.5	23.64	(13.3 ... 13.7)		N

 $h 4926; -39^\circ 7296; 7.9$ A.R.  $17^h 5^m 49^s$ ; Decl.  $-39^\circ 37'$ 

20.246	334.2	14.43	16.8	2 $\frac{1}{2}$	370
20.691	335.1	14.58	20.0	2 $\frac{1}{2}$	370
20.47	334.6	14.50	(7.4R ... 10.6)		219

AC

20.246	210.0	17.00	16.9	2 $\frac{1}{2}$	370
20.691	211.2	16.88	20.1	2 $\frac{1}{2}$	370
20.47	210.6	16.94	(7.4R ... 11.6)		

 $h 4928; -38^\circ 6759; 8.8$ A.R.  $17^h 7^m 50^s$ ; Decl.  $-38^\circ 30'$ 

20.691	300.3	13.80	20.2	2 $\frac{1}{2}$	370
20.806	301.9	14.16	21.4	2	370
20.814	300.5	14.15	21.9	2	370
20.77	300.9	14.04	(9.1 ... 9.7)		F?

 $\beta 1119; -30^\circ 4641; 7.9$ A.R.  $17^h 9^m 22^s$ ; Decl.  $-30^\circ 2'$ 

20.653	349.1	0.61	19.8	2 $\frac{1}{2}$	475
21.362	340.4	0.57	15.2	2 $\frac{1}{2}$	475
21.381	351.1	0.56	18.0	3	370
21.13	346.9	0.58	(6.8 ... 7.6)		A

\* Bris 6021 = Rus 297;  $-46^{\circ} 85'13''$ ; 7.3

A.R.  $17^{\text{h}} 9^{\text{m}} 35^{\text{s}}$ ; Decl.  $-46^{\circ} 30'$

20.644	171.5	3.09	18.9	3	370
20.653	172.7	3.10	18.9	2½	370
20.655	172.3	3.16	19.4	2½	370
20.65	172.2	3.12	(6.0Y ... 9.4R)		B

Melb. 4 =  $\beta$  416 = Rus 298;  $-34^{\circ} 68'03''$ ; 7.2

A.R.  $17^{\text{h}} 10^{\text{m}} 30^{\text{s}}$ ; Decl.  $-34^{\circ} 51'$

19.689	228.5	1.69	20.2	2	370
19.691	227.4	1.98	19.2	2½	475
19.700	226.6	2.03	19.7	2	370
19.735	225.6	1.79	19.9	3	650
20.653	222.2	1.85	20.0	2½	475
20.655	221.9	1.85	19.8	2½	370
20.814	220.2	1.92	21.6	2½	370
21.403	216.7	1.78	15.3	3½	370
19.70	227.0	1.87			
20.88	220.2	1.85	(6.6 ... 7.6)		B

AC = h 4935

19.689	133.8	31.30	20.3	2	370
19.691	134.0	31.09	19.1	2½	370
19.69	133.9	31.19	(6.6 ... 10.4)		C

AD =  $\lambda$

19.689	79.7	29.99	20.4	1½	370
19.691	79.5	30.09	19.0	2½	370
19.69	79.6	30.04	(6.6 ... 11.7)		R

h 4933;  $-75^{\circ} 13'77''$ ; 9.3

A.R.  $17^{\text{h}} 12^{\text{m}} 0^{\text{s}}$ ; Decl.  $-75^{\circ} 44'$

18.638	242.8	18.40	20.5	2	370
18.654	243.2	18.31	20.4	2	370
18.65	243.0	18.36	(9.2 ... 11.5)		N

h 4940;  $-31^{\circ} 46'64''$ ; 9.7

A.R.  $17^{\text{h}} 12^{\text{m}} 44^{\text{s}}$ ; Decl.  $-31^{\circ} 41'$

19.585	86.9	6.22	20.3	2	370
19.604	86.3	6.34	20.0	2½	370
19.610	86.2	6.53	20.4	2	370
19.60	86.5	6.36	(10.3 ... 10.3)		N

Hd 145;  $-31^{\circ} 46'81''$ ; 8.6

A.R.  $17^{\text{h}} 14^{\text{m}} 17^{\text{s}}$ ; Decl.  $-31^{\circ} 0'$

19.760	136.8	6.04	20.7	1½	370
19.763	134.4	6.14	21.5	1½	370
19.76	135.6	6.09	(9.1 ... 11.4)		

h 4937;  $-78^{\circ} 11'33''$ ; 8.0

A.R.  $17^{\text{h}} 14^{\text{m}} 35^{\text{s}}$ ; Decl.  $-78^{\circ} 2'$

18.747	227.0	34.50	22.0	2	370
18.752	226.7	34.35	21.4	1½	370
18.75	226.9	34.43	(8.2 ... 13.1)		N

AC; C = 14.8

18.752	189.1	32.09	21.5	1½	370
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$\delta$  73;  $-33^{\circ} 43'73''$ ; 9.1

A.R.  $17^{\text{h}} 14^{\text{m}} 52^{\text{s}}$ ; Decl.  $-33^{\circ} 60'$

20.480	43.3	1.14	17.0	2½	370
20.633	43.3	1.15	18.2	3	370
20.691	43.1	1.21	20.3	2½	370
20.60	43.2	1.17	(9.3 ... 11.3)		

h 4943;  $-66^{\circ} 31'14''$ ; 8.8

A.R.  $17^{\text{h}} 16^{\text{m}} 12^{\text{s}}$ ; Decl.  $-66^{\circ} 2'$

20.699	242.2	3.82	20.5	2	370
20.702	242.1	4.10	20.6	1½	370
20.710	241.6	4.04	21.4	2½	370
20.70	242.0	3.99	(9.3 ... 10.2)		N

h 4946; Cód  $-34^{\circ} 11'671''$ ; 9.5

A.R.  $17^{\text{h}} 16^{\text{m}} 27^{\text{s}}$ ; Decl.  $-34^{\circ} 4'$

19.610	111.3	16.49	10.6	2	370
19.612	111.3	16.31	20.1	2	370
19.689	111.3	16.44	20.5	2	370
19.64	111.3	16.41	(10.1 ... 11.4)		N

BC

19.610	321.8	5.5	20.7	1½	370
19.612	320.8	5.0	20.2	2	370
19.689	321.6	6.1	20.6	2	370
19.64	321.4	5.5	(11.4 ... 12.8)		

h 4947;  $-81^{\circ} 7'95''$ ; 8.6

A.R.  $17^{\text{h}} 22^{\text{m}} 38^{\text{s}}$ ; Decl.  $-81^{\circ} 49'$

18.747	72.2	9.95	22.1	2	370
18.752	71.9	10.00	21.6	2½	370
18.755	71.3	10.00	21.8	1½	370
18.75	71.8	9.98	(8.4 ... 8.7)		182

WO 136;  $-40^{\circ} 7'886''$ ; 7.5

A.R.  $17^{\text{h}} 22^{\text{m}} 55^{\text{s}}$ ; Decl.  $-40^{\circ} 56'$

20.240	107.7	1.23	17.0	3½	650
20.243	108.4	1.30	16.6	3	370
20.246	108.3	1.18	17.1	3	475
20.24	108.1	1.24	(8.0 ... 8.3)		F

*h* 4958; Cód —40° 11556; 9.8A.R. 17<sup>h</sup> 23<sup>m</sup> 17<sup>s</sup>; Decl. —40° 30'

20.240	235.0	17.77	17.2	3	370
20.243	235.5	17.76	26.8	2½	370
20.24	235.2	17.77	(10.8 ... 11.0)		F

*h* 4954; —72° 2089; 7.8A.R. 17<sup>h</sup> 23<sup>m</sup> 52<sup>s</sup>; Decl. —72° 3'

18.618	297.1	15.57	19.4	2	370
18.632	296.6	15.16	21.5	2	370
18.635	298.1	15.22	21.3	2	370
18.63	297.3	15.32	(8.4 ... 12.8)		N

*h* 4956; —62° 5631; 9.0A.R. 17<sup>h</sup> 23<sup>m</sup> 53<sup>s</sup>; Decl. —62° 52'

18.427	109.7	5.04	19.0	2	370
18.624	109.3	5.07	19.0	2½	370
18.629	107.8	5.09	17.6	1½	370
18.56	108.9	5.07	(10.1 ... 10.3)		M?

*h* 4962; —32° 4616; 6.0A.R. 17<sup>h</sup> 26<sup>m</sup> 34<sup>s</sup>; Decl. —32° 29'

19.585	103.3	5.35	20.5	2	370
19.604	101.6	5.52	20.2	2	370
19.612	101.2	5.55	20.4	2	370
19.60	102.0	5.47	(5.9 ... 10.5)		F

*h* 4963; —41° 8090; 8.6A.R. 17<sup>h</sup> 27<sup>m</sup> 48<sup>s</sup>; Decl. —41° 51'

20.240	314.8	7.03	17.3	3	370
20.243	314.4	7.02	16.9	3	370
20.246	314.4	7.04	17.2	2½	475
20.24	314.5	7.03	(8.20 ... 11.1)		F

I 1007; —34° 6907; 9.2

A.R. 17<sup>h</sup> 29<sup>m</sup> 16<sup>s</sup>; Decl. —34° 56'

19.700	119.1	0.98	19.9	2	370
19.738	116.5	0.98	19.8	2½	370
19.746	117.0	1.05	21.2	2½	370
19.73	117.5	1.00	(9.9 ... 10.2)		N

CD

19.700	249.3	2.06	20.1	2	370
19.738	248.3	2.37	19.9	2½	370
19.746	245.1	2.57	21.3	2½	370
19.752	246.2	2.48	20.4	2½	370
19.73	247.2	2.37	(12.0 ... 12.4)		N

AC = *h* 4966

19.700	275.6	12.75	20.0	2	370
19.743	274.5	12.17	21.4	2½	370
19.752	272.9	12.48	20.5	2½	370
19.73	274.3	12.47	(9.9 ... 12.0)		N

Pk 5; —34° 6937; 9.0

A.R. 17<sup>h</sup> 31<sup>m</sup> 2<sup>s</sup>; Decl. —34° 49'

19.691	258.8	4.96	19.5	2	370
19.700	259.9	4.87	20.2	2	370
19.738	258.6	5.11	20.4	2½	370
19.71	259.1	4.98	(9.3Y ... 10.6b)		F

I 107; —32° 4683; 8.6

A.R. 17<sup>h</sup> 31<sup>m</sup> 23<sup>s</sup>; Decl. —32° 16'

19.585	137.5	1.71	20.7	2½	370
19.604	136.6	1.89	20.4	2	475
19.612	138.4	1.80	20.5	2	370
19.60	137.5	1.80	(10.2 ... 10.5)		F

I 608; —32° 4726; 8.4

A.R. 17<sup>h</sup> 32<sup>m</sup> 12<sup>s</sup>; Decl. —32° 6'

19.585	303.5	1.92	20.9	2½	370
19.604	303.5	2.22	20.5	2	475
19.648	303.4	2.00	20.2	2½	475
19.61	303.5	2.05	(9.1 ... 11.2)		142

*h* 4972; —70° 2426; 9.3A.R. 17<sup>h</sup> 38<sup>m</sup> 3<sup>s</sup>; Decl. —70° 12'

18.635	281.1	7.52	21.5	1½	370
18.638	280.6	7.43	20.8	2	370
18.711	279.6	7.62	20.9	1½	370
18.66	280.4	7.52	(10.0 ... 11.7)		N

*h* 4974; —76° 1226; 8.0A.R. 17<sup>h</sup> 40<sup>m</sup> 0<sup>s</sup>; Decl. —76° 9'

18.638	120.0	26.50	20.6	1½	370
18.654	119.6	25.43	20.5	2	370
18.65	119.8	25.46	(6.8 ... 14.0)		N

*h* 4976; —70° 2438 + 9; 8.5 + 9.6A.R. 17<sup>h</sup> 41<sup>m</sup> 36<sup>s</sup>; Decl. —70° 30'

18.638	51.2	25.05	21.0	2	370
18.712	51.3	24.68	21.0	1½	370
18.722	51.1	24.82	20.5	2	370
18.69	51.2	24.85	(8.5 ... 10.1)		N

*h* 4983; —66° 3162 + 3; 9.1 + 9.9A.R. 17<sup>h</sup> 43<sup>m</sup> 14<sup>s</sup>; Decl. —66° 30'

18.624	15.8	20.75	19.6	2	370
18.638	15.3	20.62	21.3	2	370
18.63	15.6	20.68	(9.7 ... 10.8)		F?

$\beta$  1123;  $-34^{\circ} 7266$ ; 7.2

A.R.  $17^{\text{h}} 45^{\text{m}} 0^{\text{s}}$ ; Decl.  $-34^{\circ} 42'$

21.362	232.8	0.47	15.6	2½	475
21.381	230.5	0.45	18.3	3	370
21.403	235.1	0.43	17.3	3	475
21.38	232.8	0.45	(7.4 ... 7.5)		20

$\lambda$  342;  $-34^{\circ} 7270$ ; 7.4

A.R.  $17^{\text{h}} 45^{\text{m}} 3^{\text{s}}$ ; Decl.  $-34^{\circ} 52'$

21.362	272.1	0.39	15.7	2½	475
21.381	265.9	0.62	18.4	3	370
21.403	271.9	0.42	17.4	3	475
21.38	270.0	0.48	(7.3 ... 7.3)		A?

\* Rū 22 = Cape 18 = Rus 304;  $-55^{\circ} 8375$ ; 7.3

A.R.  $17^{\text{h}} 46^{\text{m}} 48^{\text{s}}$ ; Decl.  $-55^{\circ} 21'$

20.644	92.1	2.67	19.1	2½	370
20.653	91.8	2.74	19.1	2½	370
20.691	92.5	2.70	20.4	2½	370
20.66	92.1	2.70	(6.9Y ... 8.4 h)		M?

I 1011;  $-30^{\circ} 5036$ ; 7.7

A.R.  $17^{\text{h}} 47^{\text{m}} 43^{\text{s}}$ ; Decl.  $-30^{\circ} 33'$

19.585	147.9	1.33	21.4	2½	370
19.604	150.0	1.41	20.7	2	475
19.774	155.2	1.51	20.8	2½	370
19.790	152.3	1.46	21.0	2½	370
19.74	151.4	1.43	(8.1 ... 11.1)		23

$h$  4987; Anon.

A.R.  $17^{\text{h}} 49^{\text{m}} 0^{\text{s}}$ ; Decl.  $-80^{\circ} 27'$

18.734	136.5	11.53	22.5	1½	370
18.747	136.4	11.65	22.3	2	370
18.74	136.4	11.59	(10.4 ... 13.6)		N

$h$  4988;  $-78^{\circ} 1156$ ; 8.7

A.R.  $17^{\text{h}} 49^{\text{m}} 34^{\text{s}}$ ; Decl.  $-78^{\circ} 59'$

18.734	120.3	9.14	22.3	1½	370
18.747	121.2	8.94	22.4	2½	370
18.752	120.7	8.92	21.7	2½	370
18.74	120.7	9.00	(9.3 ... 9.6)		F

$\Delta$  219;  $-36^{\circ} 7836 + 3$ ; 7.5 + 8.3

A.R.  $17^{\text{h}} 50^{\text{m}} 27^{\text{s}}$ ; Decl.  $-36^{\circ} 51'$

19.692	259.8	49.55	19.7	2	370
19.752	259.4	49.13	20.6	2	370
19.757	259.3	49.42	20.3	2	370
19.73	259.5	49.37	(6.5 ... 8.5)		F?
BC = $\lambda$ 219;	Ver la nota				162

$\delta$  74;  $-30^{\circ} 5099$ ; 9.5

A.R.  $17^{\text{h}} 50^{\text{m}} 43^{\text{s}}$ ; Decl.  $-30^{\circ} 17'$

19.585	107.2	1.25	21.2	2½	370
19.774	105.2	1.22	20.9	2½	370
19.790	106.3	1.27	21.2	2½	370
19.72	106.2	1.25	(10.8 ... 11.2)		

$h$  5000;  $-36^{\circ} 7843$ ; 7.6

A.R.  $17^{\text{h}} 50^{\text{m}} 44^{\text{s}}$ ; Decl.  $-36^{\circ} 55'$

19.692	105.5	7.52	19.8	2	370
19.752	104.6	7.47	20.8	2	370
19.757	105.2	7.39	20.4	2	370
19.73	105.1	7.46	(7.9 ... 10.6)		D?

Piazzi =  $h$  5003;  $-30^{\circ} 5110$ ; 8.0

A.R.  $17^{\text{h}} 51^{\text{m}} 4^{\text{s}}$ ; Decl.  $-30^{\circ} 14'$

19.604	105.9	5.58	20.9	2	370
19.610	105.9	5.49	20.9	2	370
19.612	105.2	5.46	20.7	2	370
19.61	105.7	5.51	(5.3 Y ... 7.1 c)		F

AC = HdA

19.774	239.2	26.09	21.0	2½	370
19.790	239.5	25.93	21.4	2½	370
19.78	239.4	26.01	(5.3 ... 13.1)		220

$h$  5001;  $-72^{\circ} 2176$ ; 8.8

A.R.  $17^{\text{h}} 53^{\text{m}} 15^{\text{s}}$ ; Decl.  $-72^{\circ} 21'$

18.638	307.8	10.99	21.1	2	370
18.712	308.8	11.09	21.2	1½	370
18.722	308.2	11.11	20.6	1½	370
18.69	308.3	11.01	(8.9 ... 11.9)		N

$h$  4999;  $-75^{\circ} 1409$ ; 7.3

A.R.  $17^{\text{h}} 53^{\text{m}} 40^{\text{s}}$ ; Decl.  $-75^{\circ} 12'$

18.638	173.0	13.23	20.7	2	370
18.654	173.0	13.22	20.7	2	370
18.65	173.0	13.22	(7.9 ... 9.2)		F

$h$  5007;  $-37^{\circ} 7839$ ; 8.0

A.R.  $17^{\text{h}} 54^{\text{m}} 51^{\text{s}}$ ; Decl.  $-37^{\circ} 14'$

19.692	220.0	10.55	19.9	2	370
19.752	219.8	10.46	20.9	2	370
19.72	219.9	10.50	(9.1 ... 10.8)		F

$h$  5012;  $-34^{\circ} 7574 + 3$ ; 9.4 + 9.7

A.R.  $17^{\text{h}} 57^{\text{m}} 22^{\text{s}}$ ; Decl.  $-34^{\circ} 37'$

19.692	191.0	23.37	20.1	2	370
19.752	191.4	23.38	21.0	2	370
19.72	191.2	23.38	(8.8 ... 9.2)		N

*h* 5011;  $-41^{\circ} 8551 + 50$ ;  $8.2 + 8.9$

A.R.  $17^{\text{h}} 57^{\text{m}} 33^{\text{s}}$ ; Decl.  $-41^{\circ} 46'$

19.774	349.7	29.55	21.2	$2\frac{1}{2}$	370
19.804	349.6	29.63	21.4	$1\frac{1}{2}$	370
19.79	349.7	29.59	(8.5 ... 9.1 R)		F

Anónima;  $-41^{\circ} 8552$ ; 8.8

A.R.  $17^{\text{h}} 57^{\text{m}} 37^{\text{s}}$ ; Decl.  $-41^{\circ} 41'$

19.804	243.7	8.31	21.5	$1\frac{1}{2}$	370
19.826	243.6	8.38	22.0	2	370
19.82	243.6	8.35	(9.1 ... 10.7)		

\* *h* 5014;  $-43^{\circ} 8434$ ; 6.2

A.R.  $17^{\text{h}} 57^{\text{m}} 47^{\text{s}}$ ; Decl.  $-43^{\circ} 26'$

20.644	49.8	1.72	19.3	$2\frac{1}{2}$	370
20.653	51.3	1.64	19.0	$2\frac{1}{2}$	370
20.655	50.9	1.72	19.6	$2\frac{1}{2}$	370
20.65	50.7	1.69	(6.0 ... 6.3)		B

*h* 5008;  $-66^{\circ} 3254$ ; 9.0

A.R.  $17^{\text{h}} 58^{\text{m}} 21^{\text{s}}$ ; Decl.  $-66^{\circ} 25'$

19.624	241.1	15.10	19.7	$1\frac{1}{2}$	370
18.638	240.9	15.21	21.4	2	370
18.63	241.0	15.16	(9.2 ... 12.9)		N

*h* 5025;  $-40^{\circ} 8485 + 7$ ;  $9.1 + 9.8$

A.R.  $18^{\text{h}} 1^{\text{m}} 54^{\text{s}}$ ; Decl.  $-40^{\circ} 34'$

19.774	99.8	45.21	21.3	$2\frac{1}{2}$	370
19.804	99.8	45.51	21.6	$1\frac{1}{2}$	370
19.79	99.8	45.36	(9.2 ... 9.6)		D?

*h* 5019;  $-66^{\circ} 3280$ ; 7.0

A.R.  $18^{\text{h}} 1^{\text{m}} 56^{\text{s}}$ ; Decl.  $-66^{\circ} 50'$

18.624	334.5	38.03	19.9	$1\frac{1}{2}$	370
18.638	334.0	37.99	21.6	2	370
18.63	334.2	38.01	(7.6 ... 12.8)		N

$\beta$  759;  $-39^{\circ} 7993$ ; 8.2

A.R.  $18^{\text{h}} 3^{\text{m}} 29^{\text{s}}$ ; Decl.  $-39^{\circ} 22'$

20.240	121.1	2.02	17.5	3	370
20.243	121.8	1.97	17.2	3	370
20.246	122.0	1.93	17.3	$2\frac{1}{2}$	475
20.24	121.6	1.97	(9.0 ... 9.5)		F

AC = *h* 5028; C =  $-39^{\circ} 7994$ ; 8.8

20.240	147.1	14.80	17.6	$2\frac{1}{2}$	370
20.243	147.3	14.77	17.1	3	370
20.24	147.2	14.78	(9.0 ... 9.2)		F

\* *h* 5029;  $-57^{\circ} 8940$ ; 8.0

A.R.  $18^{\text{h}} 4^{\text{m}} 18^{\text{s}}$ ; Decl.  $-57^{\circ} 53'$

20.644	105.0	2.41	19.5	$2\frac{1}{2}$	370
20.653	105.3	2.54	19.3	$2\frac{1}{2}$	370
20.691	105.1	2.48	20.5	$2\frac{1}{2}$	370
20.66	105.1	2.48	(8.5 ... 8.8)		P

*h* 5037;  $-31^{\circ} 5467 + 3$ ;  $8.4 + 9.2$

A.R.  $18^{\text{h}} 8^{\text{m}} 6^{\text{s}}$ ; Decl.  $-31^{\circ} 12'$

19.604	227.2	37.32	19.7	$2\frac{1}{2}$	370
19.610	227.6	37.58	21.1	2	370
19.757	227.4	37.15	20.6	2	370
19.66	227.4	37.35	(7.8 ... 9.9)		N

$\beta$  760;  $\gamma$  Sagittarii; 6.6

A.R.  $18^{\text{h}} 9^{\text{m}} 10^{\text{s}}$ ; Decl.  $-36^{\circ} 48'$

20.655	101.7	3.99	19.9	2	370
20.814	100.7	3.71	22.1	2	370
20.817	100.6	3.71	21.9	2	370
20.80	101.0	3.87	(3.2 0 ... 9.9)		F

*h* 5036a;  $-34^{\circ} 7719 + 21$ ;  $7.0 + 9.0$

A.R.  $18^{\text{h}} 9^{\text{m}} 20^{\text{s}}$ ; Decl.  $-34^{\circ} 9'$

19.692	85.9	39.08	20.3	$1\frac{1}{2}$	370
19.752	85.9	38.99	21.1	2	370
19.72	85.9	39.03	(7.4 ... 9.5)		N

*h* 5036b;  $-34^{\circ} 7722$ ; 8.1

A.R.  $18^{\text{h}} 9^{\text{m}} 24^{\text{s}}$ ; Decl.  $-34^{\circ} 8'$

19.692	346.8	16.55	20.4	$1\frac{1}{2}$	370
19.752	346.8	16.37	21.2	2	370
19.72	346.8	16.46	(8.9 ... 10.2)		N

*h* 5039;  $-66^{\circ} 3336 + 7$ ;  $9.7 + 10.2$

A.R.  $18^{\text{h}} 12^{\text{m}} 52^{\text{s}}$ ; Decl.  $-66^{\circ} 9'$

18.624	129.2	17.17	20.2	$1\frac{1}{2}$	370
18.638	129.0	16.99	21.7	2	370
18.63	129.1	17.08	(10.2 ... 11.0)		F

\* *h* 5040;  $-48^{\circ} 9768$ ; 10.4

A.R.  $18^{\text{h}} 14^{\text{m}} 19^{\text{s}}$ ; Decl.  $-48^{\circ} 19'$

19.749	302.1	7.72	22.0	2	370
20.691	301.4	7.60	20.9	2	370
20.22	301.8	7.66	(11.5 ... 11.5)		221

BC

19.749	358.0	4.74	22.1	$1\frac{1}{2}$	370
20.691	356.3	4.82	21.0	2	370
20.22	357.2	4.78	(11.5 ... 12.0)		221

(Sigue Continued.)

Vecina

20.691	85.4	7.47	(11.5 ... 12.5)AB
20.691	23.1	9.22	(11.5 ... 12.6)AC 221

Howe 43 =  $\beta$  1128;  $-33^{\circ} 51'24''$ ; 6.5

A.R.  $18^{\text{h}} 22^{\text{m}} 53^{\text{s}}$ ; Decl.  $-33^{\circ} 4'$

20.653	195.4	3.35	20.5	2½	370
20.655	196.9	3.32	20.1	2	370
20.814	198.7	3.42	22.3	2	370
20.71	197.0	3.36	(6.2 ... 11.3)		F

$h$  5043;  $-83^{\circ} 664''$ ; 5.8

A.R.  $18^{\text{h}} 27^{\text{m}} 45^{\text{s}}$ ; Decl.  $-83^{\circ} 33'$

18.769	6.5	45.68	21.6	1½	370
18.827	3.2	45.16	23.2	2	370
18.80	4.9	45.42	(5.8 ... 14.3)		N

$h$  5052;  $-41^{\circ} 8734''$ ; 9.7

A.R.  $18^{\text{h}} 29^{\text{m}} 52^{\text{s}}$ ; Decl.  $-41^{\circ} 33'$

20.243	130.1	5.74	17.3	3	370
20.246	130.1	5.81	17.5	2½	475
20.656	130.9	5.92	21.7	2½	370
20.38	130.4	5.82	(10.1 ... 10.4)		N

I —;  $-51^{\circ} 11010''$ ; 8.6

A.R.  $18^{\text{h}} 37^{\text{m}} 24^{\text{s}}$ ; Decl.  $-51^{\circ} 11'$

20.708	240.3	0.67	22.2	2½	370
20.710	241.3	0.71	21.6	2½	370
20.863	241.6	0.74	22.9	3	370
20.76	241.1	0.71	(9.5 ... 9.7)		23,M

$h$  5060<sup>?</sup>;  $-51^{\circ} 11019''$ ; 8.0

A.R.  $18^{\text{h}} 38^{\text{m}} 58^{\text{s}}$ ; Decl.  $-51^{\circ} 15'$

20.691	358.8	3.92	21.2	2	370
20.708	358.2	3.68	22.1	2	370
20.710	358.1	3.58	21.7	2½	370
20.70	358.4	3.73	(8.1 ... 13.3)		222

$h$  5064;  $-37^{\circ} 8345''$ ; 8.1

A.R.  $18^{\text{h}} 39^{\text{m}} 54^{\text{s}}$ ; Decl.  $-37^{\circ} 9'$

19.757	268.4	18.50	21.4	2	370
19.790	269.5	18.63	21.6	2	370
19.826	268.0	18.65	22.2	2	370
19.79	268.6	18.59	(7.2 ... 13.4)		N

$h$  5061;  $-74^{\circ} 1718''$ ; 9.6

A.R.  $18^{\text{h}} 41^{\text{m}} 40^{\text{s}}$ ; Decl.  $-74^{\circ} 21'$

18.712	286.3	6.14	21.4	1½	370
18.722	285.7	6.03	20.8	1½	370
18.733	287.0	6.43	20.7	1½	370
18.72	286.3	6.20	(10.1 ... 11.8)		N

$h$  5066;  $-41^{\circ} 8786''$ ; 7.0

A.R.  $18^{\text{h}} 42^{\text{m}} 12^{\text{s}}$ ; Decl.  $-41^{\circ} 12'$

20.243	85.5	10.16	17.5	2½	370
20.246	85.5	10.28	17.7	2½	370
20.24	85.5	10.22	(6.6 ... 10.0)		F

$h$  5063;  $-79^{\circ} 987''$ ; 9.2

A.R.  $18^{\text{h}} 43^{\text{m}} 43^{\text{s}}$ ; Decl.  $-79^{\circ} 9'$

18.734	120.1	8.30	22.7	1½	370
18.747	118.8	8.27	22.6	2	370
18.753	118.2	8.28	21.9	1½	370
18.74	119.0	8.28	(11.0 ... 12.7)		N

$h$  5074;  $-39^{\circ} 8235''$ ; 7.2

A.R.  $18^{\text{h}} 50^{\text{m}} 32^{\text{s}}$ ; Decl.  $-39^{\circ} 42'$

20.246	246.4	16.04	17.8	2½	370
20.708	246.0	15.60	22.4	2½	370
20.710	246.2	15.85	21.9	2½	370
20.55	246.2	15.83	(7.3 ... 11.8)		22

$h$  5071;  $-80^{\circ} 894''$ ; 9.2

A.R.  $18^{\text{h}} 51^{\text{m}} 21^{\text{s}}$ ; Decl.  $-80^{\circ} 11'$

18.747	59.7	21.45	22.7	2	370
18.753	58.7	21.59	22.1	2	370
18.758	59.4	21.44	22.1	2½	370
18.75	59.3	21.49	(9.1 ... 11.8)		N

$h$  5077;  $-36^{\circ} 8631''$ ; 8.4

A.R.  $18^{\text{h}} 51^{\text{m}} 58^{\text{s}}$ ; Decl.  $-36^{\circ} 26'$

19.757	96.9	8.12	21.6	2	370
19.845	95.4	7.86	22.1	1½	370
19.848	95.8	7.76	22.4	2½	370
19.853	96.0	7.98	22.7	2	370
19.83	96.0	7.93	(9.0 ... 9.6)		F

Bris 6556;  $-37^{\circ} 8446''$ ; 6.4

A.R.  $18^{\text{h}} 52^{\text{m}} 37^{\text{s}}$ ; Decl.  $-37^{\circ} 14'$

19.757	281.2	12.67	21.7	2½	370
19.790	282.0	12.84	21.8	2	370
19.845	282.0	12.86	22.0	1½	370
19.80	281.7	12.79	(7.2 ... 7.3)		F

$h$  5073;  $-78^{\circ} 1215'' + 14''$ ; 8.3 + 9.0

A.R.  $18^{\text{h}} 53^{\text{m}} 19^{\text{s}}$ ; Decl.  $-78^{\circ} 48'$

18.734	346.0	22.95	22.9	1	370
18.747	346.2	22.71	22.9	2	370
18.74	346.1	22.83	(8.5 ... 9.7)		F?

$h$  5080;  $-36^\circ 8662$ ; 7.7A.R.  $18^h 54^m 20^s$ ; Decl.  $-36^\circ 16'$ 

19.757	246.5	5.47	21.9	$2\frac{1}{2}$	370
19.845	247.0	5.75	22.2	$1\frac{1}{2}$	370
19.848	246.8	5.57	22.5	$2\frac{1}{2}$	370
19.82	246.8	5.60	(7.9 ... 9.6)		D?

 $h$  5083;  $-36^\circ 8694 + 3$ ;  $8.5 + 9.7$ A.R.  $18^h 57^m 2^s$ ; Decl.  $-36^\circ 21'$ 

19.757	5.1	21.39	22.0	2	370
19.845	5.0	21.47	22.4	$1\frac{1}{2}$	370
19.80	5.1	21.43	(8.7 ... 10.4)		42

\*  $h$  5084;  $\gamma$  Corollae; 5.5A.R.  $18^h 57^m 58^s$ ; Decl.  $-37^\circ 14'$ 

18.318	275.0	2.10	19.5	3	475
18.427	274.7	2.25	19.4	$2\frac{1}{2}$	475
18.755	273.0	2.29	21.3	$2\frac{1}{2}$	475
19.467	272.1	2.47	18.0	$2\frac{1}{2}$	475
19.484	272.2	2.21	19.8	3	650
19.553	272.9	2.53	21.5	$2\frac{1}{2}$	370
19.558	271.1	2.38	18.6	3	475
20.240	268.9	2.29	17.8	3	650
20.246	270.4	2.29	18.1	3	370
20.644	269.7	2.29	19.7	3	370
20.653	269.7	2.87	19.5	$2\frac{1}{2}$	370
21.403	267.6	2.39	17.7	3	475
18.50	274.2	2.21			
19.52	272.1	2.40			
20.45	269.7	2.31			
21.40	267.6	2.39	(4.7 ... 4.7)		B

 $h$  5091;  $-31^\circ 5897$ ; 7.9A.R.  $19^h 0^m 31^s$ ; Decl.  $-31^\circ 10'$ 

19.553	208.8	9.19	21.8	$2\frac{1}{2}$	370
19.585	207.9	9.02	21.9	$2\frac{1}{2}$	370
19.604	207.9	8.95	21.0	2	370
19.58	208.2	9.05	(8.1 ... 9.9)		A?

 $h$  5094;  $-34^\circ 8332$ ; 7.6:A.R.  $19^h 4^m 32^s$ ; Decl.  $-34^\circ 8'$ 

19.553	200.0	18.82	22.1	$2\frac{1}{2}$	370
19.585	199.9	18.58	22.2	2	370
19.604	200.3	18.84	21.1	2	370
19.58	200.1	18.75	(7.4 ... 7.7)		A

Vecina siguiente

19.553	177.7	10.15	(11.0 ... 12.2)		
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 $h$  5095;  $-31^\circ 5930 + 29$ ;  $8.8 + 8.8$ A.R.  $19^h 5^m 14^s$ ; Decl.  $-31^\circ 8'$ 

19.553	250.3	20.08	21.9	$2\frac{1}{2}$	370
19.585	250.2	19.93	22.0	$2\frac{1}{2}$	370
19.57	250.2	20.00	(9.1 ... 9.5)		N

 $h$  5098;  $-36^\circ 8801$ ; 8.9A.R.  $19^h 6^m 18^s$ ; Decl.  $-36^\circ 28'$ 

19.757	73.9	5.59	22.1	$2\frac{1}{2}$	370
19.845	74.5	5.73	22.6	$1\frac{1}{2}$	370
19.848	74.2	5.56	22.6	2	370
19.82	74.2	5.63	(10.1 ... 10.3)		F

 $h$  5107;  $-33^\circ 5596$ ; 8.0A.R.  $19^h 12^m 46^s$ ; Decl.  $-33^\circ 17'$ 

19.553	127.5	13.62	22.4	2	370
19.604	127.6	13.70	21.3	2	370
19.58	127.5	13.66	(8.1 ... 9.4)		41

 $\delta$  75;  $-78^\circ 1240$ ; 9.4A.R.  $19^h 14^m 27^s$ ; Decl.  $-78^\circ 9'$ 

18.747	139.6	1.89	23.5	2	475
18.753	141.0	2.03	22.3	2	475
18.758	139.3	1.82	22.3	2	475
19.75	140.0	1.91	(10.6 ... 11.2)		

 $h$  5106;  $-79^\circ 1031$ ; 9.4A.R.  $19^h 16^m 28^s$ ; Decl.  $-79^\circ 3'$ 

18.747	203.1	15.76	23.7	$2\frac{1}{2}$	370
18.753	201.7	15.81	22.4	2	370
18.75	202.4	15.78	(9.4 ... 13.5)		N

 $h$  5111;  $-33^\circ 5626 + 4$ ;  $9.1 + 9.1$ A.R.  $19^h 16^m 32^s$ ; Decl.  $-33^\circ 8'$ 

19.736	271.1	25.79	21.6	$2\frac{1}{2}$	370
19.749	271.2	25.87	22.5	2	370
19.74	271.1	25.83	(9.0 ... 9.9)		N

 $h$  5115;  $-40^\circ 8988$ ; 8.7A.R.  $19^h 18^m 36^s$ ; Decl.  $-40^\circ 8'$ 

19.845	65.2	10.97	22.8	$1\frac{1}{2}$	370
19.848	65.4	10.86	22.8	2	370
19.85	65.3	10.91	(9.5 ... 9.7)		F?

 $h$  5116;  $-78^\circ 1248$ ; 9.0A.R.  $19^h 23^m 9^s$ ; Decl.  $-78^\circ 48'$ 

18.747	298.3	24.55	23.9	2	370
18.753	298.3	24.62	22.6	2	370
18.75	298.3	24.58	(9.2 ... 11.1)		N

AC; C = 11.0

18.747	117.1	32.37	23.9	$1\frac{1}{2}$	370 N
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Aa

18.747	43.3	8.15	0.0	2	370
18.753	42.2	8.09	22.8	2	370
18.75	42.7	8.12	(9.2 ... 14.2)		



*h* 5122;  $-75^{\circ} 1533$ ; 9.1  
 A.R. 19<sup>h</sup> 24<sup>m</sup> 54<sup>s</sup>; Decl.  $-75^{\circ} 54'$

18.712	270.9	13.25	21.5	1½	370
18.733	268.3	13.37	21.0	1½	370
18.747	271.3	13.44	23.0	2	370
18.73	270.2	13.35	(9.2 ... 13.3)		A?

*h* 5126;  $-79^{\circ} 1039$ ; 9.4  
 A.R. 19<sup>h</sup> 28<sup>m</sup> 50<sup>s</sup>; Decl.  $-79^{\circ} 43'$

18.753	327.4	6.52	22.9	2	370
18.758	329.4	6.66	22.7	2	370
18.761	328.4	7.16	21.5	1½	370
18.766	326.2	6.72	21.8	1½	370
18.76	327.9	6.76	(10.7 ... 11.5)		N

*h* 5131;  $-31^{\circ} 6097 + 8$ ; 9.6 + 9.6  
 A.R. 19<sup>h</sup> 29<sup>m</sup> 29<sup>s</sup>; Decl.  $-31^{\circ} 11'$

19.736	142.0	17.01	22.1	2½	370
19.749	141.9	17.06	22.6	2	370
19.74	142.0	17.03	(9.6 ... 10.0)		N

BC

19.736	215.0	11.54	22.2	2	370
19.749	215.4	11.64	22.7	2	370
19.74	215.2	11.59	(10.0 ... 10.1)		N

*h* 5134 =  $\lambda$  386;  $-41^{\circ} 9151$ ; 7.6  
 A.R. 19<sup>h</sup> 30<sup>m</sup> 44<sup>s</sup>; Decl.  $-41^{\circ} 50'$

19.848	126.3	12.34	23.0	2	370
19.853	127.1	12.44	22.9	2	370
19.859	126.9	12.19	22.8	2½	370
19.85	126.8	12.32	(8.5 ... 11.9)		198; 220

$\beta$  761 =  $\lambda$  388;  $-40^{\circ} 9066$ ; 8.1  
 A.R. 19<sup>h</sup> 31<sup>m</sup> 10<sup>s</sup>; Decl.  $-40^{\circ} 2'$

19.848	197.6	2.60	23.2	2½	370
19.853	195.0	2.60	23.0	2	370
19.859	195.1	2.66	22.9	2½	650
19.85	195.9	2.62	(7.9 ... 10.0)		220

*h* 5127;  $-86^{\circ} 378$ ; 9.6  
 A.R. 19<sup>h</sup> 37<sup>m</sup> 34<sup>s</sup>; Decl.  $-86^{\circ} 16'$

18.851	279.8	8.51	0.5	2	370
18.854	280.8	8.74	0.0	2	370
18.903	281.2	8.64	0.4	2	370
18.87	280.6	8.63	(10.1 ... 11.2)		N

*h* 5145;  $-35^{\circ} 8646$ ; 9.1  
 A.R. 19<sup>h</sup> 39<sup>m</sup> 44<sup>s</sup>; Decl.  $-35^{\circ} 18'$

19.845	162.7	24.24	23.5	2	370
19.853	162.4	24.38	23.2	2	370
19.85	162.5	24.31	(9.0 ... 11.2)		N

*h* 5147;  $-30^{\circ} 6112$ ; 9.6  
 A.R. 19<sup>h</sup> 40<sup>m</sup> 25<sup>s</sup>; Decl.  $-30^{\circ} 19'$

19.736	85.3	12.40	22.3	2½	370
19.749	84.1	12.55	22.8	1½	370
19.74	84.7	12.47	(10.1 ... 12.1)		N

*h* 5151;  $-37^{\circ} 8598$ ; 7.6  
 A.R. 19<sup>h</sup> 42<sup>m</sup> 53<sup>s</sup>; Decl.  $-34^{\circ} 13'$

19.848	358.9	7.75	23.3	2	370
19.853	358.8	7.72	23.3	2	370
19.859	358.5	7.80	23.0	3	370
19.85	358.7	7.76	(8.4 ... 9.5)		N

*h* 5149;  $-79^{\circ} 1050 + 1$ ; 7.8 + 8.5  
 A.R. 19<sup>h</sup> 45<sup>m</sup> 5<sup>s</sup>; Decl.  $-79^{\circ} 7'$

18.753	150.3	32.31	23.3	2	370
18.758	150.2	32.39	22.8	2	370
18.76	150.2	32.35	(8.2 ... 9.7)		D?

*h* 5152;  $-30^{\circ} 6131$ ; 8.4  
 A.R. 19<sup>h</sup> 45<sup>m</sup> 35<sup>s</sup>; Decl.  $-30^{\circ} 35'$

19.736	153.7	6.26	22.4	2½	370
19.749	153.9	6.28	22.9	2	370
19.774	153.5	6.31	22.5	2½	370
19.75	153.7	6.28	(8.8 ... 9.4)		N

$\delta$  76;  $-32^{\circ} 6056$ ; 9.8  
 A.R. 19<sup>h</sup> 47<sup>m</sup> 9<sup>s</sup>; Decl.  $-32^{\circ} 41'$

19.736	357.9	3.14	22.5	2½	370
19.774	357.6	3.07	22.6	2	370
19.809	360.5	3.32	22.6	2	370
19.77	358.7	3.18	(10.0 ... 10.3)		

AC = *h* 5154

19.736	209.6	14.21	22.6	2	370
19.774	209.4	14.17	22.7	2	370
19.76	209.5	14.19	(10.0 ... 11.0)		N

*h* 5156;  $-35^{\circ} 8693$ ; 9.8  
 A.R. 19<sup>h</sup> 49<sup>m</sup> 19<sup>s</sup>; Decl.  $-35^{\circ} 9'$

19.853	128.4	16.11	23.6	2	370
19.864	127.9	16.28	23.1	2	370
19.86	128.1	16.20	(9.9 ... 10.2)		F

*h* 5153;  $-79^{\circ} 1056$ ; 7.7  
 A.R. 19<sup>h</sup> 51<sup>m</sup> 10<sup>s</sup>; Decl.  $-79^{\circ} 28'$

18.753	124.4	41.76	23.4	2	370
18.761	125.5	41.03	21.7	1	370
18.766	125.5	41.34	21.9	1½	370
18.76	125.1	41.38	(7.3 ... 12.8)		N

$h$  5159;  $-40^{\circ} 9153 + 4$ ;  $10.0 + 10.2$

A.R.  $19^h 51^m 14^s$ ; Decl.  $-40^{\circ} 50'$

19.853	32.6	25.62	23.5	2	370
19.864	32.6	25.79	22.9	2	370
19.86	32.6	25.70	(9.0 ... 9.4)	F?	

$h$  5158;  $-74^{\circ} 1870$ ;  $8.5$ :

A.R.  $19^h 52^m 26^s$ ; Decl.  $-74^{\circ} 56'$

18.712	146.6	12.18	21.6	2	370
18.733	146.6	12.35	21.2	2	370
18.72	146.6	12.26	(9.6 ... 9.8)	N	

$h$  5165;  $-32^{\circ} 6074$ ;  $7.2$

A.R.  $19^h 56^m 24^s$ ; Decl.  $-32^{\circ} 24'$

19.736	305.7	51.35	22.7	2	370
19.774	305.2	51.45	22.8	2	370
19.809	306.1	51.06	22.8	2	370
19.77	305.7	51.29	(5.4 ... 12.7)	N	

I 1044;  $-81^{\circ} 890$ ;  $8.0$

A.R.  $19^h 59^m 24^s$ ; Decl.  $-81^{\circ} 39'$

18.753	46.1	0.76	23.7	2½	650
18.766	44.1	0.80	22.0	2	475
18.827	50.1	0.81	23.4	2	475
18.78	46.8	0.79	(8.7 ... 9.4)	F	

$h$  5168;  $-30^{\circ} 6190$ ;  $7.8$

A.R.  $19^h 59^m 37^s$ ; Decl.  $-30^{\circ} 5'$

19.774	80.5	18.62	22.9	1½	370
19.809	80.4	18.75	23.0	2	370
19.79	80.4	18.69	(7.10 ... 11.0b)	N	

$h$  5170;  $-35^{\circ} 8749$ ;  $7.8$

A.R.  $20^h 1^m 19^s$ ; Decl.  $-35^{\circ} 32'$

19.864	314.3	13.14	23.3	2	370
19.883	314.4	13.37	23.6	2	370
19.87	314.3	13.25	(8.5 ... 11.6)	F	

$h$  5173;  $-36^{\circ} 9037$ ;  $6.6$

A.R.  $20^h 3^m 0^s$ ; Decl.  $-36^{\circ} 25'$

19.883	120.3	8.17	23.7	2	370
19.891	121.5	8.27	23.9	2	370
19.894	121.0	8.38	0.0	2	370
19.89	120.9	8.27	(5.6 ... 12.8)	D?	

$h$  5178 =  $\lambda$  410;  $-34^{\circ} 8620$ ;  $7.1$

A.R.  $20^h 5^m 40^s$ ; Decl.  $-34^{\circ} 29'$

19.864	10.5	3.07	23.5	2	370
19.883	10.5	2.86	23.9	2	370
19.891	10.9	3.13	0.0	2½	370
19.88	10.6	3.02	(7.20 ... 8.8b)	20	

$h$  5181;  $-32^{\circ} 6098$ ;  $9.5$

A.R.  $20^h 7^m 42^s$ ; Decl.  $-32^{\circ} 16'$

19.880	6.3	11.42	23.6	2	370
19.911	5.3	11.52	0.4	2½	370
20.647	5.9	11.68	20.1	2½	370
20.15	5.8	11.54	(9.5 ... 12.1)	N	

$h$  5183;  $-36^{\circ} 9073$ ;  $7.6$

A.R.  $20^h 8^m 15^s$ ; Decl.  $-36^{\circ} 50'$

19.883	229.2	38.13	0.0	2	370
19.891	228.4	37.81	0.2	2	370
19.894	229.0	37.93	0.2	2	370
19.89	228.9	37.96	(6.8 ... 11.2)	F?	

AC

19.883	180.4	46.75	0.1	2	370
19.891	180.5	46.59	0.3	2	370
19.894	180.1	—	0.1	2	370
19.89	180.3	46.67	(6.8 ... 12.6)	F?	

\*  $h$  5184 = I 378;  $-46^{\circ} 9941$ ;  $8.6$

A.R.  $20^h 8^m 54^s$ ; Decl.  $-46^{\circ} 20'$

20.656	195.3	2.19	21.5	2	370
20.814	191.2	1.96	22.9	2	370
20.863	189.3	2.07	23.3	3½	370
20.78	191.9	2.07	(8.4 ... 13.7)	R	

$\beta$  762;  $-32^{\circ} 6100$ ;  $7.6$

A.R.  $20^h 9^m 0^s$ ; Decl.  $-32^{\circ} 60'$

20.653	302.1	2.42	21.9	2½	475
20.656	302.5	2.47	21.1	2½	370
20.806	303.4	2.48	23.1	2	370
20.70	302.7	2.46	(7.6 ... 8.4)	F	

$h$  5175;  $-82^{\circ} 811$ ;  $8.9$

A.R.  $20^h 9^m 51^s$ ; Decl.  $-82^{\circ} 19'$

AB; Ver la nota 162

AC

18.769	200.3	12.17	21.8	1	370
18.827	198.9	12.05	23.7	2	370
18.851	197.2	12.49	1.1	2	370
18.82	198.8	12.24	(9.1 ... 11.2)	N	

*h* 5182;  $-81^{\circ} 901 + 0$ ;  $7.4 + 9.2$

A.R.  $20^h 12^m 20^s$ ; Decl.  $-81^{\circ} 22'$

18.753	356.6	26.62	23.8	3	370
18.761	357.0	26.91	21.9	1	370
18.766	357.7	26.68	22.1	2	370
18.76	357.1	26.74	(6.2 ... 11.3)		N

*h* 5189;  $-37^{\circ} 8777$ ;  $7.6$

A.R.  $20^h 13^m 40^s$ ; Decl.  $-37^{\circ} 18'$

19.883	295.3	7.69	0.3	2	370
19.894	295.5	7.83	23.9	2	370
19.897	296.2	7.54	0.1	2½	370
19.900	296.0	7.54	0.0	2	370
19.89	295.8	7.65	(8.8 ... 9.6)		F

*h* 5191; Cód  $-31^{\circ} 17522$ ;  $9.4$

A.R.  $20^h 13^m 49^s$ ; Decl.  $-31^{\circ} 28'$

19.880	251.9	11.97	23.8	2	370
19.911	251.2	11.71	0.6	2½	370
20.647	251.3	11.68	20.3	3	370
20.15	251.5	11.79	(10.6 ... 11.3)		N

*h* 5186;  $-77^{\circ} 1440$ ;  $8.1$

A.R.  $20^h 15^m 22^s$ ; Decl.  $-77^{\circ} 37'$

18.758	93.7	7.78	23.0	2	370
18.766	95.4	7.91	22.3	2½	370
18.769	95.8	8.13	21.5	2	370
18.76	95.0	7.94	(8.8 ... 9.2)		F

$\beta$  763;  $\alpha_2$  Sagittarii;  $5.9$

A.R.  $20^h 15^m 23^s$ ; Decl.  $-42^{\circ} 49'$

20.656	224.9	1.11	21.3	2½	370
20.806	222.7	1.21	23.3	2	370
20.814	222.5	1.28	22.7	2½	370
20.76	223.4	1.20	(6.9 ... 8.0)		M <sup>2</sup>

*h* 5195;  $-35^{\circ} 8819 + 20$ ;  $9.4 + 10.1$

A.R.  $20^h 16^m 39^s$ ; Decl.  $-35^{\circ} 8'$

AC

19.894	315.9	19.26	0.4	2	370
19.897	317.6	19.72	0.2	2	370
19.900	318.7	18.79	0.2	1½	370
19.90	317.4	19.26	(9.8 ... 11.4)		N

BC

19.894	124.4	17.23	0.5	2	370
19.897	124.8	17.66	0.4	2	370
19.900	124.4	17.44	0.3	1½	370
19.90	124.5	17.44	(10.2 ... 11.4)		N

*h* 5198;  $-36^{\circ} 9149$ ;  $9.4$

A.R.  $20^h 18^m 26^s$ ; Decl.  $-36^{\circ} 55'$

19.880	236.0	9.43	0.0	2	370
19.900	237.6	9.33	0.5	2	370
19.903	237.2	9.47	0.5	2	370
19.89	236.9	9.41	(10.8 ... 12.2)		D <sup>2</sup>

Vecina;  $-36^{\circ} 9150$ ;  $9.8$

19.897 48.1 12.03 (11.5 ... 11.8)

*h* 5199;  $-77^{\circ} 1447$ ;  $8.0$

A.R.  $20^h 22^m 6^s$ ; Decl.  $-77^{\circ} 19'$

18.712	209.7	28.94	21.8	1½	370
18.733	210.1	28.77	21.3	1½	370
18.72	209.9	28.86	(7.9 ... 12.9)		N

*h* 5203;  $-39^{\circ} 8715$ ;  $9.8$

A.R.  $20^h 23^m 7^s$ ; Decl.  $-39^{\circ} 32'$

19.903	116.8	10.77	0.7	2	370
19.905	117.9	10.48	0.8	2	370
19.908	115.2	10.84	0.7	2	370
19.91	116.6	10.70	(10.1 ... 12.3)		N

*h* 5205;  $-35^{\circ} 8870$ ;  $8.7$

A.R.  $20^h 23^m 41^s$ ; Decl.  $-35^{\circ} 56'$

19.880	43.3	24.52	0.2	1½	370
19.897	43.8	24.87	0.7	2	370
19.900	44.8	24.84	0.7	2	370
19.89	44.0	24.74	(9.0 ... 13.3)		R

*h* 5206;  $-31^{\circ} 6288$ ;  $7.8$

A.R.  $20^h 24^m 57^s$ ; Decl.  $-31^{\circ} 48'$

18.836	193.0	16.40	23.0	1½	370
18.862	192.2	16.47	23.8	2	370
18.85	192.6	16.44	(7.9 ... 12.5)		F

$\Delta$  232 = Rus 322;  $\alpha_2$  Octantis;  $7.0$ :

A.R.  $20^h 26^m 46^s$ ; Decl.  $-75^{\circ} 46'$

18.712	17.7	17.47	22.0	1½	370
18.733	17.7	17.30	21.6	1½	370
18.72	17.7	17.38	(6.9 ... 7.9)		F

*h* 5207;  $-34^{\circ} 8764$ ;  $7.8$

A.R.  $20^h 26^m 53^s$ ; Decl.  $-34^{\circ} 21'$

19.859	257.7	10.54	23.8	2½	370
19.883	257.6	10.48	0.4	2	370
19.87	257.7	10.51	(8.2 ... 10.4)		F

$h\ 5208; -38^\circ 8058; 10.3$ A.R.  $20^h 28^m 0^s$ ; Decl.  $-38^\circ 40'$ 

19.903	271.1	9.42	0.9	2	370
19.905	272.2	9.03	1.0	2	370
19.908	275.8	9.25	0.8	2	370
19.91	273.0	9.23	(10.0 ... 13.3)		N

 $h\ 5217; -64^\circ 4061; 9.4$ A.R.  $20^h 28^m 48^s$ ; Decl.  $-64^\circ 56'$ 

20.699	232.6	8.05	21.8	1½	370
20.702	232.7	8.18	22.0	1	370
20.708	233.3	8.12	22.8	2½	370
20.70	232.9	8.12	(9.8 ... 10.8)		223

 $l\ 337; -87^\circ 303; 8.9$ A.R.  $20^h 34^m 24^s$ ; Decl.  $-87^\circ 32'$ 

18.851	278.4	1.05	0.7	2	475
18.854	293.4	1.13	0.3	2	475
18.905	280.9	1.38	1.0	2½	370
18.917	283.0	1.38	1.0	1½	475
18.88	283.9	1.23	(9.5 ... 10.9)		D?

AB,C =  $h\ 5192; C = -87^\circ 302; 9.4$ 

18.851	322.7	18.46	0.6	2½	370
18.854	322.9	18.25	0.2	2½	370
18.903	323.3	18.28	0.6	2	370
18.87	323.0	18.33	((9.3) ... 9.4)		F

 $llh\ 700 = h\ 5213; -30^\circ 6318 + 17; 9.4 + 9.9$ A.R.  $20^h 34^m 42^s$ ; Decl.  $-30^\circ 57'$ 

18.836	325.9	23.70	23.1	2	370
18.862	325.4	23.71	0.0	2	370
18.85	325.6	23.70	(9.4 ... 9.5)		198

 $h\ 5215; -35^\circ 8900; 8.4$ A.R.  $20^h 35^m 38^s$ ; Decl.  $-35^\circ 59'$ 

19.859	184.3	21.09	0.0	2½	370
19.883	185.3	21.18	0.6	1½	370
19.891	184.5	21.26	0.5	2	370
19.88	184.7	21.18	(8.7 ... 12.4)		N

 $h\ 5216; -38^\circ 8099 + 8; 9.9 + 10.2$ A.R.  $20^h 37^m 39^s$ ; Decl.  $-38^\circ 4'$ 

19.897	22.7	15.73	0.8	2	370
19.900	22.8	16.00	0.8	2	370
19.903	22.6	15.94	1.1	2	370
19.90	22.7	15.89	(9.7 ... 9.8)		F

 $h\ 5214; -75^\circ 1661 + 60; 8.8 + 10.3$ A.R.  $20^h 37^m 43^s$ ; Decl.  $-75^\circ 46'$ 

18.712	313.4	19.80	22.1	1½	370
18.733	312.6	19.72	21.7	1½	370
18.72	313.0	19.76	(9.1 ... 10.4)		D?

 $h\ 5218; -30^\circ 6340; 7.0$ A.R.  $20^h 37^m 44^s$ ; Decl.  $-30^\circ 56'$ 

18.836	190.3	9.73	23.3	2	370
18.862	191.8	10.03	0.2	2	370
18.865	191.2	9.88	0.2	2	370
18.85	191.1	9.88	(6.8 ... 13.3)		F

 $h\ 5219; Cód -35^\circ 14340; 9.6$ A.R.  $20^h 37^m 57^s$ ; Decl.  $-35^\circ 10'$ 

19.859	324.1	8.91	0.2	2½	370
19.891	323.3	8.98	0.6	2	370
19.894	322.6	8.99	0.7	2	370
19.88	323.3	8.96	(11.1 ... 11.3)		N

 $h\ 5224; \alpha\ Microscopii; 6.5$ A.R.  $20^h 42^m 9^s$ ; Decl.  $-34^\circ 14'$ 

19.859	166.1	20.46	0.3	2½	370
19.891	166.0	20.64	0.7	2	370
19.87	166.1	20.55	(5.4 ... 9.6)		F

 $h\ 5228 = h\ 5225; -41^\circ 9462 + 4; 7.8 + 9.7$ A.R.  $20^h 43^m 28^s$ ; Decl.  $-41^\circ 22'$ 

19.905	104.1	32.27	1.2	2	370
19.908	104.2	32.41	0.9	2	370
19.91	104.2	32.34	(7.8 ... 9.4)		224

 $h\ 5227; \text{Ver la nota} \quad 225$  $h\ 5230; -75^\circ 1673; 8.0$ A.R.  $20^h 47^m 6^s$ ; Decl.  $-75^\circ 54'$ 

18.712	164.9	15.79	22.3	1½	370
18.733	165.3	15.76	21.9	1½	370
18.72	165.1	15.78	(8.3 ... 9.6)		F

 $h\ 5234; -34^\circ 8814; 8.9$ A.R.  $20^h 47^m 20^s$ ; Decl.  $-34^\circ 36'$ 

19.859	90.1	15.05	0.5	2½	370
19.894	89.6	15.32	0.9	2	370
19.897	90.8	15.42	1.0	2	370
19.88	90.2	15.26	(9.3 ... 9.4)		F?

G 263; —81° 938; 7.4

A.R. 20<sup>h</sup> 47<sup>m</sup> 47<sup>s</sup>; Decl. —81° 11'

18.753	249.1	5.08	0.0	3	370
18.758	248.2	4.89	23.2	2	370
18.766	247.9	5.01	22.4	2½	370
18.76	248.4	4.99	(7.1 ... 10.2)		F

G 266; α Octantis; 6.6

A.R. 20<sup>h</sup> 49<sup>m</sup> 30<sup>s</sup>; Decl. —77° 30'

18.73	Sin compañera,				211
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h 5236; —38° 8148; 8.4

A.R. 20<sup>h</sup> 49<sup>m</sup> 52<sup>s</sup>; Decl. —38° 12'

19.848	309.0	6.08	0.2	2½	370
19.872	309.5	5.91	0.9	2½	370
19.891	308.6	6.11	0.8	2	370
19.87	309.0	6.03	(9.3 ... 9.8)		F

h 5233; —83° 709; 8.6

A.R. 20<sup>h</sup> 52<sup>m</sup> 30<sup>s</sup>; Decl. —83° 46'

18.827	270.8	11.90	23.9	2	370
18.851	270.4	11.65	1.2	1½	370
18.854	270.2	12.05	0.9	2	370
18.84	270.5	11.87	(8.1 ... 12.9)		N

β 765; —35° 8955; 7.0

A.R. 20<sup>h</sup> 52<sup>m</sup> 50<sup>s</sup>; Decl. —35° 46'

20.653	129.1	2.00	22.4	2½	370
20.803	131.0	1.93	23.7	2	370
20.806	125.8	1.97	23.5	2	370
20.75	128.6	1.97	(7.3 ... 12.2)		M?

I 257; —76° 1472; 7.8

A.R. 20<sup>h</sup> 53<sup>m</sup> 58<sup>s</sup>; Decl. —76° 28'

18.712	297.5	1.52	22.5	2	370
18.733	297.6	1.52	22.0	2	370
18.747	296.4	1.75	0.2	2	475
18.73	297.2	1.60	(8.2 ... 8.8)		A?

h 5235 = h 5245; —84° 616; 7.6

A.R. 20<sup>h</sup> 54<sup>m</sup> 57<sup>s</sup>; Decl. —84° 49'

18.827	263.8	3.50	0.1	2	370
18.851	263.7	3.18	1.4	2	475
18.854	264.6	3.28	1.0	2	475
18.84	264.0	3.32	(8.4 ... 8.5)		F

h 5242; —32° 6282; 7.6

A.R. 20<sup>h</sup> 57<sup>m</sup> 32<sup>s</sup>; Decl. —32° 50'

18.836	264.6	31.89	23.5	1	370
18.865	265.1	31.92	0.3	2	370
18.85	264.9	31.91	(7.9 ... 13.2)		N

h 5248; —31° 6463; 10.6

A.R. 21<sup>h</sup> 3<sup>m</sup> 34<sup>s</sup>; Decl. —31° 11'

18.859	319.1	7.10	23.3	2	370
18.865	318.6	7.68	0.5	2	370
18.867	317.1	8.07	0.2	2	370
18.86	318.3	7.62	(11.5 ... 12.1)		N

h 5249; —38° 8214; 9.0

A.R. 21<sup>h</sup> 4<sup>m</sup> 10<sup>s</sup>; Decl. —38° 41'

19.845	329.0	19.25	0.2	2	370
19.848	329.4	19.12	0.3	2½	370
19.85	329.2	19.18	(8.5 ... 13.9)		N

β 251; —31° 6469; 7.6

A.R. 21<sup>h</sup> 4<sup>m</sup> 36<sup>s</sup>; Decl. —31° 6'

20.653	236.1	2.87	22.6	2½	370
20.803	234.0	2.87	23.8	2	370
20.806	234.2	3.00	23.7	2	370
20.75	234.8	2.91	(7.6 ... 9.8)		F

h 5253; —39° 8905; 7.6

A.R. 21<sup>h</sup> 6<sup>m</sup> 21<sup>s</sup>; Decl. —39° 6'

19.829	183.1	10.50	0.1	1½	370
19.845	182.7	10.46	0.3	2	370
19.84	182.9	10.48	(8.3 ... 9.3)		N

h 5254; —39° 8912 + 11; 8.4 + 9.2

A.R. 21<sup>h</sup> 7<sup>m</sup> 38<sup>s</sup>; Decl. —39° 58'

19.829	185.4	58.51	0.2	1½	370
19.845	185.2	58.36	0.4	2	370
19.84	185.3	58.43	(8.6 ... 9.2)		F?

\* h 5258; θ Indi; 4.3

A.R. 21<sup>h</sup> 10<sup>m</sup> 57<sup>s</sup>; Decl. —53° 58'

20.814	279.0	5.20	23.1	2½	370
20.839	279.5	5.17	23.2	2½	370
20.861	279.5	5.10	1.1	2½	370
20.84	279.3	5.16	(5.3 ... 7.6)		M

$h$  5263;  $-31^{\circ} 65'12''$ ; 9.0A.R.  $21^h 13^m 26^s$ ; Decl.  $-31^{\circ} 26'$ 

18.835	93.8	27.92	23.3	2	370
18.859	93.9	27.95	23.4	2	370
18.85	93.8	27.94	(8.0 ... 12.4)	N	

 $h$  5264;  $-35^{\circ} 90'52''$ ; 9.2A.R.  $21^h 14^m 35^s$ ; Decl.  $-35^{\circ} 32'$ 

19.859	58.5	19.08	0.7	$2\frac{1}{2}$	370
19.872	57.6	19.01	1.1	2	370
19.883	58.0	18.98	0.9	2	370
19.87	58.0	19.02	(8.8 ... 12.7)	A	

 $\beta$  766;  $0_2$  Microscopii; 5.9A.R.  $21^h 16^m 26^s$ ; Decl.  $-41^{\circ} 32'$ 

20.803	287.3	1.02	23.9	2	370
20.806	287.6	1.05	23.9	$2\frac{1}{2}$	370
20.814	285.2	0.89	23.4	$2\frac{1}{2}$	370
20.81	286.7	0.99	(7.1 ... 7.7)	20	

 $h$  5262;  $-80^{\circ} 10'17''$ ; 6.4A.R.  $21^h 16^m 43^s$ ; Decl.  $-80^{\circ} 35'$ 

18.753	93.9	24.59	0.2	$2\frac{1}{2}$	370
18.766	94.2	24.48	22.5	2	370
18.76	94.0	24.54	(6.5 ... 11.4)	F	

 $h$  5266;  $-31^{\circ} 65'26''$ ; 8.4A.R.  $21^h 17^m 14^s$ ; Decl.  $-31^{\circ} 38'$ 

18.835	268.5	12.85	23.5	$2\frac{1}{2}$	370
18.859	268.8	12.81	23.6	2	370
18.85	268.6	12.83	(8.4 ... 12.9)	R?	

I 1122;  $-39^{\circ} 89'49''$ ; 8.4A.R.  $21^h 19^m 58^s$ ; Decl.  $-39^{\circ} 32'$ 

19.826	301.9	4.52	23.6	$2\frac{1}{2}$	370
19.829	301.2	4.30	0.4	$1\frac{1}{2}$	370
19.845	301.6	4.21	0.5	2	370
19.83	301.6	4.34	(9.4 ... 9.4)	142	

 $h$  5261 = Rus 333;  $-86^{\circ} 39'6''$ ; 8.1A.R.  $21^h 21^m 49^s$ ; Decl.  $-86^{\circ} 24'$ 

18.851	201.2	5.10	0.9	2	370
18.854	201.1	5.02	0.4	2	475
18.903	201.7	5.03	0.8	2	370
18.87	201.3	5.05	(8.8 ... 9.1)	F?	

 $h$  5274;  $-35^{\circ} 90'68'' + 9''$ ;  $9.8 + 9.8$ A.R.  $21^h 22^m 50^s$ ; Decl.  $-35^{\circ} 21'$ 

19.758	139.7	22.87	0.1	2	370
19.859	140.1	22.95	0.9	2	370
19.81	139.9	22.91	(10.2 ... 10.3)	R?	

 $h$  5275;  $-37^{\circ} 90'48''$ ; 6.6A.R.  $21^h 23^m 16^s$ ; Decl.  $-37^{\circ} 6'$ 

19.758	200.6	40.98	0.2	2	370
19.859	200.5	40.65	1.0	$1\frac{1}{2}$	370
19.872	201.1	40.89	1.3	2	370
19.83	200.7	40.84	(7.1 ... 11.3)	N	

 $h$  5279; Cód  $-32^{\circ} 16'63''$ ; 10A.R.  $21^h 26^m 38^s$ ; Decl.  $-32^{\circ} 55'$ 

18.835	290.0	11.76	23.7	2	370
18.859	290.8	11.62	0.3	$1\frac{1}{2}$	370
18.85	290.4	11.69	(11.2 ... 11.6)	N	

 $h$  5280; Cód  $-31^{\circ} 18'35''$ ; 9.2A.R.  $21^h 27^m 44^s$ ; Decl.  $-31^{\circ} 5'$ 

18.835	333.2	10.17	23.9	$2\frac{1}{2}$	370
18.859	333.2	10.29	0.5	2	370
18.85	333.2	10.23	(10.4 ... 12.2)	N	

 $h$  5278;  $\lambda$  Octantis; 6.2A.R.  $21^h 31^m 30^s$ ; Decl.  $-83^{\circ} 17'$ 

18.827	71.3	3.11	0.3	2	370
18.851	71.6	3.16	1.6	2	475
18.854	72.3	3.22	1.1	2	475
18.84	71.7	3.16	(5.9 ... 7.8)	A	

 $h$  5283;  $-39^{\circ} 89'98''$ ; 10.4A.R.  $21^h 31^m 32^s$ ; Decl.  $-39^{\circ} 2'$ 

19.826	267.9	9.92	23.8	2	370
19.845	267.1	9.89	0.5	2	370
19.848	268.1	9.89	0.4	$2\frac{1}{2}$	370
19.84	267.7	9.90	(10.9 ... 11.0)	142	

 $h$  5285;  $-30^{\circ} 65'53''$ ; 8.4A.R.  $21^h 32^m 8^s$ ; Decl.  $-30^{\circ} 2'$ 

18.835	291.7	10.18	0.0	$2\frac{1}{2}$	370
18.859	291.9	10.32	0.6	$2\frac{1}{2}$	370
18.85	291.8	10.25	(8.8 ... 10.9)	F?	

 $h$  5288;  $-38^{\circ} 82'97''$ ; 7.3A.R.  $21^h 34^m 49^s$ ; Decl.  $-38^{\circ} 30'$ 

19.826	60.4	19.69	23.9	2	370
19.845	60.5	19.91	0.6	2	370
19.84	60.4	19.80	(7.9 ... 9.2)	20	

*h* 5293; —32° 6420; 8.7  
 A.R. 21<sup>h</sup> 37<sup>m</sup> 51<sup>s</sup>; Decl. —32° 13'

18.835	249.7	19.38	0.2	2	370
18.859	250.6	19.50	0.8	2	370
18.85	250.1	19.44	(8.1 ... 13.6)		N

AC; C = 14.8

18.835	119.1	14.56	0.3	2	370
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*h* 5289; —81° 977 + 8; 9.4 + 9.8  
 A.R. 21<sup>h</sup> 38<sup>m</sup> 0<sup>s</sup>; Decl. —81° 11'

18.753	49.6	17.14	0.3	2½	370
18.766	48.6	17.18	22.6	2	370
18.76	49.1	17.16	(10.2 ... 11.3)		D?

*h* 5296; 0 Piscis Aus.; 5.5  
 A.R. 21<sup>h</sup> 40<sup>m</sup> 24<sup>s</sup>; Decl. —31° 28'

18.835	339.1	35.41	0.5	2	370
18.859	339.2	35.68	1.0	1½	370
18.865	339.4	35.44	0.6	2	370
18.85	339.2	35.51	(5.2 ... 11.1)		F?

*h* 5292; —85° 531; 9.0  
 A.R. 21<sup>h</sup> 41<sup>m</sup> 58<sup>s</sup>; Decl. —85° 20'

18.851	156.1	5.49	1.8	1½	370
18.854	154.5	5.56	1.3	2	475
18.903	152.2	5.62	1.2	2	370
18.87	154.3	5.56	(9.0 ... 12.1)		F?

*h* 5299; —40° 9617 + 18; 9.0 + 9.0  
 A.R. 21<sup>h</sup> 46<sup>m</sup> 38<sup>s</sup>; Decl. —40° 32'

19.826	59.3	33.35	0.1	2	370
19.845	59.6	33.10	0.7	2½	370
19.848	59.9	33.24	0.5	2½	370
19.84	59.6	33.23	(8.7 ... 8.7)		20

*h* 5304; Cód —31° 18535; 9.3  
 A.R. 21<sup>h</sup> 47<sup>m</sup> 59<sup>s</sup>; Decl. —31° 20'

18.835	255.0	9.48	0.6	2	370
18.865	254.8	9.24	0.8	2	370
18.867	254.4	9.22	0.4	2	370
18.86	254.7	9.31	(10.5 ... 11.2)		N

*h* 5307; —31° 6603; 8.2  
 A.R. 21<sup>h</sup> 48<sup>m</sup> 43<sup>s</sup>; Decl. —31° 31'

18.835	160.6	33.32	0.8	2	370
18.865	160.9	33.21	0.9	2	370
18.85	160.7	33.26	(7.9 ... 11.1)		N

(Sigue Continued.)

BC

18.835	158.7	20.08	0.9	2	370
18.865	159.8	20.33	1.0	2	370
18.85	159.2	20.20	(11.1 ... 12.5)		N

*h* 5305; —41° 9730 + 29; 9.4 + 9.4  
 A.R. 21<sup>h</sup> 48<sup>m</sup> 49<sup>s</sup>; Decl. —41° 37'

19.826	243.0	20.00	0.2	2	370
19.845	243.7	19.71	0.8	2½	370
19.848	242.6	19.94	0.6	2½	370
19.84	243.1	19.88	(9.2 ... 9.4)		F

β 768; —37° 9126; 5.7  
 A.R. 21<sup>h</sup> 48<sup>m</sup> 51<sup>s</sup>; Decl. —37° 51'

20.814	Sin compañera	2½	370
20.831	<0"3 si es doble	3	650
20.861	Sin compañera	3	370

*h* 5310; Anon.  
 A.R. 21<sup>h</sup> 53<sup>m</sup>; Decl. —78° 19'

18.753	247.0	8.69	0.5	2	370
18.766	245.6	8.85	0.4	2	370
18.821	247.2	8.77	0.8	2	370
18.78	246.9	8.77	(11.0 ... 12.3)		N

*h* 5315; Cód —38° 14878; 9.3  
 A.R. 21<sup>h</sup> 58<sup>m</sup> 17<sup>s</sup>; Decl. —38° 18'

19.826	149.9	23.57	0.5	2	370
19.845	150.3	23.20	0.9	2½	370
19.848	150.1	23.15	0.8	2½	370
19.84	150.1	23.31	(9.9 ... 10.0)		F?

β 769; —35° 9193; 6.8  
 A.R. 22<sup>h</sup> 4<sup>m</sup> 20<sup>s</sup>; Decl. —35° 5'

19.706	357.4	0.76	1.0	3	650
19.826	360.9	0.93	0.8	2	475
19.845	359.5	0.87	1.2	2	475
19.79	359.3	0.85	(7.0 ... 8.1)		D

*h* 5319; —38° 8368; 7.2  
 A.R. 22<sup>h</sup> 4<sup>m</sup> 37<sup>s</sup>; Decl. —38° 55'

19.826	302.3	2.51	0.6	2	370
19.845	303.2	2.53	1.0	2½	475
19.848	301.6	2.40	0.9	2½	650
19.84	302.4	2.48	(8.0 ... 8.0)		D

$h$  5318;  $-81^\circ 998$ ; 8.4A.R.  $22^h 6^m 44^s$ ; Decl.  $-81^\circ 5'$ 

18.753	299.9	9.39	0.6	2½	370
18.766	299.6	9.40	0.5	2	370
18.821	299.7	9.45	1.1	2	370
18.78	299.7	9.41	(9.2 ... 9.3)		F

 $h$  5326;  $-37^\circ 9180$ ; 9.1A.R.  $22^h 12^m 37^s$ ; Decl.  $-37^\circ 19'$ 

19.706	303.4	6.70	1.2	3	370
19.758	303.4	6.81	0.4	2	370
19.826	302.4	7.13	0.9	2	370
19.76	303.1	6.88	(10.2 ... 10.4)		F

 $h$  5330;  $-40^\circ 9688$ ; 9.3A.R.  $22^h 16^m 42^s$ ; Decl.  $-40^\circ 21'$ 

19.826	274.5	5.55	1.2	1½	370
19.845	274.0	5.50	1.3	2	370
19.848	273.6	5.55	1.0	2½	370
19.84	274.0	5.53	(9.8 ... 10.4)		F

 $\Delta$  239;  $\epsilon_2$  Gruis;  $5.6 + 8.8$ A.R.  $22^h 22^m 17^s$ ; Decl.  $-44^\circ 33'$ 

19.848	212.4	60.95	1.2	2	370
19.872	212.3	60.77	1.5	2	370
19.86	212.4	60.86	(5.3 ... 9.2)		F

 $\Delta$  240;  $\beta$  Piscis Aus.; 4.5A.R.  $22^h 24^m 24^s$ ; Decl.  $-32^\circ 59'$ 

18.835	172.2	30.35	1.0	2	370
18.865	172.1	30.40	1.2	2	370
18.85	172.2	30.38	(4.4 ... 8.6)		F

 $h$  5343;  $-42^\circ 9460$ ; 8.1A.R.  $22^h 28^m 6^s$ ; Decl.  $-42^\circ 15'$ 

19.845	49.7	5.23	1.6	2½	370
19.848	49.9	5.21	1.3	2	370
19.872	50.4	5.29	1.8	2½	370
19.86	50.0	5.24	(9.4 ... 9.8)		N

 $h$  5344;  $-39^\circ 9147$ ; 7.4A.R.  $22^h 28^m 20^s$ ; Decl.  $-39^\circ 22'$ 

19.845	168.0	5.25	1.4	2	370
19.848	168.5	5.20	1.4	2	370
19.872	168.5	5.26	2.1	2½	370
19.86	168.3	5.24	(8.1 ... 10.3)		F

 $\Delta$  241;  $-32^\circ 6516 + 17$ ;  $7.2 + 8.4$ A.R.  $22^h 29^m 34^s$ ; Decl.  $-32^\circ 18'$ 

18.835	30.9	89.54	1.1	2	370
18.865	31.2	89.50	1.4	2	370
18.85	31.1	89.52	(6.1 ... 7.9)		F

$Aa = h$  5346; Ver la nota 162

 $\beta$  771;  $-41^\circ 9812$ ; 6.0A.R.  $22^h 29^m 40^s$ ; Decl.  $-41^\circ 14'$ 

20.803	265.2	2.89	0.0	2	370
20.806	264.2	3.11	0.5	2½	370
20.831	263.9	2.96	1.2	3	370
20.81	264.4	2.99	(6.3 ... 11.3)		M

 $h$  5347;  $-35^\circ 9275$ ; 9.1A.R.  $22^h 30^m 25^s$ ; Decl.  $-35^\circ 0'$ 

19.706	9.1	11.23	1.4	2½	370
19.758	8.6	11.38	0.5	2	370
19.73	8.9	11.30	(9.0 ... 11.9)		N

 $h$  5353;  $-80^\circ 1044$ ; 9.3A.R.  $22^h 33^m 43^s$ ; Decl.  $-80^\circ 31'$ 

18.753	177.1	17.17	1.0	2½	370
18.766	178.2	16.68	0.6	1½	370
18.821	176.7	16.79	1.2	2	370
18.78	177.3	16.88	(9.6 ... 10.6)		226

AC

18.753	239.7	30.80	0.9	2½	370
18.766	239.5	30.97	0.7	1½	370
18.76	239.6	30.88	(9.6 ... 10.8)		N

 $h$  5363;  $-35^\circ 9306$ ; 10.2A.R.  $22^h 40^m 44^s$ ; Decl.  $-35^\circ 43'$ 

19.755	293.2	11.48	1.4	2½	370
19.758	292.6	11.63	0.7	2½	370
19.76	292.9	11.55	(9.5 ... 12.3)		N

 $h$  5448;  $-38^\circ 8444$ ; 9.5A.R.  $22^h 41^m 5^s$ ; Decl.  $-38^\circ 42'$ 

19.845	196.2	20.31	1.7	2	370
19.848	195.7	20.22	1.5	2	370
19.85	196.0	20.26	(8.8 ... 13.6)		N

 $h$  5365;  $-36^\circ 9661$ ; 7.4A.R.  $22^h 44^m 43^s$ ; Decl.  $-36^\circ 33'$ 

19.755	278.6	4.82	1.5	2½	370
19.758	277.5	5.03	0.8	2	370
19.788	277.2	4.79	2.1	2	370
19.77	277.8	4.88	(7.4 ... 12.4)		F

(Sigue Continued.)



AC; C = 11.0

19.758 35.2 55.61 0.9 2 370

*h* 5367;  $\gamma$  Piscis Aus.; 4.5

A.R. 22<sup>h</sup> 45<sup>m</sup> 34<sup>s</sup>; Decl. -33° 32'

18.835	267.4	4.20	1.4	2½	370
18.865	268.7	4.43	1.7	2	370
18.867	268.3	4.35	0.6	2	370
18.86	268.1	4.33	(4.4 ... 8.1) C		

*h* 5350; -88° 201; 9.2

A.R. 22<sup>h</sup> 46<sup>m</sup> 2<sup>s</sup>; Decl. -88° 38'

18.854	102.4	25.64	0.7	2½	370
18.903	101.5	25.53	1.0	1½	370
18.88	102.0	25.59	(8.5 ... 12.5) N		

$\beta$  772;  $\epsilon$  Piscis Aus.; 5.8

A.R. 22<sup>h</sup> 49<sup>m</sup> 1<sup>s</sup>; Decl. -33° 12'

20.803	241.7	5.33	0.3	2	370
20.806	241.9	5.52	0.7	2	370
20.823	242.2	5.71	2.2	2	370
20.81	241.9	5.52	(4.7 ... 11.5) M?		

*h* 5368; -85° 549; 8.9

A.R. 22<sup>h</sup> 49<sup>m</sup> 33<sup>s</sup>; Decl. -85° 12'

18.851	123.8	8.22	1.9	2	370
18.854	123.4	8.10	1.5	2½	370
18.903	122.9	8.02	1.4	2	370
18.87	123.4	8.11	(9.8 ... 9.9) F		

$\beta$  1011; -37° 9297; 7.0

A.R. 22<sup>h</sup> 55<sup>m</sup> 37<sup>s</sup>; Decl. -37° 6'

20.803	296.5	2.15	0.1	2	370
20.806	300.6	2.29	0.9	2	370
20.823	300.8	2.33	2.4	2	370
20.81	299.3	2.26	(7.2Y ... 3.3b) F		

*h* 5378; -83° 746 + 5; 9.3 + 9.3

A.R. 22<sup>h</sup> 57<sup>m</sup> 25<sup>s</sup>; Decl. -83° 4'

18.851	344.2	39.91	2.1	2	370
18.854	343.9	39.95	1.7	2	370
18.85	344.0	39.93	(9.6 ... 9.9) F		

\* J 238;  $\theta$  Gruis; 5.6

A.R. 22<sup>h</sup> 59<sup>m</sup> 50<sup>s</sup>; Decl. -44° 12'

20.806	41.6	2.11	1.6	2	370
20.831	42.7	1.95	1.4	2½	370
20.839	37.8	1.78	23.4	2	370
20.861	39.8	1.92	1.5	3	370
20.83	40.5	1.94	(4.6 ... 7.0) P		

$\beta$  773;  $\nu$  Gruis; 6.2

A.R. 22<sup>h</sup> 59<sup>m</sup> 56<sup>s</sup>; Decl. -39° 34'

20.831	213.9	1.42	1.5	3	370
20.861	211.2	1.07	1.4	3	370
20.863	211.9	1.13	23.7	3½	650
20.85	212.3	1.21	(5.8 ... 9.3) N!		

*h* 5383; Cód -35° 15673; 9.4

A.R. 23<sup>h</sup> 2<sup>m</sup> 22<sup>s</sup>; Decl. -35° 14'

19.755	141.1	10.09	1.9	3	370
19.758	140.6	9.99	1.1	2	370
19.76	140.8	10.04	(10.1 ... 11.2) 227		

*h* 5385; -79° 1229; 8.4

A.R. 23<sup>h</sup> 3<sup>m</sup> 52<sup>s</sup>; Decl. -79° 1'

18.753	325.5	39.93	1.2	1½	370
18.767	325.0	40.42	0.9	1½	370
18.821	324.8	39.98	1.6	2	370
18.78	325.1	40.10	(8.4 ... 12.0) N		

*h* 5387; -41° 9884; 7.5

A.R. 23<sup>h</sup> 6<sup>m</sup> 36<sup>s</sup>; Decl. -41° 37'

19.788	276.9	8.13	2.2	2	370
19.826	277.4	8.09	1.4	1½	370
19.845	276.7	8.17	1.9	2	370
19.82	277.0	8.13	(8.3 ... 9.7) F		

*h* 5388; -81° 1029; 7.6

A.R. 23<sup>h</sup> 7<sup>m</sup> 59<sup>s</sup>; Decl. -81° 6'

18.767	120.2	13.87	1.0	1½	370
18.821	119.5	13.70	1.9	2	370
18.79	119.8	13.78	(8.2 ... 12.1) D?		

*h* 5391; -36° 9724; 9.8

A.R. 23<sup>h</sup> 11<sup>m</sup> 7<sup>s</sup>; Decl. -36° 44'

19.755	338.7	15.17	2.1	3	370
19.758	337.7	15.01	1.3	2½	370
19.76	338.2	15.09	(10.1 ... 10.8) N		

*h* 5395; -38° 8518; 8.7

A.R. 23<sup>h</sup> 14<sup>m</sup> 9<sup>s</sup>; Decl. -38° 22'

19.788	225.5	3.60	2.4	2½	370
19.826	224.6	3.69	1.5	2	370
19.845	226.6	3.62	2.0	2	370
19.82	225.6	3.64	(8.9 ... 9.7) F?		

*h* 5399; Anon.A.R. 23<sup>h</sup> 21<sup>m</sup> 0; Decl. -81° 48'

18.767	270.6	18.62	1.2	1½	370
18.821	270.4	18.62	2.2	2	370
18.79	270.5	18.62	(10.8 ... 11.1)		N

*λ* 490; -35° 9406; 8.2A.R. 23<sup>h</sup> 27<sup>m</sup> 11<sup>s</sup>; Decl. -35° 12'

19.883	225.8	8.73	1.1	2½	370
19.891	226.6	8.89	1.6	2	370
19.89	226.2	8.81	(8.0 ... 12.8)		F

*h* 5404; Cód -30° 19607; 9.5A.R. 23<sup>h</sup> 28<sup>m</sup> 20<sup>s</sup>; Decl. -30° 3'

18.835	303.0	15.94	1.5	2	370
18.865	303.3	16.00	1.9	2	370
18.85	303.2	15.97	(10.4 ... 11.3)		N

*h* 5405; -37° 9375; 10.0A.R. 23<sup>h</sup> 28<sup>m</sup> 52<sup>s</sup>; Decl. -37° 34'

19.755	75.7	10.83	2.5	2½	370
19.758	74.3	10.95	1.5	2	370
19.76	75.0	10.89	(10.5 ... 11.2)		N

*h* 5406; -80° 1070; 9.5A.R. 23<sup>h</sup> 29<sup>m</sup> 31<sup>s</sup>; Decl. -80° 45'

18.767	356.2	25.65	1.5	1½	370
18.851	354.0	25.97	2.3	1½	370
18.854	355.2	25.75	1.9	2	370
18.82	355.1	25.79	(9.8 ... 13.0)		N

## AC

18.767	41.1	31.91	1.4	1½	370
18.851	40.7	31.45	2.5	1½	370
18.854	41.6	31.79	2.0	2	370
18.82	41.1	31.72	(9.8 ... 13.0)		N

\* *h* 5409; Anon.A.R. 23<sup>h</sup> 30<sup>m</sup> 11<sup>s</sup>; Decl. -71° 30'

20.924	50.6	7.57	2.1	2½	370
20.937	51.4	7.62	2.2	2	370
20.93	51.0	7.59	(10.4 ... 11.0)		R

## I 693; -37° 9378; 7.2

A.R. 23<sup>h</sup> 30<sup>m</sup> 18<sup>s</sup>; Decl. -37° 29'

19.755	12.0	0.89	2.4	2½	650
19.848	12.4	0.73	1.7	2½	475
19.883	5.9	0.83	1.3	2½	475
19.891	9.3	0.80	1.4	2	475
19.84	9.9	0.81	(8.0 ... 8.9)		P

## Howe = β 775 = β 1012; -32° 6630; 7.3

A.R. 23<sup>h</sup> 30<sup>m</sup> 28<sup>s</sup>; Decl. -32° 34'

20.803	251.4	5.70	0.5	2	370
20.823	251.3	5.65	2.5	2	370
20.831	251.2	5.54	1.7	3	370
20.82	251.3	5.63	(6.90 ... 11.3b)		F

*h* 5412; -31° 6809; 8.8:A.R. 23<sup>h</sup> 32<sup>m</sup> 0<sup>s</sup>; Decl. -31° 20'

18.835	50.7	16.53	1.7	2½	370
18.865	50.6	16.71	2.1	2	370
18.85	50.7	16.62	(9.5 ... 10.5)		N

## G 286; -71° 2769; 8.0

A.R. 23<sup>h</sup> 32<sup>m</sup> 49<sup>s</sup>; Decl. -71° 48'

20.924	145.3	7.66	2.2	2½	370
20.937	145.1	7.57	2.4	2	370
20.93	145.2	7.62	(8.5 ... 9.6)		F

*h* 5414; -78° 1479; 8.6A.R. 23<sup>h</sup> 36<sup>m</sup> 4<sup>s</sup>; Decl. -78° 30'

18.767	259.3	7.71	1.7	1½	370
18.851	259.0	7.93	2.7	2	370
18.854	259.4	7.74	2.1	2½	370
18.82	259.2	7.79	(8.9 ... 10.7)		F

*h* 5429; -30° 6803 + 2; 8.2 + 10.4A.R. 23<sup>h</sup> 47<sup>m</sup> 15<sup>s</sup>; Decl. -30° 6'

18.835	224.3	27.53	1.8	2½	370
18.865	224.5	27.33	2.3	2	370
18.85	224.4	27.43	(7.9 ... 10.8)		N

STARS NORTH OF  $-30^\circ$   
ESTRELLAS AL NORTE DE  $-30^\circ$

*h* 3351; Cód  $-23^\circ 32'$ ; 9.4

A.R.  $0^h 5^m 0^s$ ; Decl.  $-23^\circ 19'$

19.965	136.4	11.84	3.1	$1\frac{1}{2}$	370
20.061	—	11.67	4.4	$1\frac{1}{2}$	370
20.064	135.1	11.54	4.5	2	370
20.067	135.9	11.87	4.8	$1\frac{1}{2}$	370
20.03	135.8	11.73	(11.1 ... 11.3)		

Hd 6; Cód  $-23^\circ 59'$ ; 9.8

A.R.  $0^h 9^m 8^s$ ; Decl.  $-23^\circ 38'$

20.064	262.2	7.56	4.7	$1\frac{1}{2}$	370
20.067	263.2	7.20	5.0	1	370
20.075	263.0	6.96	4.9	2	370
20.07	262.8	7.24	(10.7 ... 11.3)		228

BC; C = 13.2

20.075	198.2	21.76	5.0	2	370
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*h* 3359; Cód  $-23^\circ 104'$ ; 9.0

A.R.  $0^h 14^m 52^s$ ; Decl.  $-23^\circ 16'$

19.894	274.7	17.40	2.6	2	370
19.903	274.8	17.17	3.0	2	370
19.908	274.3	16.88	2.9	3	370
19.90	274.6	17.15	(10.2 ... 10.4)		

*h* 1957 = *h* 3429;  $-23^\circ 24'$ ; 7.2

A.R.  $0^h 15^m 48^s$ ; Decl.  $-23^\circ 40'$

19.894	21.8	6.17	2.9	2	370
19.903	22.7	6.15	3.2	2	370
19.908	22.9	6.22	3.0	3	370
19.90	22.5	6.18	(8.1 ... 9.7)		F

**175;** *h* 3431

A.R.  $0^h 17^m 4^s$ ; Decl.  $-5^\circ 14'$

19.935	90.9	10.25	2.6	2	370
19.938	91.1	10.40	2.4	$3\frac{1}{2}$	370
19.94	91.0	10.33	(9.5 ... 12.2)		

**216;** *h* 1968

A.R.  $0^h 21^m 33^s$ ; Decl.  $-17^\circ 4'$

19.935	218.1	6.32	3.1	2	370
19.938	217.8	6.23	2.5	$3\frac{1}{2}$	370
19.941	217.1	6.16	2.1	3	370
19.94	217.7	6.24	(7.9 ... 11.4)		R

*h* 1969; Cód  $-23^\circ 161'$ ; 10

A.R.  $0^h 21^m 44^s$ ; Decl.  $-23^\circ 0'$

19.965	42.7	12.94	3.3	$1\frac{1}{2}$	370
20.056	44.0	13.15	4.5	2	370
20.01	43.4	13.05	(12.0 ... 12.4)		

*h* 1977 = *h* 3440;  $-23^\circ 37'$ ; 9.4

A.R.  $0^h 23^m 35^s$ ; Decl.  $-23^\circ 51'$

19.965	295.6	12.76	3.3	$1\frac{1}{2}$	370
20.056	295.6	12.50	4.6	2	370
20.01	295.6	12.63	(9.2 ... 10.6)		

*h* 3442;  $-26^\circ 37'$ ; 7.4

A.R.  $0^h 26^m 40^s$ ; Decl.  $-26^\circ 2'$

19.903	200.4	24.45	3.3	$1\frac{1}{2}$	370
19.908	200.4	24.38	3.1	3	370
19.91	200.4	24.41	(6.9 ... 12.2)		

*h* 3377;  $-26^\circ 39'$ ; 8.1

19.908	58.3	19.48	3.2	3	370
19.916	58.2	19.50	3.0	2	370
19.91	58.3	19.49	(7.4R ... 9.4)		D

*h* 1988; Cód  $-23^\circ 207'$ ; 9.5

A.R.  $0^h 28^m 50^s$ ; Decl.  $-23^\circ 45'$

19.965	199.7	22.69	3.4	$1\frac{1}{2}$	370
20.056	199.6	23.00	4.8	2	370
20.01	199.6	22.85	(10.4 ... 11.4)		f

*h* 3379;  $-28^{\circ} 43'$ ; 7.8A.R.  $0^{\text{h}} 30^{\text{m}} 47^{\text{s}}$ ; Decl.  $-28^{\circ} 5'$ 

19.908	231.9	14.72	3.3	3	370
19.916	231.9	14.73	3.1	2	370
19.91	231.9	14.72	(7.7 ... 12.1)	F	

*h* 1990;  $-22^{\circ} 57'$ ; 10.0A.R.  $0^{\text{h}} 32^{\text{m}} 0^{\text{s}}$ ; Decl.  $-22^{\circ} 15'$ 

19.965	344.5	19.70	3.5	$1\frac{1}{2}$	370
20.064	346.0	20.14	4.9	2	370
20.075	344.2	19.82	5.2	2	370
20.03	344.9	19.89	(10.5 ... 11.8)		

*Hu* 1205;  $-19^{\circ} 93'$ ; 8.7A.R.  $0^{\text{h}} 45^{\text{m}} 34^{\text{s}}$ ; Decl.  $-19^{\circ} 10'$ 

20.831	106.9	0.49	3.4	$3\frac{1}{2}$	650
20.864	111.5	0.46	0.8	$3\frac{1}{2}$	650
20.877	99.6	0.37	0.8	3	650
20.09	107.6	0.46	(9.5 ... 9.7)	N	

*h* 2001; Cód  $-22^{\circ} 309'$ ; 9.6A.R.  $0^{\text{h}} 50^{\text{m}} 3^{\text{s}}$ ; Decl.  $-22^{\circ} 42'$ 

20.056	47.8	17.04	5.0	2	370
20.064	46.7	17.22	5.3	$1\frac{1}{2}$	370
20.075	46.8	17.36	5.3	2	370
20.06	47.1	17.21	(11.3 ... 12.4)		

*h* 2007;  $-25^{\circ} 101'$ ; 9.6A.R.  $0^{\text{h}} 53^{\text{m}} 18^{\text{s}}$ ; Decl.  $-25^{\circ} 36'$ 

20.056	197.1	29.15	5.2	$1\frac{1}{2}$	370
20.075	197.8	28.55	5.5	2	370
20.078	197.9	28.56	4.9	$2\frac{1}{2}$	370
20.07	197.6	28.75	(8.9 ... 11.7)		

*h* 3419; Cód  $-26^{\circ} 363'$ ; 9.4A.R.  $1^{\text{h}} 1^{\text{m}} 50^{\text{s}}$ ; Decl.  $-26^{\circ} 39'$ 

19.908	326.6	11.45	3.4	3	370
19.922	326.1	11.70	3.2	2	370
19.941	327.8	11.54	2.3	$2\frac{1}{2}$	370
19.92	326.8	11.56	(10.4 ... 11.9)		

*Hd* 48 = *Hd* 47;  $-23^{\circ} 160'$ ; 7.9A.R.  $1^{\text{h}} 12^{\text{m}} 54^{\text{s}}$ ; Decl.  $-23^{\circ} 27'$ 

20.056	61.6	9.67	5.3	2	370
20.064	61.1	9.96	5.6	$1\frac{1}{2}$	370
20.075	61.2	9.84	5.7	$2\frac{1}{2}$	370
20.06	61.3	9.82	(8.6 ... 10.2)	229	

*h* 3425; Cód  $-28^{\circ} 401'$ ; 9.6A.R.  $1^{\text{h}} 13^{\text{m}} 27^{\text{s}}$ ; Decl.  $-28^{\circ} 8'$ 

20.075	254.4	7.47	5.9	2	370
20.078	255.2	7.45	5.1	$2\frac{1}{2}$	370
20.091	254.1	7.32	5.2	$2\frac{1}{2}$	370
20.08	254.6	7.41	(10.7 ... 11.2)		

 $\lambda$  13;  $-24^{\circ} 155'$ ; 8.4A.R.  $1^{\text{h}} 16^{\text{m}} 2^{\text{s}}$ ; Decl.  $-24^{\circ} 45'$ 

20.091	153.0	0.64	5.6	$2\frac{1}{2}$	650
20.094	155.2	0.61	5.6	$2\frac{1}{2}$	475
20.097	151.5	0.63	4.9	$2\frac{1}{2}$	475
20.09	153.2	0.63	(8.6 ... 8.8)	M	

*h* 2040; Cód  $-26^{\circ} 445'$ ; 9.4A.R.  $1^{\text{h}} 16^{\text{m}} 8^{\text{s}}$ ; Decl.  $-26^{\circ} 22'$ 

20.078	2.6	14.52	5.3	$2\frac{1}{2}$	370
20.091	2.5	14.54	5.4	$2\frac{1}{2}$	370
20.08	2.6	14.53	(11.2 ... 11.4)		

## AC

20.078	257.4	32.39	5.4	2	370
20.094	257.9	32.78	5.5	2	370
20.09	257.7	32.58	(11.2 ... 11.5)		

**772 (224);** *h* 3437 = *h* 3368A.R.  $1^{\text{h}} 16^{\text{m}} 31^{\text{s}}$ ; Decl.  $-17^{\circ} 53'$ 

19.935	247.7	12.16	3.5	$1\frac{1}{2}$	370
19.938	247.8	12.06	2.6	$3\frac{1}{2}$	370
19.94	247.8	12.11	(7.4 ... 9.6)	230	

*h* 2060;  $-24^{\circ} 174'$ ; 10.2A.R.  $1^{\text{h}} 28^{\text{m}} 59^{\text{s}}$ ; Decl.  $-24^{\circ} 44'$ 

20.078	94.6	27.27	5.7	2	370
20.091	94.1	27.70	5.7	$2\frac{1}{2}$	370
20.094	94.8	26.93	5.7	2	370
20.09	94.5	27.30	(10.6 ... 12.9)		

**864 (358);** *h* 2067 = *h* 3380A.R.  $1^{\text{h}} 33^{\text{m}} 33^{\text{s}}$ ; Decl.  $-18^{\circ} 24'$ 

19.935	92.1	32.87	3.7	$1\frac{1}{2}$	370
19.941	91.4	33.64	3.3	$2\frac{1}{2}$	370
19.963	91.3	33.39	3.3	2	370
19.95	91.6	33.63	(7.3 ... 13.2)	230	

*h* 2076;  $-25^{\circ} 192'$ ; 9.8A.R.  $1^{\text{h}} 35^{\text{m}} 53^{\text{s}}$ ; Decl.  $-25^{\circ} 4'$ 

20.078	289.4	7.95	5.9	$2\frac{1}{2}$	370
20.091	289.0	7.94	5.8	$2\frac{1}{2}$	370
20.094	288.4	8.06	5.9	$2\frac{1}{2}$	370
20.09	288.9	7.98	(10.3 ... 10.5)		

**901; h 3455**

A.R. 1<sup>h</sup> 37<sup>m</sup> 31<sup>s</sup>; Decl. -18° 13'

19.935	73.9	24.00	3.8	1½	370
19.938	73.7	23.74	2.7	3½	370
19.941	73.7	23.88	3.5	2½	370
19.94	73.8	23.87	(9.2 ... 9.3) F		

**h 3459 = h 3394; -20° 213 + 14; 9.0 + 9.6**

A.R. 1<sup>h</sup> 39<sup>m</sup> 25<sup>s</sup>; Decl. -20° 39'

19.941	89.2	19.69	3.7	2½	370
19.963	89.2	19.70	3.4	2½	370
19.95	89.2	19.70	(9.2 ... 10.0) 230		

**h 3470; -23° 213; 9.4**

A.R. 1<sup>h</sup> 45<sup>m</sup> 14<sup>s</sup>; Decl. -23° 14'

19.905	298.6	10.41	3.5	2½	370
19.908	298.6	10.29	3.8	3	370
19.91	298.6	10.35	(10.0 ... 10.6)		

**I 1101; -28° 164; 8.0**

A.R. 1<sup>h</sup> 46<sup>m</sup> 43<sup>s</sup>; Decl. -28° 21'

20.896	353.0	1.33	1.6	3	370
20.905	352.1	1.43	2.3	3½	370
20.987	355.7	1.60	3.8	2	370
21.017	358.9	1.16	4.9	2	370
20.95	354.9	1.38	(8.1 ... 10.6) 23		

**h 3472; -28° 165; 9.0**

A.R. 1<sup>h</sup> 47<sup>m</sup> 28<sup>s</sup>; Decl. -28° 40'

19.905	238.3	6.63	3.4	3	370
19.908	238.1	6.50	3.6	3	370
19.922	238.4	6.50	3.3	2	370
19.91	238.3	6.54	(9.8 ... 10.1) 150		

**h 2098; Cód -22° 634; 9.7**

A.R. 1<sup>h</sup> 49<sup>m</sup> 2<sup>s</sup>; Decl. -22° 8'

20.064	337.6	21.69	5.9	1½	370
20.078	337.5	21.81	6.2	2	370
20.07	337.5	21.75	(11.4 ... 12.1)		

**1053; h 3476**

A.R. 1<sup>h</sup> 54<sup>m</sup> 29<sup>s</sup>; Decl. -9° 6'

19.941	194.3	61.81	3.9	2½	370
19.963	194.4	62.02	3.5	2	370
19.95	194.4	61.91	(6.0 ... 10.7) 72		

**h 2106; -20° 232; 9.0**

A.R. 1<sup>h</sup> 56<sup>m</sup> 55<sup>s</sup>; Decl. -20° 54'

20.064	68.0	27.38	6.2	2	370
20.078	67.9	27.65	6.4	2	370
20.07	68.0	27.52	(10.2 ... 11.8)		

**h 2114; Anon.**

A.R. 2<sup>h</sup> 1<sup>m</sup> 54<sup>s</sup>; Decl. -26° 1'

20.100	288	12.4	5.5	2½	370
20.110	294	11.5	5.5	1½	370
20.116	294	12.4	5.7	2½	370
20.11	292	12.1	(13.3 ... Neb)		

**h 3498; -28° 219; 7.4**

A.R. 2<sup>h</sup> 16<sup>m</sup> 43<sup>s</sup>; Decl. -28° 25'

19.93	Sin compañera				20
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**h 3500; -21° 230 + 29; 8.6 + 8.3**

A.R. 2<sup>h</sup> 20<sup>m</sup> 12<sup>s</sup>; Decl. -21° 51'

19.905	345.0	15.64	3.7	2½	370
19.908	344.9	15.49	3.9	3	370
19.91	344.9	15.56	(8.7 ... 8.8) F		

**h 3502; -23° 265; 6.2**

A.R. 2<sup>h</sup> 24<sup>m</sup> 26<sup>s</sup>; Decl. -23° 13'

19.905	85.2	28.26	3.8	2½	370
19.908	85.3	28.38	4.0	2½	370
19.91	85.3	28.32	(6.8 ... 13.3)		

**1315; h 3505**

A.R. 2<sup>h</sup> 27<sup>m</sup> 32<sup>s</sup>; Decl. -18° 53'

19.943	21.6	18.50	1.8	2	370
19.952	19.1	18.24	1.9	2½	370
19.963	18.1	18.39	3.7	2	370
19.95	19.6	18.38	(9.2 ... 13.3)		

**h 3506; ω Fornacis; 5.3**

A.R. 2<sup>h</sup> 28<sup>m</sup> 35<sup>s</sup>; Decl. -28° 45'

19.906	243.9	11.12	4.3	2½	370
19.908	243.6	11.09	4.5	2½	370
19.91	243.8	11.10	(4.8 ... 8.9) F		

**h 2150; Cód -24° 1151; 9.6**

A.R. 2<sup>h</sup> 30<sup>m</sup> 13<sup>s</sup>; Decl. -24° 50'

19.963	253.4	13.62	3.9	2	370
19.966	253.0	13.28	3.7	1½	370
20.056	253.4	13.62	5.6	2	370
20.00	253.3	13.51	(10.6 ... 12.2)		

*h* 3511;  $-21^{\circ} 249$ ; 7.2 :A.R.  $2^h 30^m 30^s$ ; Decl.  $-21^{\circ} 56'$ 

19.905	97.7	14.86	3.9	$2\frac{1}{2}$	370
19.908	98.0	14.94	4.2	3	370
19.91	97.9	14.90	(6.9Y ... 8.9b) F		

*h* 3512; Cód  $-25^{\circ} 1021$ ; 9.7A.R.  $2^h 30^m 45^s$ ; Decl.  $-25^{\circ} 15'$ 

19.906	222.3	12.74	4.0	$2\frac{1}{2}$	370
19.908	223.4	12.81	4.3	3	370
19.922	222.8	12.75	3.5	2	370
19.91	222.8	12.77	(11.1 ... 11.3)		

*h* 3515; Cód  $-25^{\circ} 1023$ ; 9.6A.R.  $2^h 30^m 52^s$ ; Decl.  $-25^{\circ} 18'$ 

19.906	114.7	18.12	4.1	$2\frac{1}{2}$	370
19.908	114.6	18.28	4.4	$2\frac{1}{2}$	370
19.91	114.7	18.20	(10.4 ... 11.9)		

Cód—;  $-26^{\circ} 240$ ; 8.8A.R.  $2^h 31^m 27^s$ ; Decl.  $-26^{\circ} 13'$ 

20.891	230.2	4.07	2.5	4	370
20.896	230.2	4.05	1.8	3	370
20.89	230.2	4.06	(9.4 ... 9.5) F		

*h* 3518;  $-28^{\circ} 242$ ; 8.6A.R.  $2^h 33^m 38^s$ ; Decl.  $-28^{\circ} 41'$ 

19.941	14.8	13.55	4.2	2	370
19.943	16.4	13.62	2.0	$2\frac{1}{2}$	370
19.952	14.8	13.56	2.1	$2\frac{1}{2}$	370
19.95	15.3	13.58	(9.2 ... 10.5) F		

AC

19.941	230.3	16.11	4.3	2	370
19.943	228.3	16.15	2.1	$2\frac{1}{2}$	370
19.952	229.2	15.99	2.2	$2\frac{1}{2}$	370
19.95	229.3	16.08	(9.2 ... 10.8) R		

*h* 3524;  $-20^{\circ} 307 + 8$ ;  $8.0 + 9.1$ A.R.  $2^h 37^m 26^s$ ; Decl.  $-20^{\circ} 48'$ 

19.922	148.9	19.57	4.3	2	370
19.936	149.0	19.49	5.4	2	370
19.93	149.0	19.53	(8.0 ... 9.4) A		

*h* 3533;  $-20^{\circ} 316 + 15$ ;  $8.2 + 8.2$ A.R.  $2^h 44^m 17^s$ ; Decl.  $-20^{\circ} 45'$ 

19.922	272.1	39.69	4.4	2	370
19.936	272.3	39.54	5.8	$1\frac{1}{2}$	370
19.93	272.2	39.62	(7.5 ... 8.6) F		

*h* 3535;  $-28^{\circ} 260$ ; 6.0A.R.  $2^h 44^m 42^s$ ; Decl.  $-28^{\circ} 26'$ 

19.906	Redonda	3	650
19.908	Redonda	3	650
20.891	Redonda	4	650

Hd 61 = Hd 58;  $-28^{\circ} 274$ ; 8.8A.R.  $2^h 49^m 40^s$ ; Decl.  $-28^{\circ} 23'$ 

19.963	346.4	24.49	4.3	2	370
19.966	346.8	24.80	3.8	2	370
20.056	346.8	24.84	5.7	2	370
20.00	346.7	24.71	(8.8 ... 12.3) 231		

 $\hat{e}$  77;  $-29^{\circ} 341$ ; 8.0R.A.  $2^h 51^m 13^s$ ; Decl.  $-29^{\circ} 26'$ 

20.831	71.6	0.39	4.5	3	650
20.864	72.0	0.31	1.6	4	650
20.880	73.7	0.32	2.3	3	650
20.86	72.4	0.34	(8.2 ... 8.6)		

*h* 3543; Cód  $-29^{\circ} 1096$ ; 9.9A.R.  $2^h 52^m 30^s$ ; Decl.  $-29^{\circ} 28'$ 

19.941	265.1	10.14	4.7	2	370
19.943	263.5	10.44	2.3	2	370
19.954	264.4	10.90	1.8	2	370
19.95	264.3	10.49	(10.5 ... 10.9) D?		

AC

19.941	64.3	15.58	4.8	$1\frac{1}{2}$	370
19.954	62.2	15.69	1.9	2	370
19.95	63.2	15.64	(10.5 ... 12.3) R?		

O. Stone 6;  $-23^{\circ} 341$ ; 9.2A.R.  $3^h 4^m 56^s$ ; Decl.  $-23^{\circ} 11'$ 

19.963	175.6	4.89	4.5	2	370
19.966	177.1	4.96	4.0	2	370
20.056	176.9	5.07	6.1	2	370
20.00	176.5	4.97	(10.0 ... 10.2) D?		

**1631**; *h* 3557A.R.  $3^h 9^m 12^s$ ; Decl.  $-14^{\circ} 53'$ 

19.952	360.0	27.08	2.5	$2\frac{1}{2}$	370
19.954	359.8	27.00	2.1	2	370
19.95	359.9	27.04	(7.9 ... 12.3) 5		

*h* 3561;  $-20^{\circ} 365$ ; 9.6A.R.  $3^h 11^m 25^s$ ; Decl.  $-20^{\circ} 23'$ 

19.936	147.8	—	6.0	$1\frac{1}{2}$	370
19.963	148.1	22.90	4.8	2	370
19.966	146.7	22.84	4.2	2	370
19.96	147.5	22.87	(9.2 ... 13.8) M?		

Hh 83 = h 3563;  $-23^{\circ} 35'$ ; 8.2

A.R.  $3^h 11^m 53^s$ ; Decl.  $-23^{\circ} 28'$

19.906	256.0	9.15	4.5	2	370
19.908	256.3	9.09	4.9	$2\frac{1}{2}$	370
19.922	255.7	9.11	3.7	$2\frac{1}{2}$	370
19.91	256.0	9.12	(9.0 ... 9.3)		D <sup>2</sup>

$\delta$  78;  $-29^{\circ} 37'$ ; 8.2

A.R.  $3^h 13^m 40^s$ ; Decl.  $-29^{\circ} 57'$

20.831	291.9	0.32	5.1	$3\frac{1}{2}$	650
20.864	298.8	0.30	1.9	4	650
20.880	293.9	0.31	2.5	3	650
20.86	294.9	0.31	(9.6 ... 9.7)		

J 516;  $\tau_4$  Eridani; 5.7

A.R.  $3^h 14^m 12^s$ ; Decl.  $-22^{\circ} 12'$

19.906	289.2	5.97	4.6	2	370
19.908	288.1	6.02	5.0	$2\frac{1}{2}$	370
19.963	288.4	5.89	4.7	2	370
19.93	288.6	5.96	(3.5 ... 10.2)		F

h 3567; SD  $-14^{\circ} 65'$ ; 9.3

A.R.  $3^h 15^m 36^s$ ; Decl.  $-14^{\circ} 25'$

19.954	109.9	5.22	2.4	2	370
19.966	110.3	5.41	4.6	2	370
20.061	109.2	5.30	5.5	2	370
19.99	109.8	5.31	(10.3 ... 11.5)		

h 3570;  $-20^{\circ} 37'$ ; 6.4

A.R.  $3^h 16^m 18^s$ ; Decl.  $-20^{\circ} 45'$

19.963	256.1	34.33	4.9	$1\frac{1}{2}$	370
19.966	255.2	34.33	4.7	$2\frac{1}{2}$	370
20.061	255.8	34.59	5.7	2	370
20.00	255.7	34.42	(6.3 ... 13.3)		120

I —;  $-29^{\circ} 38'$ ; 9.8

A.R.  $3^h 16^m 24^s$ ; Decl.  $-29^{\circ} 50'$

20.831	68.9	1.52	5.3	$3\frac{1}{2}$	370
20.863	70.0	1.63	2.0	4	370
20.880	63.5	1.60	2.7	3	370
20.86	67.5	1.58	(9.7 ... 11.4)		23

h 3572;  $-26^{\circ} 36' + 5'$ ; 7.9 + 7.8

A.R.  $3^h 18^m 57^s$ ; Decl.  $-26^{\circ} 39'$

19.906	95.0	20.84	5.4	$2\frac{1}{2}$	370
19.908	95.2	20.81	5.2	$2\frac{1}{2}$	370
19.91	95.1	20.82	(8.3 ... 8.4)		N

h 3574; Anon.

A.R.  $3^h 19^m 24^s$ ; Decl.  $-21^{\circ} 56'$

19.906	90.5	16.22	5.3	$1\frac{1}{2}$	370
19.963	91.5	16.41	5.4	$1\frac{1}{2}$	370
19.966	89.3	16.30	4.8	$1\frac{1}{2}$	370
19.94	90.4	16.31	(10.5 ... 13.1)		228

h 3583;  $-20^{\circ} 41'$ ; 8.6:

A.R.  $3^h 32^m 25^s$ ; Decl.  $-20^{\circ} 52'$

19.963	86.9	12.17	5.6	2	370
19.966	86.4	11.97	5.1	2	370
20.061	86.3	12.27	5.8	2	370
20.00	86.5	12.14	(9.8 ... 9.9)		N

h 3594;  $-20^{\circ} 44'$ ; 8.5

A.R.  $3^h 43^m 5^s$ ; Decl.  $-20^{\circ} 47'$

19.963	92.0	13.03	5.7	2	370
20.061	88.6	13.49	6.0	$2\frac{1}{2}$	370
20.01	90.3	13.26	(9.1 ... 14.5)		N

h 3602;  $-27^{\circ} 39'$ ; 8.8

A.R.  $3^h 46^m 27^s$ ; Decl.  $-27^{\circ} 50'$

19.906	345.9	8.87	5.5	$2\frac{1}{2}$	370
19.908	346.3	8.89	5.4	3	370
19.922	346.1	9.07	4.0	$2\frac{1}{2}$	370
19.91	346.1	8.94	(9.5 ... 9.6)		D

h 3601 =  $\lambda$  33;  $-23^{\circ} 42'$ ; 7.7

A.R.  $3^h 46^m 31^s$ ; Decl.  $-23^{\circ} 18'$

19.908	300.4	10.80	5.4	3	370
19.922	299.7	10.97	3.9	$2\frac{1}{2}$	370
19.91	300.1	10.88	(8.4Y ... 9.6b)		F

1991; h 3613

A.R.  $3^h 54^m 54^s$ ; Decl.  $-14^{\circ} 51'$

19.954	132.5	8.12	2.7	$2\frac{1}{2}$	370
19.963	132.3	8.23	5.8	2	370
19.966	132.7	8.11	5.2	$1\frac{1}{2}$	370
19.96	132.5	8.15	(10.3 ... 10.6)		

$\delta$  79;  $-28^{\circ} 44'$ ; 7.6

A.R.  $3^h 57^m 30^s$ ; Decl.  $-28^{\circ} 52'$

20.864	131.7	0.56	3.0	3	650
20.880	131.4	0.60	2.9	$3\frac{1}{2}$	650
20.891	132.2	0.50	2.9	$3\frac{1}{2}$	650
20.88	131.8	0.55	(8.1 ... 8.5)		

**2017; h 3615**A.R. 3<sup>h</sup> 57<sup>m</sup> 34<sup>s</sup>; Decl. -15° 28'

19.963	156.6	24.47	5.9	2	370
20.061	156.5	24.51	6.3	2	370
20.01	156.6	24.49	(8.6 ... 9.5)		F?

**2020; h 3617**A.R. 3<sup>h</sup> 58<sup>m</sup> 22<sup>s</sup>; Decl. -12° 5'

19.963	63.6	17.00	6.1	2	370
20.061	64.8	17.14	6.9	2	370
20.075	65.0	17.07	6.4	2½	370
20.03	64.5	17.07	(8.6 ... 11.6)		F?

**h 3619; SD -12° 801; 9.4**A.R. 4<sup>h</sup> 1<sup>m</sup> 23<sup>s</sup>; Decl. -12° 6'

19.963	326.1	18.54	6.2	1½	370
20.062	326.2	18.36	7.1	2	370
20.064	325.8	18.82	6.7	2	370
20.03	326.0	18.57	(9.8 ... 11.7)		88

**Hu 1363; -22° 458; 6.8**A.R. 4<sup>h</sup> 1<sup>m</sup> 46<sup>s</sup>; Decl. -22° 19'

19.223	133.9	[0.32]	7.6	2½	650
19.234	132.3	0.23	8.3	3	1125
19.242	132.9	0.20	7.7	3	1125
19.23	133.0	0.22	(7.9 ... 8.0)		N

**Hu 1366; -30° 573; 9.6**A.R. 4<sup>h</sup> 13<sup>m</sup> 11<sup>s</sup>; Decl. -30° 10'

19.221	247.1	2.07	8.1	2½	370
19.223	247.7	1.81	7.8	2	650
19.234	245.3	1.71	8.8	3½	475
19.23	246.7	1.86	(9.6 ... 10.9)		N

**h 3637; -27° 498; 8.4**A.R. 4<sup>h</sup> 13<sup>m</sup> 58<sup>s</sup>; Decl. -27° 2'

18.230	213.0	29.67	8.6	1½	370
18.238	212.9	29.24	8.6	1½	370
18.23	213.0	29.46	(8.4 ... 11.0)		N

**β 744; -26° 520; 6.6**A.R. 4<sup>h</sup> 16<sup>m</sup> 32<sup>s</sup>; Decl. -26° 1'

19.242	21.5	0.27	8.1	2½	1125
19.251	21.2	0.30	7.8	2½	1125
20.097	38.4	0.34	5.5	2½	650
20.116	36.2	0.25	5.9	3	650
20.135	34.9	0.33	6.7	2½	650
20.865	45.0	0.21	3.9	3½	650
20.880	41.1	0.30	3.1	3½	650
20.932	56.3	0.25	7.0	3	650
19.25	21.4	0.28			
20.12	36.5	0.31			
20.89	47.1	0.25	(7.0 ... 7.2)		B

**2184; h 3647**A.R. 4<sup>h</sup> 18<sup>m</sup> 37<sup>s</sup>; Decl. -18° 22'

20.067	253.0	34.89	5.2	2	370
20.075	252.9	34.65	6.5	2½	370
20.07	252.9	34.77	(9.9 ... 10.1)		

AC

20.067	309.7	42.08	5.3	2	370
20.075	309.7	41.83	6.6	2½	370
20.07	309.7	41.95	(9.9 ... 11.4)		

**Hu 1369; -29° 572; 8.6**A.R. 4<sup>h</sup> 21<sup>m</sup> 1<sup>s</sup>; Decl. -29° 2'

19.221	301.9	0.50	8.3	2	650
19.234	298.4	0.52	9.1	3	650
19.242	293.8	0.54	8.3	3	650
20.864	294.0	0.50	3.5	3	650
20.880	293.0	0.48	3.3	3	650
20.932	292.9	0.51	7.1	3	650

19.23	298.0	0.52			
20.89	293.3	0.50	(9.5 ... 9.7)		A

**ε 80; -28° 554; 8.5**A.R. 4<sup>h</sup> 25<sup>m</sup> 5<sup>s</sup>; Decl. -28° 42'

20.864	172.1	1.78	4.0	3½	370
20.880	171.5	1.81	3.6	3	370
20.932	174.4	1.44	7.2	3	370
20.979	170.0	1.69	5.9	3½	370
20.91	172.0	1.68	(9.0 ... 12.7)		

**2240; h 3653**A.R. 4<sup>h</sup> 25<sup>m</sup> 7<sup>s</sup>; Decl. -16° 43'

20.075	156.6	42.22	6.7	2½	370
20.078	156.5	42.37	6.8	2½	370
20.08	156.6	42.30	(8.5 ... 9.1)		F

**h 3677; -29° 627 + 6; 9.1 + 9.1**A.R. 4<sup>h</sup> 35<sup>m</sup> 45<sup>s</sup>; Decl. -29° 48'

20.880	354.8	10.67	3.9	3	370
20.891	354.7	10.70	3.2	2	370
20.89	354.8	10.68	(9.1 ... 9.7)		A

BC = ε 81

20.880	17.4	3.36	4.0	3	370
20.891	16.9	3.53	3.3	2½	370
20.979	13.8	3.35	6.1	3	370
20.92	16.0	3.41	(9.7 ... 11.4)		

**2369; h 3690**A.R. 4<sup>h</sup> 42<sup>m</sup> 56<sup>s</sup>; Decl. -11° 58'

20.062	33.2	30.09	7.2	1½	370
20.075	34.2	30.90	6.8	2½	370
20.078	32.8	30.29	7.0	2	370
20.07	33.4	30.43	(8.4 ... 13.2)		F?

(Sigue Continued.)



AC

20.062	196.2	32.39	7.4	1	370
20.075	196.1	31.89	6.9	2	370
20.078	196.2	32.63	7.2	1	370
20.07	196.2	32.10	(8.4 ... 10.9)	F	

$h$  3702;  $-25^{\circ}$  729; 8.6 :

A.R.  $4^h$  48<sup>m</sup> 36<sup>s</sup>; Decl.  $-25^{\circ}$  21'

20.097	227.6	17.65	5.8	2	370
20.100	227.3	17.29	6.0	2	370
20.116	227.9	17.55	6.1	2	370
20.10	227.6	17.50	(8.9 ... 11.3)	F	

$\xi$  82;  $-29^{\circ}$  695; 9.0

A.R.  $4^h$  49<sup>m</sup> 57<sup>s</sup>; Decl.  $-29^{\circ}$  9'

20.864	182.8	3.35	4.4	34	370
20.880	183.2	3.45	4.3	3	370
20.891	184.4	3.43	3.4	24	370
20.88	183.5	3.41	(9.5 ... 10.7)		

**2438:**  $h$  3705

A.R.  $4^h$  51<sup>m</sup> 24<sup>s</sup>; Decl.  $-16^{\circ}$  19'

20.075	141.4	22.45	7.1	2	370
20.078	141.3	22.93	7.3	1	370
20.091	141.3	22.36	6.4	2	370
20.08	141.3	22.41	(7.5 ... 10.2)	F	

**2487:**  $h$  3714; Anon.

A.R.  $4^h$  56<sup>m</sup> 29<sup>s</sup>; Decl.  $-16^{\circ}$  28'

20.075	281.1	9.26	7.2	2	370
20.091	280.1	8.88	6.5	2	370
20.094	278.9	9.42	6.4	2	370
20.100	280.0	8.99	6.2	2	370
20.09	280.0	9.44	(11.0 ... 11.6)		

$\xi$  83;  $-29^{\circ}$  756; 9.0

A.R.  $4^h$  58<sup>m</sup> 55<sup>s</sup>; Decl.  $-29^{\circ}$  8'

20.864	71.7	1.31	4.6	4	370
20.880	76.8	1.29	4.4	3	370
20.891	73.5	1.20	3.7	2	370
20.88	74.0	1.27	(9.1 ... 11.3)		

$\lambda$  48;  $-28^{\circ}$  799; 9.5

A.R.  $5^h$  7<sup>m</sup> 47<sup>s</sup>; Decl.  $-28^{\circ}$  40'

Identificación anterior es errónea.

$\beta$  553; *Rigel*; BC

A.R.  $5^h$  8<sup>m</sup> 47<sup>s</sup>; Decl.  $-8^{\circ}$  20'

20.116	86.02	0.107	6.6	3	650
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Howe 12;  $-29^{\circ}$  817; 7.9

A.R.  $5^h$  10<sup>m</sup> 53<sup>s</sup>; Decl.  $-29^{\circ}$  39'

20.891	234.9	2.43	3.8	24	370
20.979	234.6	2.39	6.3	34	370
20.94	234.7	2.41	(8.5 ... 10.1)	F	

$\xi$  84;  $-29^{\circ}$  820; 8.6

A.R.  $5^h$  11<sup>m</sup> 26<sup>s</sup>; Decl.  $-29^{\circ}$  53'

20.880	104.0	0.55	4.7	3	650
20.891	103.4	0.57	4.0	3	650
20.979	106.6	0.57	6.2	34	370
20.92	104.6	0.56	(9.4 ... 9.5)		

Lalande =  $h$  3759;  $-19^{\circ}$  812; 11; 6.8 8.0

A.R.  $5^h$  16<sup>m</sup> 48<sup>s</sup>; Decl.  $-19^{\circ}$  48'

20.075	517.1	27.34	7.3	24	370
20.091	517.1	27.33	6.6	24	370
20.08	517.1	27.28	(6.6 ... 8.1)	F	

Hd 72;  $-23^{\circ}$  808; 8.7

A.R.  $5^h$  15<sup>m</sup> 40<sup>s</sup>; Decl.  $-23^{\circ}$  9'

18.130	1.7	20.33	9.2	2	370
18.138	1.5	20.12	9.0	1	370
18.13	2.1	20.18	9.1	(10.8)	

**2813:**  $h$  3766;  $\alpha$  Leporis

A.R.  $5^h$  27<sup>m</sup> 44<sup>s</sup>; Decl.  $-17^{\circ}$  55'

20.075	156.1	35.67	7.5	1	370
20.094	156.3	35.44	6.5	2	370
20.100	156.1	35.47	6.3	2	370
20.09	156.2	35.52	(3.3 ... 11.3)	RP	

$\xi$  85;  $24^{\circ}$  997; 8.8

A.R.  $5^h$  28<sup>m</sup> 3<sup>s</sup>; Decl.  $24^{\circ}$  20'

20.097	254.9	0.53	6.2	34	650
20.100	254.2	0.50	6.5	24	475
20.116	257.7	0.54	6.4	3	650
20.135	257.5	0.49	6.9	24	650
20.11	257.8	0.49	(9.0 ... 9.6)		

$h$  3770;  $-24^{\circ}$  999; 7.9

A.R.  $5^h$  28<sup>m</sup> 43<sup>s</sup>; Decl.  $24^{\circ}$  25'

20.097	18.0	4.30	6.3	3	370
20.100	15.6	4.15	6.6	2	475
20.116	18.3	4.14	6.3	34	370
20.119	21.1	4.30	5.4	2	370
20.11	18.5	4.14	(7.9 ... 12.5)	F	

**2916; h 3785**A.R. 5<sup>h</sup> 35<sup>m</sup> 48<sup>s</sup>; Decl. -14° 20'

20.075	311.1	18.73	7.7	2½	370
20.094	310.6	18.50	6.6	2	370
20.100	310.5	18.33	6.7	2	370
20.09	310.7	18.52	(10.2 ... 10.4)		

**h 3791 = Hd 79; -20° 9'13; 8.3**A.R. 5<sup>h</sup> 38<sup>m</sup> 11<sup>s</sup>; Decl. -20° 43'

20.075	58.1	10.89	7.8	2½	370
20.094	57.2	10.91	6.7	2	370
20.08	57.7	10.90	(8.7 ... 10.7)	F	

**h 3798; -24° 10'68 + 70; 8.2 + 8.4**A.R. 5<sup>h</sup> 42<sup>m</sup> 17<sup>s</sup>; Decl. -24° 32'

18.238	69.1	15.34	9.2	1½	370
18.252	69.5	15.45	9.4	1½	370
18.24	69.3	15.40	(8.6 ... 8.9)	88	

**β -; -24° 10'84; 8.5**A.R. 5<sup>h</sup> 44<sup>m</sup> 27<sup>s</sup>; Decl. -24° 30'

18.230	66.5	2.49	9.4	2	370
18.238	65.4	2.29	9.3	1½	370
18.252	62.1	2.27	9.5	1½	370
18.24	64.7	2.35	(8.8 ... 10.9)	F	

**O. Stone 12; -24° 10'87; 8.8**A.R. 5<sup>h</sup> 44<sup>m</sup> 51<sup>s</sup>; Decl. -24° 19'

18.230	3.8	6.07	9.6	2½	370
18.238	3.6	5.87	9.5	1½	370
18.23	3.7	5.97	(10.1 ... 12.0)	232	

**3025; h 3804**A.R. 5<sup>h</sup> 45<sup>m</sup> 57<sup>s</sup>; Decl. -12° 48'

20.094	34.6	11.97	6.8	1½	370
20.100	36.0	12.02	6.9	2	370
20.119	37.4	12.19	5.6	2	370
20.10	36.0	12.06	(8.9 ... 12.7)		

**h 3811; -25° 11'16; 8.6**A.R. 5<sup>h</sup> 49<sup>m</sup> 27<sup>s</sup>; Decl. -25° 33'

18.230	263.6	17.99	10.0	2	370
18.252	265.4	18.14	9.7	1½	370
18.24	264.5	18.06	(8.1 ... 10.0)		

AC; C = 13.5

18.252	19.5	12.50	9.8	1½	370
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**h 3818; -27° 10'29; 8.8**A.R. 5<sup>h</sup> 52<sup>m</sup> 33<sup>s</sup>; Decl. -27° 21'

20.094	168.0	14.95	7.2	2	370
20.097	167.5	14.72	6.5	2½	370
20.100	167.1	14.61	7.0	2	370
20.10	167.5	14.76	(8.7 ... 12.5)		

**δ 86; -28° 10'64; 8.8**A.R. 5<sup>h</sup> 54<sup>m</sup> 30<sup>s</sup>; Decl. -28° 32'

20.979	70.7	1.95	7.1	3	370
21.039	71.1	1.89	4.7	2½	370
21.050	71.0	1.82	6.5	2½	370
21.02	70.9	1.89	(9.6 ... 10.3)		

**h 3821; -21° 10'55 + 4; 8.0 + 8.7**A.R. 5<sup>h</sup> 55<sup>m</sup> 44<sup>s</sup>; Decl. -21° 0'

20.075	213.1	18.07	7.9	2½	370
20.094	212.7	17.99	7.0	2	370
20.08	212.9	18.03	(8.2 ... 9.5)		

AC; C = 12.2

20.094	87.2	19.82	7.1	1½	370
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**h 3825; -27° 10'71 + 70; 7.6 + 9.6**A.R. 5<sup>h</sup> 57<sup>m</sup> 21<sup>s</sup>; Decl. -27° 25'

20.094	338.4	32.66	7.3	2	370
20.097	338.1	32.66	6.6	2½	370
20.10	338.2	32.66	(7.3 ... 11.0)		

**h 3830; -28° 11'10; 7.8**A.R. 6<sup>h</sup> 0<sup>m</sup> 43<sup>s</sup>; Decl. -28° 40'

20.094	1.7	6.39	7.4	2	370
20.097	1.2	6.42	6.7	3	370
20.100	1.5	6.40	7.1	2½	370
20.10	1.5	6.40	(8.3 ... 8.5)	F	

**h 3833; -23° 10'57; 5.3**A.R. 6<sup>h</sup> 1<sup>m</sup> 32<sup>s</sup>; Decl. -23° 6'

20.094	71.7	44.90	7.5	2	370
20.097	71.7	44.86	6.8	3	370
20.10	71.7	44.88	(5.8 ... 10.5)	F?	

**3236; h 3839**A.R. 6<sup>h</sup> 7<sup>m</sup> 26<sup>s</sup>; Decl. -18° 17'

20.198	278.2	11.06	7.6	2½	370
20.215	279.1	10.81	8.0	2½	370
20.21	278.7	10.94	(9.1 ... 14.9)	F?	

I 752;  $-22^{\circ}$  1128; 8.5

A.R. 6<sup>h</sup> 10<sup>m</sup> 38<sup>s</sup>; Decl.  $-22^{\circ}$  9'

20.154	96.5	0.39	7.4	2	475
20.157	91.3	0.33	7.2	2½	650
20.16	93.9	0.36	(9.6 ... 9.8)		A

AB,C = h 3842; C =  $-22^{\circ}$  1127; 10.1

18.262	210.7	19.81	8.7	1½	370
18.271	210.6	19.90	10.5	2½	370
18.27	210.6	19.86	((8.8) ... 11.5)		N

**3309 (3307);** Ho 231 = h 3847

A.R. 6<sup>h</sup> 13<sup>m</sup> 45<sup>s</sup>; Decl.  $-12^{\circ}$  29'

20.176	47.2	6.73	7.6	2	370
20.198	47.5	6.70	7.9	3	370
20.215	47.7	6.73	8.2	2½	370
20.20	47.5	6.72	(8.4 ... 10.5)		D?

I 1116;  $-29^{\circ}$  1210; 8.6

A.R. 6<sup>h</sup> 13<sup>m</sup> 55<sup>s</sup>; Decl.  $-29^{\circ}$  19'

21.050	111.9	1.74	7.0	2½	370
21.061	113.2	1.59	8.7	2½	370
21.06	112.6	1.66	(9.0 ... 10.0)		23

Anonyma

A.R. 6<sup>h</sup> 14<sup>m</sup> 53<sup>s</sup>; Decl.  $-14^{\circ}$  30'

20.135	32.4	12.25	8.3	2	370
20.141	32.3	12.89	7.5	2	370
20.157	33.2	12.11	7.4	3	370
20.14	32.6	12.42	(10.6 ... 12.4)		233

**3343;** h 3850

A.R. 6<sup>h</sup> 16<sup>m</sup> 43<sup>s</sup>; Decl.  $-14^{\circ}$  33'

20.135	47.5	15.56	8.4	2	370
20.141	47.9	15.88	7.7	2	370
20.157	46.0	15.57	7.5	2½	370
20.14	47.1	15.67	(9.1 ... 11.4)		F

h 3859;  $-26^{\circ}$  1282; 8.8

A.R. 6<sup>h</sup> 21<sup>m</sup> 42<sup>s</sup>; Decl.  $-26^{\circ}$  45'

20.097	259.3	10.94	6.9	3	370
20.100	258.5	10.92	7.3	2½	370
20.10	258.9	10.93	(9.3 ... 9.4)		

h 3865; SD  $-17^{\circ}$  1512; 8.0

A.R. 6<sup>h</sup> 24<sup>m</sup> 4<sup>s</sup>; Decl.  $-17^{\circ}$  44'

20.135	66.0	23.49	8.7	2	370
20.141	66.2	23.67	8.0	2	370
20.14	66.1	23.58	(8.6 ... 10.9)		

**3430;** h 3864

A.R. 6<sup>h</sup> 25<sup>m</sup> 3<sup>s</sup>; Decl.  $-14^{\circ}$  53'

20.135	43.0	21.59	8.5	2	370
20.141	42.9	21.46	7.8	2	370
20.14	43.0	21.53	(7.8 ... 10.7)		

Hh 240 = h 3876;  $-22^{\circ}$  1345; 7.0

A.R. 6<sup>h</sup> 31<sup>m</sup> 38<sup>s</sup>; Decl.  $-22^{\circ}$  31'

20.116	335.3	9.24	6.7	3½	370
20.141	335.9	9.27	8.2	2	370
20.157	336.1	9.19	8.5	2½	370
20.14	335.8	9.23	(7.0 ... 9.9)		F

h 3877;  $-22^{\circ}$  1366 + 5; 8.8 + 8.8

A.R. 6<sup>h</sup> 33<sup>m</sup> 24<sup>s</sup>; Decl.  $-22^{\circ}$  56'

20.116	350.3	15.00	6.8	3	370
20.141	350.4	14.53	8.3	2	370
20.157	350.7	15.25	8.6	2½	370
20.14	350.5	14.93	(9.5 ... 10.2)		234

h 2334;  $-28^{\circ}$  1385; 9.9

A.R. 6<sup>h</sup> 34<sup>m</sup> 14<sup>s</sup>; Decl.  $-28^{\circ}$  40'

18.252	299.1	10.66	10.5	1½	370
18.273	298.4	10.86	10.1	2	370
18.26	298.7	10.76	(10.9 ... 11.4)		

Hd 85 = Hd 84;  $-20^{\circ}$  1518; 9.0

A.R. 6<sup>h</sup> 37<sup>m</sup> 20<sup>s</sup>; Decl.  $-20^{\circ}$  38'

18.262	235.1	4.15	9.2	1½	370
18.271	234.7	4.30	10.7	2	370
18.27	234.9	4.23	(9.5 ... 11.0)		

h 2340;  $-29^{\circ}$  1426; 9.1

A.R. 6<sup>h</sup> 41<sup>m</sup> 13<sup>s</sup>; Decl.  $-29^{\circ}$  13'

18.252	0.5	12.13	10.8	1½	370
18.273	3.1	12.19	10.3	2	370
18.26	1.8	12.16	(10.5 ... 12.4)		

h 2356;  $-29^{\circ}$  1500; 8.8

A.R. 6<sup>h</sup> 51<sup>m</sup> 55<sup>s</sup>; Decl.  $-29^{\circ}$  15'

18.273	76.6	18.45	10.5	2	370
18.287	77.2	18.19	10.2	2½	370
18.28	76.9	18.32	(9.6 ... 10.4)		

I 432;  $-28^{\circ}$  1564; 8.4

A.R. 6<sup>h</sup> 52<sup>m</sup> 11<sup>s</sup>; Decl.  $-28^{\circ}$  32'

18.273	211.7	1.57	10.7	2	370
18.287	210.4	1.45	10.3	2½	370
19.114	213.6	1.56	7.9	2	370
18.56	211.9	1.53	(8.7 ... 8.9)		F

$h$  3913;  $-28^\circ 1626$ ; 8.5A.R.  $6^h 56^m 38^s$ ; Decl.  $-28^\circ 53'$ 

20.141	129.9	7.90	8.5	$2\frac{1}{2}$	370
20.157	130.0	8.22	8.7	3	370
20.160	130.8	7.98	7.2	$2\frac{1}{2}$	370
20.15	130.2	8.03	(9.1 ... 10.8)		

 $h$  2361;  $-29^\circ 1537$ ; 9.8:A.R.  $6^h 58^m 44^s$ ; Decl.  $-29^\circ 38'$ 

18.273	127.9	18.15	10.9	$1\frac{1}{2}$	370
18.287	128.3	18.20	10.4	$2\frac{1}{2}$	370
18.28	128.1	18.18	(10.6 ... 10.9)		

 $h$  3923;  $-29^\circ 1544$ ; 8.9A.R.  $6^h 59^m 57^s$ ; Decl.  $-29^\circ 31'$ 

20.141	202.3	11.24	8.7	2	370
20.157	202.5	11.50	8.8	$2\frac{1}{2}$	370
20.160	202.0	11.58	7.3	$2\frac{1}{2}$	370
20.15	202.3	11.44	(9.7 ... 11.5)		

A y  $-29^\circ 1545$ ; 9.6

20.157	34.6	43.47	8.8	$2\frac{1}{2}$	370
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 $h$  2363;  $-27^\circ 1713$ ; 9.4A.R.  $7^h 1^m 50^s$ ; Decl.  $-27^\circ 37'$ 

18.273	322.2	13.17	11.0	$1\frac{1}{2}$	370
18.287	321.4	12.71	10.6	2	370
18.28	321.8	12.94	(10.6 ... 11.6)		

 $h$  3933;  $-19^\circ 1815$ ; 8.5A.R.  $7^h 4^m 55^s$ ; Decl.  $-19^\circ 34'$ 

20.135	150.2	14.84	9.2	$2\frac{1}{2}$	370
20.141	150.6	14.46	8.9	2	370
20.157	150.7	14.69	8.9	2	370
20.14	150.5	14.66	(8.9 ... 13.0)		

 $h$  3939; SD  $-17^\circ 1864$ ; 9.0A.R.  $7^h 8^m 52^s$ ; Decl.  $-17^\circ 46'$ 

20.135	245.9	9.98	8.9	$2\frac{1}{2}$	370
20.141	246.6	9.96	9.1	2	370
20.157	245.0	9.96	9.1	$2\frac{1}{2}$	370
20.14	245.8	9.97	(9.0 ... 11.4)		

 $\geq 87$ ; SD  $-17^\circ 1865$ ; 9.5A.R.  $7^h 8^m 55^s$ ; Decl.  $-17^\circ 51'$ 

20.141	317.5	4.13	9.3	$1\frac{1}{2}$	370
20.157	319.1	4.29	9.2	$2\frac{1}{2}$	370
20.15	318.3	4.21	(10.6 ... 10.8)		

 $h$  2370;  $-29^\circ 1624 + 5$ ; 8.6 + 9.6A.R.  $7^h 11^m 18^s$ ; Decl.  $-29^\circ 17'$ 

18.287	53.4	31.13	10.7	$2\frac{1}{2}$	370
19.114	53.6	[31.97]	8.2	1	370
19.133	53.1	31.22	10.0	$1\frac{1}{2}$	370
18.83	53.4	31.18	(9.1 ... 9.5)		

 $h$  2375;  $-28^\circ 1888$ ; 9.6A.R.  $7^h 14^m 2^s$ ; Decl.  $-28^\circ 11'$ 

18.287	170.2	9.74	10.9	2	370
19.114	168.6	9.52	8.4	1	370
19.136	167.8	10.21	10.7	$1\frac{1}{2}$	370
18.85	168.9	9.82	(10.0 ... 12.1)		

 $h$  2381; Anon.A.R.  $7^h 17^m 56^s$ ; Decl.  $-29^\circ 13'$ 

19.136	107.1	13.37	11.0	$1\frac{1}{2}$	370
19.202	108.4	13.34	8.8	$1\frac{1}{2}$	370
19.17	107.8	13.36	(11.3 ... 12.4)		228

AC; C = 13.5

19.202	234.9	10.69	8.9	$1\frac{1}{2}$	370
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 $h$  2393;  $-28^\circ 2107$ ; 8.9A.R.  $7^h 25^m 23^s$ ; Decl.  $-28^\circ 1'$ 

18.271	120.8	15.15	11.3	2	370
19.136	120.8	15.58	11.2	$1\frac{1}{2}$	370
19.202	120.7	15.27	9.0	$1\frac{1}{2}$	370
18.87	120.8	15.33	(9.0 ... 11.0)		

 $h$  2398;  $-27^\circ 2145$ ; 9.8A.R.  $7^h 27^m 34^s$ ; Decl.  $-27^\circ 23'$ 

18.271	41.6	11.73	11.8	$1\frac{1}{2}$	370
19.202	43.5	11.60	9.2	$1\frac{1}{2}$	370
18.74	42.6	11.66	(10.9 ... 11.1)		

 $h$  3978;  $-27^\circ 2161$ ; 8.7A.R.  $7^h 28^m 36^s$ ; Decl.  $-27^\circ 56'$ 

18.271	103.1	11.75	11.5	$1\frac{1}{2}$	370
19.136	102.8	12.10	11.4	1	370
19.202	102.8	12.05	9.4	$1\frac{1}{2}$	370
18.87	102.9	11.97	(9.2 ... 10.6)		

AC; C = 12.5

19.202	158.2	16.08	9.6	$1\frac{1}{2}$	370
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 $h$  2401;  $-24^\circ 2573$ ; 9.4A.R.  $7^h 29^m 49^s$ ; Decl.  $-24^\circ 40'$ 

18.238	256.0	12.15	11.3	$1\frac{1}{2}$	370
18.263	256.1	11.88	9.4	2	370
18.25	256.1	12.01	(9.6 ... 11.2)		

ε 88; —28° 2201; 8.8

A.R. 7<sup>h</sup> 30<sup>m</sup> 13<sup>s</sup>; Decl. —28° 55'

20.864	222.9	2.73	6.3	3 $\frac{1}{2}$	370
20.880	221.2	2.93	6.1	3	370
21.014	221.8	2.92	6.9	3	370
20.92	222.0	2.86	(9.5 ... 10.9)		

h 3982; —28° 2210; 5.5

A.R. 7<sup>h</sup> 30<sup>m</sup> 34<sup>s</sup>; Decl. —28° 6'

20.157	155.8	38.30	9.3	3	370
20.160	155.4	38.44	7.5	2	370
20.16	155.6	38.37	(5.2 ... 9.3)		

BC; C = —28° 2211; 9.4

20.176	129.9	42.24	7.9	1 $\frac{1}{2}$	370
20.179	129.6	42.05	7.1	2 $\frac{1}{2}$	370
20.18	129.8	42.15	(9.3 ... 10.0)		

Hd 107<sup>?</sup>; —23° 2471 + 2; 8.6 + 9.2

A.R. 7<sup>h</sup> 31<sup>m</sup> 11<sup>s</sup>; Decl. —23° 34'

18.238	156.0	20.56	11.7	1 $\frac{1}{2}$	370
18.263	156.4	20.43	9.7	2	370
18.25	156.2	20.49	(8.2 ... 10.1) 235		

ε 89; —26° 2332; 8.1

A.R. 7<sup>h</sup> 33<sup>m</sup> 22<sup>s</sup>; Decl. —26° 38'

20.157	42.2	0.25	9.6	3	650
20.179	45.7	0.29	7.2	3	650
20.190	36.6	0.31	8.0	3	650
20.18	41.5	0.28	(9.3 ... 9.3)		

h 2408; —27° 2258; 9.2

A.R. 7<sup>h</sup> 33<sup>m</sup> 48<sup>s</sup>; Decl. —27° 54'

19.202	342.9	12.23	9.8	1 $\frac{1}{2}$	370
19.218	342.3	12.18	9.0	2	370
19.21	342.6	12.20	(9.6 ... 9.9)		

ε 90; —26° 2356; 7.1

A.R. 7<sup>h</sup> 34<sup>m</sup> 35<sup>s</sup>; Decl. —26° 39'

20.190	128.7	6.68	8.2	3	370
20.193	128.2	6.63	7.5	2 $\frac{1}{2}$	370
20.19	128.4	6.66	(7.4 ... 13.0)		

ε 91; —29° 1926; 8.6

A.R. 7<sup>h</sup> 34<sup>m</sup> 46<sup>s</sup>; Decl. —29° 46'

20.864	63.1	0.87	6.6	3 $\frac{1}{2}$	370
20.880	60.3	0.93	6.2	3	475
21.014	61.3	0.90	7.1	3	370
20.92	61.6	0.90	(9.9 ... 10.1)		

ε 92; —29° 1954; 10.0

R.A. 7<sup>h</sup> 35<sup>m</sup> 51<sup>s</sup>; Decl. —29° 45'

20.880	215.6	2.50	6.3	2 $\frac{1}{2}$	475
21.014	214.8	2.45	7.3	2 $\frac{1}{2}$	370
20.95	215.2	2.48	(11.1 ... 11.3)		

I 185; —29° 1955; 8.8

A.R. 7<sup>h</sup> 35<sup>m</sup> 54<sup>s</sup>; Decl. —29° 50'

21.014	191.0	1.85	7.2	3	370
21.383	190.8	1.68	10.6	3	370
21.20	190.9	1.76	(9.8 ... 10.8) A <sup>?</sup>		

h 2411; —26° 2387; 8.9

A.R. 7<sup>h</sup> 36<sup>m</sup> 17<sup>s</sup>; Decl. —26° 43'

19.202	199.1	15.39	10.3	1 $\frac{1}{2}$	370
19.218	199.3	15.30	9.2	2	370
19.21	199.2	15.34	(9.2 ... 10.6)		

Hd 107<sup>?</sup>; —23° 2640 + 1; 8.0 + 8.7

A.R. 7<sup>h</sup> 37<sup>m</sup> 4<sup>s</sup>; Decl. —23° 50'

20.141	165.3	28.22	9.5	1 $\frac{1}{2}$	370
20.157	165.1	28.21	9.9	3	370
20.15	165.2	28.21	(8.9 ... 10.0) 235		

h 2415; —28° 2344; 9.4 :

A.R. 7<sup>h</sup> 37<sup>m</sup> 43<sup>s</sup>; Decl. —28° 41'

19.202	127.7	9.71	10.7	1 $\frac{1}{2}$	370
19.218	127.4	9.76	9.4	2	370
19.21	127.5	9.74	(10.9 ... 11.1)		

h 3995; —21° 2647; 8.1

A.R. 7<sup>h</sup> 38<sup>m</sup> 16<sup>s</sup>; Decl. —21° 50'

18.271	254.0	6.26	10.9	2 $\frac{1}{2}$	370
19.218	253.9	6.36	10.0	2	370
19.240	253.5	6.28	9.4	1 $\frac{1}{2}$	370
18.91	253.8	6.30	(8.8 ... 9.9)		

h 4003; —23° 2923; 8.7 :

A.R. 7<sup>h</sup> 42<sup>m</sup> 49<sup>s</sup>; Decl. —23° 53'

20.116	117.6	13.75	7.2	2 $\frac{1}{2}$	370
20.157	117.7	13.68	10.0	2 $\frac{1}{2}$	370
20.14	117.6	13.72	(9.8 ... 11.0) 236		

ε 93; —29° 2102; 9.8

A.R. 7<sup>h</sup> 43<sup>m</sup> 28<sup>s</sup>; Decl. —29° 9'

20.864	41.6	0.83	7.0	3	370
21.383	42.7	0.85	10.9	2	370
21.12	42.1	0.84	(10.6 ... 10.9)		

$h\ 2419; -28^\circ\ 2427; 9.9$ A.R.  $7^h\ 43^m\ 47^s$ ; Decl.  $-28^\circ\ 53'$ 

19.202	103.4	11.02	11.0	$1\frac{1}{2}$	370
19.218	102.1	11.52	9.6	2	370
19.21	102.7	11.27	(11.7 ... 12.4)		

 $\hat{e}\ 94; -29^\circ\ 2107; 8.7$ A.R.  $7^h\ 43^m\ 53^s$ ; Decl.  $-29^\circ\ 58'$ 

20.864	280.5	1.46	7.2	3	370
21.383	282.7	1.48	10.7	$2\frac{1}{2}$	370
21.12	281.6	1.47	(10.3 ... 10.5)		

 $h\ 4007; -27^\circ\ 2465 + 4; 9.2 + 9.2$ A.R.  $7^h\ 44^m\ 53^s$ ; Decl.  $-27^\circ\ 57'$ 

20.116	272.6	17.36	7.0	$2\frac{1}{2}$	370
20.160	272.4	17.42	7.7	2	370
20.14	272.5	17.39	(9.4 ... 11.2)		

 $Hd\ 109; -22^\circ\ 2781; 9.2$ A.R.  $7^h\ 45^m\ 2^s$ ; Decl.  $-22^\circ\ 52'$ 

18.271	117.9	5.21	11.1	2	370
19.218	118.1	5.51	10.2	2	370
19.240	116.5	5.76	9.6	$1\frac{1}{2}$	370
18.91	117.5	5.49	(8.8 ... 12.1)		

 $\hat{e}\ 95; -29^\circ\ 2138; 8.2$ A.R.  $7^h\ 46^m\ 56^s$ ; Decl.  $-29^\circ\ 21'$ 

20.864	97.6	1.44	7.4	3	370
21.014	99.7	1.14	7.4	$2\frac{1}{2}$	370
20.94	98.6	1.29	(8.2 ... 10.4)		

 $h\ 2421; -27^\circ\ 2506; 9.6$ A.R.  $7^h\ 47^m\ 7^s$ ; Decl.  $-27^\circ\ 29'$ 

19.218	62.1	10.02	9.8	2	370
19.240	62.1	10.18	9.9	$1\frac{1}{2}$	370
19.23	62.1	10.10	(9.6 ... 12.0)		236

 $h\ 4022; -21^\circ\ 2990 + 89; 9.0 + 9.7$ A.R.  $7^h\ 53^m\ 20^s$ ; Decl.  $-21^\circ\ 10'$ 

20.116	6.4	15.43	7.3	$2\frac{1}{2}$	370
20.179	6.6	15.62	7.4	$2\frac{1}{2}$	370
20.15	6.5	15.52	(8.30 ... 11.5)		

 $h\ 4024; -29^\circ\ 2222; 8.4$ A.R.  $7^h\ 55^m\ 16^s$ ; Decl.  $-29^\circ\ 11'$ 

20.116	82.7	10.10	7.5	3	370
20.179	83.2	10.07	7.5	$2\frac{1}{2}$	370
20.15	82.9	10.09	(8.0 ... 9.4)		F

 $h\ 4037$ 

Ver la nota

237

 $h\ 4041; -22^\circ\ 3093; 8.3$ A.R.  $7^h\ 59^m\ 49^s$ ; Decl.  $-22^\circ\ 5'$ 

20.190	127.2	36.41	8.3	$2\frac{1}{2}$	370
			(7.5 ... 14.0)		120

 $\Delta\ 61; -26^\circ\ 3033 + 5; 7.5 + 9.1$ A.R.  $8^h\ 1^m\ 53^s$ ; Decl.  $-26^\circ\ 46'$ 

20.095	34.7	70.75	10.6	$1\frac{1}{2}$	370
20.097	34.6	70.64	10.4	2	370
20.10	34.6	70.69	(7.8 ... 9.4)		195

**4544;  $h\ 4070$** A.R.  $8^h\ 11^m\ 19^s$ ; Decl.  $-14^\circ\ 47'$ 

20.193	105.2	30.34	7.7	$2\frac{1}{2}$	370
20.198	105.3	30.34	8.1	$2\frac{1}{2}$	370
20.20	105.3	30.34	(7.30 ... 11.9)		

 $h\ 4072; -19^\circ\ 3331; 8.5$ A.R.  $8^h\ 13^m\ 10^s$ ; Decl.  $-19^\circ\ 35'$ 

20.193	166.1	13.52	7.8	$2\frac{1}{2}$	370
20.198	165.3	13.62	8.3	2	370
20.20	165.7	13.57	(8.5 ... 13.3)		F

 $h\ 4078; -23^\circ\ 3667; 8.3$ A.R.  $8^h\ 15^m\ 30^s$ ; Decl.  $-23^\circ\ 43'$ 

20.097	136.7	11.06	10.6	2	370
20.116	136.8	11.12	7.6	3	370
20.11	136.8	11.09	(8.6 ... 11.1)		F

 $h\ 4088; -28^\circ\ 3093; 7.1$ A.R.  $8^h\ 18^m\ 52^s$ ; Decl.  $-28^\circ\ 35'$ 

20.198	285.2	26.84	8.4	2	370
20.204	285.0	26.90	8.1	$2\frac{1}{2}$	370
20.20	285.1	26.87	(7.1 ... 12.2)		

 $S\ 569; -25^\circ\ 3707 + 6; 8.2 + 8.8$ A.R.  $8^h\ 25^m\ 13^s$ ; Decl.  $-25^\circ\ 38'$ 

19.240	337.9	28.55	11.5	$1\frac{1}{2}$	370
19.270	338.0	28.26	9.6	2	370
19.336	338.1	28.41	10.2	2	370
19.28	338.0	28.41	(8.1 ... 9.5)		R

**4734;  $h\ 4124$** A.R.  $8^h\ 36^m\ 9^s$ ; Decl.  $-15^\circ\ 31'$ 

20.190	111.3	30.96	8.6	$2\frac{1}{2}$	370
20.193	111.8	31.07	8.1	$2\frac{1}{2}$	370
20.19	111.5	31.02	(5.0 ... 13.0)		R

*h* 2463;  $-25^{\circ} 38'41''$ ; 9.4

A.R.  $8^h 37^m 41^s$ ; Decl.  $-25^{\circ} 36'$

19.240	308.8	11.71	11.7	1½	370
19.270	309.4	11.20	9.9	2	370
19.326	309.4	11.68	10.5	2	370
19.28	309.2	11.53	(9.5R ... 11.9)		

*h* 2464;  $-27^{\circ} 33'74''$ ; 10.0

A.R.  $8^h 38^m 27^s$ ; Decl.  $-27^{\circ} 49'$

19.218	350.9	15.70	11.1	1½	370
19.240	351.2	16.15	11.9	1½	370
19.251	351.8	16.08	11.6	2	370
19.24	351.3	15.98	(10.5 ... 12.1)		

Hd 119;  $-28^{\circ} 33'64''$ ; 8.6

A.R.  $8^h 38^m 45^s$ ; Decl.  $-28^{\circ} 33'$

19.251	328.7	3.95	11.8	2½	370
19.270	329.4	3.61	10.2	1½	370
19.336	329.2	3.80	10.6	2	370
19.29	329.1	3.79	(9.1 ... 11.0)		

*h* 4141;  $-28^{\circ} 34'08''$ ; 9.0

A.R.  $8^h 43^m 52^s$ ; Decl.  $-28^{\circ} 21'$

19.218	332.0	9.88	11.2	2	370
19.251	331.2	10.26	12.0	2½	370
19.270	331.0	9.88	10.6	1½	370
19.25	331.4	10.01	(9.3 ... 10.9)		

**4838**; *h* 4146

A.R.  $8^h 46^m 48^s$ ; Decl.  $-12^{\circ} 47'$

20.190	104.4	33.45	8.7	2½	370
20.193	104.7	33.40	8.5	2	370
20.19	104.5	33.43	(5.5 ... 13.5)		51

$\hat{\epsilon}$  96;  $-28^{\circ} 34'86''$ ; 9.0

A.R.  $8^h 51^m 43^s$ ; Decl.  $-28^{\circ} 37'$

20.231	232.1	0.67	8.5	3	650
20.236	236.0	0.66	8.2	3	475
20.239	238.2	0.74	8.9	3	650
20.24	235.4	0.69	(9.7 ... 10.1)		

I 818;  $-28^{\circ} 35'06''$ ; 9.2

A.R.  $8^h 53^m 14^s$ ; Decl.  $-28^{\circ} 56'$

20.231	344.9	1.18	8.6	3	370
20.236	340.6	1.27	8.3	3	370
20.247	345.1	1.30	9.3	2½	370
20.24	343.5	1.25	(8.6 ... 11.5)		23

*h* 2481;  $-28^{\circ} 35'13''$ ; 9.5

A.R.  $8^h 53^m 39^s$ ; Decl.  $-28^{\circ} 37'$

19.218	282.6	8.56	11.5	2	370
19.251	283.7	8.29	12.2	2	370
19.270	283.5	8.45	10.9	1½	370
19.25	283.3	8.43	(9.0 ... 11.9)		238

**4892**; *h* 4160; Anon.

A.R.  $8^h 54^m 44^s$ ; Decl.  $-12^{\circ} 11'$

20.190	284.6	10.30	8.9	2½	370
20.193	284.5	10.43	8.6	2	370
20.19	284.6	10.36	(11.0 ... 13.3)		228

*h* 4162;  $-21^{\circ} 40'58''$ ; 8.5

A.R.  $8^h 55^m 41^s$ ; Decl.  $-21^{\circ} 32'$

20.179	45.4	5.66	8.1	2½	370
20.190	45.0	5.65	9.0	2½	370
20.193	45.4	5.70	8.7	2½	370
20.19	45.3	5.67	(9.7 ... 9.8)		F

*h* 4168;  $-28^{\circ} 35'71''$ ; 10.2

A.R.  $8^h 59^m 7^s$ ; Decl.  $-28^{\circ} 51'$

20.100	250.1	8.36	8.1	2½	370
20.116	249.9	8.81	7.7	2	370
20.179	248.6	8.72	8.2	2½	370
20.13	249.5	8.63	(11.2 ... 11.5)		195

*h* 4174; SD  $-15^{\circ} 27'04''$ ; 9.8

A.R.  $9^h 1^m 45^s$ ; Decl.  $-15^{\circ} 14'$

20.198	258.9	9.47	8.6	2	370
20.204	258.9	9.54	8.4	2½	370
20.20	258.9	9.50	(10.7 ... 11.0)		

IIIh 321 = *h* 4183;  $-29^{\circ} 29'33''$ ; 6.9

A.R.  $9^h 4^m 51^s$ ; Decl.  $-29^{\circ} 53'$

20.095	147.1	17.79	10.8	2½	370
20.097	147.2	17.89	10.8	2	370
20.10	147.1	17.84	(6.2 ... 9.8)		239

*h* 4199;  $-27^{\circ} 37'34''$ ; 7.6

A.R.  $9^h 14^m 43^s$ ; Decl.  $-27^{\circ} 16'$

20.100	110.6	11.76	8.4	2	370
20.116	110.9	11.72	8.1	2½	370
20.11	110.8	11.74	(8.2 ... 9.6)		

$\delta 97; -29^\circ 2970; 9.2$ A.R.  $9^h 15^m 1^s$ ; Decl.  $-29^\circ 3'$ 

20.236	184.8	2.67	8.6	3	370
20.239	183.7	2.92	9.1	3	650
20.247	183.3	2.63	9.5	$2\frac{1}{2}$	370
20.24	183.9	2.74	(10.0 ... 10.1)		

 $I 1130; -29^\circ 2972; 8.8$ A.R.  $9^h 15^m 30^s$ ; Decl.  $-29^\circ 19'$ 

20.236	244.3	2.01	8.7	3	370
20.239	243.8	1.89	9.2	3	370
20.247	250.2	1.73	9.6	$2\frac{1}{2}$	370
20.24	246.1	1.88	(9.4 ... 11.6)		23

 $I 198; -28^\circ 3706; 7.4$ A.R.  $9^h 15^m 31^s$ ; Decl.  $-28^\circ 43'$ 

20.100	184.6	0.39	8.2	$2\frac{1}{2}$	475
20.179	188.3	0.46	8.7	$2\frac{1}{2}$	650
20.193	185.8	0.46	8.9	$2\frac{1}{2}$	650
20.16	186.2	0.44	(8.8 ... 9.0)		23

 $h 4201; \text{Cód} -28^\circ 7169; 9.5$ A.R.  $9^h 16^m 13^s$ ; Decl.  $-28^\circ 29'$ 

20.116	85.3	5.35	7.9	2	370
20.179	85.5	5.54	8.6	$2\frac{1}{2}$	370
20.193	85.2	5.77	8.8	$2\frac{1}{2}$	370
20.16	85.3	5.55	(11.1 ... 11.9)		

 $I 834; -29^\circ 3050; 9.0$ A.R.  $9^h 32^m 28^s$ ; Decl.  $-29^\circ 40'$ 

20.231	210.2	0.98	8.9	3	475
20.236	210.5	0.91	9.0	3	475
20.239	209.9	0.98	9.4	$3\frac{1}{2}$	370
20.24	210.2	0.96	(9.7 ... 9.8)		23

 $h 4227; \text{Cód} -28^\circ 7475; 9.3$ A.R.  $9^h 32^m 45^s$ ; Decl.  $-28^\circ 42'$ 

18.287	337.4	11.43	12.8	$1\frac{1}{2}$	370
19.218	336.1	11.75	12.7	$1\frac{1}{2}$	370
19.251	336.6	12.52	12.4	$1\frac{1}{2}$	370
18.92	336.7	11.90	(10.0 ... 13.2)		

 $h 2501; -26^\circ 4008; 9.0$ A.R.  $9^h 33^m 15^s$ ; Decl.  $-26^\circ 12'$ 

19.218	94.9	11.34	11.6	$1\frac{1}{2}$	370
19.251	94.5	11.48	12.5	2	370
19.23	94.7	11.41	(9.3 ... 9.6)		

BC; C = 11.3

19.251	136.3	20.40	12.7	$1\frac{1}{2}$	370
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 $h 4233; -20^\circ 4693 + 2; 8.4 + 9.6$ A.R.  $9^h 36^m 55^s$ ; Decl.  $-20^\circ 35'$ 

20.179	281.8	16.64	8.8	2	370
20.193	281.1	16.95	9.0	$2\frac{1}{2}$	370
20.198	281.3	16.89	8.8	2	370
20.19	281.4	16.83	(8.5 ... 11.4)		

 $\delta 98; -29^\circ 3116; 8.4$ A.R.  $9^h 44^m 5^s$ ; Decl.  $-29^\circ 53'$ 

20.236	57.4	0.41	9.3	3	650
20.239	48.3	0.46	9.6	3	650
20.277	46.7	0.53	9.4	3	650
20.25	50.8	0.47	(9.0 ... 9.9)		

**5242; h 4262**A.R.  $9^h 48^m 38^s$ ; Decl.  $-12^\circ 21'$ 

20.179	102.9	7.87	9.0	2	370
20.193	102.8	7.80	9.1	$2\frac{1}{2}$	370
20.198	102.8	7.62	9.0	2	370
20.19	102.8	7.76	(9.0 ... 11.3)		F

 $\delta 99; -29^\circ 3172; 8.6$ A.R.  $9^h 57^m 39^s$ ; Decl.  $-29^\circ 41'$ 

20.231	248.8	0.48	9.4	3	1300
20.236	255.2	0.45	9.5	3	650
20.239	250.2	0.51	9.9	$3\frac{1}{2}$	650
20.24	251.4	0.48	(9.4 ... 10.0)		

**5299; h 4279; Anon.**A.R.  $9^h 57^m 58^s$ ; Decl.  $+16^\circ 55'$ 

20.198	297.2	10.76	9.4	2	370
20.204	297.6	10.76	8.6	$2\frac{1}{2}$	370
20.20	297.4	10.76	(10.9 ... 11.3)		72; 228

 $h 4285; -22^\circ 4608; 7.4$ A.R.  $10^h 1^m 5^s$ ; Decl.  $-22^\circ 33'$ 

20.116	358.4	9.29	9.0	$1\frac{1}{2}$	370
20.179	357.8	8.88	9.3	$2\frac{1}{2}$	370
20.193	357.4	8.91	9.3	3	370
20.16	357.9	9.03	(8.0 ... 10.7)		

 $h 4309; \text{Cód} -29^\circ 8297; 9.5$ A.R.  $10^h 16^m 37^s$ ; Decl.  $-29^\circ 44'$ 

19.218	207.6	17.58	12.9	1	370
19.235	208.1	17.43	13.4	2	370
19.23	207.9	17.50	(11.1 ... 11.8)		



*h* 4313; —28° 4130; 9.0

A.R. 10<sup>h</sup> 18<sup>m</sup> 2<sup>s</sup>; Decl. —28° 58'

19.218	313.2	10.33	13.1	1½	370
19.235	313.4	10.33	13.6	2½	370
19.23	313.3	10.33	(9.8 ... 9.9)		

Hh 352 = *h* 4321; ε Antliae; 6.2

A.R. 10<sup>h</sup> 24<sup>m</sup> 4<sup>s</sup>; Decl. —30° 0'

19.999	226.2	11.04	9.6	2½	370
20.057	226.3	11.06	11.9	2	370
20.03	226.2	11.05	(6.2 ... 9.6)		F

*h* 4322; —24° 4520; 8.6

A.R. 10<sup>h</sup> 24<sup>m</sup> 42<sup>s</sup>; Decl. —24° 16'

20.198	102.1	13.99	10.1	2½	370
20.215	105.7	14.21	13.3	2½	370
20.228	103.2	14.59	10.0	2½	370
20.21	103.7	14.26	(8.6 ... 13.6)		

*h* 4336; —29° 3281; 9.7

A.R. 10<sup>h</sup> 30<sup>m</sup> 41<sup>s</sup>; Decl. —29° 52'

18.274	24.8	3.53	13.8	1½	370
19.218	25.8	3.94	13.3	1½	370
19.235	25.2	3.79	13.8	2½	370
18.91	25.3	3.75	(10.3 ... 10.8)		N

*h* 4365; —27° 4221; 10.2

A.R. 10<sup>h</sup> 40<sup>m</sup> 43<sup>s</sup>; Decl. —27° 31'

20.179	100.2	16.37	9.7	2	370
20.187	100.7	16.39	10.2	3	370
20.18	100.5	16.38	(9.9 ... 13.9)		198

*h* 4372; Cód —28° 8436; 9.6

A.R. 10<sup>h</sup> 41<sup>m</sup> 53<sup>s</sup>; Decl. —28° 7'

19.232	313.1	12.34	14.0	2½	370
19.235	312.4	12.66	14.2	2	370
19.23	312.8	12.50	(10.9 ... 12.2)		

*h* 4384; Cód —26° 8247; 9.6

A.R. 10<sup>h</sup> 51<sup>m</sup> 13<sup>s</sup>; Decl. —26° 16'

19.232	30.0	17.94	14.2	2	370
19.235	29.1	17.61	14.4	2	370
19.23	29.6	17.78	(10.8 ... 11.3)		

*h* 4412; —28° 4233; 7.8

A.R. 11<sup>h</sup> 4<sup>m</sup> 11<sup>s</sup>; Decl. —28° 57'

20.179	266.1	12.79	9.9	2½	370
20.198	266.5	12.63	10.3	2½	370
20.19	266.3	12.71	(8.2 ... 9.0)		D?

*h* 4418; —29° 3458; 8.6

A.R. 11<sup>h</sup> 8<sup>m</sup> 34<sup>s</sup>; Decl. —29° 15'

20.198	255.1	7.38	10.5	2½	370
20.215	254.7	7.39	13.5	2½	370
20.228	254.7	7.35	10.5	3	370
20.21	254.8	7.37	(9.3 ... 9.8)		

ε 100; —29° 3464; 9.8

A.R. 11<sup>h</sup> 10<sup>m</sup> 33<sup>s</sup>; Decl. —29° 53'

20.198	325.2	2.17	10.8	2½	370
20.228	324.3	2.10	10.7	3	370
20.239	325.3	1.96	10.6	3½	370
20.22	324.9	2.08	(9.8 ... 12.9)		

*h* 4422; —29° 3466; 8.9

A.R. 11<sup>h</sup> 10<sup>m</sup> 50<sup>s</sup>; Decl. —29° 28'

20.198	348.7	9.91	11.1	2	370
20.215	349.4	9.84	13.6	2½	370
20.228	349.0	9.99	10.6	3	370
20.21	349.0	9.91	(9.4 ... 10.2)		

ε 101; Cód —29° 8971; 9.6

A.R. 11<sup>h</sup> 11<sup>m</sup> 9<sup>s</sup>; Decl. —29° 43'

20.198	282.3	3.54	11.0	2	370
20.215	285.1	3.56	13.8	2½	370
20.228	283.7	3.53	10.8	2½	370
20.21	283.7	3.54	(10.3 ... 10.3)		

*h* 4437; —23° 5153; 9.0

A.R. 11<sup>h</sup> 21<sup>m</sup> 38<sup>s</sup>; Decl. —23° 3'

20.228	319.5	11.65	11.0	3	370
20.237	320.5	11.46	10.9	2	370
20.242	319.8	11.46	10.1	3	370
20.24	319.9	11.52	(9.6 ... 11.0)		

Hh 376 = Δ 111; N Hydrae; 6.0

A.R. 11<sup>h</sup> 26<sup>m</sup> 19<sup>s</sup>; Decl. —28° 36'

20.242	210.2	9.23	10.3	3	370
20.247	209.9	9.22	9.8	2½	370
20.24	210.1	9.23	(6.0 ... 6.2)		C

Hu 1484; —22° 5036; 9.1

A.R. 11<sup>h</sup> 30<sup>m</sup> 15<sup>s</sup>; Decl. —22° 11'

20.228	330.5	2.01	11.1	3½	370
20.239	330.4	2.12	10.9	3½	370
20.242	329.7	1.99	10.4	3	475
20.24	330.2	2.04	(9.6 ... 11.0)		F?

*h* 4470;  $-29^{\circ} 3532$ ; 8.4A.R.  $11^h 39^m 29^s$ ; Decl.  $-29^{\circ} 50'$ 

19.516	316.0	11.01	15.5	$2\frac{1}{2}$	370
19.552	316.2	11.01	15.0	3	370
19.53	316.1	11.01	(8.8 ... 10.1)		

*h* 4472; Cód  $-28^{\circ} 9079$ ; 9.6A.R.  $11^h 40^m 20^s$ ; Decl.  $-28^{\circ} 29'$ 

19.221	34.9	19.60	14.4	2	370
19.232	35.3	19.81	14.4	$2\frac{1}{2}$	370
19.23	35.1	19.70	(10.0 ... 10.2)		

Hu 1489;  $-21^{\circ} 5116$ ; 7.8A.R.  $11^h 49^m 48^s$ ; Decl.  $-21^{\circ} 31'$ 

20.229	215.8	1.63	11.3	$3\frac{1}{2}$	370
20.239	214.9	1.81	11.1	$3\frac{1}{2}$	370
20.242	216.2	1.62	10.5	$2\frac{1}{2}$	475
20.24	215.6	1.69	(7.5 ... 12.3)		N

Hu 1490;  $-24^{\circ} 4754$ ; 8.2A.R.  $11^h 50^m 56^s$ ; Decl.  $-24^{\circ} 49'$ 

20.229	81.5	0.86	11.4	$3\frac{1}{2}$	650
20.239	80.1	0.83	11.2	$3\frac{1}{2}$	650
20.242	79.3	0.87	10.6	3	475
20.24	80.3	0.85	(8.5 ... 9.3)		D?

Hu 1492;  $-25^{\circ} 4872$ ; 8.4A.R.  $11^h 59^m 52^s$ ; Decl.  $-25^{\circ} 7'$ 

20.229	104.9	0.68	11.6	$3\frac{1}{2}$	650
20.239	105.4	0.63	11.3	3	650
20.242	105.4	0.61	10.7	3	475
20.24	105.2	0.64	(9.3 ... 9.8)		N

 $\delta$  102;  $-26^{\circ} 4688$ ; 7.8A.R.  $12^h 10^m 6^s$ ; Decl.  $-26^{\circ} 26'$ 

20.229	351.3	2.12	11.8	$3\frac{1}{2}$	370
20.239	354.0	2.25	11.4	$2\frac{1}{2}$	370
20.242	354.4	2.45	10.9	$2\frac{1}{2}$	370
20.24	353.2	2.27	(8.2 ... 13.3)		

AC = *h* 4509

20.229	115.1	26.89	11.9	3	370
20.239	115.1	27.42	11.5	$2\frac{1}{2}$	370
20.242	114.5	26.85	11.0	$2\frac{1}{2}$	370
20.24	114.9	27.05	(8.2 ... 13.3)		

*h* 4517;  $-19^{\circ} 5142 + 3$ ; 9.3 + 9.7A.R.  $12^h 17^m 12^s$ ; Decl.  $-19^{\circ} 36'$ 

20.247	186.0	14.39	9.9	$2\frac{1}{2}$	370
20.256	186.1	14.66	11.5	$2\frac{1}{2}$	370
20.267	185.7	14.35	11.0	$1\frac{1}{2}$	370
20.26	185.9	14.27	(9.5 ... 10.3)		F

 $\delta$  103;  $-29^{\circ} 3646$ ; 8.7A.R.  $12^h 31^m 11^s$ ; Decl.  $-29^{\circ} 55'$ 

20.229	281.6	0.68	12.1	$3\frac{1}{2}$	650
20.239	277.7	0.63	11.6	3	650
20.242	281.3	0.61	11.3	$2\frac{1}{2}$	650
20.24	280.2	0.64	(9.6 ... 10.3)		

 $\delta$  104;  $-21^{\circ} 5398$ ; 9.1A.R.  $12^h 35^m 4^s$ ; Decl.  $-21^{\circ} 47'$ 

19.221	273.0	3.07	15.7	3	370
19.232	273.0	3.00	14.8	$2\frac{1}{2}$	475
19.235	271.9	3.03	14.8	2	370
19.23	272.6	3.03	(9.7 ... 10.0)		

Hu 1497;  $-25^{\circ} 4995$ ; 9.2A.R.  $12^h 37^m 59^s$ ; Decl.  $-25^{\circ} 25'$ 

19.221	338.5	2.00	14.6	2	370
19.232	341.2	1.97	14.6	$2\frac{1}{2}$	475
19.235	335.0	2.01	14.6	2	370
19.23	338.2	1.99	(9.3 ... 10.3)		142

\* *h* 4549;  $-23^{\circ} 5599$ ; 9.4 :A.R.  $12^h 39^m 34^s$ ; Decl.  $-23^{\circ} 46'$ 

19.221	115.2	12.71	14.8	$2\frac{1}{2}$	370
19.232	114.9	12.85	15.6	$2\frac{1}{2}$	370
19.23	115.0	12.78	(10.0 ... 11.2)		142

O. Stone 24 = I 515;  $-21^{\circ} 5440$ ; 8.7A.R.  $12^h 40^m 0^s$ ; Decl.  $-21^{\circ} 23'$ 

19.221	309.3	1.32	15.9	$2\frac{1}{2}$	370
19.232	309.2	1.32	15.5	$2\frac{1}{2}$	475
19.484	310.6	1.08	16.9	$2\frac{1}{2}$	650
19.31	309.7	1.24	(9.1 ... 10.7)		M

 $\delta$  105;  $-28^{\circ} 4540$ ; 8.6A.R.  $12^h 40^m 58^s$ ; Decl.  $-28^{\circ} 56'$ 

20.229	232.1	0.26	12.4	$3\frac{1}{2}$	1300
20.239	235.0	0.28	11.9	3	650
20.264	232.6	0.35	12.4	$3\frac{1}{2}$	650
20.24	233.2	0.30	(9.1 ... 9.4)		

\* *h* 4551;  $-24^{\circ} 4920$ ; 8.8 :A.R.  $12^h 41^m 50^s$ ; Decl.  $-24^{\circ} 9'$ 

19.221	312.5	12.61	15.0	$2\frac{1}{2}$	370
19.232	312.2	12.59	15.8	3	370
19.23	312.3	12.60	(9.2 ... 10.1)		142

*h* 4553;  $-29^{\circ} 3669$ ; 9.2

A.R.  $12^h 44^m 19^s$ ; Decl.  $-29^{\circ} 5'$

19.221	347.2	11.78	16.3	2	370
19.232	345.9	11.58	16.0	3	370
19.23	346.5	11.68	(9.9 ... 11.0)		

$\delta$  106;  $-29^{\circ} 3672$ ; 8.1

A.R.  $12^h 45^m 30^s$ ; Decl.  $-30^{\circ} 0'$

20.239	247.1	1.75	12.1	3	370
20.242	245.6	1.88	11.4	$2\frac{1}{2}$	370
20.636	249.8	1.44	16.7	$2\frac{1}{2}$	370
20.644	249.0	1.72	16.6	$2\frac{1}{2}$	370
20.44	247.9	1.70	(8.3 ... 12.6)		

*h* 4558;  $-29^{\circ} 3684 + 3$ ; 9.8 + 9.3

A.R.  $12^h 49^m 54^s$ ; Decl.  $-29^{\circ} 29'$

20.229	184.1	31.77	12.6	$2\frac{1}{2}$	370
20.239	183.9	31.73	12.2	3	370
20.23	184.0	31.75	(9.5 ... 9.8)		R

Hu 1500;  $-23^{\circ} 5703$ ; 7.8

A.R.  $13^h 4^m 20^s$ ; Decl.  $-23^{\circ} 32'$

20.240	29.9	3.53	12.4	3	370
20.264	29.0	3.43	12.6	$3\frac{1}{2}$	370
20.442	27.2	3.17	15.2	$2\frac{1}{2}$	475
20.540	29.5	3.75	16.9	$2\frac{1}{2}$	370
20.37	28.9	3.47	(7.6 ... 12.4)		142

Hu 1501;  $-24^{\circ} 5022$ ; 9.0

A.R.  $13^h 8^m 30^s$ ; Decl.  $-24^{\circ} 16'$

20.240	197.6	0.58	12.6	3	650
20.264	200.5	0.46	12.7	$3\frac{1}{2}$	650
20.540	204.3	0.53	17.1	$2\frac{1}{2}$	650
20.35	200.8	0.52	(9.4 ... 9.4)		M <sup>2</sup>

\* Hu 1502;  $-25^{\circ} 5153$ ; 8.8

A.R.  $13^h 13^m 8^s$ ; Decl.  $-25^{\circ} 15'$

19.484	29.0	1.19	17.1	$2\frac{1}{2}$	650
19.590	36.2	1.19	15.8	2	475
20.229	33.3	1.23	12.8	$2\frac{1}{2}$	475
19.77	32.8	1.20	(9.6 ... 10.1)		142

\* *h* 2655;  $-22^{\circ} 5615$ ; 9.8

A.R.  $13^h 24^m 8^s$ ; Decl.  $-22^{\circ} 50'$

19.233	274.4	14.22	16.2	3	370
19.306	275.5	14.42	13.3	$1\frac{1}{2}$	370
19.27	274.9	14.32	(9.4 ... 12.5)		142

$\delta$  107;  $-29^{\circ} 3785$ ; 8.2

A.R.  $13^h 28^m 14^s$ ; Decl.  $-29^{\circ} 18'$

20.229	84.6	2.10	13.2	$2\frac{1}{2}$	475
20.240	85.2	2.21	12.9	$2\frac{1}{2}$	370
20.242	84.8	2.15	11.5	$2\frac{1}{2}$	370
20.24	84.9	2.15	(8.5 ... 8.6)		

$\delta$  108;  $-29^{\circ} 3790$ ; 9.0

A.R.  $13^h 29^m 30^s$ ; Decl.  $-29^{\circ} 3'$

20.264	138.1	0.82	13.0	3	370
20.540	135.0	0.78	17.3	$2\frac{1}{2}$	475
20.644	138.0	0.86	16.8	$2\frac{1}{2}$	650
20.48	137.0	0.82	(9.8 ... 9.8)		

*h* 4599;  $-29^{\circ} 3795$ ; 10.3

A.R.  $13^h 30^m 30^s$ ; Decl.  $-29^{\circ} 19'$

20.229	214.8	10.38	13.3	$2\frac{1}{2}$	370
20.240	215.5	10.37	13.0	$2\frac{1}{2}$	370
20.23	215.2	10.38	(10.4 ... 11.2)		

*h* 4613;  $-29^{\circ} 3842 + 1$ ; 9.6 + 10.3

A.R.  $13^h 40^m 27^s$ ; Decl.  $-29^{\circ} 46'$

20.242	213.2	19.78	11.7	$2\frac{1}{2}$	370
20.256	213.0	20.11	12.2	1	370
20.338	213.5	20.19	12.0	$1\frac{1}{2}$	370
20.28	213.2	20.03	(9.7 ... 10.3)		

\* Hu 1262;  $-21^{\circ} 5633$ ; 7.1

A.R.  $13^h 47^m 52^s$ ; Decl.  $-21^{\circ} 39'$

19.484	297.3	1.13	17.2	$2\frac{1}{2}$	650
			(7.0 ... 13.5)		

*h* 4639;  $-28^{\circ} 4823$ ; 9.0

A.R.  $13^h 53^m 31^s$ ; Decl.  $-28^{\circ} 41'$

20.242	337.4	9.22	11.9	$2\frac{1}{2}$	370
20.338	337.6	9.22	12.2	$1\frac{1}{2}$	370
20.636	337.8	9.44	17.2	2	370
20.41	337.6	9.29	(9.4 ... 10.8)		

**6697**; *h* 4640 Ver la nota 162

$-28^{\circ} 4889 + 90$ ; 8.6 + 8.8

A.R.  $14^h 7^m 34^s$ ; Decl.  $-28^{\circ} 40'$

A, BC = *h* 4664

20.242	16.4	17.88	12.0	$2\frac{1}{2}$	370
20.264	16.1	17.82	13.8	$2\frac{1}{2}$	370
20.540	16.1	17.89	17.5	$2\frac{1}{2}$	370
20.35	16.2	17.86	(8.8 ... (9.3))		F

(Sigue Continued)

BC =  $\delta$  109

20.242	228.8	0.35	12.1	2½	650
20.264	230.5	0.41	13.7	2½	650
20.25	229.6	0.38	(9.9 ... 10.3)		

*h* 4678;  $-23^\circ 59'01''$ ; 10.0A.R. 14<sup>h</sup> 18<sup>m</sup> 21<sup>s</sup>; Decl.  $-23^\circ 51'$ 

19.306	311.5	8.82	14.0	1½	370
19.503	310.7	8.61	18.4	1½	370
19.585	314.3	8.49	16.7	2	370
19.46	312.2	8.64	(9.6 ... 12.7)		F

6995; *h* 4700A.R. 14<sup>h</sup> 39<sup>m</sup> 49<sup>s</sup>; Decl.  $-10^\circ 35'$ 

20.540	221.6	25.92	17.7	2	370
20.543	221.6	25.79	16.9	1½	370
20.54	221.6	25.86	(8.9 ... 10.4)		F

\* Hu 1511;  $-24^\circ 53'76''$ ; 9.2A.R. 14<sup>h</sup> 41<sup>m</sup> 18<sup>s</sup>; Decl.  $-24^\circ 7'$ 

19.484	309.5	0.77	17.4	2½	650
19.648	311.0	0.84	17.2	2½	475
19.57	310.2	0.80	(9.8 ... 9.9)		F

\* Hu 1512;  $-23^\circ 59'87''$ ; 8.6A.R. 14<sup>h</sup> 42<sup>m</sup> 20<sup>s</sup>; Decl.  $-23^\circ 11'$ 

19.484	228.9	1.01	17.5	3	650
19.648	228.6	1.07	17.3	3	475
19.57	228.8	1.04	(9.2 ... 9.3)		F

7017; *h* 4708; Anon.A.R. 14<sup>h</sup> 44<sup>m</sup> 4<sup>s</sup>; Decl.  $-4^\circ 56'$ 

20.541	338.8	20.37	18.1	2	370
20.543	338.9	20.69	17.1	1½	370
20.647	339.1	20.65	17.2	2	370
20.58	338.9	20.57	(10.9 ... 11.1)		228

*h* 4720; SD  $-5^\circ 39'72''$ ; 9.2A.R. 14<sup>h</sup> 50<sup>m</sup> 56<sup>s</sup>; Decl.  $-5^\circ 23'$ 

20.541	213.5	[13.57]	18.4	1	370
20.543	213.1	13.07	17.2	1½	370
20.647	213.5	13.02	17.3	2½	370
20.58	213.4	13.04	(10.0 ... 10.3)		

*h* 4736;  $-24^\circ 54'55''$ ; 9.8A.R. 15<sup>h</sup> 2<sup>m</sup> 16<sup>s</sup>; Decl.  $-24^\circ 36'$ 

19.503	135.7	10.79	18.5	1½	370
19.585	138.6	10.82	16.9	1½	370
19.598	137.2	10.48	16.2	2	370
19.56	137.2	10.70	(10.2 ... 11.7)		

*h* 4756 =  $\beta$  227;  $-23^\circ 6'142''$ ; 7.0A.R. 15<sup>h</sup> 12<sup>m</sup> 8<sup>s</sup>; Decl.  $-23^\circ 50'$ 

19.222	174.4	1.99	17.1	2½	475
19.233	174.0	2.15	16.5	3	475
19.268	171.2	2.06	15.0	2½	650
19.24	173.2	2.07	(7.6 ... 9.2)		240

 $\beta$  228;  $-23^\circ 6'146''$ ; 7.1A.R. 15<sup>h</sup> 12<sup>m</sup> 38<sup>s</sup>; Decl.  $-23^\circ 50'$ 

19.222	310.6	0.99	17.2	2½	475
19.233	313.1	0.83	16.7	3	475
19.268	312.1	1.01	15.2	2	650
19.24	311.9	0.94	(8.0 ... 8.1)		240

Hu 1515;  $-24^\circ 55'01''$ ; 8.4A.R. 15<sup>h</sup> 13<sup>m</sup> 10<sup>s</sup>; Decl.  $-24^\circ 32'$ 

19.484	154.3	2.08	17.6	2½	650
19.648	158.2	2.21	17.5	3	475
* 18.89	155.3	2.09	(9.0 ... 12.7)		F

Lv 6 = Egbert 4;  $-26^\circ 54'44''$ ; 8.1A.R. 15<sup>h</sup> 13<sup>m</sup> 26<sup>s</sup>; Decl.  $-26^\circ 35'$ 

19.503	28.1	16.78	18.6	1½	370
19.585	28.8	16.52	17.0	1½	370
19.598	28.9	16.68	16.4	2	370
19.56	28.6	16.66	(8.2 ... 10.3)		241

*h* 4775;  $-19^\circ 58'24''$ ; 9.1 :A.R. 15<sup>h</sup> 21<sup>m</sup> 48<sup>s</sup>; Decl.  $-19^\circ 28'$ 

20.541	185.9	12.31	18.6	1½	370
20.543	185.5	12.20	17.4	2	370
20.54	185.7	12.25	(10.2 ... 10.4)		

\* Hu 1516;  $-22^\circ 60'64''$ ; 8.8A.R. 15<sup>h</sup> 37<sup>m</sup> 18<sup>s</sup>; Decl.  $-22^\circ 57'$ 

19.484	248.5	1.34	17.7	2½	650
19.648	243.9	1.49	18.3	2½	475
19.57	246.2	1.41	(9.2 ... 10.3)		F

7378; *h* 4804A.R. 15<sup>h</sup> 39<sup>m</sup> 22<sup>s</sup>; Decl.  $-8^\circ 59'$ 

20.543	283.4	19.34	17.6	2	370
20.639	283.6	19.62	18.6	2	370
20.647	283.3	19.43	18.3	2	370
20.61	283.4	19.46	(9.6 ... 10.2)		F?

*h* 4807;  $-20^\circ 62'33''$ ; 8.2A.R. 15<sup>h</sup> 40<sup>m</sup> 31<sup>s</sup>; Decl.  $-20^\circ 52'$ 

20.543	2.7	11.02	17.8	2	370
20.647	3.3	10.96	18.5	2	370
20.60	3.0	10.99	(8.0 ... 13.0)		F?

\* Hu 1274 Ver la nota 242

Glasenapp 6;  $-27^{\circ} 5361 + 60$ ; 9.6 + 9.6

A.R.  $16^{\text{h}} 0^{\text{m}} 41^{\text{s}}$ ; Decl.  $-27^{\circ} 19'$

19.639	282.5	46.32	17.7	2	370
19.645	281.8	46.38	17.5	$1\frac{1}{2}$	370
19.64	282.1	46.35	(9.3 ... 9.6)		243

Hh 507 = h 4850;  $-29^{\circ} 4411$ ; 6.9

A.R.  $16^{\text{h}} 17^{\text{m}} 8^{\text{s}}$ ; Decl.  $-29^{\circ} 25'$

19.752	352.0	6.16	19.6	$2\frac{1}{2}$	370
19.757	353.0	6.24	20.1	2	370
19.75	352.5	6.20	(5.9 ... 6.9)		C

h 4859;  $-28^{\circ} 5328$ ; 9.4

A.R.  $16^{\text{h}} 23^{\text{m}} 20^{\text{s}}$ ; Decl.  $-28^{\circ} 4'$

19.639	273.5	11.35	17.8	2	370
19.708	274.5	11.35	19.7	2	370
19.67	274.0	11.35	(9.8 ... 10.1)		

h 1295; Cód  $-26^{\circ} 11622$ ; 10

A.R.  $16^{\text{h}} 44^{\text{m}} 35^{\text{s}}$ ; Decl.  $-26^{\circ} 28'$

19.640	137.5	11.45	19.3	2	370
19.708	137.6	11.78	20.1	$1\frac{1}{2}$	370
19.784	137.6	11.48	20.7	2	370
19.71	137.6	11.57	(11.1 ... 11.5)		

h 1296; Anon.

A.R.  $16^{\text{h}} 44^{\text{m}} 51^{\text{s}}$ ; Decl.  $-26^{\circ} 28'$

19.640	214.2	15.03	19.4	2	370
19.708	216.4	[16.23]	20.2	$1\frac{1}{2}$	370
19.784	215.5	15.12	20.8	2	370
19.71	215.4	15.08	(12.2 ... 13.1)		228

z 110; Cód  $-26^{\circ} 11661$ ; 9.6

A.R.  $16^{\text{h}} 47^{\text{m}} 3^{\text{s}}$ ; Decl.  $-26^{\circ} 34'$

19.787	64.5	2.69	20.8	2	370
19.801	59.4	2.75	21.1	$2\frac{1}{2}$	370
19.79	62.0	2.72	(10.8 ... 10.9)		

h 4898;  $-26^{\circ} 5761$ ; 9.0

A.R.  $16^{\text{h}} 48^{\text{m}} 23^{\text{s}}$ ; Decl.  $-26^{\circ} 58'$

19.785	123.6	13.99	21.0	$1\frac{1}{2}$	370
19.787	122.9	13.63	20.9	2	370
19.801	122.0	13.47	21.2	2	370
19.79	122.8	13.70	(9.3 ... 12.1)		

h 4902;  $-27^{\circ} 5531$ ; 7.4

A.R.  $16^{\text{h}} 50^{\text{m}} 26^{\text{s}}$ ; Decl.  $-27^{\circ} 25'$

20.541	30.4	11.30	19.3	2	370
20.543	30.7	11.10	19.3	$2\frac{1}{2}$	370
20.54	30.5	11.20	(7.8 ... 10.9)		F

h 4907;  $-24^{\circ} 5783$ ; 8.5

A.R.  $16^{\text{h}} 52^{\text{m}} 40^{\text{s}}$ ; Decl.  $-24^{\circ} 1'$

19.787	40.6	7.85	21.2	$2\frac{1}{2}$	370
19.801	40.9	7.78	21.3	2	370
19.79	40.7	7.82	(9.2 ... 9.6)		F

7827; h 4911 Ver la nota 162

Anonyma;  $-25^{\circ} 5913$ ; 9.8

A.R.  $16^{\text{h}} 54^{\text{m}} 17^{\text{s}}$ ; Decl.  $-25^{\circ} 31'$

19.787	60.2	5.63	21.0	2	370
19.801	61.3	5.78	21.4	2	370
19.79	60.8	5.70	(10.6 ... 11.4)		244

h 4919;  $-28^{\circ} 5539$ ; 8.3

A.R.  $17^{\text{h}} 0^{\text{m}} 16^{\text{s}}$ ; Decl.  $-28^{\circ} 25'$

20.636	262.8	22.92	19.0	2	370
20.639	262.9	23.10	19.7	2	370
20.647	262.8	23.16	18.6	2	370
20.64	262.8	23.06	(8.4 ... 10.8)		F?

BC

20.636	176.9	10.14	19.2	2	370
20.639	177.4	10.44	19.8	$1\frac{1}{2}$	370
20.647	179.0	10.51	18.7	2	370
20.64	177.8	10.36	(10.8 ... 13.2)		

\* Hu 1280;  $-19^{\circ} 6123$ ; 8.6

A.R.  $17^{\text{h}} 1^{\text{m}} 12^{\text{s}}$ ; Decl.  $-19^{\circ} 38'$

20.633	6.9	0.31	18.6	$3\frac{1}{2}$	650
			(9.5 ... 9.7)		P

AB,C; C = 10.5

19.648	3.7	8.77	19.1	$2\frac{1}{2}$	475
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\* Hu 1522;  $-25^{\circ} 5947$ ; 8.8

A.R.  $17^{\text{h}} 4^{\text{m}} 6^{\text{s}}$ ; Decl.  $-25^{\circ} 10'$

19.484	95.1	1.18	17.9	$2\frac{1}{2}$	650
19.648	92.4	0.88	18.9	$2\frac{1}{2}$	475
19.705	91.1	1.00	19.6	3	650
19.61	92.9	1.02	(9.7 ... 9.8)		142

$h\ 4948 = h\ 4851; -22^\circ 6368; 8.3$

A.R.  $17^h\ 17^m\ 9^s$ ; Decl.  $-22^\circ\ 41'$

20.636	105.1	13.40	19.4	$1\frac{1}{2}$	370
20.639	105.2	13.15	20.2	2	370
20.647	104.7	13.21	18.9	2	370
20.64	105.0	13.25	(8.7 ... 11.1)		230

$h\ 4953; -19^\circ 6221 + 2; 8.6 + 9.7$

A.R.  $17^h\ 19^m\ 20^s$ ; Decl.  $-19^\circ\ 25'$

20.636	174.6	18.51	19.6	2	370
20.639	174.6	18.75	20.8	$2\frac{1}{2}$	370
20.645	174.6	19.09	20.4	2	370
20.64	174.6	18.78	(9.1 ... 10.7)		F

**8063;  $h\ 4964$**

A.R.  $17^h\ 28^m\ 6^s$ ; Decl.  $-11^\circ\ 10'$

20.636	225.6	54.26	19.7	2	370
20.639	225.5	54.11	20.9	2	370
20.64	225.5	54.18	(6.2 ... 9.9)		F

$h\ 591; -22^\circ 6418; 8.3 :$

A.R.  $17^h\ 35^m\ 27^s$ ; Decl.  $-22^\circ\ 18'$

19.752	12.8	17.38	21.3	2	370
19.760	12.8	17.46	20.9	$1\frac{1}{2}$	370
19.76	12.8	17.42	(9.0 ... 10.4)		R

$h\ 4986; -26^\circ 6007; 8.3$

A.R.  $17^h\ 42^m\ 50^s$ ; Decl.  $-26^\circ\ 18'$

20.634	226.3	10.82	19.7	$2\frac{1}{2}$	370
20.636	226.9	10.85	20.0	2	370
20.63	226.6	10.83	(8.2 ... 11.1)		F

$h\ 4991; -26^\circ 6060 + 59; 9.4 + 9.2$

A.R.  $17^h\ 45^m\ 52^s$ ; Decl.  $-26^\circ\ 38'$

20.634	358.9	23.21	19.9	2	370
20.636	359.3	23.09	20.2	2	370
20.63	359.1	23.15	(9.4 ... 9.7)		F

$h\ 4990; -22^\circ 6466; 8.8$

A.R.  $17^h\ 46^m\ 1^s$ ; Decl.  $-22^\circ\ 19'$

20.636	300.5	23.30	20.5	$2\frac{1}{2}$	370
20.639	300.3	23.49	21.1	2	370
20.64	300.4	23.39	(9.5 ... 11.0)		F

A 2253; SD  $-18^\circ 4674; 8.7$

A.R.  $17^h\ 47^m\ 14^s$ ; Decl.  $-18^\circ\ 27'$

20.633	98.2	0.55	18.9	3	650
			(8.5 ... 13.5)		

**8216;  $h\ 4995$**

A.R.  $17^h\ 47^m\ 26^s$ ; Decl.  $-11^\circ\ 19'$

20.645	155.2	28.85	20.6	2	370
20.647	155.6	28.80	19.1	$1\frac{1}{2}$	370
20.65	155.4	28.82	(6.1 ... 13.2)		120

A 2254; SD  $-18^\circ 4722; 8.8$

A.R.  $17^h\ 50^m\ 20^s$ ; Decl.  $-18^\circ\ 3'$

20.634	180.3	$0.20 \pm$	19.0	3	650
			(9.5 ... 9.5)		

A 2255;  $-19^\circ 6349; 8.4$

A.R.  $17^h\ 50^m\ 21^s$ ; Decl.  $-19^\circ\ 56'$

19.648	290.8	1.15	19.5	$2\frac{1}{2}$	475
20.633	293.3	1.38	19.2	$2\frac{1}{2}$	650
20.653	292.3	1.39	20.1	$2\frac{1}{2}$	475
20.31	292.1	1.31	(8.8 ... 10.1)		

$h\ 5002; \text{C6D } -23^\circ 13702; 9.7$

A.R.  $17^h\ 50^m\ 53^s$ ; Decl.  $-23^\circ\ 58'$

20.634	39.1	9.16	20.2	$1\frac{1}{2}$	370
20.636	39.0	8.90	20.8	2	370
20.639	39.3	8.90	21.3	2	370
20.64	39.1	8.99	(10.9 ... 11.0)		F?

O. Stone 38 = Fox  $-; -27^\circ 5975; 9.5$

A.R.  $17^h\ 54^m\ 14^s$ ; Decl.  $-27^\circ\ 37'$

20.634	84.2	6.59	19.4	$2\frac{1}{2}$	370
20.639	84.0	6.54	21.5	2	370
20.64	84.1	6.57	(9.5 ... 11.7)		198

\* Fox 24;  $-24^\circ 6154; 8.4$

A.R.  $17^h\ 56^m\ 54^s$ ; Decl.  $-24^\circ\ 15'$

19.484	22.1	3.84	18.3	$2\frac{1}{2}$	650
19.785	21.1	4.11	21.3	2	370
19.787	20.6	3.95	21.3	2	370
19.69	21.3	3.97	(9.3 ... 10.8)		142

AC; C = 11.7

19.785	137.7	24.89	21.4	2	370
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Egbert 6 = Hd 148;  $-25^\circ 6276; 8.6$

A.R.  $17^h\ 56^m\ 34^s$ ; Decl.  $-25^\circ\ 29'$

19.763	197.1	4.77	22.1	$1\frac{1}{2}$	370
19.785	196.0	4.64	21.2	2	370
19.787	196.7	4.63	21.4	2	370
19.78	196.6	4.68	(9.9 ... 10.0)		

\* I 625; —18° 384; 9.1

A.R. 18<sup>h</sup> 1<sup>m</sup> 19<sup>s</sup>; Decl. —18° 57'

19.648	44.5	1.67	19.9	2½	475
20.653	45.7	1.88	20.3	2½	475
20.15	45.1	1.78	(9.8 ... 10.5)		D?

h 5082; —19° 7265; 7.3

A.R. 18<sup>h</sup> 56<sup>m</sup> 1<sup>s</sup>; Decl. —19° 25'

20.636	89.2	7.52	21.2	2	370
20.639	89.3	7.59	21.9	2	370
20.645	88.7	7.60	20.8	2½	370
20.64	89.1	7.57	(5.8R ... 9.3c)		F?

AC

20.636	113.8	20.18	21.3	1½	370
20.639	112.7	20.20	21.8	2	370
20.645	113.3	20.04	21.0	3	370
20.64	113.3	20.14	(5.8R ... 10.9)		F?

9017; h 5090

A.R. 18<sup>h</sup> 59<sup>m</sup> 42<sup>s</sup>; Decl. —10° 54'

20.639	247.6	12.75	22.0	2½	370
20.645	247.4	12.82	21.1	3	370
20.64	247.5	12.79	(9.2 ... 9.3)		F

h 5101; —25° 6742; 8.4

A.R. 19<sup>h</sup> 9<sup>m</sup> 2<sup>s</sup>; Decl. —25° 33'

20.639	305.6	21.43	22.4	2½	370
20.647	305.4	21.66	19.4	2½	370
20.653	305.7	21.48	20.8	2½	370
20.65	305.6	21.52	(8.5 ... 9.4)		F

Howe—; —25° 6744; 9.4

A.R. 19<sup>h</sup> 9<sup>m</sup> 17<sup>s</sup>; Decl. —25° 38'

20.653	21.9	2.94	20.9	2½	370
20.655	23.5	2.89	20.3	2	370
20.708	23.0	2.88	22.5	2½	370
20.67	22.8	2.90	(9.4 ... 10.7)		23

h 5110; —29° 6024; 9.7

A.R. 19<sup>h</sup> 16<sup>m</sup> 19<sup>s</sup>; Decl. —29° 52'

19.736	118.2	5.96	21.9	2½	370
19.749	118.1	5.85	22.4	2	370
19.809	116.9	5.91	22.4	2	370
19.76	117.7	5.91	(10.4 ... 10.5)		

Σ 111; —28° 6905; 8.8

A.R. 19<sup>h</sup> 16<sup>m</sup> 27<sup>s</sup>; Decl. —28° 55'

20.653	285.2	1.53	21.2	2½	370
20.708	288.3	1.35	22.7	2	370
20.710	287.1	1.20	22.2	2	370
20.863	284.4	1.25	23.1	3	370
20.73	286.2	1.33	(8.8 ... 13.4)		

h 5113; —29° 6031; 7.7

A.R. 19<sup>h</sup> 17<sup>m</sup> 30<sup>s</sup>; Decl. —29° 32'

20.639	166.7	14.58	22.6	2½	370
20.645	166.3	14.42	21.3	3	370
20.64	166.5	14.50	(6.1 ... 11.1)		R

Barnard; —27° 6760; 9.2

A.R. 19<sup>h</sup> 18<sup>m</sup> 52<sup>s</sup>; Decl. —27° 55'

20.647	200.2	1.73	21.3	2½	370
20.653	201.8	1.75	21.1	2½	370
20.656	202.1	1.82	20.5	2½	370
20.65	201.4	1.77	(10.0 ... 10.1)		

Σ 423; —29° 6060; 8.4

A.R. 19<sup>h</sup> 20<sup>m</sup> 18<sup>s</sup>; Decl. —29° 44'

20.645	126.3	1.33	21.7	3	370
20.647	125.7	1.42	21.7	2	370
20.653	125.7	1.57	21.3	2½	370
20.65	125.9	1.44	(8.1 ... 8.4)		F?

h 2902; —21° 7532 + 1; 9.4 + 9.4

A.R. 19<sup>h</sup> 46<sup>m</sup> 3<sup>s</sup>; Decl. —21° 44'

19.749	211.8	16.31	23.0	2	370
19.763	212.1	16.37	22.3	1½	370
19.76	211.9	16.34	(10.1 ... 10.1)		

h 5164; —27° 6913; 8.2

A.R. 19<sup>h</sup> 53<sup>m</sup> 31<sup>s</sup>; Decl. —27° 30'

20.639	122.9	9.26	22.9	2	370
20.647	122.6	9.33	19.7	2½	370
20.653	122.7	9.28	21.5	2½	370
20.65	122.7	9.29	(9.1 ... 9.5)		F

λ 405; —28° 7134; 7.6

A.R. 19<sup>h</sup> 59<sup>m</sup> 15<sup>s</sup>; Decl. —28° 43'

20.645	233.0	0.65	22.2	3	370
20.653	234.1	0.62	21.6	2½	475
20.656	238.6	0.72	20.8	2½	370
20.65	235.2	0.66	(8.4 ... 8.9)		

h 5180; —28° 7165; 9.4

A.R. 20<sup>h</sup> 6<sup>m</sup> 37<sup>s</sup>; Decl. —28° 29'

20.647	220.6	10.45	19.9	2½	370
20.653	222.3	10.36	21.7	2	475
20.656	222.1	10.48	21.0	2½	370
20.65	221.7	10.43	(10.4 ... 12.0)		

*h* 2942;  $-25^{\circ} 7027$ ; 10.1 :A.R. 20<sup>h</sup> 9<sup>m</sup> 59<sup>s</sup>; Decl.  $-25^{\circ} 38'$ 

19.749	216.5	13.10	23.2	1½	370
19.763	216.9	13.04	22.4	1½	370
19.76	216.7	13.07	(10.4 ... 10.9)		

*h* 2957; Cód  $-24^{\circ} 16031$ ; 9.5A.R. 20<sup>h</sup> 18<sup>m</sup> 35<sup>s</sup>; Decl.  $-24^{\circ} 4'$ 

19.749	267.3	15.72	23.3	1½	370
19.774	266.0	16.16	23.1	1½	370
19.790	266.5	15.93	23.0	2	370
19.77	266.6	15.94	(10.5 ... 11.1)		

AC

19.774	61.4	19.41	23.2	1	370
19.790	61.1	19.06	23.1	2	370
19.78	61.2	19.24	(10.5 ... 12.2)		

*h* 5202; Cód  $-30^{\circ} 1794$ ; 9.6A.R. 20<sup>h</sup> 22<sup>m</sup> 8<sup>s</sup>; Decl.  $-30^{\circ} 25'$ 

19.880	83.3	15.04	23.9	2	370
19.911	83.4	15.53	0.7	2½	370
20.647	83.2	15.14	20.5	2½	370
20.15	83.3	15.24	(9.9 ... 10.8)		246

*Hh* 692; Cód  $-26^{\circ} 15102$ ; 9.4A.R. 20<sup>h</sup> 26<sup>m</sup> 32<sup>s</sup>; Decl.  $-26^{\circ} 5'$ 

19.749	165.0	14.47	23.8	1	370
19.774	165.9	14.61	23.4	1½	370
19.790	165.0	14.91	23.4	2	370
19.77	165.3	14.66	(9.7 ... 12.9)		

AC

19.749	338.6	15.03	23.7	1½	370
19.774	338.8	15.51	23.5	2	370
19.790	338.2	15.08	23.6	2½	370
19.77	338.5	15.21	(9.7 ... 10.5)		F?

AD

19.749	227.6	20.29	23.6	1½	370
19.774	227.9	20.63	23.6	2	370
19.790	227.0	20.16	23.3	2	370
19.77	227.5	20.36	(9.7 ... 10.4)		F?

*h* 2982;  $-27^{\circ} 7064$ ; 10.2A.R. 20<sup>h</sup> 30<sup>m</sup> 6<sup>s</sup>; Decl.  $-27^{\circ} 42'$ 

19.790	130.9	14.10	23.9	2	370
19.911	131.6	14.25	0.8	2½	370
19.921	131.8	13.71	1.0	2	370
19.87	131.4	14.02	(10.6 ... 11.1)		

*h* 5210;  $-27^{\circ} 7068$ ; 9.2A.R. 20<sup>h</sup> 32<sup>m</sup> 20<sup>s</sup>; Decl.  $-27^{\circ} 29'$ 

19.911	264.6	11.06	0.9	2½	370
19.921	263.9	10.79	1.1	2	370
20.647	262.8	10.77	20.7	2½	370
20.653	263.8	10.83	22.1	2½	370
20.28	263.8	10.86	(9.4 ... 11.1)		

*h* 5212;  $-24^{\circ} 7049$ ; 9.4A.R. 20<sup>h</sup> 33<sup>m</sup> 1<sup>s</sup>; Decl.  $-24^{\circ} 36'$ 

19.774	289.4	25.96	23.7	2	370
19.922	289.7	25.62	1.3	2	370
19.927	290.4	25.74	1.0	2½	370
19.87	289.8	25.77	(9.2 ... 10.6)		

*h* 5220;  $-27^{\circ} 7096$ ; 7.4 :A.R. 20<sup>h</sup> 39<sup>m</sup> 17<sup>s</sup>; Decl.  $-27^{\circ} 18'$ 

19.911	354.2	18.08	1.1	2	370
20.647	354.2	18.09	20.9	2	370
20.28	354.2	18.09	(7.3 ... 8.9)		F

*Hd* 161;  $-24^{\circ} 7078$ ; 10.4A.R. 20<sup>h</sup> 40<sup>m</sup> 43<sup>s</sup>; Decl.  $-24^{\circ} 0'$ 

19.774	22.4	29.40	0.1	2	370
19.927	20.8	28.36	1.3	2	370
19.930	21.5	28.66	1.1	1½	370
19.88	22.6	28.81	(9.9 ... 13.0)		

AC

19.774	244.8	37.82	0.2	1½	370
19.927	244.7	37.69	1.1	2	370
19.85	244.7	37.76	(9.9 ... 10.7)		

*h* 5226;  $-27^{\circ} 7113 + 14$ ; 7.8 + 8.2A.R. 20<sup>h</sup> 42<sup>m</sup> 54<sup>s</sup>; Decl.  $-27^{\circ} 49'$ 

20.647	68.0	18.75	21.0	2	370
20.653	67.8	18.76	22.3	2½	370
20.65	67.9	18.76	(7.6 ... 9.6)		F

*h* 5265;  $-22^{\circ} 8014$ ; 10.0A.R. 21<sup>h</sup> 15<sup>m</sup> 9<sup>s</sup>; Decl.  $-22^{\circ} 54'$ 

19.911	192.3	31.78	1.3	2	370
19.916	192.1	31.86	1.2	2	370
19.91	192.2	31.82	(9.8 ... 10.2)		F

*h* 5269;  $-23^{\circ} 7972$ ; 8.6A.R. 21<sup>h</sup> 19<sup>m</sup> 13<sup>s</sup>; Decl.  $-23^{\circ} 56'$ 

19.911	159.8	8.82	1.4	2	370
19.916	159.5	8.67	1.4	2	370
19.922	160.1	8.61	1.5	2	370
19.92	159.8	8.70	(9.6 ... 9.7)		F



*h* 5271; —25° 7311; 11.2

A.R. 21<sup>h</sup> 20<sup>m</sup> 43<sup>s</sup>; Decl. —25° 24'

19.763	43.4	6.63	23.8	1½	370
19.774	42.4	6.66	0.4	2	370
19.790	45.4	6.63	0.2	1½	370
19.78	43.7	6.64	(10.6 ... 12.1)		F?

\* H<sub>11</sub> 1313; SD —18° 5951; 8.9

A.R. 21<sup>h</sup> 24<sup>m</sup> 19<sup>s</sup>; Decl. —18° 12'

20.806	243.9	[0.75]	0.1	2	475
20.863	249.0	0.39	23.5	3½	650
20.83	246.5	0.39	(9.3 ... 9.5)		

*h* 3030; Cód —22° 15433; 9.8

A.R. 21<sup>h</sup> 24<sup>m</sup> 35<sup>s</sup>; Decl. —22° 48'

19.763	112.8	9.56	23.6	1½	370
19.774	112.4	9.29	0.5	1½	370
19.77	112.6	9.42	(11.0 ... 12.0)		

**11087**; *h* 5284

A.R. 21<sup>h</sup> 30<sup>m</sup> 52<sup>s</sup>; Decl. —16° 50'

19.935	269.0	51.06	1.5	2	370
19.938	268.7	50.83	1.5	2½	370
19.94	268.8	50.94	(8.4 ... 9.9)		20

**11159**; *h* 5291

A.R. 21<sup>h</sup> 35<sup>m</sup> 12<sup>s</sup>; Decl. —14° 44'

19.935	106.4	24.62	1.7	2	370
19.938	106.0	24.66	1.8	2½	370
19.94	106.2	24.64	(9.0 ... 9.3)		F

Cód —23° 17189; 9.2 :

A.R. 21<sup>h</sup> 51<sup>m</sup> 26<sup>s</sup>; Decl. —22° 59'

19.774	336.8	21.18	0.6	2½	370
19.864	336.6	21.55	0.7	1½	370
19.82	336.7	21.36	(9.5 ... 10.2)		245

*h* 5311; —29° 6656; 8.0

A.R. 21<sup>h</sup> 52<sup>m</sup> 35<sup>s</sup>; Decl. —29° 38'

19.916	291.7	40.61	1.8	2	370
19.922	291.8	40.57	1.7	2	370
19.92	291.8	40.59	(7.8 ... 10.6)		

AC

19.916	227.1	48.69	1.9	2	370
19.922	227.2	48.40	1.9	1½	370
19.92	227.1	48.55	(7.8 ... 10.9)		

H.C.W. 24; —23° 8071 + 2; 10.4 + 10.2

A.R. 21<sup>h</sup> 53<sup>m</sup> 53<sup>s</sup>; Decl. —22° 59'

19.774	45.0	20.95	0.7	2½	370
19.864	45.4	21.14	0.9	1½	370
19.911	44.6	21.32	1.6	2½	370
19.85	45.0	21.14	(10.3 ... 10.6)		

H.C.W. 26; —23° 8090; 9.1

A.R. 21<sup>h</sup> 58<sup>m</sup> 1<sup>s</sup>; Decl. —23° 47'

19.774	333.1	10.62	0.8	2	370
19.864	333.8	9.82	1.1	1	370
19.911	333.3	—	1.8	2	370
19.916	332.3	10.35	1.7	2	370
19.87	333.1	10.26	(9.4 ... 11.8)		

\* Fox 45; —23° 8125; 9.1

A.R. 22<sup>h</sup> 7<sup>m</sup> 22<sup>s</sup>; Decl. —23° 44'

19.706	153.8	4.70	0.3	3	370
19.905	153.6	4.86	1.5	2	370
19.908	153.2	4.78	1.1	2	370
19.84	153.5	4.78	(9.9 ... 11.0)		D?

AC

19.706	82.4	29.87	0.5	3	370
19.908	82.1	30.36	1.2	2	370
19.81	82.3	30.11	(9.9 ... 11.0)		

*h* 5324; —24° 7342; 8.4

A.R. 22<sup>h</sup> 10<sup>m</sup> 50<sup>s</sup>; Decl. —24° 19'

19.916	357.6	10.49	2.0	1½	370
19.927	357.1	10.48	1.5	2½	370
19.92	357.3	10.48	(8.8 ... 10.7)		F?

λ 471; —28° 7571; 10.0

A.R. 22<sup>h</sup> 11<sup>m</sup> 52<sup>s</sup>; Decl. —28° 45'

19.774	36.0	5.08	1.0	2	370
19.905	34.4	5.00	1.6	2	370
19.908	34.6	4.83	1.3	2	370
19.86	35.0	4.97	(10.5 ... 11.6)		F

λ 472; Cód —25° 15880; 9.8

A.R. 22<sup>h</sup> 14<sup>m</sup> 50<sup>s</sup>; Decl. —25° 58'

19.774	57.4	5.54	1.2	2½	370
19.905	57.9	5.20	1.7	2	370
19.908	57.1	5.41	1.3	2	370
19.86	57.5	5.38	(11.8 ... 11.8)		F

*h* 3123; —22° 8255; 9.4

A.R. 22<sup>h</sup> 30<sup>m</sup> 22<sup>s</sup>; Decl. —22° 17'

19.774	159.8	18.49	1.4	2	370
19.848	159.3	18.52	1.9	2½	370
19.81	159.5	18.51	(9.0 ... 13.2)		

**11855; h 5355**A.R. 22<sup>h</sup> 32<sup>m</sup> 10<sup>s</sup>; Decl. -14° 42'

19.927	293.7	78.12	2.0	2	370
19.930	293.9	77.98	1.3	1½	370
19.93	293.8	78.05	(7.9 ... 8.7)		F?

**AC**

19.927	1.8	107.01	2.3	2	370
19.930	1.8	107.43	1.5	1½	370
19.93	1.8	107.22	(7.9 ... 9.0R)		F?

**Hb 770; -28° 7623 -4; 7.1 + 7.1**A.R. 22<sup>h</sup> 33<sup>m</sup> 3<sup>s</sup>; Decl. -28° 57'**AB (= Δ 242)**

19.916	159.6	86.97	2.2	2	370
19.922	159.6	86.56	2.1	1½	370
19.927	159.6	86.97	1.7	2½	370
19.92	159.6	86.83	(6.8 ... 7.5)		F

**BC (= h 5356)**

19.916	64.2	3.43	2.3	1½	370
19.922	64.2	3.58	2.2	1½	370
19.927	63.9	3.41	1.9	2½	370
19.92	64.1	3.47	(7.5 ... 9.1)		F

**h 5371; -26° 7431; 7.0**A.R. 22<sup>h</sup> 51<sup>m</sup> 15<sup>s</sup>; Decl. -26° 44'

19.916	343.3	8.94	2.4	2	370
19.922	343.1	9.08	2.4	1½	370
19.927	343.7	9.03	2.5	2	370
19.92	343.4	9.02	(7.8 ... 9.7)		F

**h 3166; Cód -22° 16189; 10**A.R. 23<sup>h</sup> 0<sup>m</sup> 4<sup>s</sup>; Decl. -22° 30'

19.848	138.4	8.19	2.1	2	370
19.903	140.1	8.38	2.3	2	370
19.927	139.0	7.69	2.6	2	370
19.935	139.8	8.12	2.2	2	370
19.90	139.3	8.10	(12.7 ... 12.8)		

**h 3178; Anon.**A.R. 23<sup>h</sup> 7<sup>m</sup> 44<sup>s</sup>; Decl. 21° 47'

19.903	136.9	18.58	2.5	2	370
19.935	138.1	17.81	2.3	2	370
19.938	137.8	17.82	2.0	2	370
19.93	137.6	18.07	(12.7 ... 13.1)		228

**h 3206; -22° 8388; 8.6**A.R. 23<sup>h</sup> 30<sup>m</sup> 46<sup>s</sup>; Decl. -22° 20'

19.894	350.3	3.74	2.3	2	370
19.903	348.3	3.42	2.5	2	370
19.911	348.5	3.48	2.1	2½	370
19.90	349.0	3.55	(9.3 ... 9.7)		F

**h 5410; -24° 7471; 9.8**A.R. 23<sup>h</sup> 32<sup>m</sup> 49<sup>s</sup>; Decl. -24° 22'

19.903	70.7	14.10	2.6	2	370
19.911	70.6	13.98	2.2	2	370
19.91	70.6	14.04	(9.9 ... 12.7)		

**Có—; -27° 7563; 8.2**A.R. 23<sup>h</sup> 37<sup>m</sup> 52<sup>s</sup>; Decl. -27° 52'

20.803	162.1	6.38	0.6	2	370
20.823	161.4	6.48	2.7	2	370
20.81	161.7	6.43	(9.3 ... 9.3)		

**h 3218; -22° 8410; 9.4**A.R. 23<sup>h</sup> 43<sup>m</sup> 34<sup>s</sup>; Decl. -22° 40'

19.848	65.3	10.99	2.3	2	370
19.894	65.3	10.99	2.5	2	370
19.87	65.3	10.99	(11.0 ... 11.6)		

**Δ 253; -27° 7584; 6.4**A.R. 23<sup>h</sup> 48<sup>m</sup> 9<sup>s</sup>; Decl. -27° 43'

19.938	269.5	6.79	2.2	3	370
19.941	269.2	6.87	1.9	3	370
19.94	269.4	6.83	(7.1 ... 7.9)		F

**12634; h 5433; Anon.**A.R. 23<sup>h</sup> 49<sup>m</sup> 31<sup>s</sup>; Decl. -18° 25'

19.927	60.4	23.98	2.8	2	370
19.930	60.3	24.17	1.8	1½	370
19.93	60.4	24.07	(10.2 ... 10.3)		

**12649; h 5435**A.R. 23<sup>h</sup> 51<sup>m</sup> 12<sup>s</sup>; Decl. -16° 46'

19.927	7.5	14.66	2.9	2	370
19.930	7.9	15.08	2.1	2	370
19.935	7.7	14.99	1.9	2	370
19.93	7.7	14.91	(9.1 ... 10.1)		F

**AC; C = 11.5**

19.935	51.7	29.18	2.1	2	370
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**h 5440; -27° 7603; 7.8**A.R. 23<sup>h</sup> 56<sup>m</sup> 6<sup>s</sup>; Decl. -27° 48'

19.903	287.7	3.51	2.8	2½	370
19.908	287.7	3.53	2.6	2½	370
19.911	287.5	3.61	2.4	2	370
19.91	287.6	3.55	(3.5 ... 9.0)		F

**h 3236 = h 5441; -21° 8323; 9.8**A.R. 23<sup>h</sup> 59<sup>m</sup> 49<sup>s</sup>; Decl. -21° 19'

19.908	219.2	24.38	2.7	3	370
19.916	218.8	24.37	2.7	2	370
19.91	219.0	24.38	(9.8 ... 10.4)		

1246, 1387, 3689, 13; 1026, 1153, 3002, 34; 2204, 2469, 6691, 47.  
82, 87, 179, 11; 342, 371, 921, 9; 467, 439, 1100, 20.

NOTES

5. 1° south of Herschel's place.
7. Noted as double with the Gautier meridian circle.
9. Apparently a mistaken wire in Herschel's R.A.
11. Noted as double in *Uranometría Argentina*.
20. Previous measures discordant.
21. Fixed. Some error in Hargrave's measure.
22. No other measures. The Sydney measure purporting to be of this is of another pair.
23. Picked up independently and measured in the belief that it was new.
41. Greater R.A. correct.
42. Lesser R.A. correct.
51. 1<sup>m</sup> preceding Herschel's place.
72. 1° north of Herschel's place.
76. Adjusted means, using all the measures.
84. This agrees with Herschel's place, but not with his description.
88. 1<sup>m</sup> following Herschel's place.
120. I am practically certain that there is no closer companion.
142. The only measures are too recent to warrant comparison.
150. No other measures of distance: no change in the angle.
159. Appears stellar with 150 magnification, but diffuse with 370.
160. Certainly less than 0".25 and probably less than 0".15.
161. Less than 4° change in sixty years.
162. Examined under good conditions without showing signs of duplicity.
163. The nebula is in the given place, but has nothing stellar.
164. Found while looking for *h* 3469 which I could not find.
165. Both these stars have an error of 30° in declination in *Results*. Consequently *h* 3523 = Δ 7.
166. δ 34 is about 1<sup>m</sup> following the place given for *h* 3526. I cannot find this latter unless it be the same as *h* 3509.
167. With an error of 2<sup>m</sup>5 in the R.A. of *h* 3531. There is an error of 1<sup>m</sup> in the R.A.'s of Cód -40° 730 to 736.
168. I 12 was examined with power 1125 and seemed elongated, but the distance is certainly less than 0".2.
169. 1920.91 « Certainly less than 0".3 unless very unequal » 2n. See also note 18.
170. 1919.755 « Round, less than 0".2, 3½ 650 ». This star has been called υ<sub>4</sub> Eridani.

NOTAS

5. 1° al sur de la posición asignada por Herschel.
7. Notada como doble con el círculo meridiano Gautier.
9. La A.R. de Herschel parece tener error del hilo.
11. Anotada como doble en la *Uranometría Argentina*.
20. Las medidas anteriores son discordantes.
21. Fija. La medida de Hargrave tiene algún error.
22. No hay otras medidas. La medida anotada en la lista de Sydney Obs. como de esta estrella es de otra.
23. Fué encontrada independientemente y medida en la creencia que era nueva.
41. La A.R. mayor es correcta.
42. La A.R. menor es correcta.
51. 1<sup>m</sup> precedente de la posición asignada por Herschel.
72. 1° al norte de la posición asignada por Herschel.
76. Cada promedio incluye el efecto de todas las medidas.
84. Ésta corresponde a la posición de Herschel, pero no a su descripción.
88. 1<sup>m</sup> siguiente de la posición asignada por Herschel.
120. Estoy casi seguro que no hay compañera más cercana.
142. Las únicas medidas son demasiado recientes para justificar comparación.
150. No hay otras medidas de distancia. El ángulo no ha cambiado.
159. Con aumento de 150 tiene aspecto estelar, pero con 370 es completamente difusa.
160. Seguramente menor de 0".25 y probablemente menor de 0".15.
161. Ha cambiado menos de 4° en 60 años.
162. Ha sido examinado en buenas condiciones sin mostrar compañera.
163. La nebulosa está en la posición dada, pero no tiene nada de estelar.
164. Encontrada mientras buscaba *h* 3469, que no he podido encontrar.
165. Las declinaciones de estas estrellas en *Results* tienen error común de 30°. Por consecuencia *h* 3523 = Δ 7.
166. δ 34 está como 1<sup>m</sup> al siguiente de la posición dada para *h* 3526. No puedo encontrar ésta a no ser que es igual a *h* 3509.
167. Con error de 2<sup>m</sup>5 en la A.R. de *h* 3531. Cód -40° 730 al 736 tienen error de 1<sup>m</sup> en su A.R.
168. I 12 fué examinada con aumento de 1125, y mostraba indicios de ser alargada, pero la distancia es seguramente menor de 0".2.
169. 1920.91 « Seguramente menor de 0".3 si no son muy desiguales » 2 noches. Ver también nota 18.
170. 1919.755 « Redonda, menor de 0".2 3½ 650 ». Esta estrella ha tenido el nombre υ<sub>4</sub> Eridani.

171. The principal star appears nebulous.  
 172. I find nothing else near the place given for *h* 3708.  
 173. This « star » is  $-67^{\circ} 375$ , and is a nebula with a medial condensation  $10''$  long in position angle  $120^{\circ}$  and a 13 magnitude star  $5''$  from the north preceding tip.
174. The measures are difficult because of a nebula which involves the principal star.  
 175. A nebula between the stars has its principal nucleus in  $275^{\circ} 2''5$ .  
 176. The whole is a nebula with stellar nuclei.  
 177. Burnham's identification of this star is erroneous. Previous measures discordant in distance.
178. No other measures. A star 10.5 in  $228^{\circ} 46''$ , another 11.5 in  $187^{\circ} 34''$  and many others more distant.  
 179. This star is  $1^{\circ}$  south of Herschel's place, and is not equal to Hu 1416. No other measures. Note 35 should be struck out.  
 180. And a star 13.0 in  $285^{\circ} 18''$ .  
 181. And a star 13.5 in  $301^{\circ} 18''$ .  
 182. The apparent change in angle is due to procession.
183. This seems very faint to be Dunlop's star but I find no other.  
 184.  $3^{\circ}$  south of the place given in the original observation.
185. And a star 12.0 in  $281^{\circ} 30''$ .  
 186. 1' following is a pair 13 and 13.5,  $73^{\circ} 6''$ .  
 187. There is no stellar companion, and nothing closer than this.
188. The star  $-37^{\circ} 2911$ , visual manitude 9.9, is at  $207^{\circ} 55''$ .  
 189. This is the star measured by Cogshall and appears fixed. It is possible that the discordance arises from an error in Herschel's distance.  
 190. There is no 3' star near Herschel's place except  $\lambda$  Argus, and its companion is not class IV and could not have been seen with his equatorial.  
 191. This is not preceding but following the globular cluster, which is  $-64^{\circ} 1012$ .  
 192. Either the descriptions or the places of these stars must be interchanged in *Results*. I have adopted the numbers according to the places, supposing the descriptions interchanged. There is another pair 2' south of *h* 4236.
193. There is no star in the neighborhood corresponding to Herschel's description.  
 194. This is the only star near Herschel's place which could answer to his description.  
 195.  $2^{\circ}$  north of the place given in the original observation.  
 196. Fixed. A star 14.0 in  $170^{\circ} \pm 10'' \pm$ .
171. La estrella principal parece nebulosa.  
 172. Lo único que encuentro cerca de la posición de *h* 3708.  
 173. Esta « estrella » es  $-67^{\circ} 375$ , y es una nebulosa con una condensación mediana de  $10''$  de largo en dirección  $120^{\circ}$  y con una estrella de manitud 13, distante  $5''$  del extremo norte precedente.
174. Las medidas de éstas son muy difíciles a causa de una nebulosa que envuelve la estrella principal.  
 175. Una nebulosa situada entre las dos estrellas tiene su núcleo principal en  $273^{\circ} 2''5$ .  
 176. Todo este conjunto es una nebulosa con núcleos estelares.  
 177. La identificación de esta estrella por Burnham es errónea. Las medidas anteriores de distancia son discordantes.
178. No hay otras medidas. Hay una estrella 10.5 en  $228^{\circ} 46''$ , otra 11.5 en  $187^{\circ} 34''$  y muchas otras alrededor.  
 179. Esta estrella está  $1^{\circ}$  al sur de la posición asignada por Herschel y no es igual a Hu 1416. No hay otras medidas. La nota 35 debe tacharse.  
 180. Y una estrella 13.0 en  $285^{\circ} 18''$ .  
 181. Y una estrella 13.5 en  $301^{\circ} 18''$ .  
 182. El cambio aparente en el ángulo se debe al efecto de precesión.
183. Parece muy débil para ser la estrella notada por Dunlop, pero no encuentro otra.  
 184.  $3^{\circ}$  al sur de la posición indicada en la observación original.  
 185. Y una estrella 12.0 en  $281^{\circ} 30''$ .  
 186. 1' siguiente hay un par de 13 y 13.5,  $73^{\circ} 6''$ .  
 187. No hay compañera estelar, y nada más cercana que ésta.
188. La estrella  $-37^{\circ} 2911$ , de magnitud visual 9.9, está en  $207^{\circ} 55''$ .  
 189. Ésta es la estrella que midió Cogshall y parece fija. Es posible que la discordancia proviene de error en la distancia dada por Herschel.  
 190. Cerca de la posición de Herschel no hay otra estrella de magnitud 3' que  $\lambda$  Argus, y la compañera de ésta no es de clase IV ni podría haber sido vista con su ecuatorial.  
 191. Ésta no está precedente sino al siguiente del cúmulo globular, que es  $-64^{\circ} 1012$ .  
 192. Hay que intercambiar o las descripciones o las posiciones de estas dos estrellas en *Results*. He adoptado los números en correspondencia con las posiciones, suponiendo intercambiadas las descripciones. Hay otro par 2' al S. de *h* 4236.
193. No hay estrella en la región que corresponde a la descripción dada por Herschel.  
 194. Ésta es la única estrella cerca de la posición de Herschel que pudiera corresponder a su descripción.  
 195.  $2^{\circ}$  al norte de la posición indicada en la observación original.  
 196. Fija. Hay una estrella 14.0 en  $170^{\circ} \pm 10'' \pm$ .

197. And a star 13.0 in  $32^{\circ} 23''$  from B.  
 198. The identification in  $\beta$ .G.C. is erroneous.  
 199. 7<sup>m</sup> following Herschel's place.  
 200. Noted by Tapia while observing AB (=Có). Measured at his request on account of faintness.

201. 3<sup>m</sup> preceding Herschel's place.  
 202. No other measures, 4<sup>m</sup> error in Dunlop's place.

203. And a star 13.5 inside the curve :  $356^{\circ} 21''9$  from A ;  $302^{\circ} 16''3$  from B and  $258^{\circ} 17''6$  from C.  
 204. Reducing the measures to the equator of 1900.0 there results :

$$\Delta\delta = 89''547 + 0''2461(t - 1900)$$

$$\cos\delta\Delta z = 57.796 - 0.0369(t - 1900),$$

and a relative proper motion of  $0''249$  towards  $171^{\circ}5$ . The minimum distance was about  $70''$  near the end of the 16th century.

205. Reducing the measures to the equator of 1900.0 there results :

$$\Delta\delta = 12''741 + 0''0849(t - 1900)$$

$$\cos\delta\Delta z = 6.169 + 0.2348(t - 1900),$$

and a relative proper motion of  $0''250$  towards  $250^{\circ}1$ . The minimum separation was  $9''9$  in 1859.

206. No nebulosity seen.  
 207. And a star 13.0 in  $38^{\circ} 34''$ . No other measures.  
 208. There is no star exactly in Herschel's place. If this is the star observed by him, his angle should be subtracted from  $180^{\circ}$ .  
 209. The difference of magnitude was recorded on the three nights as  $-0.3$ ,  $+1.5$  and  $+1.0$ . Variable?  
 210. No certain change. Possibly also equal to Rus 265.  
 211.  $1^{\circ}$  south of Herschel's place of his 4820 and is not Bris 5550.  
 212. See's identification of his 252 is wrong. Possibly some change in distance.  
 213. Probably fixed with  $30^{\circ}$  error in Herschel's angle.  
 214.  $1^{\circ}$  north of Herschel's place and equals *h* 4873, of which measures are given in part I.  
 215. A 13.0 star forms with these an almost equilateral triangle.  
 216. See *Cape Annals* vol IX p. 52A, star N<sup>o</sup> 230.  
 217.  $20'$  south of Herschel's place. No other measures.  
 218. And a star 13.2 in  $95^{\circ} 20''6$ .  
 219. The principal star is extremely red, and has been noted as double under the name  $\lambda$  321. This and  $\lambda$  320,  $\lambda$  323 and  $\lambda$  324 were examined with 650 power, seeing 4, and appeared perfectly round.

197. Y una estrella 13.0 en  $32^{\circ} 23''$  desde B.  
 198. La identificación de  $\beta$ .G.C. es errónea.  
 199. 7<sup>m</sup> al siguiente de la posición asignada por Herschel.  
 200. Notada por Tapia mientras observaba AB (=Có), Yo la medí en vez de él por tener más práctica con compañeras débiles.

201. 3<sup>m</sup> precedente de la posición asignada por Herschel.  
 202. No hay otras medidas. La A.R. de Dunlop tiene 4<sup>m</sup> de error.

203. Y una estrella 13.5 en el medio :  $356^{\circ} 21''9$  desde A ;  $302^{\circ} 16''3$  desde B y  $258^{\circ} 17''6$  desde C.  
 204. Reduciendo todas las medidas al ecuador de 1900.0, se obtiene :

$$\Delta\delta = 89''547 + 0''2461(t - 1900)$$

$$\cos\delta\Delta z = 57.796 - 0.0369(t - 1900).$$

El movimiento propio relativo resulta de  $0''249$  hacia  $171''5$ , y la distancia mínima era de  $70''$  aproximadamente, a fines del siglo XVI.

205. Reduciendo todas las medidas al ecuador de 1900.0, se obtiene :

$$\Delta\delta = 12''741 + 0''0849(t - 1900)$$

$$\cos\delta\Delta z = 6.169 + 0.2348(t - 1900).$$

El movimiento propio relativo resulta de  $0''250$  hacia  $250^{\circ}1$ , y la distancia mínima era de  $9''9$  en 1859.

206. No ví nebulosidad alguna.  
 207. Y una estrella 13.0 en  $38^{\circ} 34''$ . No hay otras medidas.  
 208. No hay estrella exactamente en la posición de Herschel. Si ésta es la observada por él, su ángulo dado debe restarse de  $180^{\circ}$ .  
 209. Las diferencias de magnitud anotadas en las tres noches eran de  $-0.3$ ,  $+1.5$  y  $+1.0$ . ¿Será variable?  
 210. No hay cambio cierto. Posiblemente es igual también a Rus 265.  
 211. Está  $1^{\circ}$  al sur de la posición de Herschel para su 4820 y no es igual a Bris 5550.  
 212. La identificación de See para su 253 es errónea. Algo de cambio en distancia es posible.  
 213. Probablemente fija, con  $30^{\circ}$  de error en el ángulo de Herschel.  
 214.  $1^{\circ}$  al norte de la posición dada por Herschel e igual a su 4873. Medidas de ésta aparecen en la primera parte.  
 215. Una estrella 13.0 forma con éstas un triángulo casi equilátero.  
 216. Ver *Cape Annals* tomo IX, página 52A, estrella 230.  
 217.  $20'$  al sur de la posición de Herschel. No hay otras medidas.  
 218. Y una estrella 13.2 en  $95^{\circ} 20''6$ .  
 219. La estrella principal es extremadamente roja y ha sido anotada como doble bajo el nombre  $\lambda$  321. Ella y  $\lambda$  320,  $\lambda$  323 y  $\lambda$  324 fueron examinadas con aumento 650, imágenes 4, pareciendo perfectamente redondas.

220. The frequency of errors of about  $-16^\circ$  in See's measures makes one suspect an instrumental defect.
221. Change, which appears to be caused by proper motion in B. The neighboring star is north following and was measured once by mistake.
222.  $40'$  south of Herschel's place, but this is with his equatorial. The second part of my note 123 should be struck out.
223. This star is  $10^m$  preceding Herschel's place, as was pointed out to me by Innes. The star of which measures are given in part I is consequently an anonyma.
224. Error of a wire in the R.A. and of  $20'$  in the Decl. of *h* 5225.
225. 1920.863, « Round, less than  $0''.2$  »,  $3\frac{1}{2} 650$ ; no companion within  $100''$ .
226. The original observation should probably be read 179.9 for 119.9. A star 13.5 in  $96^\circ 32''$ .
227.  $4^m$  following Herschel's place; no other measures.
228. Place determined by rough measures with micrometer.
229. Jones' measure of 1892 needs  $-180^\circ$ .
230.  $1^h$  error in the R.A.'s. of *h* 3368, *h* 3380, *h* 3394 and *h* 4851.
231. The R.A. of Hd 58 needs  $+9^m$  correction.
232. Stone's measure needs  $-180^\circ$ .
233. Measured for *h* 3847, which is  $2^\circ$  north.
234. A star  $1^m 5$  preceding also has a faint companion at  $15''$ .
235. The description of Hd 107 is so vague as to make identification uncertain.  $-23^\circ 2471 + 2$  is near the given place and seems to me to be the star: Innes gave me  $-23^\circ 2640 + 1$ . I have measured both pairs.
236. See (1898) and Innes (1903) measured  $-23^\circ 2780$  which is  $3^m$  preceding.
- 236 a. And a star 15.0 in  $10^\circ 7'' 7$ .
237. I do not find *h* 4037 at his Decl. within  $\pm 10^m$ , nor at his R.A. within  $\pm 3^\circ$ . I am inclined to believe that his R.A. needs  $-1^m$ , his angle,  $+100^\circ$  and the star identical with  $\beta$  203.
238.  $4^m$  preceding Herschel's place.
239. Probably fixed with  $10^\circ$  error in Wilson's measure.
240. The stars  $\beta$  227 and  $\beta$  228 are in the same field, and it is certain that *h* 4756 is one or other of them.  
To make it correspond to  $\beta$  227, one must suppose the corrections:  $-34^s$  (wire interval) in R.A., magnitude of the principal star 7 instead of 9, and distance about double that recorded.  
To make it correspond to  $\beta$  228, one must suppose the corrections:  $-4^s$  in R.A., magnitudes 8 8' instead of 9 9' and  $180^\circ$  in the angle.
220. La frecuencia de errores del orden de  $-16^\circ$  en las medidas de See hace sospechar un defecto instrumental.
221. Cambio, que parece provenir de movimiento propio de B. La estrella vecina está al norte siguiente, y fué medida una vez por equivocación.
222.  $40'$  al sur de la posición de Herschel, pero ésta es con su ecuatorial. La segunda parte de mi nota 123 debe tacharse.
223. Esta estrella está  $10^m$  precedente de la posición dada por Herschel, dato que me comunicó Innes. La estrella de que publiqué medidas en parte I es, pues, una anónima.
224. *h* 5225 tiene error del hilo en A.R. y de  $20'$  en Decl.
225. 1920.863, « Redonda, menor de  $0''.20$  »,  $3\frac{1}{2} 650$ ; ninguna compañera dentro de  $100''$ .
226. Parece que la observación original debe leerse 179.9 en vez de 119.9. Hay una estrella de magnitud 13.5 en  $96^\circ 32''$ .
227.  $4^m$  al siguiente de la posición de Herschel. No hay otras medidas.
228. Posición determinada por medidas micrométricas aproximadas.
229. La medida de Jones en 1892 necesita  $-180^\circ$ .
230. Error de una hora en las A.R. de *h* 3368, *h* 3380, *h* 3394 y *h* 4851.
231. La A.R. de Hd 58 necesita corrección de  $+9^m$ .
232. La medida de Stone necesita  $-180^\circ$ .
233. Observada en vez de *h* 3847, que está  $2^\circ$  al norte.
234. Una estrella  $1^m 5$  precedente también tiene compañera débil a  $15''$  de distancia.
235. La descripción de Hd 107 es tan vaga que es difícil asegurar la identificación.  $-23^\circ 2471 + 2$  está cerca de la posición dada y me parece ser la estrella: Innes me indicó  $-23^\circ 2640 + 1$ . He medido ambos pares.
236. See en 1898 e Innes en 1903 observaron  $-23^\circ 2780$ , que está  $3^m$  precedente.
- 236 a. Y una estrella 15.0 en  $10^\circ 7'' 7$ .
237. No encuentro *h* 4037 en su Decl. dentro de  $\pm 10^m$ , ni en su A.R. dentro de  $\pm 3^\circ$ . Me inclino a creer que su A.R. necesita  $-1^m$ , su ángulo,  $+100^\circ$ , y que es igual a  $\beta$  203.
238.  $4^m$  precedente de la posición de Herschel.
239. Probablemente fija con error de  $10^\circ$  en la medida de Wilson.
240. Las estrellas  $\beta$  227 y  $\beta$  228 están en el mismo campo visual, y es seguro que *h* 4756 es una u otra de ellas.  
Para hacerla corresponder con  $\beta$  227 es necesario suponer las correcciones:  $-34^s$  (intervalo de sus hilos) en A.R., magnitud de la principal, 7 en vez de 9, distancia como el doble de la anotada.  
Para hacerla corresponder con  $\beta$  228 es necesario suponer las correcciones:  $-4^s$  en A.R., magnitudes 8 8' en vez de 9 9' y  $180^\circ$  en el ángulo.

I consider that  $\beta$  227 is the star observed by Herschel for it is much wider than  $\beta$  228, and it seems unlikely that Herschel should have seen the latter as double without seeing the companion of the former.

- 241. 5<sup>m</sup> error in Egbert's R.A.
- 242. 1920.633 « Angle 150° if really elongated, but certainly less than  $\frac{1}{4}''$  ».
- 243. 5<sup>m</sup> error in Glasenapp's R.A.
- 244. Is perhaps *h* 1297.
- 245. Declination, magnitudes and distance similar to those of H.C.W. 24.
- 246. See *Cape Annals* vol. IX, p. 53A, star N° 258. This star, on account of its declination, should appear on p. 217 with the place :

A.R. 20<sup>h</sup> 21<sup>m</sup> 49<sup>s</sup>; Decl. —30° 27'.

Me inclino a creer que la estrella observada por Herschel es la  $\beta$  227, porque es mucho más separada que la  $\beta$  228, y me parece difícil que Herschel haya separado ésta sin ver la compañera de aquella.

- 241. Error de 5<sup>m</sup> en la A.R. de Egbert.
- 242. 1920.633 « Ángulo 150° si realmente es alargada, pero distancia seguramente menor de  $\frac{1}{4}''$  ».
- 243. Error de 5<sup>m</sup> en la A.R. de Glasenapp.
- 244. Posiblemente igual a *h* 1297.
- 245. Declinación, magnitudes y distancia casi iguales a las de H.C.W. 24.
- 246. Ver *Cape Annals*, tomo IX, página 53A, estrella 258. Esta estrella, por su declinación, debe figurar en página 217 con las coordenadas :

A.R. 20<sup>h</sup> 21<sup>m</sup> 49<sup>s</sup>; Decl. —30° 27'.

## INDEXES ÍNDICES

### A. — CONSTELLATION NAMED STARS.

### ESTRELLAS CON LETRA

Antlia	Centaurus	Fornax	Lupus	Piscis Austr.
$\delta$ *10 <sup>h</sup> 24 <sup>m</sup> 4 <sup>s</sup>	$z$ 13 <sup>h</sup> 39 <sup>m</sup> 39 <sup>s</sup>	$\eta_3$ 2 <sup>h</sup> 45 <sup>m</sup> 11 <sup>s</sup>	$\gamma$ 15 <sup>h</sup> 51 <sup>m</sup> 51 <sup>s</sup>	$\beta$ 22 <sup>h</sup> 24 <sup>m</sup> 24 <sup>s</sup>
$\zeta_1$ 9 25 26	Chamaeleon	$\omega$ *2 28 35	$\delta$ 15 48 54	$\gamma$ 22 45 34
$\eta$ 9 53 31		Grus	* $\mu_1$ 15 9 51	$\delta$ 22 49 1
Apus	$\epsilon$ 11 53 26		* $\pi$ 14 56 37	$\theta$ 21 40 24
$\alpha_1$ 15 17 56	Circinus	$\delta_2$ 22 22 17	Mensa	( $\tau$ 22 29 34)
$\delta$ 16 1 45	$z$ 14 32 26	* $\theta$ 22 59 50	$\gamma$ 5 36 51	Puppis
Argo	Columba	( $\tau_2$ 22 29 40)	Microscopium	$h_2$ 8 9 37
* $\delta$ 8 41 17	$\gamma$ 5 53 6	$\nu$ 22 59 56	$\alpha$ 20 42 9	Sagittarius
$\lambda$ Nota 190	Corolla	Hydra	$\theta_2$ 21 16 26	$\alpha$ 18 9 10
$\pi$ 7 12 45	* $\gamma$ 18 57 58	$\beta$ 11 46 36	Musca	$\alpha_2$ 20 15 23
$\nu$ 9 43 59		$\zeta$ 11 26 52	* $\beta$ 12 38 38	$\lambda_1$ 0 36 42
* $\psi$ 9 25 47	Crux	$N$ *11 26 19	$\theta$ 13 0 5	$\tau$ 1 30 22
Caelum	* $\gamma$ 12 24 14	Hydrus	$\lambda$ 11 39 43	$R$ 1 21 13
$\gamma$ 4 59 55	$\zeta$ 12 11 41	$\tau_1$ 1 41 18	Octans	Triang. Austr.
Carina	$\eta$ 12 0 22	$\tau_2$ 1 48 59	$\alpha$ Nota 162	$\epsilon$ 15 25 18
* $t_2$ 10 34 0	Eridanus	Indus	$\zeta$ Nota 162	$\iota$ 16 16 22
Centaurus		Lepus	$\lambda$ 21 31 30	Tucana
* $z$ 14 30 59	$\theta$ 2 53 31	$\alpha$ *5 27 24	$\mu_2$ 20 26 46	Phoenix
* $\gamma$ 12 34 38	$\tau_4$ *3 14 12	Lupus	Phoenix	* $\beta_1$ 0 25 49
$d$ 13 23 49	( $\nu_1$ 4 13 10)	* $\gamma$ 15 26 50	* $\beta$ 1 0 30	* $\gamma$ 1 11 31
$h$ 13 46 2	$X$ 4 13 10	* $\epsilon$ 15 14 12	Pictor	Volans
$k$ 13 44 37	$f$ 3 44 0		* $\alpha$ 6 30 6	$\epsilon$ 8 7 33
$\gamma$ 13 46 15	* $p$ 1 35 4			* $\theta$ 8 38 37

B. — STARS OF OBSERVERS OTHER THAN HERSCHEL  
ESTRELLAS DE OTROS OBSERVADORES

Aguilar	$\beta$ = Burnham	$\delta$ = Dawson	$\delta$ = Dawson	$\Delta$ = Dunlop
* 8 9 <sup>h</sup> 31 <sup>m</sup> 2 <sup>s</sup>	771 22 <sup>h</sup> 29 <sup>m</sup> 40 <sup>s</sup>	38 5 <sup>h</sup> 11 <sup>m</sup> 57 <sup>s</sup> *	95 * 7 <sup>h</sup> 46 56 <sup>s</sup>	148 13 <sup>h</sup> 44 <sup>m</sup> 37 <sup>s</sup> *
* 9 10 19 51	772 22 49 1	39 5 13 7	96 * 8 51 43	* 151 13 49 0
— 2 1 15	773 22 59 56	40 6 31 52	97 * 9 15 1	154 13 58 4
— 12 8 48	775 23 30 28	41 6 31 53	98 * 9 44 5	166 14 32 26
— 13 52 56	1000 1 29 14	42 7 46 27	99 * 9 57 39	173 Redonda
A = Ailken	1004 3 57 16	43 8 6 24	100 * 11 10 33	181 15 12 11
2253 *17 47 14	1011 22 55 37	44 8 15 4	101 * 11 11 9	188 15 25 18
2254 *17 50 20	1012 23 30 28	45 8 19 50	102 * 12 10 6	192 15 39 3
2255 *17 50 21	1108 13 46 15	46 8 54 2	103 * 12 31 11	196 15 48 54
Barnard	1110 14 12 11	47 9 15 10	104 * 12 35 4	197 15 51 51
— *19 18 52	1112 14 25 46	48 9 32 31	105 * 12 40 58	199 16 0 12
Brisbane	1119 17 9 22	49 10 3 28	106 * 12 45 39	201 16 16 22
1523 7 12 7	1123 17 45 0	50 10 7 56	107 * 13 28 14	209 16 39 50
*3574 11 19 15	1128 18 22 53	51 10 31 0	108 * 13 29 30	214 17 0 31
3706 11 34 0	1197 13 55 47	52 10 31 1	109 * 14 7 34	219 17 50 27
5584 16 1 45	1229 1 13 32	53 10 33 29	110 * 16 47 3	232 20 26 46
*6021 17 9 35	— * 5 44 27	54 10 39 31	111 * 19 16 27	239 22 22 17
6556 18 52 37	Cape	55 10 57 2	$\Delta$ = Dunlop	240 22 24 24
	8 8 10 53	56 11 0 16	3 1 21 13	241 22 29 34
	* 18 17 46 48	57 11 25 4	* 5 1 35 4	242 * 22 33 3
	* 23 6 11 10	58 11 38 50	9 2 53 31	253 * 23 48 9
	— 5 40 36	59 11 55 26	15 3 35 18	Egbert
	C.P.D. — 57°	60 11 56 47	16 3 44 0	4 * 15 13 26
$\beta$ = Burnham	3506 10 31 1	61 12 17 32	23 6 1 32	6 * 17 56 34
227 *15 12 8	3524 10 31 12	62 12 18 37	28 6 19 41	Fox
228 *15 12 38	3526 10 31 13	63 12 32 57	29 6 25 4	* 24 * 17 56 54
251 21 4 36	Copeland	64 12 55 45	32 6 38 1	* 45 * 22 7 22
343 13 44 51	* — 9 25 47	65 15 4 35	36 6 45 40	— * 17 54 14
347 14 47 0	* — 15 14 12	66 15 19 8	43 7 12 45	Gale
414 14 34 24	Có = Córdoba	67 15 41 4	49 7 24 3	* 3 15 14 12
416 17 10 30	5 2 11 32	68 15 43 56	54 7 40 59	G = Gilliss
423 *19 20 18	7 2 51 44	69 15 49 19	56 7 42 55	* 10 1 11 31
454 8 10 53	* 45 16 16 1	70 15 59 11	61 * 8 1 53	* 11 1 12 43
555 * 5 8 47	— 11 33 48	71 16 36 21	66 8 7 33	19 3 11 50
735 0 58 39	— 13 9 27	72 16 53 11	71 8 26 2	22 3 45 32
738 2 17 47	— * 2 31 27	73 17 14 52	78 9 25 26	24 3 49 30
739 2 19 21	— * 21 51 26	74 17 50 43	82 9 48 8	30 4 30 24
744 * 4 16 32	— * 23 37 52	75 19 14 27	86 10 25 48	31 4 39 45
* 746 4 27 2	$\delta$ = Dawson	76 19 47 9	87 10 26 13	* 36 5 34 40
747 4 28 40	* 1 2 24 15	77 * 2 51 13	93 10 30 40	38 5 46 32
750 4 59 55	* 5 10 32 47	78 * 3 13 40	94 10 34 0	42 6 15 38
753 6 24 1	31 1 29 14	79 * 3 57 30	97 10 38 27	44 6 21 10
754 6 30 11	32 1 44 40	80 * 4 25 5	111 * 11 26 19	45 6 21 47
755 6 31 4	33 2 0 42	81 * 4 35 45	113 11 30 50	49 6 49 41
757 7 8 0	34 2 38 36	82 * 4 49 57	114 11 33 49	* 51 6 57 58
759 18 3 29	35 2 43 8	83 * 4 58 55	115 11 33 49	54 7 1 0
760 18 9 10	36 3 9 14	84 * 5 11 26	116 11 50 24	55 7 2 0
761 19 31 10	37 4 55 21	85 * 5 28 3	117 11 58 21	60 7 12 45
762 20 9 0		86 * 5 54 30	118 12 0 12	63 7 17 46
763 20 15 23		87 * 7 8 55	* 124 12 24 14	65 7 20 21
765 20 52 50		88 * 7 30 13	129 13 0 5	
766 21 16 26		89 * 7 33 22	137 13 23 39	
768 Nota 162		90 * 7 34 35	140 13 35 50	
769 22 4 20		91 * 7 34 46	145 13 45 16	
		92 * 7 35 51	146 13 41 51	
		93 * 7 43 28		
		94 * 7 43 53		



G = Gilliss		G = Gilliss		W. Herschel		Hu = Hussey		I = Innes	
66	7 <sup>h</sup> 22 <sup>m</sup> 23 <sup>s</sup> *	222	15 <sup>h</sup> 36 <sup>m</sup> 36 <sup>s</sup> *	♃ V 108 = Hh 251	1500	*13 <sup>h</sup> 4 <sup>m</sup> 20 <sup>s</sup> *	815	8 <sup>h</sup> 40 <sup>m</sup> 7 <sup>s</sup> *	
68	7 29 32	228	16 22 9	VI 119 = 770	1501	*13 8 30	818	* 8 53 14	
* 70	7 37 54	231	16 43 51	N 7 = 692	*1502	*13 13 8	834	* 9 32 28	
73	7 46 27	233	16 53 37	N 18 = 83	*1511	*14 41 18	* 859	10 36 22	
79	7 58 27	234	16 58 15	N 39 = 507	*1512	*14 42 20	869	11 1 23	
83	8 5 31	235	17 0 31	N 48 = 454	*1515	*15 13 10	909	12 43 37	
85	8 7 33	237	17 22 38	N 50 = 352	*1516	*15 37 18	951	14 42 37	
89	8 10 50	239	17 49 34	N 51 = 428	*1522	*17 4 6	1007	17 29 16	
90	8 7 58	240	17 53 40	N 96 = 321	1558	1 56 40	1011	17 47 43	
94	8 21 43	* 243	18 4 18	N 101 = 700			1044	19 59 24	
97	8 25 35	250	18 53 19	N 117 = Hh 770			1091	10 34 22	
103	8 55 27	256	19 45 5				1101	* 1 46 43	
105	9 5 28	258	20 15 22	Hh 83 * 3 <sup>h</sup> 11 <sup>m</sup> 53 <sup>s</sup> *			1110	13 41 30	
107	9 16 23	260	20 26 46	240 * 6 31 38			1116	* 6 13 55	
108	9 17 38	261	20 34 24	251 6 45 40			1122	21 19 58	
109	9 21 3	263	20 47 47	321 * 9 4 51			1130	* 9 15 30	
111	9 29 51	265	20 47 6	352 *10 24 4			—	8 10 12	
114	9 41 59	266	Nota 162	376 *11 26 19			—	18 37 24	
115	9 43 26	267	20 54 57	426 13 44 37			—	* 3 16 24	
116	9 43 59	269	21 21 49	428 13 46 2					
117	9 44 43	271	21 31 30	454 14 44 11					
118	9 44 29	273	21 6 44	507 *16 17 8					
120	9 47 25	279	22 49 33	692 *20 26 32					
122	9 48 8	281	22 57 25	700 20 34 42					
123	9 52 29	286	23 32 49	770 *22 33 3					
126	9 56 20								
129	10 3 4								
130	10 10 10								
136	10 11 16								
139	10 15 12								
143	10 17 15								
149	10 28 33								
151	10 30 40								
* 152	10 34 14								
156	10 45 8								
157	10 52 57								
160	10 59 7								
163	11 13 2								
164	11 17 57								
166	11 33 13								
167	11 34 0								
172	11 56 8								
173	11 59 55								
174	12 2 8								
177	12 18 24								
179	12 35 2								
180	12 35 15								
182	12 37 39								
184	12 40 39								
191	13 22 27								
193	13 28 44								
194	13 35 50								
196	13 45 16								
197	13 49 57								
202	14 11 3								
203	14 14 7								
209	14 39 2								
210	14 39 15								
215	14 57 52								
216	15 9 45								
218	15 16 28								
219	15 21 8								
220	15 22 25								
221	15 30 44								

$\gamma$ = Lowell Obs.	Piazz	Rü = Rümker	Rus = Russell	S = South
342 17 <sup>h</sup> 45 <sup>m</sup> 3 <sup>s</sup>	— 1 <sup>h</sup> 34 <sup>m</sup> 10 <sup>s</sup>	16 13 <sup>h</sup> 0 <sup>m</sup> 5 <sup>s</sup>	210 12 <sup>h</sup> 54 <sup>m</sup> 12 <sup>s</sup>	569 * 8 <sup>h</sup> 25 13 <sup>s</sup>
344 Nota 162	— 2 43 39	17 13 23 39	222 13 28 42	O. Stone
386 19 30 44	— 2 53 31	20 15 36 31	243 14 14 7	6 * 3 4 56
388 19 31 10	— 7 24 3	21 15 51 51	262 15 26 53	12 * 5 44 51
405 *19 59 15	— 7 58 12	* 22 17 46 48	267 15 36 31	24 *12 40 0
410 20 5 40	— 9 25 26	Rus = Russell	278 16 16 22	38 *17 54 14
471 *22 11 52	— 13 46 2	1 0 1 17	283 16 34 8	— 0 58 39
472 *22 14 50	— 15 48 54	11 1 37 41	* 297 17 9 35	Tapia
490 23 27 11	— 17 51 4	* 12 1 51 18	298 17 10 30	— 10 53 20
— 16 50 10	Pk = Pollock	56 4 59 55	* 304 17 46 48	H. C. Wilson
— 17 10 30	5 17 31 2	118 9 21 24	322 20 26 46	24 *21 53 53
Melbourne	Rü = Rümker	134 9 48 8	333 21 21 49	26 *21 58 1
— 12 3 35	7 8 7 33	153 10 34 14	Sellors	
— 17 10 30	10 9 16 23	160 10 45 8	* 1 1 0 30	
Olivier	11 9 43 59	* 161 10 44 27	* 19 13 59 37	
16 16 50 10	12 9 52 29	174 11 33 13	* 20 15 13 58	
		* 207 12 38 38	* 25 3 8 2	

C. — HERSCHEL STARS OUT OF THE REGULAR ORDER  
ESTRELLAS DE HERSCHEL FUERA DEL ORDEN NUMÉRICO

591 *17 35 27	2744 14 40 18	3380 * 1 33 33	3526 Nota 166	5443 6 37 10
1295 *16 44 35	2748 14 44 11	3394 * 1 39 25	3708 Nota 172	5444 10 32 33
1296 *16 44 51	2765 15 3 53	3429 * 0 15 48	4037 Nota 237	5448 22 41 5
2446 8 19 27	2778 15 18 14	3431 * 0 17 4	4351 10 45 8	
2731 14 28 10	2787 15 30 30	3440 * 0 23 35	4510 12 20 18	
2736 14 33 22	2789 15 34 15	3442 * 0 26 40	4851 *17 17 9	
2742 14 38 15	3368 * 1 16 31	3469 Nota 164	5217 20 28 48	

NOTE. — I have considered as in order the stars of his fifth catalogue (1938 — 3241) north of  $-30^\circ$  and those of *Results* (3347 — 5442) with less than  $1^m$  error in R. A.

NOTA. — Se consideran como en orden las de su quinto catálogo (1938 — 3241) al norte de  $-30^\circ$  y las de *Results* (3347 — 5442) cuya A. R. no tenga error de más de  $1^m$ .

D. — CIRCUMPOLAR STARS. ESTRELLAS CIRCUMPOLARES

Estrella	1830.0		1875.0		1900.0		1950.0	Prec.
<i>h</i> 3392	0 <sup>h</sup> 36 <sup>m</sup> 1	—79° 26'	<i>d</i>	0 <sup>h</sup> 37 <sup>m</sup> 8	—79° 11'		0 <sup>h</sup> 40 <sup>m</sup> 1	+ 0° 49
3420	1 5.8	82 33	<i>a</i>	1 6.0	82 19		1 6.4	81 55
3443	1 24.6	80 46	<i>a</i>	1 24.6	80 33		1 24.9	80 9
3453	1 32.7	79 22	<i>a</i>	1 32.8	79 8		1 33.3	78 45
3467	1 41.5	80 0	<i>a</i>	1 41.3	79 47		1 41.3	79 24
<i>h</i> 3474	1 49.7	—81 1	<i>a</i>	1 49.0	—80 48		1 48.2	—80 25
3508	2 26.9	78 31	<i>b</i>	2 26.2	78 19		2 25.4	77 59
3519	2 32.2	83 14	<i>b</i>	2 29.4	83 2		2 25.2	82 42
3530	2 40.8	81 29	<i>b</i>	2 38.9	81 18		2 35.9	80 58
3539	2 47.3	78 50	<i>b</i>	2 46.2	78 39		2 44.6	78 20

NOTA. — Las *a* son posiciones de catálogo meridiano, *b* de Durchmusterung, *c* obtenidas diferencialmente con micrómetro o círculos, y *d* por diagrama.

Estrella	1830.0		1875.0	1900.0	1950.0	Prec.
<i>h</i> 3560	3 <sup>h</sup> 7 <sup>m</sup> 4 —84°53'	<i>d</i>	3 <sup>h</sup> 1 <sup>m</sup> 5 —84°42'	2 <sup>h</sup> 58 <sup>m</sup> 6 —84°36'	2 <sup>h</sup> 53 <sup>m</sup> 1 —84°24'	+ 4.916
3568	3 13.5 79 38	<i>a</i>	3 11.8 79 28	3 10.9 79 22	3 9.1 79 11	2.23
3577	3 20.7 82 27	<i>b</i>	3 17.2 82 17	3 15.5 82 11	3 11.9 82 0	3.08
3581	3 27.7 81 6	<i>d</i>	3 24.8 80 57	3 23.5 80 52	3 20.8 80 41	2.71
3582	3 27.7 84 10	<i>a</i>	3 22.8 83 59	3 20.0 83 54	3 14.8 83 43	4.01
<i>h</i> 3585	3 32.5 —85 1	<i>d</i>	3 25.5 —84 52	3 22.1 —84 47	3 15.5 —84 36	+ 4.73
3595	3 41.5 83 11	<i>c</i>	3 37.0 83 1	3 34.7 82 56	3 29.9 82 46	3.65
3605	3 47.3 80 52	<i>b</i>	3 44.8 80 43	3 43.3 80 38	3 40.3 80 29	2.83
3607	3 48.7 81 24	<i>a</i>	3 45.5 81 15	3 43.8 81 10	3 40.5 81 1	3.00
3612	3 52.1 80 33	<i>a</i>	3 49.5 80 24	3 48.0 80 20	3 45.2 80 11	2.78
<i>h</i> 3673	4 32.6 —78 3	<i>a</i>	4 30.4 —77 57	4 29.3 —77 54	4 27.1 —77 48	+ 2.45
3692	4 43.0 83 15	<i>a</i>	4 37.5 83 10	4 34.5 83 7	4 28.6 83 1	4.33
3708	4(52±) (87)52	<i>d</i>	4 41± 88 22	4 25± 88 19	3 55± 88 11	17.35
3721	4 58.9 80 55	<i>a</i>	4 55.4 80 51	4 53.3 80 49	4 49.4 80 44	3.34
3733	5 6.2 79 38	<i>b</i>	5 3.3 79 34	5 1.7 79 32	4 58.4 79 27	2.96
<i>h</i> 3741	5 9.5 —78 31	<i>a</i>	5 7.0 —78 28	5 5.6 —78 26	5 2.9 —78 22	+ 2.70
3773	5 29.5 82 27	<i>b</i>	5 24.7 82 25	5 21.8 82 24	5 16.1 82 21	4.15
3809	5(47±) (86)24	<i>b</i>	5 20.4 87 20	5 10.0 87 18	4 49.9 87 14	11.58
Cape —		<i>b</i>	5 40.6 89 32	4 36.9 89 30	3 4.5 89 21	59.65
<i>h</i> 3817	5 49.4 80 27	<i>b</i>	5 46.0 80 25	5 44.0 80 25	5 39.9 80 23	3.33
<i>h</i> 3872	6 28.2 —79 54	<i>c</i>	6 24.9 —79 55	6 23.0 —79 56	6 19.0 —79 58	+ 3.17
3888	6 39.0 78 46	<i>a</i>	6 36.3 78 49	6 34.8 78 50	6 31.8 78 52	2.84
3892	6 41.4 80 57	<i>b</i>	6 37.6 80 59	6 35.4 81 1	6 31.0 81 3	3.52
3899	6 47.9 80 29	<i>c</i>	6 44.5 80 32	6 42.5 80 33	6 38.5 80 36	3.33
3903	6 50.0 84 58	<i>b</i>	6 41.0 85 1	6 36.0 85 3	6 25.7 85 5	6.37
<i>h</i> 3975	7 26± —81 18	<i>b</i>	7 25.0 —81 22	7 22.8 —81 23	7 18.4 —81 31	+ 3.49
3987	7 31.0 78 49	<i>a</i>	7 28.6 78 55	7 27.3 78 58	7 24.5 79 4	2.70
3996	7 38.4 84 8	<i>a</i>	7 31.6 84 14	7 27.8 84 17	7 19.9 84 23	5.18
4010	7 45.1 87 2	<i>b</i>	7 29.7 87 9	7 20.5 87 12	7 0.9 87 18	10.73
4047	8 0.6 88 43	<i>b</i>	7 21.6 88 49	6 56.4 88 52	6 0.7 88 54	27.30
<i>h</i> 4067	8( 8.8) —83 14	<i>a</i>	8 8.4 —83 22	8 5.6 —83 27	7 59.7 —83 35	+ 4.17
4086	8 16.4 85 27	<i>a</i>	8 8.0 85 35	8 3.0 85 39	7 52.6 85 47	6.31
4105	8 23.9 78 41	<i>b</i>	8 22.0 78 50	8 21.0 78 55	8 18.9 79 4	2.37
4132	8 36.8 82 43	<i>b</i>	8 32.8 82 53	8 30.6 82 58	8 25.9 83 8	3.60
4158	8 52.0 84 4	<i>b</i>	8 47.0 84 14	8 44.1 84 20	8 37.9 84 31	4.45
<i>h</i> 4194	9 10.0 —83 0	<i>b</i>	9 6.7 —83 11	9 4.7 —83 17	9 0.6 —83 30	+ 3.30
4204	9 16.3 80 28	<i>b</i>	9 14.6 80 39	9 13.6 80 45	9 11.5 80 58	2.30
4205	9 17.1 80 26	<i>c</i>	9 15.4 80 37	9 14.4 80 43	9 12.4 80 56	2.28
<i>h</i> 4211 = $\xi$ Oct.	9 20— 84 58	<i>a</i>	9 14.4 85 10	9 11.2 85 16	9 4.5 85 28	4.53
<i>h</i> 4226	9 30.4 77 31	<i>b</i>	9 29.9 77 42	9 29.7 77 49	9 29.3 78 2	1.61
<i>h</i> 4265	9 48.2 —79 43	<i>b</i>	9 47.4 —79 56	9 47.0 —80 3	9 46.0 —80 16	+ 1.77
$\Delta$ 82 = <i>h</i> 4272	9 52.6 85 13	<i>a</i>	9 48.1 85 26	9 45.5 85 33	9 39.9 85 47	3.97
<i>h</i> 4276	9 53.4 77 56	<i>b</i>	9 53.2 78 9	9 53.1 78 16	9 52.8 78 30	1.44
4281	9 56.9 79 36	<i>b</i>	9 56.3 79 50	9 26.0 79 57	9 55.3 80 11	1.64
4310	10 14.6 83 15	<i>a</i>	10 11.3 83 28	10 10.4 83 36	10 8.2 83 51	2.30
<i>h</i> 5444	10 32.6 —81 3	<i>a</i>	10 32.5 —81 17	10 32.4 —81 24	10 32.2 —81 40	+ 1.39
4390	10 50.6 82 19	<i>b</i>	10 50.7 82 33	10 50.7 82 41	10 50.6 82 57	1.30
4406	10 59.1 83 0	<i>b</i>	10 59.1 83 15	10 59.1 83 23	10 59.1 83 39	1.27
4427	11(14.1) 82 50	<i>b</i>	11 19.0 83 5	11 19.5 83 13	11 20.4 83 29	0.83
4440	11 21.4 77 35	<i>a</i>	11 22.9 77 50	11 23.8 77 58	11 25.5 78 15	0.42

Estrella	1830.0			1875.0		1900.0		1950.0		Prec.
<i>h</i> 4462 = Rus 174	11 <sup>h</sup> 31 <sup>m</sup> 8	-82° 8'	<i>b</i>	11 <sup>h</sup> 33 <sup>m</sup> 2	-82° 23'	11 <sup>h</sup> 34 <sup>m</sup> 0	-82° 31'	11 <sup>h</sup> 35 <sup>m</sup> 7	-82° 48'	+ 0.48
<i>h</i> 4468	11 35.3	82 10	<i>a</i>	11 36.7	82 24	11 37.6	82 33	11 39.3	82 49	0.42
4490	11 53.8	84 46	<i>b</i>	11 56.1	84 56	11 57.3	85 4	11 59.8	85 21	+ 0.07
4504	12 2.8	82 25	<i>b</i>	12 5.1	82 40	12 6.5	82 48	12 9.3	83 5	- 0.13
4529	12 25.3	78 3	<i>b</i>	12 28.0	78 18	12 29.6	78 26	12 32.8	78 42	0.36
<i>h</i> 4538	12 31.7	-82 44	<i>b</i>	12 35.0	-82 58	12 37.0	-83 7	12 41.2	-83 23	- 0.75
4544	12 33.9	78 32	<i>b</i>	12 36.9	78 47	12 38.6	78 55	12 42.2	79 11	0.49
4565	12 52.5	81 48	<i>a</i>	12 56.6	82 3	12 58.9	82 11	13 3.6	82 27	1.04
4566	12 54.9	77 32	<i>a</i>	12 58.4	77 47	13 0.3	77 55	13 4.3	78 11	0.69
4581	13 13.1	78 53	<i>b</i>	13 17.1	79 7	13 19.4	79 15	13 24.0	79 31	1.01
<i>h</i> 4584	13 14.6	-83 31	<i>c</i>	13 19.7	-83 44	13 22.8	-83 51	13 29.2	-84 7	- 1.84
4585	13 15.5	83 35	<i>b</i>	13 20.6	83 48	13 23.8	83 56	13 30.3	84 12	1.88
4594	13 24.3	79 42	<i>b</i>	13 28.7	79 56	13 31.2	80 4	13 36.3	80 19	1.25
4610	13 35.5	79 25	<i>b</i>	13 40.0	79 39	13 42.6	79 47	13 48.0	80 2	1.36
4629	13 45.6	77 34	<i>b</i>	13 50.0	77 48	13 52.4	77 55	13 57.5	78 10	1.25
<i>h</i> 4635	13 46.6	-77 50	<i>b</i>	13 50.9	-78 4	13 53.4	-78 11	13 58.6	-78 26	- 1.29
4644	13 55.5	82 42	<i>b</i>	14 1.6	82 56	14 5.3	83 3	14 12.8	82 17	2.39
<i>h</i> 4671 = Rus 243	14 8.8	79 19	<i>a</i>	14 14.1	79 32	14 17.0	79 39	14 23.2	79 53	1.74
<i>h</i> 4689	14 26.1	78 3	<i>b</i>	14 31.3	78 15	14 34.2	78 22	14 40.3	78 35	1.72
4703	14 38.8	77 48	<i>b</i>	14 44.1	78 0	14 47.1	78 6	14 53.3	78 19	1.80
<i>h</i> 4744	15 1.6	-79 35	<i>b</i>	15 7.9	-79 46	15 11.5	-79 51	15 18.8	-80 2	- 2.35
<i>h</i> 4759 = <i>h</i> 4762	15 10.6	79 36	<i>b</i>	15 17.0	79 46	15 20.7	79 51	15 28.1	80 2	2.43
<i>h</i> 4780 = Rus 262	15 20.2	79 59	<i>b</i>	15 26.9	80 8	15 30.7	80 13	15 38.5	80 23	2.61
<i>h</i> 4787	15 24.3	79 4	<i>b</i>	15 30.7	79 13	15 34.4	79 18	15 41.8	79 28	2.41
4790	15 26.9	78 11	<i>b</i>	15 34.2	78 19	15 37.7	78 24	15 44.8	78 34	2.25
<i>h</i> 4798	15 32.0	-83 43	<i>a</i>	15 41.4	-83 52	15 47.0	-83 57	15 58.6	-84 6	- 4.40
4816	15 42.9	83 38	<i>b</i>	15 52.2	83 46	15 57.8	83 50	16 9.5	83 59	4.46
Brisb.	15 55.2	78 15	<i>a</i>	16 1.7	78 23	16 5.4	78 27	16 12.8	78 34	2.44
<i>h</i> 4860	16 20.4	79 19	<i>b</i>	16 27.6	79 25	16 31.7	79 28	16 39.9	79 34	2.82
4865	16 24.3	83 41	<i>b</i>	16 34.8	83 47	16 40.9	83 50	16 53.3	83 55	4.88
<i>h</i> 4884	16 34.6	-82 3	<i>a</i>	16 43.8	-82 8	16 49.0	-82 10	16 59.3	-82 15	- 3.89
4912	16 51.2	82 34	<i>a</i>	17 1.0	82 39	17 6.4	82 41	17 18.6	82 44	4.25
4937	17 7.5	77 58	<i>b</i>	17 14.6	78 2	17 18.4	78 3	17 26.2	78 6	2.64
4947	17 13.6	81 47	<i>b</i>	17 22.6	81 49	17 27.8	81 50	17 38.0	81 52	3.88
4987	17 40.6	80 26	<i>d</i>	17 48.9	80 27	17 53.5	80 28	18 2.7	80 28	3.36
<i>h</i> 4988	17 42.0	-78 58	<i>b</i>	17 49.6	-78 59	17 53.7	-78 59	18 2.0	-79 0	- 2.91
5043	18 16.9	83 35	<i>a</i>	18 27.8	83 33	18 33.9	83 32	18 46.2	83 30	4.89
5063	18 36.2	79 11	<i>b</i>	18 43.7	79 9	18 47.8	79 7	18 56.0	79 3	2.89
5071	18 43.5	80 14	<i>b</i>	18 51.4	80 11	18 55.8	80 9	19 4.5	80 5	3.16
5073	18 46.0	78 51	<i>b</i>	18 53.3	78 48	18 57.3	78 46	19 5.3	78 41	2.77
575			<i>b</i>	19 14.4	-78 9	19 18.2	-78 7	19 25.8	-78 1	- 2.55
<i>h</i> 5106	19 9.1	79 8	<i>b</i>	19 16.5	79 3	19 20.4	79 0	19 28.3	78 54	2.74
5116	19 16.1	78 52	<i>b</i>	19 23.2	79 48	19 27.0	78 45	19 34.8	78 38	2.65
5126	19 22.5	79 49	<i>b</i>	19 28.8	79 43	19 33.0	79 40	19 41.0	79 33	2.85
5127	19 22.9	86 30	<i>b</i>	19 37.6	86 16	19 46.5	86 13	20 3.6	86 5	7.54
<i>h</i> 5149	19 38.0	-79 13	<i>a</i>	19 45.1	-79 7	19 49.0	-79 3	19 56.6	-78 55	- 2.61
5153	19 44.0	79 34	<i>a</i>	19 51.2	79 28	19 55.1	79 24	20 2.8	79 15	2.65
<i>l</i> 1044			<i>b</i>	19 59.4	81 39	20 4.0	81 35	20 12.9	81 26	3.26
<i>h</i> 5175	20 0.7	82 27	<i>b</i>	20 9.8	82 19	20 14.6	82 15	20 23.3	82 5	3.44
5182	20 4.4	81 31	<i>a</i>	20 12.3	81 22	20 16.6	81 18	20 25.1	81 8	3.07

Estrella	1830.0		1875.0		1900.0		1950.0		Prec.
I 337 + h 5192	20 <sup>h</sup> 12 <sup>m</sup> .4	-87°42'	b	20 <sup>h</sup> 34 <sup>m</sup> .4	-87°32'		21 <sup>h</sup> 5 <sup>m</sup> .3	-87°15'	- 9.40
G 263			a	20 47.8	81 11		20 59.3	80 54	2.63
h 5233	20 43.4	83 56	a	20 52.5	83 46		21 6.9	83 28	3.61
h 5235 = h 5245	20 45.3	84 59	a	20 55.0	84 49		21 11.3	84 31	4.29
h 5261 = Rus 333	21 8.9	86 35	a	21 21.8	86 24		21 40.9	86 4	5.41
h 5262	21 10.2	-80 46	a	21 16.7	-80 35		21 26.9	-80 16	- 2.16
h 5278 = λ Oct.	21 23.8	83 29	a	21 31.5	83 17		21 43.4	82 57	2.77
h 5289	21 32.5	81 23	b	21 38.0	81 10		21 47.8	80 50	2.04
5292	21 33.6	85 32	b	21 42.0	85 20		21 56.5	84 59	3.66
5310	21 49.1	78 32	d	21 52.9	78 18		21 59.0	77 54	1.41
h 5318	22 1.3	-81 18	a	22 6.7	-81 5		22 15.3	-80 42	- 1.64
5350	22 28.8	88 52	a	22 46.0	88 38		23 5.9	88 14	6.04
5353	22 29.2	80 45	b	22 33.7	80 31		22 41.0	80 7	1.19
5368	22 43.9	85 26	a	22 49.6	85 12		22 58.8	84 50	1.87
5378	22 52.8	83 19	a	22 57.4	83 4		23 4.6	82 40	1.17
h 5385	23 0.2	-79 16	b	23 3.9	-79 1		23 9.7	-78 37	- 0.68
5388	23 4.1	81 21	a	23 8.0	81 6		23 14.0	80 42	0.77
5399	23 17.5	82 3	d	23 21.0	81 48		23 26.7	81 23	0.62
5406	23 26.4	80 59	b	23 29.5	80 45		23 34.6	80 20	0.43
5414	23 33.1	78 45	b	23 36.1	78 30		23 40.7	78 5	0.27
h 5442 = Rus 1	23 59.0	-78 26	b	0 1.3	-78 11		0 5.0	-77 46	+ 0.03

# CONNECTIONS OF CLUSTER STARS

## CONEXIONES DE ESTRELLAS DE CÚMULOS

### A. — CONEXIONES DEL AÑO 1917

* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.	* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.
		Δ A. R.	Δ Decl.				Δ A. R.	Δ Decl.	
— 60° 925	.167	+ 2 <sup>s</sup> .45	—3' 15 <sup>h</sup> .2	— 60° 924	— 60° 974	.285	+ 8 <sup>s</sup> .57	—3' 14 <sup>h</sup> .8	— 60° 969
	.167	— 68.30	—4 31.1	60 935		.285	— 10.91	+2 32.3	60 979
60 930	.167	+ 43.63	+5 10.4	60 924	60 975	.296	— 9.56	—3 56.6	60 979
	.167	— 27.27	+3 53.9	60 935		.296	— 15.06	+1 39.7	60 985
60 933	.167	+ 55.61	+1 22.4	60 924	60 978	.296	— 5.33	—1 57.4	60 979
	.167	— 15.28	+0 6.2	60 935		.296	— 10.81	+3 39.1	60 985
60 939	.282	— 25.01	+0 48.7	60 944	60 980	.296	+ 1.81	—2 10.9	60 979
	.285	— 60.56	—2 5.8	60 953		.296	— 3.68	+3 25.2	60 985
60 942	.282	— 6.78	+2 20.4	60 944		.296	— 40.71	+0 23.2	60 1006
	.285	— 42.42	—0 34.9	60 953	60 981	.296	— 2.56	+0 29.1	60 985
60 945	.282	+ 2.24	—1 32.8	60 944		.296	— 39.58	—2 33.1	60 1006
	.285	— 33.33	—4 27.7	60 953					
— 60 948	.282	+ 14.20	+1 54.0	— 60 944	— 60 982	.296	+ 4.92	—1 14.5	— 60 979
	.285	— 21.32	—1 0.8	60 953		.296	— 0.61	+4 22.0	60 985
60 949	.282	+ 26.20	—4 23.5	60 944	60 984	.285	+ 25.33	—2 29.3	60 969
	.285	— 34.42	+2 11.5	60 967		.285	+ 6.11	+3 17.9	60 979
60 952	.282	+ 34.54	+0 11.6	60 944	60 989	.296	+ 11.04	—0 3.1	60 985
	.285	— 1.10	—2 43.8	60 953		.296	— 25.97	—3 5.0	60 1006
60 954	.285	+ 7.90	—4 20.9	60 953	60 990	.296	+ 19.25	—1 15.7	60 979
	.285	— 38.98	—3 37.7	60 979		.296	— 23.29	+1 18.1	60 1006
60 955	.170	— 30.93	—1 0.9	60 976	60 991	.285	+ 40.38	—0 45.9	60 969
	.176	— 17.63	+3 8.7	60 969		.307	+ 27.14	—4 55.0	60 976
60 961	.307	— 7.42	+1 2.6	60 967	60 993	.285	+ 41.69	—2 39.9	60 969
	.307	— 34.74	—2 8.3	60 985		.296	+ 22.22	+3 7.5	60 979
— 60 964	.170	— 19.57	—0 59.4	— 60 976	— 60 995	.307	+ 31.62	+2 50.5	— 60 976
	.176	— 6.27	+3 10.0	60 969		.307	— 39.52	+1 3.8	60 1012
60 966	.170	— 15.22	+0 16.9	60 976	60 1000	.307	+ 34.88	—2 23.9	60 976
	.176	— 1.87	+4 26.5	60 969		.315	— 36.35	—4 9.8	60 1012
60 968	.285	+ 25.13	—3 29.5	60 953	60 1003	.285	+ 54.24	—0 59.2	60 969
	.285	— 21.76	—2 46.7	60 979		.296	+ 34.83	+4 48.0	60 979
60 970	.285	+ 27.43	—2 51.5	60 953	60 1008	.315	— 30.28	—6 53.8	60 1012
	.296	— 19.58	—2 8.9	60 979		.307	— 21.47	—0 58.9	60 1012
60 971	.285	+ 0.65	—2 15.7	60 969		.307	— 44.32	—	60 1018
	.285	— 18.89	+3 31.5	60 979	60 1013	.321	— 44.11	—1 1.3	60 1018
60 973	.285	+ 8.51	—4 25.6	60 969		.296	+ 24.92	—2 34.8	60 1006
	.285	— 10.91	+1 22.6	60 979		.296	— 5.63	—3 9.8	60 1015

* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.	* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.
		Δ A. R.	Δ Decl.				Δ A. R.	Δ Decl.	
— 60°1017	.296	+ 5.99	+1' 9.6	— 60°1015	— 58°3000	.389	+ 8.40	—6' 21.4	— 58°2995
	.296	— 29.82	—3 1.7	60 1022		.389	— 17.27	—6 7.6	58 3005
60 1019	.315	+ 7.11	—5 4.8	60 1018	58 3003	.389	+ 19.24	+2 13.4	58 2995
	.315	— 13.91	+4 28.3	60 1022		.389	— 6.50	+2 27.3	58 3005
57 3486	.425	— 11.88	—0 34.4	57 3499	57 4181	.373	+ 20.42	—4 7.0	57 4170
	.427	— 10.57	+0 35.6	57 3500		.373	+ 39.91	+5 45.4	57 4156
57 3502	.425	+ 1.86	—3 8.0	57 3499	58 3014	.389	+ 14.42	+4 30.9	58 3005
	.427	+ 3.17	—1 57.9	57 3500		.389	— 22.38	—1 42.9	57 4208
	.427	— 62.59	+3 7.2	57 3563	58 3016	.389	+ 16.54	+0 49.8	58 3005
57 3504	.425	+ 3.15	—0 49.5	57 3499		.389	— 20.10	—5 24.7	57 4208
	.427	+ 4.38	+0 20.7	57 3500		.392	— 40.39	+1 37.6	58 3056
57 3506	.425	+ 4.62	—2 37.8	57 3499	58 3019	.389	+ 19.69	+5 3.5	58 3005
	.427	+ 5.87	—1 27.5	57 3500		.389	— 17.00	—1 10.5	57 4208
					58 3020	.389	+ 19.27	—3 19.3	58 3005
— 57 3507	.425	+ 6.14	—0 58.6	— 57 3499		.392	— 37.51	—2 30.3	58 3056
	.427	+ 7.46	+0 11.4	57 3500					
57 3508	.425	+ 7.28	—1 52.5	57 3499	— 58 3027	.389	+ 24.83	+4 26.2	— 58 3005
	.427	+ 8.56	—0 42.5	57 3500		.389	— 11.90	—1 48.1	57 4208
	.427	— 57.13	+4 22.4	57 3563	58 3028	.389	+ 25.41	+4 2.2	58 3005
57 3515	.425	+ 12.86	—1 24.1	57 3499		.389	— 11.23	—2 12.0	57 4208
	.427	+ 14.10	—0 13.8	57 3500	58 3031	.389	+ 30.60	+3 8.7	58 3005
57 3516	.425	+ 12.23	—3 52.3	57 3499		.389	— 6.14	—3 5.4	57 4208
	.427	+ 13.51	—2 41.9	57 3500	57 4206	.411	— 37.17	+4 14.2	57 4235
57 3517	.425	+ 11.66	—3 12.9	57 3499		.417	— 37.08	+4 13.6	57 4235
	.427	+ 12.92	—2 3.0	57 3500	58 3036	.389	+ 34.55	+3 3.2	58 3005
57 3521	.425	+ 14.51	—2 59.8	57 3499		.389	— 2.15	—3 11.1	57 4208
	.427	+ 15.79	—1 50.5	57 3500	58 3037	.389	+ 35.52	+1 12.4	58 3005
57 3523	.425	+ 15.61	—1 45.6	57 3499		.389	— 1.13	—5 1.2	57 4208
	.427	+ 16.84	—0 35.5	57 3500		.392	— 21.40	+2 1.2	58 3056
— 57 3524	.425	+ 16.48	—0 56.9	— 57 3499	— 58 3038	.389	+ 38.48	—1 31.1	— 58 3005
	.427	+ 17.73	+0 12.8	57 3500		.392	— 18.47	—0 41.8	58 3056
57 3526	.425	+ 16.83	—2 51.3	57 3499	58 3040	.389	+ 40.21	—1 59.5	58 3005
	.427	+ 18.11	—1 40.9	57 3500		.392	— 16.66	—1 11.4	58 3056
57 3527	.425	+ 19.53	—3 34.3	57 3499	58 3043	.389	+ 5.89	—2 15.7	57 4208
	.427	+ 20.89	—2 24.2	57 3500		.411	— 28.81	—4 52.4	57 4235
57 3533	.425	+ 26.11	—1 28.9	57 3499	58 3044	.389	+ 6.76	—1 10.5	57 4208
	.427	+ 27.39	—0 18.7	57 3500		.411	— 27.94	—3 47.3	57 4235
57 3540	.427	+ 35.22	—3 52.3	57 3500	58 3048	.392	+ 8.42	+0 5.5	58 3039
	.427	— 30.51	+1 13.7	57 3563		.406	+ 8.41	+0 5.0	58 3039
58 2949	.373	— 14.28	—1 52.4	58 2953	58 3049	.392	— 8.70	+0 15.8	58 3056
	.381	— 14.35	—1 52.0	58 2953		.406	— 8.66	+0 15.7	58 3056
58 2963	.373	+ 18.62	—3 32.3	58 2953		.409	— 8.66	+0 15.6	58 3056
	.381	— 28.24	+4 20.5	58 2979	58 3050	.392	— 8.64	—4 35.4	58 3056
						.406	— 8.66	—4 35.1	58 3056
— 58 2968	.373	+ 24.77	+3 30.5	— 58 2953					
	.381	— 62.16	+3 44.7	58 2995	— 58 3051	.406	— 4.30	—4 51.6	— 58 3056
57 4133	.373	+ 12.88	—5 37.9	57 4127		.417	— 4.37	—4 52.0	58 3056
	.373	— 42.82	+3 1.8	57 4156	58 3053	.392	— 3.47	—3 31.7	58 3056
57 4141	.373	+ 33.49	+1 28.3	57 4127		.406	— 3.41	—3 31.5	58 3056
	.363	— 41.70	+0 15.0	57 4170	58 3055	.392	+ 16.65	—3 51.4	58 3039
58 2986	.381	— 23.57	—1 14.7	58 2995		.406	+ 16.47	—3 52.3	58 3039
	.381	— 49.25	—1 1.2	58 3005	58 3057	.406	+ 1.74	+0 45.9	58 3056
58 2987	.381	— 22.12	+0 40.0	58 2995		.409	+ 1.76	+0 45.9	58 3056
	.381	— 47.86	+0 53.9	58 3005	58 3058	.389	+ 22.27	—0 38.3	57 4208
58 2993	.381	— 8.75	—1 19.8	58 2995		.411	— 12.34	—3 14.9	57 4235
	.381	— 34.41	—1 6.5	58 3005	58 3066	.406	+ 16.00	+3 12.6	58 3056
58 2999	.389	+ 3.22	—5 44.4	58 2995		.409	— 55.68	—3 20.6	58 3112
	.389	— 22.60	—5 30.0	58 3005	58 3069	.406	+ 18.99	+0 51.9	58 3056
						.406	— 36.99	+4 27.7	58 3103

* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.	* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.
		Δ A. R.	Δ Decl.				Δ A. R.	Δ Decl.	
— 58°3073	.406	+ 23.64	+3' 9.2	— 58°3056	— 57°4295	.417	+ 6.62	+4' 24.8	— 57°4293
	.409	— 48.12	—3 23.6	58 3112		.417	— 1.15	+8 12.4	57 4296
58 3075	.406	+ 25.48	—3 8.7	58 3056	58 3144	.417	— 33.23	+2 24.0	58 3161
	.406	— 30.39	+0 27.6	58 3103		.419	+ 31.96	+1 40.7	58 3120
58 3077	.409	— 43.19	—0 10.2	58 3112		.425	+ 13.18	+4 37.9	58 3132
	.411	+ 14.04	—3 17.9	57 4235	58 3145	.417	— 30.48	—3 33.8	58 3161
58 3079	.406	+ 31.08	—2 50.9	58 3056		.425	+ 16.14	—1 19.9	58 3132
	.406	— 24.76	+0 45.5	58 3103	58 3168	.409	+ 37.99	—2 48.0	58 3147
57 4247	.411	+ 17.33	+4 51.8	57 4235		.419	— 45.13	+1 12.0	58 3189
	.417	+ 17.31	+4 51.4	57 4235	58 3174	.417	+ 18.13	—5 33.0	58 3161
58 3080	.409	— 39.33	—1 42.8	58 3112		.419	— 28.70	+2 19.8	58 3186
	.419	— 46.01	+2 26.5	58 3120	57 4322	.417	+ 53.12	+1 36.5	57 4296
58 3081	.409	— 37.86	—3 23.2	58 3112		.417	— 26.32	—4 8.5	57 4335
	.419	— 44.52	+0 45.0	58 3120	58 3175	.419	— 29.84	—1 40.8	58 3189
— 57 4253	.409	— 35.37	+0 43.7	— 58 3112		.419	— 23.08	—6 51.3	58 3186
	.411	+ 21.84	—2 23.5	57 4235	— 58 3178	.419	— 20.24	+1 58.3	— 58 3189
58 3085	.409	— 34.18	—0 1.3	58 3112		.419	— 13.64	—3 12.6	58 3186
	.411	+ 23.07	—3 9.1	57 4235	58 3181	.430	+ 37.99	+6 54.5	58 3163
58 3087	.409	— 32.31	—1 3.9	58 3112		.430	— 2.47	—8 37.4	58 3184
	.419	— 38.97	+3 5.3	58 3120	58 3183	.417	+ 42.38	—4 9.1	58 3161
58 3090	.409	— 30.16	—3 0.0	58 3112		.419	— 4.39	+3 45.0	58 3186
	.419	— 36.75	+1 8.6	58 3120	58 3198	.419	+ 24.44	+3 29.3	58 3186
58 3092	.409	— 25.16	—0 46.4	58 3112		.428	— 47.01	+0 22.2	58 3217
	.411	+ 32.07	—3 54.1	57 4235	58 3199	.419	+ 29.37	—4 12.7	58 3186
	.419	— 31.80	+3 22.4	58 3120		.419	+ 22.69	+0 57.7	58 3189
57 4257	.409	— 21.60	+2 11.1	58 3112	58 3219	.425	+ 33.37	+1 22.6	58 3203
	.411	+ 35.64	—0 56.6	57 4235		.425	+ 3.24	+8 9.8	58 3217
58 3097	.406	— 5.05	—2 53.7	58 3103	58 3228	.425	+ 22.19	—1 2.3	58 3217
	.409	— 62.92	+0 52.8	58 3147		.428	+ 22.20	—1 2.6	58 3217
— 58 3099	.409	— 18.41	—1 20.3	— 58 3112	— 58 3229	.430	— 8.07	+1 40.3	— 58 3231
	.419	— 25.00	+2 49.3	58 3120		.430	— 9.19	+3 10.3	58 3232
58 3102	.409	— 16.37	—3 47.0	58 3112	58 3233	.425	+ 38.75	—4 54.6	58 3217
	.419	— 22.93	+0 21.4	58 3120		.428	+ 38.74	—4 54.8	58 3217
58 3104	.419	— 22.16	—3 59.2	58 3120	58 3243	.430	+ 33.18	—4 20.0	58 3231
	.425	— 40.73	—1 2.9	58 3132		.430	+ 32.05	—2 49.7	58 3232
58 3107	.409	— 5.76	—1 12.4	58 3112	58 3244	.430	+ 37.76	—1 58.2	58 3231
	.419	— 12.36	+2 56.5	58 3120		.430	+ 36.65	—0 27.6	58 3232
57 4272	.417	— 35.17	—3 48.3	57 4293	58 3255	.430	+ 37.93	—2 1.4	58 3242
	.417	— 42.94	+0 0.7	57 4296		.430	+ 1.35	+7 14.0	58 3253
58 3108	.430	— 7.40	—4 16.8	58 3116	58 3262	.430	+ 1.05	+7 39.7	58 3261
	.430	— 23.84	+4 24.1	59 3045		.430	+ 16.31	+4 59.0	58 3253
58 3110	.419	— 8.37	—1 8.1	58 3120	58 3307	.430	+ 28.48	+2 10.3	59 3193
	.425	— 27.08	+1 48.3	58 3132		.430	— 17.40	—1 21.7	58 3314
— 58 3114	.406	+ 15.70	+2 20.6	— 58 3103	— 60 3094	.493	— 2.12	—1 3.1	— 60 3095
	.425	— 25.26	—0 43.3	58 3132		.493	— 10.40	+1 32.4	60 3102
58 3123	.406	+ 23.92	—0 59.8	58 3103		.515	— 42.99	+5 12.8	60 3155
	.409	— 33.84	+2 47.2	58 3147	60 3096	.469	+ 1.33	+4 18.6	60 3095
57 4279	.417	— 25.45	—3 27.3	57 4296		.493	— 6.92	+6 54.0	60 3102
	.417	— 17.64	—7 15.0	57 4293	60 3098	.501	— 3.16	—1 53.9	60 3102
58 3128	.419	+ 13.46	+0 6.9	58 3120		.515	— 35.75	+1 46.7	60 3155
	.425	— 5.26	+3 3.9	58 3132	60 3108	.501	+ 5.55	—1 4.7	60 3102
58 3131	.409	+ 21.72	—1 54.1	58 3112		.515	— 26.97	+2 35.9	60 3155
	.419	+ 15.14	+2 15.1	58 3120	60 3112	.493	+ 17.17	—1 44.4	60 3095
58 3133	.419	+ 18.79	—1 30.6	58 3120		.501	+ 8.94	+0 51.3	60 3102
	.425	+ 0.17	+1 26.4	58 3132		.515	— 23.72	+4 31.7	60 3155
58 3140	.436	+ 11.83	+2 50.8	59 3045	60 3116	.493	+ 17.56	—1 11.1	60 3095
	.430	— 42.66	+0 10.2	58 3163		.493	+ 9.30	+1 25.0	60 3102



* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.	* Obs. C. P. D.	1917 +	1925.0		* Ref. C. P. D.
		Δ A. R.	Δ Decl.				Δ A. R.	Δ Decl.	
- 60°3122	.501	+ 12.41	- 2' 24.2	- 60°3102	- 60°3168	.469	+ 54.02	+ 2' 1.75	- 60°3095
	.515	- 20.18	+ 1 16.1	60 3155		.518	- 49.83	- 2 32.0	60 3195
60 3126	.501	+ 14.53	- 1 25.7	60 3102	60 3175	.501	+ 54.31	- 3 46.2	60 3102
	.515	- 18.05	+ 2 14.3	60 3155		.518	+ 21.80	- 0 6.3	60 3155
60 3128	.493	+ 24.44	- 2 12.0	60 3095	60 3191	.518	- 10.81	+ 3 0.9	60 3195
	.501	+ 16.22	+ 0 24.0	60 3102		.518	+ 18.24	- 9 3.9	60 3182
	.515	- 16.44	+ 4 3.9	60 3155	60 6319	.469	- 13.43	- 1 2.1	60 6326
60 3129	.469	+ 24.93	+ 0 54.0	60 3095		.469	+ 6.82	+ 1 11.7	60 6317
	.493	+ 16.66	+ 3 29.1	60 3102	60 6325	.469	+ 18.74	- 2 40.4	59 6555
60 3133	.501	+ 18.38	- 1 21.6	60 3102		.469	- 1.38	+ 1 34.7	60 6326
	.515	- 14.26	+ 2 18.2	60 3155	60 6332	.469	+ 27.60	- 3 39.2	60 6317
						.469	- 22.37	- 0 18.4	60 6348
- 60 3136	.469	+ 29.54	+ 5 37.1	- 60 3095	- 59 6562	.469	+ 28.88	+ 0 29.7	- 59 6555
	.518	- 74.36	+ 1 3.4	60 3195		.469	+ 8.73	+ 4 44.3	60 6326
60 3145	.501	+ 25.31	- 2 48.8	60 3102	60 6334	.469	+ 29.76	- 2 30.6	59 6555
	.515	- 7.21	+ 0 51.3	60 3155		.469	+ 9.62	+ 1 43.9	60 6326
60 3147	.493	+ 25.56	+ 0 59.4	60 3102	60 6338	.469	+ 34.59	- 2 38.2	60 6317
	.518	- 6.91	+ 4 39.4	60 3155		.469	- 15.42	+ 0 42.8	60 6348
60 3148	.501	+ 26.23	+ 0 35.6	60 3102		.469	+ 14.29	- 4 52.1	60 6326
	.518	- 6.27	+ 4 15.5	60 3155	60 6339	.469	+ 15.44	- 1 58.7	60 6326
60 3157	.493	+ 35.61	+ 1 48.4	60 3102		.469	- 14.28	+ 3 37.4	60 6348
	.518	+ 3.15	+ 5 29.6	60 3155	59 6563	.469	+ 38.45	- 0 5.8	59 6555
60 3161	.501	+ 38.85	- 0 20.6	60 3102		.469	+ 18.33	+ 4 8.8	60 6326
	.515	+ 6.28	+ 3 19.0	60 3155	60 6349	.469	+ 49.90	- 4 14.1	60 6317
	.518	+ 6.42	+ 3 19.3	60 3155		.469	- 0.05	- 0 53.2	60 6348

B. — CONEXIONES DE 1918 A 1921

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.		Δ Decl.
- 58° 402	9.0	4 <sup>h</sup> 33 <sup>m</sup> 26 <sup>s</sup>	- 58°44'9	20.357	9.2	358°35	+ 4 <sup>h</sup> 55 <sup>m</sup>	4.521	+ 4 <sup>h</sup> 51 <sup>m</sup>	- 0.19	+ 0' 52.2	- 58° 403
				20.365	9.2	358°23	4 56	4.509	4 59	- 0.20	+ 0 52.4	58 403
54 1325	9.0	7 34 32	54 59.2	18.522	9.0	23.202	6 6	35.700	6 1	- 31.41	+ 6 53.8	54 1327
60 979	7.6	56 53	60 34.6	20.354	8.0	29.734	3 13	3.719	2 55	+ 46.71	- 0 43.3	60 953
				20.354	8.2	9.322	3 6	23.882	2 58	- 14.64	+ 4 36.7	60 988
				20.354	8.1	27.089	3 9	13.387	3 2	- 42.58	+ 2 35.3	60 1006
60 980	7.6	56 55	60 36.7	20.354	7.0	30.838	3 16	14.995	3 38	+ 48.46	- 2 53.9	60 953
				20.354	6.8	8.125	3 23	12.617	3 31	- 12.78	+ 2 26.2	60 988
60 982	7.4	56 58	60 35.8	20.354	7.6	32.833	3 20	10.140	3 42	+ 51.61	- 1 57.7	60 953
				20.354	7.4	6.111	3 26	17.449	3 34	- 9.60	+ 3 22.1	60 988
- 60 985	8.0	7 56 59	- 60 40.2	20.420	7.9	17.255	+ 2 56	16.484	+ 2 41	+ 27.24	+ 3 10.8	- 60 967
				20.420	8.2	5.756	2 59	5.147	2 45	- 9.08	- 0 59.6	60 988
				20.420	7.9	23.470	2 53	15.705	2 49	- 36.98	- 3 1.7	60 1006
60 1005	7.8	57 34	60 26.3	20.420	9.0	29.956	3 5	8.736	3 21	+ 46.85	- 1 41.4	60 976
				20.420	8.9	3.793	3 14	17.842	3 18	+ 5.96	+ 3 26.6	60 1003
				20.420	8.6	15.512	3 9	17.913	3 24	- 24.28	- 3 27.3	60 1012
54 2209	8.7	9 19 8	55 4.9	18.522	8.4	32.321	4 51	13.098	4 34	+ 43.58	- 2 32.0	54 2198
				18.522	8.2	18.686	4 46	35.452	4 37	- 25.22	+ 6 50.8	54 2213
54 2245	8.4	21 35	54 31.0	18.522	8.3	14.746	4 57	17.154	4 54	+ 19.65	+ 3 18.5	54 2239
				18.531	8.2	14.749	4 49	17.146	4 44	+ 19.66	+ 3 18.4	54 2239

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.		Δ Decl.
-59°1741	9.0	10 <sup>h</sup> 0 <sup>m</sup> 23 <sup>s</sup>	-59°28'5	19.445	8.9	11.014	+2 <sup>h</sup> 18 <sup>m</sup>	14.676	+2 <sup>h</sup> 1 <sup>m</sup>	+ 16 <sup>m</sup> 74	+ 2'49 <sup>m</sup> 9	-59°1724
				19.445	9.0	—	—	37.295	2 7	0±	+ 7 11.9	59 1740
59 1751	9.0	0 35	59 51.9	19.445	9.2	12.534	+2 14	0.702	2 11	- 19.05	+ 0 8.2	59 1756
				19.445	9.3	180°00	2 23	15.380	3 0	- 0.01	- 2 58.1	59 1752
59 1791	8.5	1 14	59 50.2	19.445	9.1	20.756	2 28	5.397	2 57	- 31.91	- 1 2.4	59 1784
				19.445	8.0	25 197	2 30	6.380	2 53	+ 38.69	- 1 14.0	59 1752
59 1809	9.0	1 31	59 47.2	19.445	7.8	4.484	2 43	3.583	2 46	+ 6.89	+ 0 41.5	59 1784
				19.445	9.1	36.328	2 34	9.009	2 49	+ 55.74	+ 1 44.1	59 1752
61 1536	8.9	12 2	62 4.9	19.445	9.0	15.560	2 39	19.007	3 1	+ 23.91	+ 3 40.0	59 1784
				19.459	8.9	38.882	2 52	16.448	2 35	+ 64.18	+ 3 10.3	61 1519
				19.459	9.0	15.990	2 56	41.700	2 39	- 26.38	+ 8 3.1	61 1541
58 2225	8.8	24 58	58 54.1	19.459	9.1	39.139	2 48	25.220	2 44	- 64.59	+ 4 52.3	61 1553
				18.342	8.9	19.899	1 21	18.186	0 50	- 29.73	- 3 30.5	58 2232
				18.342	9.0	9.244	1 15	21.433	1 1	- 13.81	+ 4 8.3	58 2229
-58°2233	8.8	10 25 29	-58 54.8	18.342	8.7	1.390	+1 33	22.184	+0 55	+ 2.05	- 4 16.9	-58 2232
				18.342	8.9	11.987	1 28	17.432	1 7	+ 17.95	+ 3 21.8	58 2229
60 1945	8.6	27 50	60 57.6	19.445	7.3	3.410	2 48	6.266	2 44	+ 5.42	- 1 12.6	60 1944
				19.459	6.2	3.402	2 45	6.272	2 33	+ 5.41	- 1 12.7	60 1944
57 3403	9.2	29 42	57 48.8	18.328	8.4	20.215	2 18	9.098	1 45	+ 29.32	+ 1 45.3	57 3387
				18.328	8.4	27.730	2 8	9.046	2 1	- 40.18	- 1 44.6	57 3423
57 3406	9.0	29 44	58 14.1	18.328	9.1	9.970	2 23	23.370	1 51	+ 11.65	- 4 30.7	57 3397
				18.328	9.1	10.188	2 13	14.121	1 56	- 14.93	+ 2 43.4	58 2285
60 1976	9.2	30 43	60 45.0	18.361	8.4	9.274	0 38	32.326	0 33	- 14.64	+ 6 14.5	60 1978
				18.364	8.6	9.233	0 44	32.329	0 48	- 14.58	+ 6 14.5	60 1978
60 1977	9.0	30 45	61 0.4	18.361	9.0	18.377	0 45	42.724	0 21	+ 29.37	+ 8 14.7	60 1967
				18.361	9.0	8.382	0 41	47.570	0 26	- 13.36	- 9 10.9	60 1978
				18.364	9.1	37.148	0 39	24.144	0 51	+ 59.23	- 5 14.6	60 1962
57 3464	9.0	31 57	57 45.7	19.423	—	5.046	1 15	11.285	1 8	- 7.30	+ 2 10.7	57 3468
				20.439	9.2	1.386	2 24	1.809	2 5	+ 2.01	+ 0 20.9	57 3463
-57 3468	8.8	10 32 5	-57 47.9	19.423	8.8	6.460	+1 11	9.477	+1 4	+ 9.35	- 1 49.8	-57 3463
				20.439	8.9	6.433	2 21	9.473	2 8	+ 9.31	- 1 49.7	57 3463
				20.439	8.8	31.477	2 17	1.769	2 12	- 45.60	+ 0 20.6	57 3499
58 2348	9.0	32 56	58 12.7	19.505	9.0	16.576	2 20	89°10	2 8	+ 24.88	+ 0 3.0	58 2337
				19.505	8.9	16.554	2 23	11.988	2 13	+ 24.87	+ 2 18.8	58 2338
57 3535	8.8	33 19	57 28.4	19.505	9.1	23.808	2 26	11.474	2 16	- 35.72	- 2 12.8	58 2371
				19.423	8.3	1.462	1 20	30.473	1 36	+ 2.08	- 5 52.9	57 3534
				19.423	8.0	8.216	1 25	24.599	1 33	- 11.79	+ 4 44.9	57 3545
58 2370	8.7	33 33	58 38.7	19.423	8.0	28.745	1 29	6.269	1 40	- 41.26	- 1 12.5	57 3566
				19.500	8.5	22.225	3 10	4.513	3 2	+ 32.96	- 0 52.3	58 2349
57 3553	9.0	33 45	57 36.8	19.500	8.4	1.035	2 14	25.658	3 5	- 1.55	- 4 57.2	58 2372
				19.440	9.0	10.106	1 36	18.938	1 28	+ 14.54	- 3 39.4	57 3545
				19.445	8.9	10.122	2 51	18.948	2 54	+ 14.56	- 3 39.5	57 3545
-58 2388	8.4	10 33 51	-58 55.2	19.505	8.4	1.718	+2 31	14.448	+2 57	+ 2.58	+ 2 47.3	-58 2386
				20.442	8.3	1.742	0 58	14.490	1 10	+ 2.61	+ 2 47.8	58 2386
				20.442	—	5.812	1 1	36.736	1 18	+ 8.65	- 7 5.4	58 2380
58 2389	9.0	33 54	58 47.2	20.442	8.3	22.648	1 5	21.583	1 14	- 33.84	- 4 9.9	58 2404
				19.505	9.1	7.329	2 34	4.565	3 0	+ 10.92	+ 0 52.8	58 2380
				19.505	9.1	2.630	2 38	2.363	3 2	+ 3.92	+ 0 27.4	58 2387
57 3567	8.8	34 3	58 14.3	19.505	—	25.224	2 41	1.204	3 11	- 37.57	+ 0 13.8	58 2406
				19.462	8.7	18.828	3 14	1.786	2 54	- 27.61	- 0 20.6	57 3584
58 2404	8.7	34 25	58 51.0	19.462	—	22.253	3 11	32.537	3 0	- 32.66	+ 6 16.9	58 2411
				19.505	—	28.454	2 44	15.186	3 5	+ 42.42	- 2 56.0	58 2380
				19.505	8.9	23.788	2 47	22.236	3 8	+ 35.45	- 4 17.6	58 2387
				19.505	8.7	4.070	2 50	18.550	2 54	+ 6.08	- 3 34.8	58 2406
57 3580	8.6	34 27	58 14.3	19.462	8.9	2.471	3 17	1.621	2 56	- 3.62	- 0 18.8	57 3584
				19.462	—	5.894	3 20	32.641	3 5	- 8.63	+ 6 18.1	58 2411
				19.464	8.9	21.821	2 16	16.466	2 11	- 31.99	- 3 10.6	57 3599

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	l	Δ Decl.	l	Δ A. R.		Δ Decl.
-57°35'79	8.8	10 <sup>b</sup> 34 <sup>m</sup> 27 <sup>s</sup>	-58° 2'2	18.339	9.0	22.105	+2 <sup>h</sup> 36 <sup>m</sup>	39.902	+2 <sup>h</sup> 23'	+ 32 <sup>s</sup> 14	- 7'42 <sup>s</sup> 3	-57°35'63
				18.339	8.9	21.873	+2 42	46.173	+2 28	- 31.93	+ 8 55.0	57 3599
58 2417	9.0	34 45	58 54.8	20.217	9.2	35.793	-0 26	1.906	-0 41	+ 53.48	+ 0 21.9	58 2388
				20.217	9.2	13.240	0 22	19.606	0 37	+ 19.75	- 3 47.1	58 2404
				20.217	9.3	9.187	0 19	38.204	0 34	+ 13.68	- 7 22.6	58 2406
58 2418	9.0	34 49	58 44.5	20.217	9.1	14.911	0 13	31.015	-0 31	- 22.29	+ 5 59.3	58 2431
				20.217	9.0	12.137	0 10	14.926	+0 8	+ 18.06	+ 2 52.8	58 2406
				20.217	8.9	7.553	-0 2	5.707	0 5	+ 11.22	- 1 6.1	58 2413
				20.218	9.1	15.807	+0 41	18.116	0 25	- 23.49	- 3 29.8	58 2434
				20.218	8.8	37.816	0 48	2.436	0 36	- 56.18	- 0 28.1	58 2457
60 2064	8.8	34 50	60 25.5	18.364	8.8	29.688	1 3	27.306	0 58	+ 46.34	- 5 16.4	60 2040
				18.369	8.9	29.797	+1 5	27.379	1 10	+ 46.51	- 5 17.3	60 2040
-58 2421	9.0	10 34 53	-58 42.9	20.217	9.3	14.732	-0 4	23.382	+0 11	+ 21.92	+ 4 30.8	-58 2406
				20.217	9.2	10.132	+0 1	2.738	0 3	+ 15.05	+ 0 31.7	58 2413
				20.218	9.3	13.214	0 44	9.677	0 30	- 19.63	- 1 52.0	58 2434
				20.218	9.0	35.244	0 51	5.971	0 38	- 52.34	+ 1 9.3	58 2457
58 2440	9.0	35 23	58 46.3	20.218	9.5	6.554	0 55	27.062	1 31	+ 9.72	- 5 13.5	58 2434
				20.218	9.3	15.495	1 0	11.413	1 40	- 23.05	+ 2 12.1	58 2457
				20.218	—	20.749	1 6	6.477	1 51	- 30.88	+ 1 15.1	58 2460
				20.218	9.3	34.495	1 12	5.895	1 23	+ 51.34	+ 1 8.1	58 2406
58 2441	9.0	35 23	58 44.6	20.218	9.2	6.784	0 57	18.694	1 25	+ 10.06	- 3 36.5	58 2434
				20.218	9.2	15.247	1 4	2.999	1 55	- 22.67	- 0 34.7	58 2457
				20.218	—	20.532	1 8	14.947	1 35	- 30.53	+ 2 53.2	58 2460
				20.218	9.1	34.723	1 17	14.281	+1 20	+ 51.67	+ 2 45.3	58 2406
58 2471	8.1	36 6	58 52.7	19.314	—	7.889	0 3	1.970	-0 1	+ 11.78	- 0 22.9	58 2462
				19.314	—	8.309	0 10	26.709	+0 8	+ 12.37	- 5 9.4	58 2460
-57 3628	8.8	10 36 7	-58 13.6	18.342	8.9	8.122	+1 34	33.605	+1 41	+ 11.95	+ 6 29.2	-58 2461
				18.345	8.9	8.081	1 42	33.695	1 35	+ 11.90	+ 6 30.2	58 2461
58 2475	8.6	36 10	58 25.5	20.218	8.5	1.768	2 1	0.480	1 58	+ 2.61	+ 0 5.6	58 2474
				20.218	8.3	1.919	2 5	14.809	2 10	- 2.83	- 2 51.5	58 2478
				20.218	8.4	10.632	2 7	27.946	2 14	+ 15.59	- 5 23.7	58 2461
60 2117	8.8	36 34	60 36.7	18.364	8.8	2.803	1 10	25.480	2 2	- 4.39	+ 4 55.1	60 2120
				18.364	8.8	4.880	1 25	5.399	1 42	- 7.68	- 1 2.5	60 2122
60 2118	8.9	36 35	60 35.9	18.364	8.9	2.594	1 16	29.905	1 55	- 4.06	+ 5 46.4	60 2120
				18.364	8.9	4.704	1 29	1.013	1 47	- 7.40	- 0 11.7	60 2122
60 2126	8.8	36 57	60 31.2	18.364	9.0	10.233	1 32	23.286	2 5	+ 16.09	+ 4 29.6	60 2122
				18.369	8.7	10.210	1 17	23.289	1 12	+ 16.06	+ 4 29.7	60 2122
60 2129	8.6	37 3	60 36.3	18.364	8.6	15.782	1 20	27.709	1 58	+ 24.94	+ 5 20.8	60 2130
				18.364	8.6	13.705	1 36	3.183	1 51	+ 21.55	- 0 36.9	60 2122
59 2408	8.8	37 24	60 6.3	18.347	8.8	179°50	1 14	7.023	1 8	+ 0.09	- 1 21.3	59 2409
				18.364	8.7	179°41	+2 16	7.049	+2 10	+ 0.10	- 1 21.6	59 2409
-59 2411	8.5	10 37 31	-59 34.1	19.322	8.5	32.591	-0 51	3.956	-1 1	- 49.68	+ 0 46.0	-59 2447
				19.322	—	—	—	41.330	0 53	- 17±	+ 7 58.6	59 2420
				19.325	8.5	32.630	-1 16	3.890	-1 19	- 49.74	+ 0 45.2	59 2447
58 2545	9.0	38 37	58 40.8	19.314	8.8	11.701	+0 20	24.572	+0 39	+ 17.41	+ 4 44.5	58 2540
				19.314	8.9	15.889	0 34	11.230	0 36	- 23.60	+ 2 11.1	58 2552
58 2548	9.2	38 55	58 44.3	18.369	8.7	3.701	1 56	6.480	3 4	- 5.52	- 1 15.0	58 2552
				18.369	8.6	16.509	2 0	9.845	3 10	- 24.56	+ 1 54.1	58 2565
58 2553	9.0	39 2	58 52.7	19.314	—	31.096	0 25	7.087	0 9	+ 46.41	- 1 22.3	58 2538
				19.314	8.9	29.579	0 21	17.519	0 12	- 44.15	- 3 22.8	58 2581
				19.314	9.1	8.338	0 19	18.412	0 16	- 12.45	+ 3 33.2	58 2561
60 2176	8.6	39 8	60 40.4	18.372	8.9	18.138	1 28	11.102	0 17	+ 28.56	- 2 8.7	60 2162
				18.372	8.8	41.792	1 32	24.655	0 22	- 65.80	- 4 45.4	60 2199
58 2560	9.2	39 13	58 9.9	18.369	8.5	17.470	2 34	10.592	2 50	- 26.32	+ 2 2.8	58 2575
				18.369	8.5	3.863	2 38	17.424	2 47	- 5.83	- 3 21.8	58 2564
				18.552	8.7	3.850	3 56	17.390	3 36	- 5.81	- 3 21.4	58 2564

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	l	Δ Decl.	l	Δ A. R.		Δ Decl.
-59°2479	8.9	10 <sup>h</sup> 39 <sup>m</sup> 18 <sup>s</sup>	-59°34'14"	19.322	8.9	1.876	-0 <sup>h</sup> 27 <sup>m</sup>	18.748	-0 <sup>h</sup> 4 <sup>m</sup>	+ 2 <sup>s</sup> 84	- 3'37 <sup>2</sup>	-59°2478
				19.322	8.5	28.788	0 43	1.409	0 10	- 43.78	+ 0 16.5	59 2509
				19.322	—	26.300	-0 40	25.311	-0 6	- 40.12	+ 4 53.3	59 2507
58 2567	8.8	39 22	58 44.7	18.369	8.8	14.425	+2 4	8.334	+3 7	+ 21.45	- 1 36.6	58 2552
				18.369	8.7	1.620	2 8	8.026	3 12	+ 2.42	+ 1 32.9	58 2565
				18.369	8.7	6.136	2 12	6.042	3 15	- 9.13	+ 1 10.0	58 2573
58 2570	8.8	39 25	58 46.7	18.369	8.8	4.060	2 17	2.444	3 20	+ 6.04	- 0 28.3	58 2565
				18.369	8.8	3.696	2 21	4.398	3 17	- 5.51	- 0 50.9	58 2573
				18.369	—	14.076	2 25	13.888	3 0	- 20.96	+ 2 40.9	58 2581
60 2183	8.8	39 29	60 31.3	18.372	9.0	28.123	1 38	22.341	0 29	- 44.14	+ 4 18.9	60 2199
				18.377	8.9	28.026	0 6	22.339	0 10	- 44.00	+ 4 18.8	60 2199
59 2493	9.0	39 41	60 6.7	18.347	9.1	21.733	1 25	20.651	2 0	- 33.68	+ 3 59.3	59 2516
				18.347	9.0	38.543	+1 31	19.267	+2 4	- 59.75	+ 3 43.4	59 2532
-59 2496	9.0	10 39 44	-59 39.0	19.322	9.4	9.214	-0 18	1.712	-0 14	- 14.08	+ 0 19.9	-59 2507
				19.322	9.2	21.795	0 33	31.588	+0 3	+ 33.36	+ 6 5.7	59 2476
				19.322	9.1	11.704	-0 21	22.133	-0 1	- 17.88	- 4 16.3	59 2509
58 2579	9.0	39 45	59 4.7	18.369	8.9	18.038	+2 29	9.673	+2 53	+ 27.12	+ 1 51.9	58 2564
				18.369	8.9	4.279	2 42	37.673	2 57	+ 6.47	+ 7 16.3	58 2575
				18.552	8.9	18.024	4 6	9.670	3 52	+ 27.10	+ 1 52.1	58 2564
				18.552	9.0	20.450	+4 6	43.594	+3 45	+ 30.71	- 8 24.8	58 2561
59 2499	8.7	39 49	59 49.6	19.325	8.8	25.166	-0 19	23.623	-0 31	+ 38.59	- 4 33.7	59 2476
				19.333	8.9	30.980	+0 44	29.360	+1 10	- 47.63	+ 5 40.2	59 2528
				19.333	8.8	23.601	1 24	26.953	1 15	- 36.23	- 5 12.1	59 2522
60 2192	8.9	39 50	60 49.2	18.372	9.0	18.567	1 47	13.679	2 13	- 29.39	- 2 38.3	60 2203
				18.372	9.0	20.694	+1 52	20.607	+2 23	- 32.75	- 3 58.6	60 2204
59 2502	8.5	39 52	59 30.7	19.322	8.3	23.497	-0 37	0.822	-0 7	+ 35.74	+ 0 9.4	59 2478
				19.322	8.5	7.205	0 25	21.010	0 3	- 10.96	+ 4 3.3	59 2509
-59 2503	8.7	10 39 52	-59 28.7	19.325	8.4	6.363	-0 15	31.107	-0 43	- 9.67	+ 6 0.3	-59 2509
				19.325	8.7	24.341	1 15	10.959	0 38	+ 37.03	+ 2 6.8	59 2478
59 2505	8.6	39 54	59 48.4	19.325	8.8	27.981	-0 22	17.342	-0 26	+ 42.90	- 3 21.0	59 2476
				19.333	8.7	28.142	+0 49	35.594	+1 7	- 43.24	+ 6 52.4	59 2528
				19.333	8.9	20.754	1 28	20.717	1 18	- 31.84	- 3 59.8	59 2522
60 2195	8.6	39 57	60 44.1	18.372	8.7	14.600	1 5	12.443	0 50	- 23.06	+ 2 24.2	60 2203
				18.372	8.7	16.722	1 1	5.516	0 54	- 26.41	+ 1 4.0	60 2204
58 2588	8.9	39 58	59 43.5	19.314	9.1	8.058	1 15	30.397	0 43	+ 12.02	+ 5 52.0	58 2581
				19.314	9.2	18.498	1 7	12.126	0 52	+ 27.53	+ 2 20.3	58 2573
59 2508	9.3	39 59	60 3.3	18.347	8.8	36.243	1 34	12.024	1 55	- 56.03	- 2 19.0	59 2544
				18.347	8.8	21.981	1 44	36.198	1 50	- 33.97	- 6 59.2	59 2526
58 2592	8.8	40 9	58 41.4	19.314	8.9	25.864	1 3	23.055	0 55	+ 38.47	+ 4 26.9	58 2573
				19.314	9.0	15.344	1 12	41.290	0 58	+ 22.87	+ 7 58.2	58 2581
-60 2200	8.5	10 40 15	-60 50.0	18.372	8.5	2.913	+1 56	18.182	+2 16	- 4.63	- 3 30.6	-60 2203
				18.372	8.5	5.019	1 59	25.089	2 30	- 7.96	- 4 50.6	60 2204
58 2594	9.0	40 22	58 46.8	19.314	9.0	34.085	1 20	5.112	1 45	+ 50.75	- 0 59.4	58 2573
				19.314	8.9	23.662	1 24	13.124	1 42	+ 35.27	+ 2 31.9	58 2581
				19.314	9.0	21.398	+2 8	22.748	+1 51	- 31.90	- 4 23.4	58 2612
59 2519	9.0	40 23	59 27.5	19.325	9.2	44.180	-1 11	—	—	+ 67.18	+ 3.4+	59 2478
				19.325	9.3	29.123	1 5	6.907	-0 53	- 41.25	+ 1 20.2	59 2556
				19.325	9.2	3.163	-0 57	34.982	0 50	+ 4.78	- 6 45.2	59 2518
				19.325	9.1	—	—	37.625	-0 47	+ 23+	+ 7 15.5	59 2509
59 2521	8.3	40 23	59 48.5	19.333	8.4	8.926	+0 53	35.490	+1 4	- 13.70	+ 6 51.1	59 2528
				19.333	8.4	1.575	2 6	20.827	1 20	- 2.43	- 4 1.2	59 2522
				19.333	8.5	23.712	2 12	26.106	2 26	- 36.38	- 5 2.2	59 2548
60 2206	8.8	40 26	60 41.1	18.372	8.9	8.088	1 10	28.575	0 35	+ 12.71	- 5 31.0	60 2199
				18.372	9.0	4.232	1 16	27.860	0 40	+ 6.71	+ 5 22.7	60 2203
				18.372	8.9	2.120	1 20	20.991	0 45	+ 3.37	+ 4 3.1	60 2204

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.		Δ Decl.
-60°2207	8.9	10 <sup>h</sup> 40 <sup>m</sup> 28 <sup>s</sup>	-60°49'2	18.372	9.0	5.479	+2 <sup>h</sup> 2 <sup>m</sup>	13.827	+2 <sup>h</sup> 19 <sup>m</sup>	+ 8.66	- 2'40"2	-60°2203
				18.372	9.0	3.345	+2 5	20.732	+2 27	+ 5.27	- 4 0.1	60 2204
59 2526	9.0	40 33	59 56.3	19.325	8.1	2.143	-0 12	5.289	-0 2	- 3.29	- 1 1.2	59 2528
				19.333	8.2	2.149	+0 38	5.274	+0 28	- 3.30	- 1 1.1	59 2528
58 2602	8.3	40 34	58 42.4	19.314	—	31.826	1 27	36.233	1 38	+ 47.41	+ 6 59.5	58 2581
				19.314	8.6	42.296	1 31	—	—	+ 62.93	+ 3.3+	58 2573
				19.314	8.7	13.272	2 12	271°41	1 56	- 19.73	+ 0 3.9	58 2612
60 2214	9.0	40 42	61 0.5	18.377	9.1	28.955	0 26	12.344	0 15	+ 46.08	- 2 23.1	60 2193
				18.377	9.1	34.506	+0 23	12.132	+0 19	- 54.93	- 2 20.3	60 2240
59 2538	8.6	40 51	59 56.8	19.325	8.5	9.368	-0 9	7.922	-0 6	+ 14.43	- 1 31.8	59 2528
				19.333	8.5	9.401	+0 38	7.963	+0 33	+ 14.49	- 1 32.3	59 2528
59 2540	8.8	40 54	59 42.2	19.333	9.3	18.701	2 27	11.694	2 28	+ 28.64	+ 2 15.3	59 2522
				19.333	9.3	12.660	2 42	0.550	2 31	+ 19.36	+ 0 6.3	59 2527
				19.382	9.4	3.446	1 42	6.448	1 57	- 5.27	+ 1 14.7	59 2548
-59 2545	8.9	10 40 57	-59 40.0	19.333	8.9	14.455	+2 46	11.900	+2 33	+ 22.12	+ 2 17.8	-59 2527
				19.382	9.0	1.709	1 37	17.824	1 34	- 2.60	+ 3 26.5	59 2548
				19.382	9.1	21.323	2 40	21.011	2 9	- 32.58	- 4 3.3	59 2572
58 2617	8.4	41 0	59 9.3	19.316	8.8	1.999	0 31	0.537	0 44	- 3.01	- 0 6.2	58 2618
				19.316	8.8	8.516	0 36	8.006	0 40	- 12.82	+ 1 32.8	58 2631
59 2551	9.0	41 4	59 41.8	19.382	9.2	3.302	1 44	8.344	1 30	+ 5.06	+ 1 36.6	59 2548
				19.382	9.2	16.299	+2 44	30.540	+2 17	- 24.92	- 5 53.6	59 2572
				19.388	9.3	3.297	-0 20	8.300	-0 29	+ 5.05	+ 1 36.1	59 2548
59 2555	8.6	41 7	59 41.5	19.382	8.6	5.060	+1 47	9.907	+1 32	+ 7.75	+ 1 54.7	59 2548
				19.382	8.6	14.559	+2 53	28.962	+2 21	- 22.26	- 5 35.4	59 2572
				19.388	8.7	5.021	-0 17	9.899	-0 26	+ 7.69	+ 1 54.6	59 2548
59 2554	8.7	41 7	59 42.4	19.382	8.9	5.206	+1 49	5.602	+1 25	+ 7.97	+ 1 4.9	59 2548
				19.382	9.0	14.327	+2 47	33.257	+2 14	- 21.92	- 6 25.1	59 2572
				19.388	8.9	5.218	-0 14	5.550	-0 23	+ 7.99	+ 1 4.3	59 2548
-58 2628	9.0	10 41 11	-58 42.5	19.314	9.1	11.955	+2 15	91°20	+1 59	+ 17.78	- 0 3.0	-58 2612
				19.317	9.2	11.949	1 45	0.258	1 29	+ 17.76	- 0 3.1	58 2612
59 2560	8.4	41 12	59 36.1	19.336	8.8	—	—	38.253	1 27	+ 13+	+ 7 23.0	59 2548
				19.382	8.6	11.042	+2 38	0.521	+2 34	- 16.84	- 0 6.0	59 2572
				19.388	—	11.050	-0 11	0.566	-0 33	- 16.86	- 0 6.5	59 2572
59 2561	8.6	41 16	59 19.5	19.317	8.4	20.651	+2 5	19.343	+1 41	- 31.27	+ 3 44.2	59 2600
				19.317	8.4	34.798	2 21	11.133	2 46	- 52.64	- 2 8.8	59 2620
59 2563	8.6	41 18	59 39.7	19.336	8.8	12.097	1 50	19.297	1 33	+ 18.52	+ 3 43.4	59 2548
				19.382	8.8	7.555	2 55	19.532	2 26	- 11.55	- 3 46.2	59 2572
57 3748	9.4	41 24	58 0.4	19.440	8.5	5.983	1 41	4.909	1 44	+ 8.71	- 0 56.9	57 3741
				19.459	8.6	5.982	2 50	4.925	2 46	+ 8.71	- 0 57.1	57 3741
59 2575	8.6	41 32	59 49.1	19.333	8.7	36.224	0 56	32.149	1 0	+ 55.73	+ 6 12.2	59 2528
				19.333	—	21.498	2 15	29.400	2 19	+ 32.94	- 5 40.6	59 2548
-59 2577	8.4	10 41 34	-59 29.4	19.388	8.6	—	—	33.745	+0 11	+ 4+	+ 6 30.8	-59 2572
				19.404	8.5	17.722	+2 9	3.171	2 54	+ 26.93	- 0 36.8	59 2556
				19.404	8.4	2.873	2 58	33.722	2 55	+ 4.40	+ 6 30.4	59 2572
				19.407	8.3	9.029	+0 42	31.984	0 30	- 13.73	- 6 10.3	59 2600
59 2580	8.4	41 36	59 33.6	19.388	8.3	4.174	-0 8	11.942	0 7	+ 6.37	+ 2 18.3	59 2572
				19.404	8.6	19.114	+2 14	24.936	2 37	+ 29.07	- 4 48.9	59 2556
58 2649	9.0	41 36	59 13.8	19.317	9.5	15.263	0 58	15.091	0 48	+ 22.97	- 2 54.9	58 2631
				19.317	9.7	9.506	1 1	18.398	1 7	- 14.37	- 3 33.0	58 2661
				19.317	9.5	21.887	1 19	18.716	1 9	- 33.04	+ 3 36.9	59 2620
59 2584	8.6	41 38	59 20.9	19.317	8.7	6.212	2 8	12.501	1 46	- 9.51	+ 2 24.9	59 2600
				19.317	8.7	20.337	2 27	18.041	2 48	- 30.77	- 3 28.9	59 2620
59 2587	8.6	41 39	59 20.6	19.317	8.2	5.330	2 12	13.885	1 50	- 8.06	+ 2 40.9	59 2600
				19.317	8.0	19.430	2 31	16.652	2 52	- 29.41	- 3 12.8	59 2620
59 2590	8.2	41 43	59 41.8	19.382	8.2	28.385	1 54	8.385	2 4	+ 43.35	+ 1 37.0	59 2548
				19.382	8.0	8.812	2 58	30.407	2 30	+ 13.44	- 5 52.2	59 2572

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
N°	Mag.	A. R.	Decl.		Mag.	Δ A. R.	Δ t	Δ Decl.	Δ t	Δ A. R.		Δ Decl.
-58°2652	8.6	10 <sup>h</sup> 41 <sup>m</sup> 43 <sup>s</sup>	-59° 9'3	19.314	8.9	5.013	+2 <sup>h</sup> 52 <sup>m</sup>	5.103	+2 <sup>h</sup> 48 <sup>m</sup>	- 7.55	+ 0'59"1	-58°2661
60 2243	8.5	41 46	60 50.3	19.317	9.0	19.782	0 53	8.375	0 50	+ 29.80	+ 1 36.9	58 2631
				18.383	8.4	5.838	1 51	40.724	+2 3	+ 9.31	+ 7 51.6	60 2240
				18.385	8.6	6.020	0 0	40.680	-0 18	+ 9.68	+ 7 51.1	60 2240
				18.470	8.5	5.842	2 23	40.571	+2 10	+ 9.31	+ 7 49.9	60 2240
				18.470	8.5	54.475	2 17	19.624	2 4	+ 86.09	- 3 47.5	60 2203
57 3756	8.8	41 51	57 40.8	19.440	9.0	11.162	1 51	22.780	1 47	- 16.14	+ 4 23.9	57 3763
				19.459	8.9	11.144	+2 55	22.793	2 58	- 16.12	+ 4 24.0	57 3763
59 2602	8.7	41 51	59 31.0	19.388	9.0	14.314	-0 4	25.531	0 3	+ 21.82	+ 4 55.6	59 2572
				19.404	9.0	29.261	+2 17	11.364	2 40	+ 44.49	- 2 11.7	59 2556
				19.407	8.8	2.452	0 44	40.168	0 33	+ 3.78	- 7 45.2	59 2600
58 2663	9.8	41 52	59 1.1	19.314	8.3	2.295	2 26	17.526	2 40	+ 3.42	- 3 23.0	58 2659
				19.314	-	37.640	2 30	-	-	- 56.45	- 0.4+	58 2680
				19.314	-	-	-	47.195	2 45	+ 2±	+ 9 6.6	58 2661
-59 2603	8.6	10 41 53	-59 20.2	19.317	8.7	3.512	+2 14	15.827	+1 52	+ 5.33	+ 3 3.3	-59 2600
				19.317	8.8	10.558	2 34	14.703	2 41	- 15.98	- 2 50.2	59 2620
				19.317	8.8	19.097	2 37	1.508	2 55	- 28.90	- 0 17.4	59 2641
59 2604	8.9	41 53	59 34.3	19.404	9.0	15.878	1 5	8.475	0 53	+ 24.22	+ 1 38.1	59 2572
				19.404	9.2	30.824	2 21	28.428	2 43	+ 46.90	- 5 29.4	59 2556
59 2610	9.0	42 0	59 32.3	19.404	9.3	20.489	1 9	18.621	0 57	+ 31.17	+ 3 35.6	59 2572
				19.404	9.5	35.418	+2 25	18.336	+2 47	+ 53.87	- 3 32.5	59 2556
				21.006	9.3	20.606	-1 42	18.636	-2 4	+ 31.43	+ 3 35.8	59 2572
				21.006	-	8.714	1 27	-	-	+ 13.22	- 9.1+	59 2600
				21.006	-	35.641	-1 53	-	-	+ 54.24	- 3.5+	59 2556
59 2611	9.0	42 3	59 32.4	19.404	8.3	22.183	+1 12	18.260	+1 0	+ 33.82	+ 3 31.4	59 2572
				19.404	8.6	37.161	+2 28	18.688	2 50	+ 56.53	- 3 36.6	59 2556
				19.407	-	-	-	47.459	+0 36	+ 16±	- 9 9.7	59 2600
				21.006	8.3	22.338	-1 35	18.271	-2 7	+ 34.07	+ 3 31.5	59 2572
				21.006	-	10.492	1 20	-	-	+ 15.92	- 9.2+	59 2600
				21.006	-	37.310	1 48	-	-	+ 56.76	- 3.6+	59 2556
-59 2623	8.6	10 42 11	-59 16.4	19.319	8.4	1.510	-0 45	5.040	-0 52	+ 2.29	+ 0 58.4	-59 2620
				19.322	8.2	7.063	1 37	18.186	1 51	- 10.67	+ 3 30.7	59 2641
				19.322	8.5	13.906	-1 41	31.985	-1 45	+ 21.03	- 6 10.5	58 2661
59 2636	9.0	42 18	59 20.6	19.317	9.1	20.220	+2 0	13.692	+1 56	+ 30.65	+ 2 38.5	59 2600
				19.319	9.1	2.365	+1 25	3.652	-0 59	- 3.58	- 0 42.3	59 2641
				19.322	9.0	6.208	-2 11	16.859	-2 0	+ 9.38	- 3 15.3	59 2620
58 2674	8.9	42 22	58 59.9	19.314	8.8	22.339	+2 18	11.298	+2 39	+ 33.46	- 2 11.0	58 2659
				19.314	8.8	17.597	2 32	4.286	+2 35	- 26.32	+ 0 49.7	58 2680
59 2644	9.0	42 26	59 19.2	19.319	9.1	2.627	+1 30	3.978	-0 52	+ 3.98	+ 0 46.1	59 2641
				19.322	9.1	11.174	-2 6	9.202	-1 55	+ 16.89	- 1 46.6	59 2620
60 2262	9.0	42 53	60 55.5	18.383	9.0	15.661	+1 54	13.978	+1 58	- 24.87	- 2 41.8	60 2268
				18.385	8.7	15.653	0 3	13.866	-0 14	- 24.85	- 2 40.5	60 2268
				18.478	9.0	15.646	+2 8	13.912	+2 13	- 24.85	- 2 41.0	60 2268
-60 2271	8.8	10 43 21	-60 25.8	18.385	8.6	1.055	-0 5	23.965	-0 9	- 1.64	+ 4 37.6	-60 2272
				18.388	8.5	1.077	+0 43	23.973	+0 48	- 1.67	+ 4 37.7	60 2272
57 3793	8.8	44 0	57 32.7	19.440	8.7	1.089	1 53	5.620	1 57	- 1.56	+ 1 5.1	57 3794
				19.459	8.7	1.088	+3 12	5.625	+3 9	- 1.56	+ 1 5.2	57 3794
59 2692	8.8	44 13	59 23.7	19.322	8.8	23.725	-1 29	12.316	-1 15	+ 36.00	+ 2 22.6	59 2679
				19.322	8.7	23.114	-1 25	25.810	-1 21	- 35.08	+ 4 59.1	59 2713
59 2696	8.8	44 17	59 42.1	19.407	8.0	12.183	+0 46	5.888	+0 53	+ 18.63	- 1 8.2	59 2687
				19.407	8.0	5.264	0 50	36.780	0 56	- 8.04	+ 7 6.0	59 2703
61 1894	9.0	45 41	61 19.8	18.383	9.0	1.710	2 18	5.687	2 5	+ 2.75	- 1 5.9	61 1893
				18.386	9.0	1.697	0 52	5.694	0 56	+ 2.73	- 1 5.9	61 1893
57 3837	8.8	46 8	57 16.7	19.464	8.9	21.198	2 10	0.853	2 13	+ 30.27	- 0 10.0	57 3825
				19.467	8.7	21.151	1 29	0.846	1 24	+ 30.20	- 0 9.9	57 3825
				18.383	8.6	29.350	2 13	8.434	2 9	- 47.36	- 1 37.5	61 1905
61 1898	8.7	46 26	61 26.1	18.386	8.7	29.335	1 14	8.415	1 10	- 47.34	- 1 37.3	61 1905

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.		Δ Decl.
-57°3867	9.0	10 <sup>h</sup> 47 <sup>m</sup> 34 <sup>s</sup>	-57°27'11"	19.467	8.9	23.872	+1 <sup>m</sup> 33 <sup>s</sup>	7.631	+1 <sup>m</sup> 59 <sup>s</sup>	+ 34 <sup>s</sup> 24	+ 1'28 <sup>s</sup> 5	-57°3856
				19.467	9.0	28.585	1 42	26.479	1 55	- 40.98	- 5 6.6	57 3880
				19.467	8.8	31.660	1 45	39.510	1 49	- 45.33	+ 7 37.7	57 3883
60 2320	8.7	47 51	60 24.0	18.383	8.6	29.340	2 21	0.486	2 25	- 45.85	+ 0 5.8	60 2334
				18.386	-	29.328	1 20	0.465	1 25	- 45.83	+ 0 5.5	60 2334
57 3893	8.8	48 52	57 36.4	19.467	8.8	22.745	2 18	8.532	2 0	+ 32.76	- 1 38.9	57 3883
				19.467	8.9	24.513	2 15	29.125	2 4	+ 35.29	+ 5 37.3	57 3881
				19.467	-	38.933	2 11	3.744	2 8	- 56.11	+ 0 43.5	57 3914
57 3905	8.5	49 16	57 48.0	19.467	8.7	27.206	2 22	15.872	2 36	+ 39.45	+ 3 3.7	57 3887
				19.467	8.9	41.308	2 26	31.041	2 39	+ 59.74	- 5 59.6	57 3881
				19.467	9.0	3.840	2 30	16.580	+2 33	- 5.58	+ 3 12.0	57 3909
58 2826	8.7	50 4	59 6.4	18.396	8.6	17.876	0 8	27.514	-0 13	+ 26.82	- 5 18.8	58 2817
				18.396	8.5	32.672	0 4	23.911	0 8	- 49.16	+ 4 37.1	58 2848
				18.396	8.3	27.790	0 0	38.185	-0 4	- 41.72	- 7 22.4	58 2846
-57 3929	8.8	10 50 11	-57 27.0	19.481	8.7	4.342	+2 27	8.370	+2 11	+ 6.21	- 1 36.9	-57 3927
				19.481	8.6	1.681	2 35	2.187	2 24	+ 2.41	+ 0 25.3	57 3928
				19.481	8.7	4.286	2 37	11.757	2 43	- 6.15	+ 2 16.2	57 3933
57 3936	8.8	50 19	57 27.5	19.481	8.9	10.168	2 29	11.032	2 19	+ 14.65	- 2 7.7	57 3927
				19.481	8.7	7.514	2 32	0.456	2 22	+ 10.83	- 0 5.3	57 3928
				19.481	8.8	1.546	+2 40	9.130	+2 16	+ 2.23	+ 1 45.7	57 3933
58 2847	9.0	50 48	58 22.4	18.402	9.3	13.512	-0 12	20.147	-0 26	+ 19.92	+ 3 53.3	58 2836
				18.402	9.2	6.354	0 16	2.464	0 19	+ 9.36	+ 0 28.5	58 2844
				18.402	9.1	29.676	-0 8	8.554	-0 22	- 43.69	+ 1 39.2	58 2856
58 2857	8.8	51 34	58 30.4	18.396	8.7	1.733	+0 12	33.222	+0 23	+ 2.54	- 6 24.8	58 2856
				18.396	8.7	17.572	0 17	22.220	0 20	- 25.95	- 4 17.3	58 2863
59 2856	8.6	53 3	60 5.6	20.218	9.0	29.517	2 23	7.889	2 4	+ 45.70	+ 1 31.3	59 2840
				20.218	8.7	4.877	2 13	12.515	2 7	- 7.55	- 2 24.9	59 2860
				20.218	8.8	19.072	2 20	9.246	2 9	- 29.52	+ 1 47.2	59 2863
-57 3998	8.4	10 53 3	-57 40.4	19.481	8.7	5.030	+2 40	6.849	+2 44	- 7.26	- 1 19.3	-57 4002
				19.483	8.8	5.023	2 50	6.846	2 29	- 7.26	- 1 19.3	57 4002
60 2395	9.0	53 21	60 58.0	18.372	9.0	19.986	2 35	17.473	2 28	- 31.80	+ 3 22.5	60 2406
				18.386	9.0	19.965	1 49	17.452	1 44	- 31.77	+ 3 22.2	60 2406
60 2410	8.8	54 4	60 47.2	18.386	8.6	4.435	1 52	24.148	1 34	+ 6.99	- 4 39.7	60 2409
				18.386	8.6	9.454	1 57	25.042	1 38	- 14.95	- 4 50.0	60 2413
57 4019	9.0	54 28	57 33.6	19.481	9.3	11.408	2 51	4.168	2 47	- 16.41	- 0 48.2	57 4026
				19.483	9.1	11.384	2 52	4.211	2 32	- 16.34	- 0 48.7	57 4026
57 4029	9.0	54 57	57 25.7	19.483	8.8	8.668	2 55	36.810	2 35	+ 12.49	+ 7 6.3	57 4026
				19.483	9.1	27.587	2 58	4.803	2 38	- 39.64	+ 0 55.7	57 4040
57 4052	8.5	56 13	57 43.3	19.481	8.5	22.204	2 53	13.089	2 57	- 32.11	+ 2 31.6	57 4062
				19.483	8.5	22.186	3 0	13.080	2 40	- 32.08	+ 2 31.6	57 4062
57 4070	8.8	57 0	57 56.8	19.483	8.9	8.225	3 2	18.429	2 42	- 11.96	+ 3 31.5	57 4076
				19.500	8.7	8.240	+2 56	18.392	+3 0	- 11.97	+ 3 31.0	57 4076
-58 2931	9.0	10 57 43	-58 46.7	20.220	9.2	69.319	-0 55	-	-	+103.14	- 0.6±	-58 2907
				20.220	9.1	16.067	1 6	9.940	-2 0	- 23.90	- 1 55.1	58 2937
				20.220	-	-	-	61.605	1 53	+ 27±	-11 53.6	58 2926
				20.220	9.0	28.518	1 20	57.738	1 42	+ 42.57	+11 8.7	58 2922
58 2933	8.8	57 44	58 35.6	20.220	9.0	28.508	1 13	34.850	1 32	+ 42.12	- 6 43.8	58 2923
				20.220	8.8	15.839	1 2	47.551	1 30	- 23.48	+ 9 10.8	58 2937
				20.220	8.9	18.328	-1 10	4.147	-1 25	+ 27.12	- 0 48.1	58 2926
61 2032	8.8	58 47	61 28.8	18.386	9.0	0.636	+3 6	34.217	+2 31	+ 1.00	- 6 36.3	61 2031
				18.386	8.8	12.748	3 3	30.770	2 37	+ 20.67	+ 5 56.4	61 2027
				18.386	8.9	8.954	3 9	21.659	2 41	- 14.48	+ 4 10.9	61 2036
61 2033	9.0	58 51	61 39.1	18.386	9.0	6.746	3 12	31.266	2 34	- 10.98	- 6 2.1	61 2036
				18.386	8.9	14.862	3 0	22.185	2 44	+ 24.12	- 4 17.0	61 2027
				18.386	-	10.172	2 54	16.720	2 50	+ 16.57	+ 3 13.6	61 2028
61 2037	8.8	59 2	61 45.5	18.386	8.7	17.185	2 57	16.771	2 47	+ 27.90	- 3 14.3	61 2028
				18.388	8.7	17.156	0 46	16.823	0 50	+ 27.95	- 3 14.9	61 2028

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
N°	Mag.	A. R.	Decl.		Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.		Δ Decl.
-60°2466	9.0	10 <sup>h</sup> 59 <sup>m</sup> 4 <sup>s</sup>	-61° 31.3	18.386	9.0	17.256	+2 <sup>h</sup> 0 <sup>m</sup>	32.301	+2 <sup>h</sup> 5 <sup>m</sup>	+ 27.59	+ 6' 14" 0	-60°2460
				18.388	9.0	17.364	0 43	32.244	0 38	+ 27.75	+ 6 13.4	60 2460
				18.500	9.1	17.207	2 26	32.188	2 38	+ 27.52	+ 6 12.7	60 2460
				18.500	8.9	32.507	+2 26	61.001	+2 11	+ 51.65	-11 46.7	60 2456
59 2961	9.0	59 13	59 24.3	20.220	8.8	15.360	-0 4	29.901	-0 26	+ 23.32	+ 5 46.3	59 2956
				20.220	8.9	11.548	0 12	26.500	0 23	- 17.51	+ 5 7.0	59 2968
				20.220	—	17.098	0 14	20.911	0 21	- 25.90	- 4 2.2	59 2972
				20.220	8.9	19.962	0 7	5.638	0 18	- 30.26	+ 1 5.4	59 2973
57 4133	9.0	59 41	58 6.3	21.006	—	8.747	1 3	29.319	1 23	+ 12.76	- 5 39.6	57 4127
				21.006	—	29.283	1 10	15.806	1 16	- 42.82	+ 3 3.2	57 4156
58 2978	8.7	11 0 3	58 43.6	20.220	8.9	4.458	0 47	5.890	0 29	+ 6.62	- 1 8.2	58 2975
				20.220	8.9	4.419	0 44	30.115	0 32	- 6.57	- 5 48.8	58 2981
				20.220	8.6	14.580	0 39	22.874	0 35	- 21.68	+ 4 25.0	58 2990
-57 4181	8.7	11 1 4	-58 3.6	21.050	8.4	14.034	-0 16	21.418	-0 28	+ 20.46	- 4 8.1	-57 4170
				21.050	8.4	27.455	-0 23	29.938	-0 32	+ 40.14	+ 5 46.7	57 4156
59 2998	9.0	1 17	59 21.3	20.220	8.8	360°03	+0 29	16.351	+0 7	+ 0.02	+ 3 9.5	59 2995
				20.220	8.9	20.880	0 36	30.981	0 9	- 31.63	+ 5 58.9	59 3017
				20.220	8.8	24.463	0 34	14.247	0 17	- 37.00	- 2 44.9	59 3019
59 3026	9.0	2 0	59 25.0	20.220	9.1	3.601	0 48	33.613	0 13	+ 5.43	- 6 29.3	59 3019
				20.220	9.2	7.166	0 44	11.616	0 22	+ 10.88	+ 2 14.5	59 3017
				20.220	9.0	28.066	0 39	2.977	0 24	+ 42.55	- 0 34.6	59 2995
60 2510	8.8	2 19	60 30.3	18.388	9.1	3.970	1 27	25.661	1 23	+ 6.21	- 4 57.2	60 2509
				18.396	9.2	3.962	0 28	25.692	0 24	+ 6.19	- 4 57.6	60 2509
60 2516	9.0	2 42	60 44.2	18.391	9.0	11.546	1 44	27.110	1 30	- 18.23	- 5 13.9	60 2522
				18.391	9.0	24.080	2 56	10.982	2 4	+ 38.06	+ 2 7.1	60 2508
				18.391	9.1	11.700	2 41	31.611	2 30	- 18.48	+ 6 6.2	60 2520
-60 2517	8.5	11 2 54	-60 46.3	18.388	8.7	31.285	+1 52	89°65	+2 22	+ 49.46	+ 0 2.1	-60 2508
				18.391	8.8	31.274	2 58	89°66	2 17	+ 49.44	+ 0 2.0	60 2508
				18.391	8.7	4.492	2 46	20.863	2 36	- 7.09	+ 4 1.7	60 2520
60 2521	8.4	3 1	60 44.8	18.391	9.0	179°81	2 52	30.559	1 36	+ 0.14	- 5 53.9	60 2522
				18.391	9.0	359°77	2 49	28.176	2 33	- 0.18	+ 5 26.3	60 2520
				18.391	9.0	35.712	+3 1	7.557	+2 12	+ 56.44	+ 1 27.4	60 2508
58 3140	8.5	3 49	59 15.7	21.015	8.5	18.888	-2 9	30.339	-2 27	+ 28.48	- 5 51.5	58 3116
				21.015	8.6	23.725	2 13	8.048	2 24	+ 35.83	- 1 33.3	58 3108
				21.015	8.6	7.804	-2 4	14.800	-2 20	+ 11.80	+ 2 51.4	59 3045
59 3059	8.3	4 9	59 24.7	20.220	8.2	20.486	+0 57	31.576	+1 2	+ 31.00	- 6 5.8	59 3045
				20.220	8.4	9.395	0 54	7.864	1 8	+ 14.23	- 1 31.1	59 3052
				20.220	8.4	3.223	0 51	17.426	1 5	+ 4.90	+ 3 21.8	59 3057
58 3163	8.4	4 32	59 15.9	18.405	7.8	28.303	2 30	0.973	2 9	+ 42.75	- 0 11.4	58 3140
				18.405	7.7	24.912	2 27	37.481	2 13	+ 37.71	+ 7 14.0	59 3052
				18.405	7.7	25.251	2 22	35.762	2 18	- 38.10	- 6 54.1	58 3181
-59 3077	9.0	11 4 58	-59 33.4	18.405	9.2	23.633	+2 33	89°81	+2 45	+ 36.00	+ 0 0.3	-59 3064
				18.418	9.1	23.625	0 45	89°76	0 40	+ 35.99	+ 0 1.1	59 3064
59 3079	9.0	5 1	59 32.9	18.405	8.9	25.553	2 36	2.825	2 42	+ 38.93	+ 0 32.6	59 3064
				18.418	8.9	25.544	0 49	2.772	0 35	+ 38.91	+ 0 32.0	59 3064
60 2552	8.9	5 14	60 46.7	18.397	8.9	0.417	1 16	31.092	1 58	- 0.64	+ 6 0.1	60 2553
				18.397	9.1	22.202	1 24	34.847	1 50	- 35.06	- 6 43.5	60 2562
60 2555	8.7	5 24	60 34.5	18.397	8.7	16.204	1 31	28.647	1 44	- 25.48	+ 5 31.8	60 2562
				18.397	8.7	14.589	1 36	20.701	1 40	- 22.91	- 3 59.7	60 2561
60 2556	9.0	5 24	61 8.3	18.397	9.0	2.648	2 17	25.234	2 10	+ 4.26	+ 4 52.3	60 2554
				18.397	9.0	10.667	2 23	4.292	2 14	- 17.06	+ 0 49.7	60 2558
60 2563	8.8	5 57	60 25.2	18.397	9.2	9.442	2 31	21.040	2 41	+ 14.73	- 4 3.7	60 2559
				18.397	9.0	6.533	2 35	27.223	2 47	+ 10.25	+ 5 15.3	60 2561
60 2569	8.9	6 20	60 47.0	18.419	8.7	5.576	+2 2	28.498	+2 23	- 8.81	+ 5 30.1	60 2571
				18.421	8.8	5.599	0 0	28.520	-0 9	- 8.85	+ 5 30.3	60 2571
58 3219	8.5	6 31	58 17.7	21.015	8.6	22.704	-1 55	7.123	-1 45	+ 33.37	+ 1 22.4	58 3203



C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
N°	Mag.	A. R.	Decl.		Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.		Δ Decl.
-60°2572	8.9	11 <sup>h</sup> 6 34 <sup>s</sup>	-60°48'7"	18.419	8.7	2.999	+2 <sup>h</sup> 8 <sup>m</sup>	19.794	+2 <sup>h</sup> 17	+ 4.76	+ 3'49"2	-60°2571
				18.421	9.1	3.101	0 4	19.723	-0 6	+ 4.92	+ 3 48.4	60 2571
				18.470	9.0	3.029	2 48	19.751	+2 37	+ 4.81	+ 3 48.7	60 2571
60 2576	9.2	6 49	60 48.2	18.419	8.7	12.387	2 13	22.699	+2 19	+ 19.63	+ 4 22.8	60 2571
				18.421	9.0	12.470	0 7	22.603	-0 4	+ 19.76	+ 4 21.7	60 2571
				18.470	8.8	12.379	2 44	22.708	+2 41	+ 19.62	+ 4 23.0	60 2571
60 2587	9.0	7 7	60 30.9	18.419	8.5	8.294	2 45	17.940	2 27	+ 13.03	+ 3 27.7	60 2578
				18.419	8.4	8.831	2 41	2.840	2 30	+ 13.85	+ 0 32.9	60 2577
				18.419	8.6	3.133	2 49	18.190	2 34	+ 4.91	- 3 30.7	60 2582
				18.419	8.4	12.390	2 52	0.735	2 37	- 19.43	- 0 8.5	60 2593
60 2598	8.7	7 41	60 20.1	18.421	8.6	25.274	0 14	37.730	0 20	+ 39.51	+ 7 16.9	60 2582
				18.421	8.6	22.033	1 40	32.826	0 25	- 34.33	- 6 20.1	59 3151
				18.421	8.5	36.313	1 43	13.108	0 30	- 56.61	- 2 31.7	60 2629
				18.500	8.7	30.851	2 46	11.123	2 40	- 48.12	- 2 8.7	60 2623
				20.477	8.4	25.056	3 20	37.801	3 33	+ 39.17	+ 7 17.7	60 2582
				20.477	8.5	13.418	3 15	48.562	3 37	+ 20.85	- 9 22.4	59 3113
				20.477	8.4	21.953	3 19	32.791	3 26	- 34.20	- 6 19.7	59 3151
				20.477	8.4	30.856	3 22	11.087	3 29	- 48.11	- 2 8.5	60 2623
-60 2615	8.9	11 8 8	-60 44.5	18.421	9.0	8.411	+2 26	9.829	+2 12	+ 13.20	- 1 53.9	-60 2606
				18.421	9.2	28.085	2 21	16.976	2 17	- 44.10	- 3 16.5	60 2638
60 2619	8.7	8 15	60 16.2	18.421	8.6	14.293	1 47	6.652	0 35	- 22.25	+ 1 17.1	60 2629
				18.421	8.5	8.906	1 51	8.668	2 8	- 13.86	+ 1 40.4	60 2623
				18.421	8.5	179°72	1 56	13.125	2 4	+ 0.09	- 2 32.0	59 3151
58 3286	8.9	9 18	58 26.7	18.347	8.7	17.845	2 50	14.900	2 28	+ 26.30	- 2 52.6	58 3268
				18.347	8.6	9.926	2 59	32.366	2 31	+ 14.75	+ 6 14.8	58 3279
				18.347	9.0	20.427	3 7	15.149	2 35	- 30.15	+ 2 55.5	58 3299
58 3293	8.6	9 44	58 20.8	18.347	8.9	15.792	3 3	34.619	2 41	+ 23.18	- 6 41.0	57 4420
				18.347	8.5	35.565	+2 55	15.170	2 46	+ 52.37	+ 2 55.8	58 3268
				21.023	-	35.542	-1 51	-	-	+ 52.34	+ 2.9±	58 3268
-59 3371	8.7	11 17 10	-60 5.1	20.220	8.8	4.161	+1 18	3.717	+1 0	- 6.44	- 0 43.0	-59 3375
				20.220	8.7	20.901	1 11	6.734	1 3	- 32.36	+ 1 18.0	59 3379
				20.220	8.9	4.810	1 15	17.786	1 8	+ 7.46	+ 3 26.0	59 3368
58 3510	8.7	18 3	58 50.5	18.383	8.2	6.206	2 11	24.191	2 7	- 9.27	+ 4 40.2	58 3512
				18.421	8.6	6.160	2 29	24.176	2 45	- 9.19	+ 4 40.0	58 3512
57 4621	8.7	18 4	57 54.5	18.339	8.8	43.095	2 9	13.518	2 27	+ 62.64	- 2 36.7	57 4601
				18.339	8.7	20.251	2 15	8.227	2 22	- 29.47	+ 1 35.4	57 4630
60 2893	8.9	20 38	60 56.5	18.421	9.0	34.854	+2 53	22.990	+2 48	- 55.35	- 4 26.2	60 2914
				18.426	9.0	34.935	-0 10	23.013	-0 14	- 55.46	- 4 26.4	60 2914
59 3549	9.0	27 35	59 50.2	19.481	9.1	6.772	+3 0	21.258	+2 51	+ 10.35	+ 4 6.2	59 3545
				19.483	9.1	6.761	2 43	21.274	2 47	+ 10.34	+ 4 6.4	59 3545
59 3551	9.0	27 39	59 37.1	19.481	9.0	25.947	2 53	3.593	2 37	+ 39.86	- 0 41.6	59 3541
				19.481	9.0	13.465	2 56	1.494	2 44	+ 20.69	- 0 17.3	59 3544
				19.481	-	6.765	3 2	16.448	2 47	- 10.40	+ 3 10.5	59 3552
-59 3559	9.0	11 28 12	-60 2.7	18.405	9.1	5.315	+2 46	21.124	+2 42	- 8.21	+ 4 4.7	-59 3561
				18.421	9.1	5.332	2 51	21.095	2 55	- 8.24	+ 4 4.3	59 3561
60 3037	8.2	29 8	60 20.0	18.405	8.5	29.802	+2 49	16.799	+2 53	+ 46.44	- 3 14.6	60 3017
				18.426	8.2	11.892	-0 13	32.911	-0 1	+ 18.58	+ 6 21.2	60 3028
				18.426	8.2	31.826	-0 9	6.653	-0 5	- 49.65	+ 1 17.1	60 3053
56 4600	8.9	30 43	57 6.8	18.478	9.1	24.284	+1 12	36.456	+0 51	+ 34.60	+ 7 2.2	56 4596
				18.478	9.3	4.150	1 8	30.943	0 55	- 5.90	+ 5 58.4	56 4603
				18.478	9.1	16.961	1 4	26.349	0 59	- 24.10	- 5 5.1	56 4605
58 3720	8.8	31 2	58 44.4	18.342	8.9	22.937	1 54	9.743	2 13	+ 34.09	- 1 53.0	58 3712
				18.342	8.8	10.734	2 1	3.887	2 8	- 15.97	- 0 45.0	58 3727
58 3741	9.0	32 52	59 1.0	18.342	8.3	16.198	2 49	22.433	2 41	- 24.27	- 4 19.8	58 3748
				18.383	8.4	16.125	2 14	22.451	2 34	- 24.16	- 4 20.0	58 3748
59 3638	8.9	32 55	59 21.2	18.383	8.8	17.182	2 24	41.881	2 30	- 26.05	+ 8 5.1	59 3640
				18.402	9.0	17.142	2 47	41.936	2 42	- 26.00	+ 8 5.7	59 3640

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	Δ	Δ Decl.	Δ	Δ A. R.		Δ Decl.
-60°3152	9.0	11°32'56"	-60°54'3	18.383	8.3	27.286	+2°56'	9.773	+2°43"	+ 43.30	- 1'53.3	-60°3090
				18.383	8.2	22.888	2 59	11.209	2 47	- 36.32	- 2 9.8	60 3182
58 3742	8.9	33 0	58 30.7	18.342	8.9	10.619	3 0	14.677	2 38	- 15.69	+ 2 50.0	58 3746
				18.383	9.0	10.634	2 18	14.638	2 37	- 15.72	+ 2 49.6	58 3746
60 3171	9.4	33 17	60 43.8	18.427	8.6	15.987	0 20	28.626	0 0	+ 25.18	- 5 31.6	60 3140
				18.427	8.8	11.480	0 14	3.349	0 11	+ 18.10	+ 0 38.8	60 3156
60 3178	8.7	33 26	60 46.1	18.402	7.9	17.092	2 52	8.546	2 55	+ 27.00	- 1 39.9	60 3156
				18.427	8.0	17.091	0 17	8.579	0 8	+ 26.97	- 1 39.4	60 3156
				18.427	7.8	3.804	0 22	31.335	0 5	- 6.01	+ 6 2.9	60 3182
60 3181	8.7	33 31	60 50.4	18.383	8.9	0.830	2 53	8.902	2 50	- 1.31	+ 1 43.1	60 3182
				18.386	8.9	0.781	2 44	8.919	2 47	- 1.23	+ 1 43.3	60 3182
60 3243	8.7	37 24	60 36.1	18.427	8.8	5.424	0 30	11.213	0 51	+ 8.51	- 2 9.9	60 3239
				18.427	9.0	3.140	0 33	29.082	0 54	- 4.93	- 5 36.8	60 3246
-60 3254	8.6	11 37 58	-60 34.8	18.427	9.3	26.887	+0 36	4.525	+0 47	+ 42.19	- 0 52.5	-60 3239
				18.427	9.5	18.316	0 39	22.368	0 43	+ 28.71	- 4 19.1	60 3246
				18.427	9.1	29.319	1 36	10.280	1 31	- 45.99	- 1 59.0	60 3266
57 4963	8.9	41 0	57 45.0	18.339	9.1	25.068	2 58	34.450	2 23	+ 36.34	+ 6 39.0	57 4958
				18.339	9.2	6.066	3 4	30.246	2 28	- 8.78	+ 5 50.3	57 4964
				18.339	9.1	33.002	3 8	12.252	2 33	- 47.73	- 2 21.8	57 4969
61 2590	9.0	41 32	61 38.2	18.419	9.0	4.564	2 58	38.106	2 53	- 7.42	- 7 21.3	61 2594
				18.421	8.9	4.562	2 50	38.092	2 46	- 7.41	- 7 21.2	61 2594
57 4970	9.0	41 58	57 27.7	18.339	9.0	31.200	2 47	6.119	2 37	- 44.79	+ 1 10.9	57 4978
				18.339	8.8	25.108	+2 51	33.699	+2 42	- 36.08	+ 6 30.3	57 4974
60 3315	8.3	42 8	61 2.9	21.023	8.6	0.688	-1 49	5.966	-1 41	+ 1.10	- 1 9.1	60 3314
				21.031	8.8	0.651	-1 15	5.931	-1 18	+ 1.04	- 1 8.7	60 3314
60 3319	8.9	42 25	61 1.3	19.505	9.2	11.530	+2 31	2.093	+2 49	+ 18.38	+ 0 24.2	60 3314
				19.505	9.1	10.916	+2 34	8.019	+2 46	+ 17.40	+ 1 32.9	60 3315
				21.023	9.3	11.542	-1 53	2.132	-1 44	+ 18.40	+ 0 24.7	60 3314
-61 2616	8.7	11 43 11	-61 55.7	18.421	9.0	4.688	+2 51	15.434	+2 57	+ 7.68	- 2 58.8	-61 2615
				18.421	8.8	17.690	2 54	28.448	3 0	- 29.05	+ 5 29.5	61 2622
60 3333	8.9	43 16	61 2.8	18.386	8.8	31.667	2 52	7.517	2 42	+ 50.47	- 1 27.1	60 3319
				18.386	8.8	14.721	2 49	6.610	2 45	- 23.48	+ 1 16.6	60 3337
60 3334	8.7	43 24	60 42.9	19.505	8.9	14.705	2 37	6.645	2 42	- 23.46	+ 1 17.0	60 3337
				18.402	8.8	19.548	2 57	14.650	2 48	+ 30.88	+ 2 49.6	60 3325
				18.405	8.9	6.081	2 57	27.989	2 47	+ 9.57	- 5 24.2	60 3330
				18.503	8.8	19.497	1 16	14.635	1 34	+ 30.80	+ 2 49.5	60 3325
60 3335	8.8	43 35	60 44.7	18.503	8.8	6.072	1 29	27.911	1 43	+ 9.56	- 5 23.3	60 3330
				18.402	9.0	26.588	3 0	5.017	2 54	+ 42.01	+ 0 58.1	60 3325
				18.405	9.2	13.240	2 54	37.586	2 50	+ 20.86	- 7 15.3	60 3330
				18.503	9.0	26.510	1 20	5.009	1 38	+ 41.89	+ 0 58.0	60 3325
60 3338	9.4	43 40	60 46.8	18.503	9.0	13.160	1 25	37.422	1 47	+ 20.74	- 7 13.4	60 3330
				18.402	8.8	30.098	3 3	5.951	2 51	+ 47.57	- 1 9.0	60 3325
				18.419	8.7	30.147	2 47	5.993	2 42	+ 47.66	- 1 9.5	60 3325
-60 3457	8.9	11 48 51	-60 47.5	18.427	9.2	32.197	+1 40	16.740	+1 50	+ 50.88	- 3 13.9	-60 3442
				18.427	9.4	34.066	1 43	22.230	1 47	- 53.94	+ 4 17.5	60 3473
				18.432	9.2	34.079	0 14	22.325	0 10	- 53.96	+ 4 18.6	60 3473
61 2898	9.0	57 55	62 6.5	18.503	9.2	34.056	2 2	22.197	1 56	- 53.94	+ 4 17.1	60 3473
				18.419	8.4	12.853	2 51	26.202	2 58	+ 21.25	+ 5 3.5	61 2888
61 2901	9.0	58 7	61 56.9	18.419	8.6	23.443	2 54	35.043	3 1	- 38.63	- 6 45.8	61 2906
60 3664	8.7	59 45	60 39.6	19.505	9.2	15.846	2 43	14.774	2 39	- 26.03	+ 2 51.1	61 2906
				18.369	8.5	2.350	2 33	6.641	2 21	+ 3.70	+ 1 16.9	60 3663
60 3744	8.8	2 54	60 46.2	18.369	8.7	30.122	2 29	12.827	2 25	- 47.43	- 2 28.6	60 3683
60 3748	9.0	3 3	60 51.1	18.369	-	2.547	2 33	25.753	2 56	- 4.02	+ 4 58.3	60 3746
				18.369	9.1	5.762	2 37	24.760	2 53	+ 9.11	- 4 46.8	60 3744
60 3757	8.7	3 17	60 50.8	18.369	9.0	8.540	2 44	0.946	2 47	- 13.53	- 0 10.9	60 3757
60 3763	8.7	3 52	60 19.2	18.383	-	11.793	2 41	1.946	2 50	+ 18.69	+ 0 22.5	60 3746
						13.879	2 42	13.721	2 55	- 21.65	+ 2 38.9	60 3771

C. P. D.		1925		1900 +	Aparentes				1925.0		* Ref. C. P. D.	
Nº	Mag.	A. R.	Decl.		Mag.	Δ A. R.	t	Δ Decl.	t	Δ A. R.		Δ Decl.
-60°3777	8.4	12 <sup>h</sup> 4 <sup>m</sup> 29 <sup>s</sup>	-60°25'8"	18.383	—	9.642	+2 <sup>h</sup> 47 <sup>m</sup>	20.292	+2 <sup>h</sup> 51 <sup>m</sup>	+ 15°06'	- 3'55"0	-60°3771
57 5524	9.0	26 30	58 6.3	18.369	8.9	14.199	2 47	2.088	2 43	+ 20.75	+ 0 24.2	57 5521
				18.383	9.0	14.197	2 43	2.109	2 39	+ 20.74	+ 0 24.4	57 5521
59 4449	8.8	43 12	59 45.3	18.370	9.1	179°49'	2 57	25.965	2 42	+ 0.35	- 5 0.7	59 4448
				18.370	8.9	22.126	2 52	14.322	2 47	- 33.94	+ 2 45.9	59 4460
57 5706	8.9	43 17	58 0.4	18.369	9.0	2.042	2 35	5.098	2 39	- 2.98	+ 0 59.0	57 5708
				18.383	9.0	2.068	+2 32	5.123	+2 35	- 3.01	+ 0 59.3	57 5708
59 4555	8.7	49 19	59 58.1	21.053	—	17.432	-2 7	14.946	-2 25	+ 26.88	- 2 53.1	59 4529
				21.053	—	7.333	2 4	6.071	2 23	+ 11.31	- 1 10.3	59 4543
				21.053	—	1.119	2 0	13.823	2 20	+ 1.73	- 2 40.1	59 4551
				21.053	—	1.601	1 57	8.544	2 17	+ 2.47	+ 1 39.0	59 4552
				21.053	—	5.549	1 54	12.515	2 14	- 8.57	+ 2 25.0	59 4564
				21.053	—	7.022	1 50	12.801	2 11	- 10.83	- 2 28.3	59 4566
58 4660	8.5	58 45	59 11.8	21.023	9.2	10.054	2 41	2.908	2 46	+ 15.16	+ 0 33.7	58 4659
				21.031	9.2	10.000	2 24	2.920	2 19	+ 15.08	+ 0 33.8	58 4659
-57 6144	8.4	13 30 16	-58 0.2	21.168	—	1.376	-1 20	6.721	-1 27	+ 2.01	- 1 17.8	-57 6143
				21.170	—	1.406	0 28	6.751	0 33	+ 2.05	- 1 18.2	57 6143
58 5640	8.8	14 33 19	58 50.2	21.023	8.7	0.683	3 39	11.251	3 48	- 1.01	- 2 10.3	58 5641
				21.050	8.6	0.689	3 20	11.325	3 37	- 1.02	- 2 11.2	58 5641
				21.050	—	4.010	3 25	6.794	3 33	- 5.98	- 1 18.7	58 5644
60 6159	9.0	15 46 51	60 30.3	21.050	8.9	7.257	4 22	3.480	4 18	- 11.39	+ 0 40.2	60 6162
				21.053	—	7.224	-4 37	3.488	-4 41	- 11.34	+ 0 40.4	60 6162
57 7791	9.0	16 12 9	57 40.4	19.558	9.0	20.718	+0 58	24.951	+0 44	+ 29.92	+ 4 49.2	57 7769
				19.558	8.8	17.733	1 10	22.892	1 25	- 25.66	+ 4 25.0	57 7816
				19.558	9.2	19.813	1 20	13.237	1 31	- 28.64	+ 2 33.1	57 7821
57 7793	8.8	12 12	57 38.5	19.558	8.8	22.177	1 2	34.865	0 48	+ 32.08	+ 6 43.8	57 7769
				19.558	8.5	16.219	1 17	32.882	1 27	- 23.47	+ 6 20.7	57 7816
				19.558	8.8	18.309	1 23	23.220	1 29	- 26.47	+ 4 28.8	57 7821
-57 7803	8.5	16 12 24	-57 45.3	19.558	9.0	30.742	+1 6	0.436	+0 53	+ 44.49	- 0 4.7	-57 7769
				19.558	9.0	9.854	1 55	12.085	1 33	- 14.24	- 2 20.1	57 7821
				19.558	8.9	7.722	1 59	2.395	1 41	- 11.17	- 0 27.8	57 7816
				19.558	8.8	8.740	2 2	1.733	1 46	- 12.65	+ 0 20.0	57 7818
57 7811	9.0	12 33	57 45.7	19.558	9.3	3.514	2 13	14.268	1 38	- 5.07	- 2 45.3	57 7821
				19.558	9.2	2.457	2 5	0.415	1 50	- 3.56	- 0 4.8	57 7818
				19.558	9.3	1.390	+2 7	4.567	+1 43	- 2.01	- 0 52.9	57 7816
57 7847	8.3	13 4	57 42.4	19.574	9.7	17.855	-0 31	3.247	-0 43	+ 25.71	+ 0 37.8	57 7821
				19.574	9.8	19.922	0 20	12.948	+0 7	+ 28.79	+ 2 30.2	57 7816
				19.574	9.9	18.855	-0 9	17.175	0 14	+ 27.24	+ 3 19.1	57 7818
				19.574	9.8	14.198	+0 34	5.683	+0 44	- 20.53	+ 1 5.7	57 7859
57 7848	8.8	13 5	57 42.6	19.574	8.8	18.271	-0 27	1.717	-0 40	+ 26.41	+ 0 20.1	57 7821
				19.574	8.6	20.326	0 16	11.450	+0 10	+ 29.38	+ 2 12.8	57 7816
				19.574	8.9	19.246	-0 5	15.645	0 16	+ 27.82	+ 3 1.4	57 7818
				19.574	9.0	13.811	+0 37	4.168	+0 46	- 19.97	+ 0 48.1	57 7859
-57 7854	8.4	16 13 11	-57 42.2	19.574	8.5	22.980	-0 24	4.045	-0 35	+ 33.21	+ 0 47.1	-57 7821
				19.574	8.7	25.012	0 12	13.755	+0 12	+ 36.15	+ 2 39.6	57 7816
				19.574	8.6	23.960	-0 2	17.967	0 17	+ 34.63	+ 3 28.3	57 7818
				19.574	8.7	9.078	+0 38	6.499	0 48	- 13.13	+ 1 15.2	57 7859
57 7858	8.8	13 23	57 45.1	19.574	8.9	31.722	0 27	2.593	0 19	+ 45.90	+ 0 30.3	57 7818
				19.574	8.8	32.774	0 29	1.642	0 22	+ 47.42	- 0 18.7	57 7816
				19.574	8.9	30.729	0 32	11.321	0 24	+ 44.46	- 2 10.8	57 7821
				19.574	8.7	1.344	+0 41	8.859	+0 50	- 1.93	- 1 42.6	57 7859
61 5851	8.8	17 7 4	61 27.5	21.165	—	2.556	-3 1	1.657	-3 6	+ 4.13	+ 0 19.2	61 5849
				21.170	—	2.527	-3 52	1.664	-3 57	+ 4.09	+ 0 19.3	61 5849
60 7435	8.6	20 48 0	59 57.9	21.006	8.8	8.683	+6 27	19.528	+6 9	+ 13.47	- 3 46.1	60 7433
				21.006	—	8.350	6 20	8.339	6 13	+ 12.88	+ 1 36.6	60 7434
60 7682	8.7	23 42 49	60 21.0	21.017	—	13.050	4 44	41.303	4 38	- 20.32	- 7 58.4	60 7683
				21.022	8.7	13.075	4 47	41.266	4 43	- 20.35	- 7 57.9	60 7683

# OBSERVATIONS OF ASTEROIDS

## OBSERVACIONES DE ASTEROIDES

T. M. Greenwich	Mag.	Cp.	*	Planeta—Estrella			Posición Media o Astrográfica		Log. $p \Delta$	
				$\Delta$ A. R.	$\Delta$ A. R.	$\Delta$ Decl.	A. R.	Decl.	en A. R.	en Decl.

### (16) Psyche

1919							1919.0		1919.0		
Ago.	24.77388	—	8,8	1	— 26.6	— 1.87	+3.53.4	20 <sup>b</sup> 13 17.32	—18 23 54.6	9.678	0.598 <sub>n</sub>
	25.60460	—	8,8	1	—411.2	— 28.90	+1 14.2	20 12 50.29	—18 26 33.8	8.94	0.398 <sub>n</sub>
	27.69252	—	8,8	2	—156.1	— 10.98	+6 29.5	20 11 45.91	—18 32 57.5	9.546	0.490 <sub>n</sub>

### (112) Iphigenia

Ago.	24.75728	—	10,10	3	+ 32.5	+ 2.31	+5 19.2	20 17 42.72	—20 23 55.3	9.660	0.549 <sub>n</sub>
	25.72058	—	10,10	4	+183.1	+ 13.03	+1 16.2	20 17 9.55	—20 23 58.2	9.599	0.491 <sub>n</sub>
	26.68433	—	10,10	4	—259.8	— 18.48	+1 20.6	20 16 38.04	—20 23 53.8	9.506	0.436 <sub>n</sub>
	27.59218	—	21,10t	3	—	— 90.18	+5 29.9	20 16 10.23	—20 23 44.6	8.76	0.341 <sub>n</sub>

### (381) Myrrha

Ago.	24.73023	—	10,12	5	+266.6	+ 19.13	—1 8.5	20 14 59.27	—21 45 5.7	9.618	0.483 <sub>n</sub>
	25.73489	—	10,10	7	+119.0	+ 8.55	+3 51.0	20 14 30.69	—21 50 17.9	9.636	0.500 <sub>n</sub>
	26.70296	—	10,10	7	—239.5	— 17.21	—1 0.9	20 14 4.93	—21 55 9.8	9.572	0.443 <sub>n</sub>
	27.66231	—	10,10	8	+341.9	+ 24.59	+3 48.1	20 13 40.52	—21 59 51.6	9.445	0.373 <sub>n</sub>
	28.63526	—	10,10	8	+ 12.6	+ 0.91	—0 52.8	20 13 16.84	—22 4 32.5	9.320	0.333 <sub>n</sub>

### (29) Amphitrite

1920							1920.0		1920.0		
Junio	20.72455	9.4	8,8	9	—205.6	— 16.27	—0 53.0	17 10 4.47	—32 36 47.7	9.510	0.003 <sub>n</sub>
	22.58316	—	8,8	10	+153.8	+ 12.16	—1 51.1	17 8 10.10	—32 33 21.3	9.144	9.65 <sub>n</sub>

### (324) Bamberga

Junio	12.75881	10.4	8,8	11	+112.5	+ 9.38	—0 56.0	15 46 7.41	—36 58 7.1	9.717	0.261 <sub>n</sub>
	12.76936	—	8,8	12	+ 65.9	+ 5.49	—3 45.0	15 46 6.91	—36 58 3.4	9.733	0.318 <sub>n</sub>
	14.58835	10.2	8,8	13	—266.2	— 22.16	—4 1.3	15 44 19.23	—36 48 27.0	7.94	9.50
	17.52164	10.0	8,8	15	— 65.8	— 5.47	+9 3.7	15 41 34.05	—36 32 10.5	9.304 <sub>n</sub>	8.46

### (404) Arsinoë

Junio	22.56418	11.2	8,8	16	—120.0	— 8.41	+1 38.8	16 58 5.14	—17 59 47.7	9.205 <sub>n</sub>	0.422 <sub>n</sub>
	23.76540	10.7	10,8t	17	—	—166.45	—7 31.8	16 57 0.76	—18 9 13.6	9.621	0.541 <sub>n</sub>

T. M. Greenwich	Mag.	Cp.	*	Planeta—Estrella			Posición Media o Astrográfica		Log. p Δ	
				Δ A. R.	Δ A. R.	Δ Decl.	A. R.	Decl.	en A. R.	en Decl.

(545) *Messalina*

1920				1920.0			1920.0				
Junio	23.81019	11.3	8,8	18	-491.6	-42.71	-0'39.4	17 <sup>b</sup> 14 <sup>m</sup> 19.82	-39°53'31.3	9.763	0.312 <sup>n</sup>
	24.52896	—	8,8	19	+208.4	+18.09	-5 33.5	17 13 40.32	-39 50 47.6	9.535 <sup>n</sup>	8.53
	24.53504	—	8,8	20	-41.1	-3.57	-7 24.4	17 13 40.02	-39 50 45.5	9.508 <sup>n</sup>	9.11

(695) *Bella*

Junio	14.54292	11.0	8,8	21	-132.3	-10.16	-1 52.1	15 24 50.40	-29 46 24.4	9.013 <sup>n</sup>	9.91 <sup>n</sup>
	17.50031	11.2	8,8	23	+182.4	+13.94	-4 20.9	15 22 54.67	-29 19 21.7	9.323 <sup>n</sup>	0.039 <sup>n</sup>
	22.54282	12.5	10,8 <sup>t</sup>	24	—	-156.87	-2 55.5	15 20 11.43	-28 33 59.3	8.21 <sup>n</sup>	9.98 <sup>n</sup>

(779) *Nina*

Junio	22.60183	—	8,8	25	-217.6	-17.01	-8 9.3	17 20 48.11	-31 26 5.7	9.014 <sup>n</sup>	9.75 <sup>n</sup>
	22.61138	—	8,8	26	-446.9	-34.91	-1 16.2	17 20 47.56	-31 26 1.9	8.84 <sup>n</sup>	9.73 <sup>n</sup>
	24.59158	—	8,8	27	+164.6	+12.81	-9 14.6	17 18 43.44	-31 8 28.6	9.059 <sup>n</sup>	9.80 <sup>n</sup>

(784) [1914 UM]

Junio	12.73927	11.5	8,8	28	+131.1	+10.90	+5 25.4	15 37 23.70	-36 40 46.1	9.692	0.189 <sup>n</sup>
	14.57172	11.5	8,8	29	-18.4	-1.53	-0 6.8	15 36 4.06	-36 38 15.0	8.51 <sup>n</sup>	9.46

(925) *Alfonsina*

1921				1921.0			1921.0				
Mayo	4.77410	12.8	8,8	30	+66.2	+6.78	+0 9.7	15 37 4.17	-49 22 11.2	9.555	0.185
	8.58022	13.5	10,10	32	+207.4	+21.15	-0 22.3	15 32 40.21	-49 11 40.9	9.635 <sup>n</sup>	0.064
	12.54362	12.9	8,8	34	-192.0	-19.47	-4 14.1	15 27 57.39	-48 55 39.5	9.707 <sup>n</sup>	9.80
	13.60756	12.7	8,8	36	+79.7	+8.07	+1 0.0	15 26 41.17	-48 50 30.6	9.390 <sup>n</sup>	9.26
	13.62192	—	10,10	37	-325.2	-32.91	-5 5.2	15 26 39.96	-48 50 24.5	9.260 <sup>n</sup>	0.295
	13.64927	—	8,8	39	+68.6	+6.94	+0 14.6	15 26 37.84	-48 50 16.9	8.76 <sup>n</sup>	0.328
	27.58585	12.8	10,10	40	+59.1	+5.80	+7 13.5	15 10 48.98	-47 11 5.2	9.075 <sup>n</sup>	0.260
	28.54245	12.5	10,10	42	-357.9	-33.40	-5 57.9	15 9 50.80	-47 2 23.2	9.460 <sup>n</sup>	0.150
Junio	6.49785	—	8,8	43	+74.6	-7.10	-0 42.1	15 1 50.17	-45 32 29.0	9.527 <sup>n</sup>	9.995
	7.49776	—	10,10	44	+134.0	+12.70	-7 4.7	15 1 5.01	-45 21 38.2	9.510 <sup>n</sup>	0.005
	8.61175	—	8,8	47	+197.5	+18.69	+7 52.1	15 0 16.47	-45 9 29.4	9.223	0.157
	8.62057	13.5	8,8	48	+57.7	+5.45	-4 53.0	15 0 15.91	-45 9 24.2	9.309	0.133

(927) [1920 GO]

Mayo	12.61636	14.0	12,12	49	+467.5	+38.17	+1 24.5	15 27 25.64	-35 15 12.6	9.251 <sup>n</sup>	9.06 <sup>n</sup>
	13.54061	13.3	10,10	49	-205.5	-16.78	+1 19.0	15 26 30.69	-35 15 18.1	9.610 <sup>n</sup>	0.031 <sup>n</sup>
	13.56538	13.5	10,10	50	+333.4	+27.48	+6 49.5	15 26 29.09	-35 15 17.1	9.527 <sup>n</sup>	9.82 <sup>n</sup>
	28.60177	13.8	10,10	51	-11.2	-0.91	-4 38.2	15 12 2.64	-34 59 33.3	8.52 <sup>n</sup>	8.54
Junio	6.65957	—	10,10	53	+79.5	+6.44	-0 26.9	15 4 37.91	-34 37 22.4	9.444	9.71 <sup>n</sup>
	6.68869	—	10,10	54	—	+102.24	—	15 4 36.79	—	9.565	—

MEAN PLACES OF THE COMPARISON STARS  
LUGARES MEDIOS DE LAS ESTRELLAS DE COMPARACIÓN

* A. R. 1919.0	Decl. 1919.0	Autoridad	* A. R. 1921.0	Decl. 1921.0	Autoridad
1 20 <sup>h</sup> 13 19.19	-18° 27' 48".0	Bord. 6095.	30 15 <sup>h</sup> 36 <sup>m</sup> 57.39	-49° 22' 20".9	* 31 +35".4, -490".9.
2 20 11 56.89	-18 39 27.0	Hyd. Astr. —19°. 56436.	31 15 36 53.77	-49 14 10.0	GZ. XV, 2322, Gou 21244.
3 20 17 40.41	-20 29 14.5	CiZ 3384.	32 15 32 19.06	-49 11 18.6	* 33 +350".7, -25".1.
4 20 16 56.52	-20 25 14.4	* 3 -43".89 + 240".1.	33 15 31 43.29	-49 10 53.5	GZ. XV, 1962.
5 20 14 40.14	-21 43 57.2	* 6 -129".87 - 214".5.	34 15 28 16.86	-48 51 25.4	* 35 -50".0, -456".6.
6 20 16 50.01	-21 40 22.7	CiZ 3382.	35 15 28 21.92	-48 43 48.8	GZ. XV, 1699, Gou 21047.
7 20 14 22.14	-21 54 8.9	A.G. C6.A. 14101.	36 15 26 33.10	-48 51 30.6	GZ. XV, 1595.
8 20 13 15.93	-22 3 39.7	A.G. C6.A. 14091.	37 15 27 12.87	-48 45 19.3	* 38 -370".9, -79".5.
	1920.0		38 15 27 50.37	-48 43 59.8	GZ. XV, 1668, Gou 21036.
9 17 10 20.75	-32 35 54.7	GZ. XVII, 481.	39 15 26 30.90	-48 50 31.5	GZ. XV, 1593.
10 17 7 57.94	-32 31 30.2	Gou 23290.	40 15 10 43.18	-47 18 18.7	* 41 -222".7, +360".3.
11 15 45 58.03	-36 57 11.1	GZ. XV, 3028.	41 15 11 5.10	-47 24 19.0	GZ. XV, 544, Gou 20676.
12 15 46 1.43	-36 54 18.4	GZ. XV, 3034.	42 15 10 24.20	-46 56 25.3	GZ. XV, 505.
13 15 44 41.39	-36 44 25.7	* 14 -293".8 + 01".1.	43 15 1 43.07	-45 31 46.9	GZ. XIV, 3744.
14 15 45 5.83	-36 44 26.8	GZ. XV, 2964.	44 15 0 52.31	-45 14 33.5	* 45 -160".0, -257".0.
15 15 41 39.52	-36 41 14.2	GZ. XV, 2715, Gou 21359.	45 15 1 7.45	-45 10 16.5	GZ. XIV, 3701.
16 16 58 13.55	-18 1 22.5	* 17 -93".66 + 19".1.	46 15 1 34.89	-45 6 35.5	GZ. XIV, 3735, Gou 20472.
17 16 59 47.21	-18 1 41.8	A.G. Wash. 6096 incl. $\mu$ .	47 14 59 57.78	-45 17 21.5	GZ. XIV, 3617, Gou 20435.
18 17 15 2.53	-39 52 51.9	GZ. XVII, 804.	48 15 0 10.46	-45 4 31.2	GZ. XIV, 3635, Gou 20433.
19 17 13 22.23	-39 45 14.1	GZ. XVII, 699.	49 15 26 47.47	-35 16 37.1	GZ. XV, 1628.
20 17 13 43.59	-39 43 21.1	GZ. XVII, 732.	50 15 26 1.61	-35 22 6.6	GZ. XV, 1579, Gou 21003.
21 15 25 0.56	-29 47 32.3	* 22 -451".3 + 26".4.	51 15 12 3.55	-34 54 55.1	* 52 -88".13, +9".7.
22 15 25 35.21	-29 44 58.7	GZ. XV, 1563.	52 15 13 31.68	-34 55 4.8	GZ. XV, 731.
23 15 22 40.73	-29 15 0.8	GZ. XV, 1357.	53 15 4 31.47	-34 36 55.5	* 54 +97".02, -99".9.
24 15 22 48.30	-28 31 3.8	Gou 20924.	54 15 2 54.45	-34 35 15.6	GZ. XV, 2.
25 17 21 5.12	-31 34 15.8	GZ. XVII, 1236.			
26 17 21 22.49	-31 24 45.7	GZ. XVII, 1258.			
27 17 18 30.63	-30 59 14.0	GZ. XVII, 1065, Gou 23535.			
28 15 37 12.80	-36 46 11.5	GZ. XV, 2283.			
29 15 36 5.59	-36 38 8.2	* 28 -67".21 + 483".3.			

NOTA. — \* 51, del Catálogo Astrográfico de Perth; —34°, 15<sup>h</sup> 9<sup>m</sup>, \* 33; resulta con 15<sup>h</sup> 10<sup>m</sup> 44.46, —34° 50' 15".3 (1900.0).

# ECLIPSES OF THE SATELLITES OF JUPITER

## ECLIPSES DE LOS SATÉLITES DE JÚPITER

1920	T. Sid. La Plata	T. Med. Greenw.	Fenómeno	Imág.	Notas
Nov. 17	7 <sup>h</sup> 12 <sup>m</sup> 0 <sup>s</sup> .1	19 <sup>h</sup> 15 38 <sup>s</sup>	I. Des.	F.	150x. Velado.
24	6 48 50 51 50 57 50 59 50	18 25 0 28 0 33 59 35 58	III. — III. 2.0 < II = I = II	G.	150x. Nube. Velado. Velado. Velado.
Dic. 3	6 29 13.3	17 30 3	I. Des.	G.	150x.
10	8 14 36.3	18 47 38	II. Des.	V. P.	150x.
10	8 50 14.3	19 23 10	I. Des.	P.	370x y diafragma.
1921					
Ene. 2	10 27 42.5	19 29 56	I. Des.	V. P.	370x y diafragma de aquí en adelante.
11	10 3 41.4	18 30 36	II. Des.	G.	
13	10 29 0 33 40 35 13.2	18 47 58 52 37 54 10	III. = II 12 Des.	G.	
18	9 45 16.3	17 44 42	I. Des.	G.	
Feb. 10	11 22 12 23 13 23 41.6	17 50 55 51 56 52 25	I. Dic. P. Des.	F.	
18	8 36 37 39 7 42 43 44 21.6	14 34 21 36 50 40 26 42 4	III. Pr. I. Dic. P. Des.	V. P.	
19	8 18 5 19 5 20 10 20 24.8	14 11 56 12 56 14 1 14 15	I. Pr. I. Dic. P. Des.	P.	

EXPLICACIÓN DE LAS ABREVIACIONES. — Pr. I., Primeras indicaciones; Dic., Dicotomía; P., Punto; Des., Desaparición; Ap., Reapareció; Números romanos son los de satélites; números arábigos, las magnitudes apreciadas.  
 IMÁGENES. — G., Buenas; F., Pasables; P., Malas y V. P., muy malas.

1921	T. Sid. La Plata	T. Med. Greenw.	Fenómeno	Imág.	Notas
Feb. 25	13 <sup>b</sup> 6 <sup>m</sup> 5 <sup>s</sup> 10 19 11 10.2	18 <sup>b</sup> 35 <sup>m</sup> 34 <sup>s</sup> 39 47 40 38	III. Dic. P. Des.	V. P.	Velado.
Mar. 2	7 28 13 30 13 30 22.6	12 38 57 40 57 41 7	II. Pr. I. P. Des.	F. P.	
Abr. 15	10 54 28.9 54 51 55 31	13 11 39 12 1 12 41	I. Ap. 12 10	V. P.	☉
22	13 17 35.4 17 52 18 45	15 6 51 7 8 8 1	I. Ap. 11.5 8.5	V. P.	
28	10 45 12.0 45 40 46 45	12 11 17 11 45 12 50	II. Ap. 12 9	G.	
30	14 55.0 58.0 15 0 30 1 36 3 12 4 48 5 42 7 4.8	16 12.5 15.5 18 1 19 7 20 43 22 19 23 13 24 35	IV. 7.5 8.5 9.5 10 11 12 13 Des.	P.	
Mayo 1	10 16 2.8 16 20 16 36 17 21 18 40	11 30 25 30 42 30 58 31 43 33 2	I. Ap. 12 10 Dic. —	F.	Redonda.
5	13 48.0 49.0	14 46.1 47.1	II. — —	F.	Nube cubrió Júpiter. Visto al salir de ella
8	9 37 24 38 44 41 9 42 4 42 52 44 16.1	10 24 21 25 41 28 6 29 1 29 48 31 12	III. Pr. I. = II. 9 11 P. Des.	P.	
8	12 39 16.1 39 59 40 59	13 25 44 26 27 27 26	I. Ap. 10 8	F.	
8	12 42 12.1 42 32 43 44 45 24 46 19 47 19 48 14	13 28 39 28 59 30 11 31 50 32 45 33 45 34 40	II. Ap. 13 11 9 0.8 < 1 Dic. = I	F.	
Junio 6	15 31 31.0 32 7 32 24 33 2	14 23 29 24 5 24 22 25 0	II. Ap. 11 10 8.5	V. P.	



1921	T. Sid. La Plata	T. Med. Greenw.	Fenómeno	Imág.	Notas
Junio 16	13 <sup>h</sup> 46 <sup>m</sup> 15 <sup>s</sup> 0 46 59	11 <sup>h</sup> 59 <sup>m</sup> 11 <sup>s</sup> 59 55	I. Ap. 10½	V. P.	
20	12 24 36 27 45 29 20 30 0 30 20 31 10 31 56 32 20 32 40 33 19.5	10 22 2 25 11 26 45 27 25 27 45 28 35 29 21 29 45 30 4 30 44	III. Pr. I. Dic. 8 9 9.5 11 P. 12.5 13.5 Des.	P.	
20	15 25 51.6 27 0 28 0 28 45	13 22 48 23 56 24 55 25 40	III. Ap. 11.5 10 9	V. P.	

FIN DEL TOMO IV











